COLUMBIA COUNTY

West End Flood Mitigation Study FINAL REPORT

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VOLUME I

Prepared for: Columbia County

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Executive Summary

Columbia County West End Flood Mitigation Study

BORTON the Town of Bloomsburg located along the confluence of the Susquehanna River LAWSON and Fishing Creek in Columbia County, Pennsylvania, has led to significant and repetitive flood losses at an increased frequency in these communities. Repetitive flooding in this area known as the "West End of Bloomsburg" has created a hardship on residents, businesses, the municipalities, and community at large. While progress has been made with the completion of over two (2) miles of earthen levees and flood wall systems in the Town of Bloomsburg, the West End of Bloomsburg and adjacent communities remain in need of flood mitigation strategies to reduce risk to loss of life and property damage, as well as build community resiliency to flooding events.

Realizing the need to address the Fishing Creek watershed with comprehensive flood mitigation strategies, Columbia County sought to develop flood mitigation strategies for the West End of Town of Bloomsburg and the surrounding areas. This flood mitigation study was completed to enable the County to capitalize on resources at the federal, state and county level to assist the County and local municipalities with implementation of impactful flood mitigation strategies proposed by the study.

The West End study area includes limited sections of three (3) municipalities that are located within the Floodplains of Fishing Creek including the Town of Bloomsburg, Hemlock Township, and Montour Township. This study outlines the various flood mitigation projects considered for each municipality that would be impactful, economically justified, technically feasible, and environmentally sound for securing funding for flood mitigation in all three municipalities.

The history of Susquehanna River and Fishing Creek flooding was reviewed to understand the flooding issues in the three communities. A detailed hydrologic and hydraulic (H&H) analysis of the Susquehanna River and Fishing Creek was then performed to assess flooding impacts in each community. Damages were calculated and utilized to review multiple non-structural and structural alternatives to d determine impacts to the communities in the study area. High water marks from historical flood events on Fishing Creek in 2006, 2011, and 2018 were relied upon when calibrating the Fishing Creek hydraulic model.

For the structural flood mitigation alternatives (levee/floodwall systems) which were found to create induced flooding, additional hydraulic modeling was performed to evaluate actions that could be taken to reduce the induced flooding. The hydraulic analysis was completed with a one-dimensional (1D) model which has a degree of uncertainty when determining the extent of induced flooding and evaluating mitigating alternatives. Additional analysis and

coordination with state and federal agencies, specifically the Federal Emergency Management Agency (FEMA), United States Army Corps of Engineers (USACE), and Pennsylvania Department of Environmental Protection (PADEP), not included as part of this study, will be required if Columbia County desires to pursue a levee/floodwall system around the West End of Bloomsburg and the Fairgrounds. These actions would be necessary to resolve uncertainties inherent to one-dimensional modeling and construction of structures, such as a levee/floodwall system, within a regulated floodway.

After extensive outreach with stakeholders in each community, structural and non-structural flood mitigation alternatives were identified with the goal of minimizing risk to loss of life, property damages, and economic losses, while increasing flood resiliency of the communities in the study area. Non-structural mitigation options evaluated within each community included acquisition/demolitions, structure elevations, structure mitigation-reconstruction, and wet and dry flood proofing of commercial properties. Structural mitigation alternatives considered included levee/floodwall systems, bridge replacements, and modifications to the channel and floodplain of Fishing Creek. Opinions of costs were developed for the most impactful and technically feasible alternatives. Benefit-Cost Analyses were completed for both structural and non-structural alternatives.

Conclusions:

Findings from this study indicate that nonstructural flood mitigation alternatives are viable alternatives for Montour Township and Hemlock Township. Structural mitigation is not feasible for these municipalities since the low density of structures results in a low benefit to cost ratio. This is consistent with the current and projected goals of each community to pursue additional acquisitions of flood prone properties for removal from the floodplain.

Both types of mitigation are feasible for the Town of Bloomsburg. The nonstructural measures would include approximately 290 structures eligible for acquisition and demolition. This type of program is voluntary and the level of participation would be uncertain. The large floodway in the West End restricts the options for about 106 of the West End structures to only acquisition and demolition. Elevations or demolition/reconstruction of structures is not permitted in floodways.

The structural alternative, to construct a levee/floodwall system around the West End of Bloomsburg, is cost effective utilizing the FEMA Benefit-Cost Analysis (BCA) methodology. Cost effectiveness is defined by FEMA as having a Benefit-Cost Ratio (BCR) greater than one (1). The construction of a benched floodplain along a segment of Fishing Creek in Hemlock Township offers the most promising flood mitigation benefits when combined with a levee/floodwall system around the West End of Bloomsburg. Total project cost is approximately \$29,000,000.

With completion of the West End Flood Mitigation Study, funding and implementation of the flood mitigation projects identified is the priority of Columbia County. Funding opportunities through the FEMA Building Resilient Infrastructure and Communities (BRIC) program and the FEMA Flood Mitigation Assistance (FMA) program as well as Pennsylvania state funding sources should be explored as potential funding sources for identified projects. Passage of the 2021 Infrastructure Investment and Jobs Act allocated several billion dollars toward the aforementioned FEMA programs.



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SECTION 1 - INTRODUCTION

1.1 General

The communities of Hemlock Township, Montour Township, and the West End of the Town of Bloomsburg experience frequent and devastating flooding from Fishing Creek and the Susquehanna River. Although the Susquehanna River has been the primary cause of record flood levels in the region, Fishing Creek is the flooding source of most concern to residents of these areas. The fast rising creek provides less warning than the Susquehanna River and brings with flooding fierce velocities, which in the past have pushed homes from their foundations. Residents experienced these impacts during Tropical Storm Lee in 2011 when Fishing Creek rushed through these communities and subsided only to have the Susquehanna River rise to records levels a few days later. Most recently, residents again experienced flooding from Fishing Creek in 2018 with several other storms threatening to swell the creek to flood stage and creating undue anxiety for residents.

Previously completed flood mitigation projects in Columbia County include the Phase 1 Flood Mitigation Project which protects the Autoneum facility, a large regional employer, and the Phase 2 Flood Mitigation Project providing protection to the Bloomsburg High School and many residences in the area. With the completion of these projects, Columbia County desires to continue their flood mitigation efforts in other areas of the county impacted by frequent flooding such as the West End of the Town of Bloomsburg, and neighboring communities Hemlock Township and Montour Township.

In addition to homes, small business, and commercial establishments in this region of the County, the study area also includes the Bloomsburg Fairgrounds where several high profile events and festivals take place each year producing significant benefits to the local economy. As a direct result of the severe flooding from Tropical Storm Lee and other storms, many businesses were forced to cease operations until floodwaters receded and damage from the storm was repaired. Therefore, in addition to the direct flood damage to private property, the economic impacts cause additional hardship to the residents of the area.

1.2 Study Area

The primary focus of the study was the communities located along both banks of Fishing Creek from the Railroad Street Bridge to Fishing Creek's confluence with the Susquehanna River (see Figure 1.1 below). The Townships of Hemlock and Montour are situated along the north bank of Fishing Creek whereas the West End of the Town of Bloomsburg and the Fairgrounds are located on the south bank of the creek. The remainder of the study area south of the creek is primarily comprised of open fields which serve as parking for Fairground events. Maps of the study area are provided in Appendices A & F of this report.

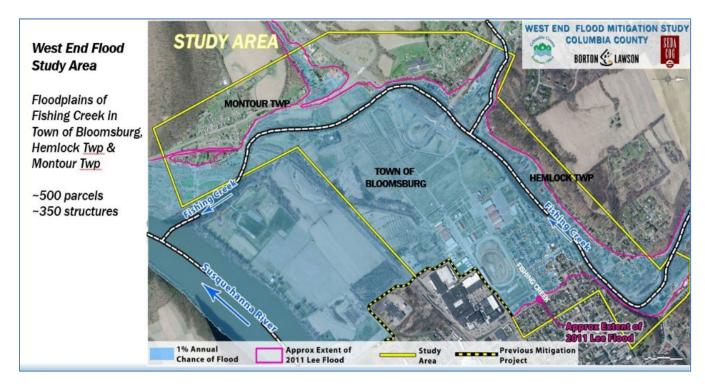


Figure 1.1 Study Area Map

1.3 Purpose and Goals

The purpose of the study is to formulate plans to mitigate the impact of flooding from the Susquehanna River and Fishing Creek in the West End of Bloomsburg, specifically Montour and Hemlock Townships and the Town of Bloomsburg. The primary water resources problem is recurrent destructive flooding. Flood damages are attributable to overbank and backwater flooding from the Susquehanna River and flooding along Fishing Creek. Past flood events have resulted in extensive damages to structures and their contents and have threatened public safety. In addition, floods have disrupted major transportation systems, requiring closure of roads, railroads, and the municipal airport. As indicated in Figure 1.1, extensive portions of the West End study area are within the 500-year floodplain of the Susquehanna River and Fishing Creek. The 500-year floodplain within the study area that was evaluated includes approximately 500 parcels and approximately 350 structures, primarily residential. The largest number of commercial structures within the study area are located within the Bloomsburg Fairgrounds area.

This study contains proposed flood mitigation actions and projects that if implemented would reduce future flood loss and support sustainable communities. Through this study, the proposals can be elevated to the county, state and regional level. The study and the recommendations in it, if adopted, will make the communities more disaster resilient thereby reducing long-term risks to loss of life and property damage from flooding.

This study is unique in that while it will meet the flood mitigation plan requirements of each municipality, it will also employ a watershed management approach through the related and

concurrent Fishing Creek Watershed Study to ensure that final mitigation actions address both local jurisdictional needs and regional multi-jurisdictional needs. Flooding is a hazard that does not recognize political boundaries. To effectively manage the floodplains, mitigation funds need to be administered within politically defined boundaries. As political boundaries seldom coincide with watershed boundaries, this Plan encourages municipalities to consider their watershed and consult with the County and upstream and downstream neighbors when identifying mitigation actions. Local collaboration and partnerships are an effective and necessary means to reducing future flood losses.

There are two types of natural hazard mitigation plans (HMP) recognized by the Federal Emergency Management Agency (FEMA): a Flood Mitigation Plan and an All Hazards Mitigation Plan. As the name suggests, a Flood Mitigation Plan is specific to flooding. For participating municipalities, this Flood Mitigation Plan is an important and significant step towards update of the Columbia County All Hazards Mitigation Plan. It also is a stand-alone document that details regional, county-wide and municipal mitigation actions that when implemented will reduce future flood loss.

The purpose of the Flood Mitigation Plan is to enable participating municipalities to get one step closer to becoming eligible to compete for FEMA funding aimed at flood mitigation. Following a municipal or county-led process to expand this document into the All Hazards Mitigation Plan, municipalities will become eligible for future mitigation funding opportunities through FEMA's Hazard Mitigation Assistance (HMA) Grant Programs. The grant programs include the Flood Mitigation Assistance (FMA) program, the Building Resilient Infrastructure and Communities (BRIC) formally known as Pre-Disaster Mitigation (PDM) program, the Repetitive Flood Claims (RFC) program, the Severe Repetitive Loss (SRL) program and the post disaster Hazard Mitigation Grant Program (HMGP). As a note, an All Hazards Mitigation Plan is not required for the RFC program.

The objectives of this Flood Mitigation Plan are to:

- Increase the coordination and cooperation among intergovernmental entities in carrying out flood mitigation;
- o Demonstrate a firm local commitment to flood mitigation:
- Leverage a wide array of funding opportunities to implement actions;
- o Comply with federal legislative requirements for local mitigation plans;
- Protect life, safety and property by reducing the potential for future damages and economic losses that result from flooding;
- Safeguard essential public facilities and infrastructure;
- Promote a sustainable regional and local economy;
- Heighten public awareness of flood risk; and
- Support natural resource protection.

In summary, this study identified and determined the best structural and nonstructural project(s) to:

- Provide flood resiliency to reduce long-term risk to loss of life and property damage
- Reduce impacts of increasing insurance premiums
- Minimize flooding impacts on the community
- Identify possible funding sources for flood mitigation projects

The recommendations for nonstructural and structural flood mitigation projects have been developed in accordance with the step by step planning process as follows:

- 1. Specify water and related land resources problems and opportunities:
- 2. Inventory and forecast existing conditions;
- 3. Formulate alternative plans;
- 4. Evaluate alternative plans;
- 5. Develop benefit to cost for each alternative
- 6. Compare alternative plans; and
- 7. Select the recommended plans for each community.

The basis for selection of the recommended plans in this study is fully documented below. When any proposed flood mitigation measures would increase existing flood levels in neighboring areas, this study has evaluated measures to mitigate or protect neighboring areas from increased flood levels and associated flood damages. More information on increased flood impacts and mitigation recommendations are provided in this report.

1.4 Prior Studies, Reports, Existing Water Projects

The Susquehanna River Basin is subject to frequent and severe flooding. As such, the United States Army Corps of Engineers (USACE) has conducted numerous studies to identify comprehensive solutions to reduce flood damages throughout the basin. Each of the prior studies was reviewed to identify any and all information that could be used in the current feasibility study.

USACE Studies and Reports

The first known USACE report documenting Bloomsburg's flood problems was submitted to Congress in December 1934. A flood control project for Bloomsburg consisting of levees along the Susquehanna River was authorized by the Flood Control Act of 1936. The authorized plan was reevaluated in April 1942 and found to lack economic justification. As a result, the USACE recommended abandonment of the authorized project.

The Bloomsburg area was evaluated again in 1956, 1970 and 1980 as part of Susquehanna River basin studies conducted by the USACE. Flooding from Fishing Creek was not considered in any of the studies mentioned. Additionally, all of the studies reported a lack of economic justification to proceed with construction of a Federal flood damage reduction project at Bloomsburg.

Section 205 Reconnaissance Study Report - Bloomsburg, Pennsylvania Local Flood Protection, December 1983

The Baltimore District conducted a Section 205 reconnaissance study¹ in 1983. Previous USACE studies had found that providing flood protection for the entire town lacked economic

justification, and that nearly all of the expected annual damages for the Town were found to occur in the area between Fishing Creek, the Susquehanna River, and Railroad Street. Therefore, the USACE 1983 reconnaissance study focused on providing protection for this more downstream, western end of the Town. The study evaluated three (3) structural alternatives, including two levee and floodwall alternatives that provided 100-year level of protection, and a third alternative that provided 500-year level of protection. None of the three plans evaluated as part of the reconnaissance study were found to be economically feasible, with the highest BCR being 0.6 to 1.

Section 205 Initial Appraisal - Bloomsburg, Pennsylvania, August 1994

By the early 1990s, changes to existing conditions in the study area since the time of the 1983 reconnaissance study prompted the Town of Bloomsburg to request a new USACE study to evaluate flood damage reduction measures. In 1994, the USACE completed an initial appraisal study under the Section 205 Continuing Authorities Program. With anticipated increased benefits and decreased construction costs, conservative preliminary calculations indicated that a BCR would range from 0.7 to 1.1. The expected improvement in the BCR warranted another, more thorough, investigation of a flood control project for the Town.

Based on the 1994 study, the cost for construction of a flood control project for Bloomsburg was estimated to range from \$6.5 to \$10 million (1994 dollars). In light of the \$5 million dollar Federal cost-sharing limit at the time for Section 205 projects, it was anticipated a project could not be pursued through the Section 205 Program. Therefore, the 1994 Initial Appraisal Report stated that further study to determine the feasibility of constructing a Federal flood damage reduction project at Bloomsburg was warranted, but recommended that the reconnaissance study be pursued under the General Investigations (GI) Program, which is not subject to the cost limits of the Section 205 Continuing Authorities Program.

Section 905(b) (WRDA 86) Analysis - Bloomsburg Pennsylvania Flood Protection Reconnaissance Study, May 1998

A General Investigations reconnaissance study for Bloomsburg, Pennsylvania, flood damage reduction was authorized by a resolution adopted by the Committee on Transportation and Infrastructure of the United States House of Representatives on 14 September 1995. Federal funds were provided in 1998 for the USACE to undertake the reconnaissance phase evaluation.

The objectives of the reconnaissance phase were to:

- 1. determine if the water resource(s) problems warrant Federal participation in feasibility studies.
- 2. define the Federal interest,
- 3. complete a 905(b) Analysis (refers to Section 905(b) of the Water Resources Development Act of 1986) or a reconnaissance report,
- 4. prepare a project management plan (PMP) that outlines tasks and responsibilities for the feasibility phase of study,
- 5. assess the level of interest and support from non-Federal entities, and

6. negotiate and execute a feasibility cost sharing agreement (FCSA).

Achievement of the six objectives determines whether or not planning to develop a project should proceed to the more detailed feasibility stage. The reconnaissance phase is 100-percent Federally funded and the target for completion is 6-12 months from initial obligation of reconnaissance funds to a signed FCSA.

Past projects were examined with an emphasis on flood protection along the Susquehanna River. The 905(b) analysis evaluated structural alternatives previously considered in past reports, with nonstructural measures evaluated at a lower level of protection. Existing USACE dams that contribute to the reduction of Susquehanna River flooding at Bloomsburg were taken into consideration during this reconnaissance level evaluation. Flood forecast and warning systems for the Susquehanna River just upstream of Bloomsburg were already under consideration as part of the Wyoming Valley Levee Raising Project, so were not specifically examined as part of the Bloomsburg 905(b) Analysis. Further analysis of potential flood forecast and warning system modifications or improvements will be completed during the next phase of the project, preconstruction engineering and design phase (PED).

The 905(b) reconnaissance study determined that there was a Federal interest in proceeding to the feasibility phase of study for Bloomsburg, based on the strong likelihood that flood damage reduction measures for the Town would be economically justified. Following the successful Section 905(b) analysis, the Town of Bloomsburg and the USACE completed negotiations on the feasibility phase project study plan (PSP) in March 1999. The FCSA was executed in June 1999 and the Bloomsburg Flood Damage Reduction Feasibility Study was initiated in August 1999.

The FR/EIS investigated the feasibility of Federal action to address flooding problems and flood damage reduction opportunities for the Town of Bloomsburg. It was performed consistent with Federal water resources policies and practices, including *Economic and Environmental Principles and Guidelines for Water and Related Land Resources Implementation Studies* (P&G, 1983), the USACE *Planning Guidance Notebook* (ER-1105-2-100, 22 April 2000), and *Procedures for Implementing NEPA* (ER 200-2-2, 4 March 1988). Throughout the investigation, the USACE worked closely with the non-Federal sponsor, the Town of Bloomsburg, as well as the Pennsylvania Department of Environmental Protection (PADEP), to (1) describe the range of potential Federal participation in flood damage reduction projects and (2) explain the roles and responsibilities of the USACE and the non-Federal partner in project planning and implementation.

April 2005 – The Bloomsburg, Pennsylvania, Flood Damage Reduction Feasibility Study was conducted under the USACE General Investigations Program. The study was authorized by a resolution of the Committee on Transportation and Infrastructure of the U.S. House of Representatives, adopted 14 September 1995. The resolution states:

Resolved by the Committee on Transportation and Infrastructure of the United States House of Representatives, that, the Secretary of the Army review the report of the Chief of Engineers on the Susquehanna River, New York, Pennsylvania and Maryland, published as House Document No. 702, 77th Congress, to determine whether flood damage reduction measures should be implemented in the town of Bloomsburg, Pennsylvania...

Under this study authorization, a reconnaissance report was completed in May 1998. The reconnaissance study concluded that there is Federal interest in addressing flooding problems in the Town of Bloomsburg. Based on preliminary analysis, the reconnaissance report identified at least one project that would be in the Federal interest. On the basis of these findings, the USACE and the Town of Bloomsburg, Pennsylvania entered into an agreement to perform a cost-shared feasibility study for a flood damage reduction project.

The purpose of the Bloomsburg Flood Damage Reduction Feasibility Study was to evaluate the feasibility of Federal participation in implementing solutions to problems and opportunities of flood damage reduction along the Susquehanna River and Fishing Creek. More specifically, the study:

- identified flooding problems associated with periodic flooding from storms along the Susquehanna River and Fishing Creek, particularly in the Town of Bloomsburg;
- evaluated the technical, economic, environmental, and institutional feasibility of Federal participation in the implementation of a flood damage reduction project; and
- determined if there is local support for implementation of the recommended plan.

As part of the plan formulation process, reconnaissance phase plans were re-evaluated, and other potential flood damage reduction measures were formulated in order to evaluate and select the plan that would maximize net contributions to National Economic Development (NED).

The recommended NED plan was developed to a level of engineering, economic, and environmental detail sufficient to proceed to the preconstruction engineering and design (PED) phase, pending recommendation by the Baltimore District, support by USACE Headquarters and the Assistant Secretary of the Army (Civil Works), and authorization of project construction by Congress. The project was dropped from further consideration due to funding issues related to more stringent federal criteria resulting from the Hurrican Katrina disaster in the southern U.S.

Other Federal Agency Studies

The Federal Emergency Management Agency's Federal Insurance Administration (FIA) completed a flood insurance study of Bloomsburg in 1979 in order to convert Bloomsburg to the regular program of the National Flood Insurance Program (NFIP).

Local Studies

In 1979, the Fernville-Scottown Survival Committee, a citizen's flood control group in Bloomsburg, hired a consulting engineer to develop a flood control plan for the Bloomsburg side of Fishing Creek. The consultant recommended construction of an open-ended levee and floodwall along the Bloomsburg side of Fishing Creek and the removal of the Route 44 bridge in order to provide a 100-year level of protection. In 1980, the citizens group asked the same consultant to develop a plan to provide additional flood protection for the Town of Bloomsburg. The consultant developed a combination road and levee plan to provide 100-year protection for additional areas of the Town, primarily on the west side. This plan was designed to tie into the USACE previously-proposed open-ended levee and floodwall plan for the Bloomsburg side of Fishing Creek in order to provide a continuous system of protection. Projects described in both

of these local studies were found to lack economic justification in the USACE 1983 Reconnaissance Study.

1.5 Existing Upstream Water Projects

Nine upstream USACE dams detain floodwaters from the Susquehanna River:

- 1.5.1 Almond Dam, located about 2 miles northwest of Hornell, New York, on Canacadea Creek:
- 1.5.2 Arkport Dam, located in Steuben County, New York, on the Canisteo River about 1 mile west of the village of Arkport and 5 miles upstream of Hornell, New York;
- 1.5.3 Aylesworth Creek Lake, located on Aylesworth Creek in Lackawanna County, Pennsylvania, about 10 miles upstream from Scranton, Pennsylvania.
- 1.5.4 Cowanesque Lake, located on the Cowanesque River approximately 2 miles above the confluence with the Tioga River at Lawrenceville, Pennsylvania.
- 1.5.4.1 East Sidney Lake, located on Ouleout Creek in Delaware County, New York:
- 1.5.5 Stillwater Reservoir, located about 9 miles north of Carbondale, Pennsylvania, on the Lackawanna River;
- 1.5.6 Tioga-Hammond Dams (two structures); located about 20 miles southwest of Elmira, New York, on the Tioga River and Crooked Creek; and
- 1.5.7 Whitney Point Dam, located on the Otselic River in Broome County, New York.

In addition to the upstream dams, thirty-two local flood protection projects have been constructed (or are currently being constructed) by the USACE along the North Branch of the Susquehanna River basin in New York and Pennsylvania.

The Wyoming Valley lies along the Susquehanna River in Luzerne and Lackawanna Counties in northeastern Pennsylvania. From 1891 to 2003, the Wyoming Valley experienced 57 significant floods along the Susquehanna River. In response to recurrent flood damages, Federally authorized flood damage reduction projects were constructed in the Wyoming Valley during the late 1930s, 1940s, and 1950s to protect against the flood of record up to that time (March 1936). The Federal flood damage reduction projects significantly reduced flood damages along this reach of the Susquehanna River.

In June 1972, Tropical Storm Agnes struck and established a new flood of record for the Susquehanna River basin. During this flood, the Susquehanna River overtopped the levee system in the Wyoming Valley, causing severe damage in the City of Wilkes-Barre and in other communities along the river.

Following Tropical Storm Agnes, the U.S. Congress authorized a project to increase the level of flood protection provided by the existing Wyoming Valley levee system, with limited additional project upgrades. The purpose of the Wyoming Valley Levee Raising Project is to provide protection against a recurrence of the storm of record Tropical Storm Agnes. The project consisted of raising existing levees and floodwalls between three and five feet. The project included a mitigation plan for 32

identified communities (one of which is Bloomsburg) subject to adverse flood impacts related to the Wyoming Valley Levee Raising Project. The levee and floodwall raising was completed in January 2003, but construction of related project elements is ongoing.

1.6 Columbia County Flood Risk Management System

The Columbia County Flood Risk Management system is a local flood risk management system established by Columbia County and the Town of Bloomsburg to mitigate the impacts of flooding. The project is owned by the County and operated, and maintained by the Columbia County Water Mitigation Authority.

The project was constructed in two phases. The first, completed in 2016, extends from Railroad and Fifth Street to West Eleventh Street about 500 feet west of Barton Street. The second phase, completed in December of 2020, extends from West Eleventh Street where the first project ties out to high ground, to Twelfth and Center Street, with a separate length of backwater levee 100 feet east of Catherine Street between Ninth and Tenth Streets.

Columbia County created the Columbia County Water Mitigation Authority by resolution to operate and maintain the entire Columbia County Flood Risk Management System. This action guaranteed all requirements shall be complied with for the constructed project, and specifically to maintain and operate or cause to be operated, without expense to the United States or State of Pennsylvania, all completed flood mitigation structures in accordance with the Code of Federal Regulation, 33 CFR Ch. II, Part 208.

Location

The Columbia County Flood Risk Management System is located approximately 250 feet north of the right bank of the Susquehanna River extending from 4.000 feet upstream of the confluence of Fishing creek with the Susquehanna River to 1,000 downstream of State Route 487 in the Town of Bloomsburg, Columbia County, Pennsylvania.

Brief Description

The project provides a system of levees and appurtenant works consisting of the following features:

- Approximately 12,000 feet of earthen and mechanically stabilized earth (MSE) levees,
- 2,300 feet of H-pile flood wall,
- six (6) stormwater and sanitary pump stations,
- fifteen (15) roadway and railroad closure structures,
- ten (10) drainage structures,
- and overhead and underground electrical transmission lines.

Construction History

Local authorities, with the assistance of Federal and State legislative officials, obtained grant funding, in addition to private funding, to engage an engineering consultant in 2014 to design a mile long flood risk mitigation project for two major community employers, Autoneum and Windsor Foods.

Autoneum, a private company, contributed \$2,000,000 toward the construction cost. The construction of the system was completed in 2016.

Additional funding to extend the system upstream was secured to encompass the Bloomsburg Area School District campus, then extend to Catherine Street at Ninth Street to prevent backwater from entering the protected area. The school district was a major contributor to the cost of the extension project. The extended system of levees and floodwalls reduces flood risks for many residential and commercial structures in the Port Noble section of the Town. This system extension was completed in December of 2020, resulting in a two-mile long overall system constructed over a six year period.

The constructed Columbia County Flood Risk Management System has three distinct but connected segments designed to provide flood risk mitigation for the proposed update to the effective FEMA base flood elevation (BFE) to be adopted during or after the year 2021. The results of the USACE and FEMA study in 2013 after the Lee Flood (Year 2011) formed the basis for the proposed update of the BFE's utilized for design. The risk management levels provided for each system are described below.

System 1- Constructed in 2016, System 1, shown on Figure 1.2, extends from a point 100 feet north of the intersection of Railroad and Fifth Street in a westerly direction. They system then continues along Sixth Street to the rear of the Autoneum manufacturing facility, then in a southerly direction crossing the SEDA-COG Railroad, south to West Eleventh Street, and east to high ground 400 feet west of Barton Street.

The system was designed with a top of system of 484.00 which equates to a river stage of 34.25 feet at the Bloomsburg gauge. The maximum flood of record, Tropical Storm Lee, occurred in 2011 with a river stage of 32.75 feet or Elevation 482.50 at the project location, which is about 1.5' lower than the top of system. FEMA, as of 2021, expects to update the BFE to a river stage of approximately 30.80 feet. This would equate to a freeboard of approximately 3.5 feet for System 1.

System 2 - Constructed in 2020, System 2, shown in Figure 1.3, extends from high ground approximately 300 feet north of West Eleventh Street and 400 feet west of Barton Street, then in a southerly direction. The system then continues east around the campus of the Bloomsburg Area School District to Railroad Street, then east to a tie out to high ground at the intersection of Twelfth and Center Street.

The top of system was constructed to an elevation of 485.00 at its western tie out to high ground where System 1 ends. The increase of one foot versus system 1 provides an increase in the freeboard versus System 1. System 2 features, such as extensive use of full earth levees, permitted higher levels of freeboard while meeting the design standards for the increased heights of system features.

System 3 - (Catherine Street) – System 3 shown in Figure 1.3 was constructed in 2020 under the same contract along a line 100 feet east of Catherine Street, starting 400 feet north of Ninth Street extending south, crossing Ninth Street and then 300 feet south to high ground at Elevation 486.00 approximately 100 feet south of Tenth Street. The updated BFE, 481.30 at this location results in a freeboard of approximately 4.7 feet. This system provides flood mitigation in a backwater area of the Susquehanna River. The system is 1300 feet from the right bank of the river. If a flood management project in the future extended System 2 upstream to a tie-out east of State Route 487, this backwater system would no longer be required.

In addition to the constructed systems, a flood forecasting and warning system serves to further reduce flood damage and loss of life in the Bloomsburg area. It was developed by the Susquehanna River Basin Commission (SRBC) in coordination with the National Weather Service and was deployed in 1980. The system has been continuously updated and enhanced to improve the advanced notice required for emergency operation of the Columbia County Flood Risk Mitigation System.

Local Cooperation

Local cooperation for the Columbia County Flood Risk Management System is not governed by the authorization laws as enacted by Congress since it is a local system funded by non - federal flood control sources, however, the County established a Water Mitigation Authority to operate and maintain the system all in accordance with the federal regulations for flood risk management projects.

Real Estate

System 1 - Autoneum, on behalf of Columbia County, acquired all necessary interests in the real estate and right-of-way required for System 1 of the project including 29-year easement leases for the levee system rights-of-way. The project also required the acquisition of real estate to accommodate wetland mitigation including 15-foot-wide access easements on the landside and flood side of the walls and levees.

Systems 2 & 3 -The Town of Bloomsburg and Bloomsburg Area School District granted or acquired all necessary interests in the real estate and right-of-way required for System 2 & 3 of the project including perpetual easements for the levee system rights-of-way.

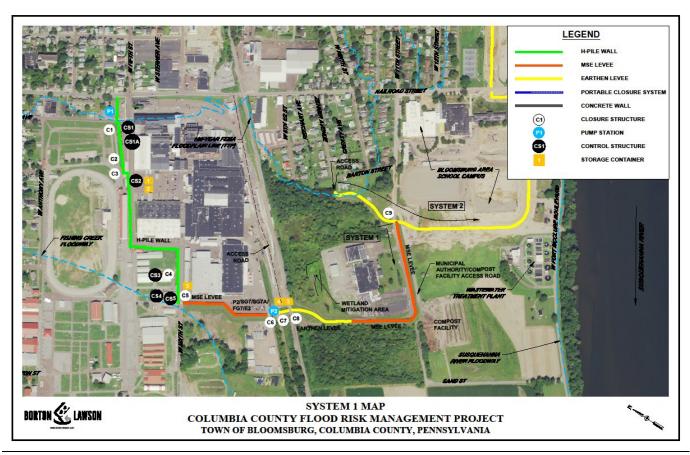


Figure 1.2 -System 1, Location Map

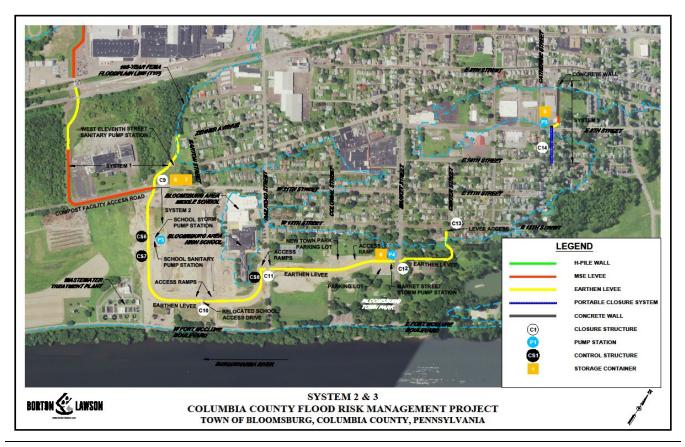


Figure 1.3 –Systems 2 and 3, Location Map

1.7 Scope of Study

The scope of this study addressed the following items:

- Inventory existing conditions;
- Perform building elevation summary;
- Gather community input on possible solutions;
- Assess flood reduction opportunities from upstream mitigation options identified in the separate Fishing Creek Watershed Study;
- Formulate alternatives for flood mitigation;
- Suggest funding alternatives.

The detailed scope as provided in the request for proposals for the study is further outlined below.

Detailed Scope:

- Feasibility of the construction of a potential flood control system,
- Hydraulic and hydrology assessment,
- Permits required,
- Project costs of identified mitigation projects,
- Documentation of needed easements,
- Surveying, mapping, and other plans as necessary to complete the mitigation study.
- 1. Gather and evaluate all existing data available from the County of Columbia, municipalities, industries, and others, including topographical data, hydrology, hydraulics, geotechnical, etc.
- 2. Conduct necessary survey(s) and fill any survey data gaps, establish the need of preliminary right-of-way requirements, including temporary and permanent easements and deed restrictions and delineate the prospective rights-of-way, and prepare conceptual designs for flood protection.
- 3. Perform Technical studies. Any biological assessment, wetland delineation, subsurface geotechnical investigation, and soil testing for hazardous materials were previously identified through the USACE study of 2005 and the need to perform additional work for these issues was not included in the scope.
- 4. Mitigation strategies were to include riparian buffers, wetland and floodplain restoration, flood control structures, buyouts, elevations, and the outcomes realized from these types of strategies, and land use/recreational opportunities in or near the floodway that is in compliance with local, state and federal floodplain regulations.
- 5. Feasibility of constructing a flood control system and/or other flood mitigation actions for the West End of Bloomsburg.
- 6. A detailed geomorphic, hydraulic, and hydrology assessment, identifying the potential impacts to upstream and downstream areas outside of the study area.

- 7. Identify areas prone to flooding (historic and predicted). Assess vulnerabilities under a range of flooding scenarios.
- 8. Recommend mitigation solutions to reduce or eliminate impacts or risks to the upstream and/or downstream areas impacted by proposed mitigation actions.
- 9. Identify other mitigation actions that will decrease flooding in the area, thereby lowering the risk to life and property. Show how the mitigation actions can work as a standalone project or as a larger project or with a combination of activities.
- 10. Estimate all costs and the benefits of each suggested design or solution. Detailed BCA for mitigation actions to enabling the governing body to make an informed decision when ranking potential projects based upon the return of investment of all potential mitigation strategies.
- 11. Listing of permits required for each action identified mitigation action.
- 12. Participate in public outreach by attending public participation meetings and presentations.
- 13. Coordinate and participate in community meetings required to complete this project.
 - An opening kickoff meeting with key stakeholders, which could include local and county officials, community groups, watershed groups, businesses, and landowners,
 - A project mid-way public meeting,
 - A final public meeting to deliver findings.

14. Technical reports

 Final report to summarize the methods, community engagement, field work, findings, and suggested solutions. Includes an itemized list of potential projects identified as a result of the study, potential funding sources and an estimated timeline of completion and return on investment. The report would include electronic copies of any spatial GIS data.

1.8 Participating Jurisdictions

The West End study area included parts of Montour Township, Hemlock Township, and the Town of Bloomsburg in Columbia County, Pennsylvania. As such, the three communities and their businesses and residents were considered stakeholders in the study.

1.9 Report Organization

The main report summarizes the results of the study. Technical appendices, which present details of technical investigations conducted during the study, public meeting presentations, and all other relevant data are provided in a separate volume.

SECTION 2.0 - DESCRIPTION OF THE STUDY AREA / BASELINE CONDITIONS

2.1 LOCATION / DESCRIPTION OF THE STUDY AREA

Bloomsburg is located in the north central portion of the Commonwealth of Pennsylvania approximately 40 miles west of Scranton and 90 miles northwest of Harrisburg, Pennsylvania. The study area is in the Upper Susquehanna Basin along the North Branch of the Susquehanna River, approximately 8 miles above its confluence with the West Branch at Sunbury.

The primary focus of the study was the communities located along both banks of Fishing Creek from the Railroad Street Bridge to Fishing Creek's confluence with the Susquehanna River. The Townships of Hemlock and Montour are situated along the north bank of Fishing Creek whereas the West End of the Town of Bloomsburg and the Fairgrounds are located on the south bank of the creek. The remainder of the study area south of the creek is primarily comprised of open fields which serve as parking for Fairground events. Figure 2.1 below shows the study area.

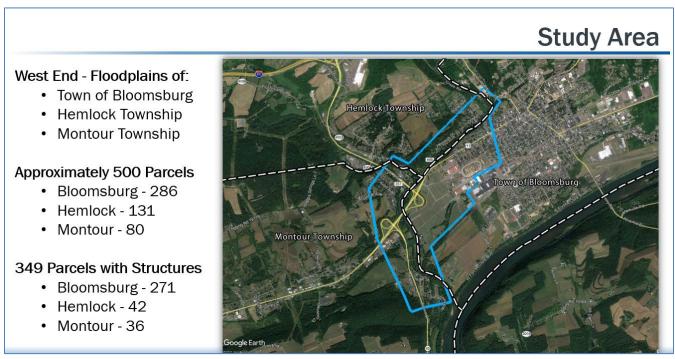


Figure 2.1 Study Area Location Map

Fishing Creek flows into the Susquehanna River and is generally aligned north to south downstream (south) of SR 0011 (Main Street). Upstream (north) of SR 0011 Fishing Creek bends to the east, flowing parallel to SR 0011, north of the roadway. Upstream of the Railroad Street Bridge, Fishing Creek turns back to the north. Given the proximity of the site to the Susquehanna River and Fishing Creek, the West End is subject to extensive flooding from the river and the creek.

The preliminary (2022) FEMA 100-Year Floodplain within the study area is primarily the backwater from the Susquehanna River; conversely, the 100-Year FEMA regulatory floodway in the study area is primarily due to overbank conveyance of Fishing Creek. The Fishing Creek floodway generally

parallels the main channel of the creek but is substantially wider on the south side of the creek. This is because Fishing Creek tends to overtop its banks in the residential area of the West End and flows across Main Street into the open fields owned by the Fairgrounds. This area is low and flat allowing the floodway to spread out considerably on its path to the Susquehanna River.

Past flooding events have impacted property values and the density of housing units and commercial establishments. The flooding of the Storm Lee event in 2011 (Record Flood) and the Fishing Creek flood of 2018 prompted local and state legislative leaders to again request a study to address the repeated flooding issues with flood mitigation proposals.

On the north side of Fishing Creek, Montour and Hemlock Township have conducted buyout projects since the 2011 flooding, thereby mitigating flooding impact for those parcels.

With so many changes in the landscape of the West End since 2011, 2021 aerial mapping was obtained to ensure accuracy of mapping for this study,

2.2 CENSUS DATA

The study area is located in two census tracts; Montour and Hemlock Township are located in Census Tract 503 and the West End of Bloomsburg is located in Census Tract 512.

The two areas were evaluated using two techniques. The first is the FEMA Resilience Analysis and Planning Tool. The tool has 20 Community Resilience Indicators identified at the County level and the census tract level has 12 of the indicators. The indicators are show in the chart. Results for the two census tracts and the county are shown below.

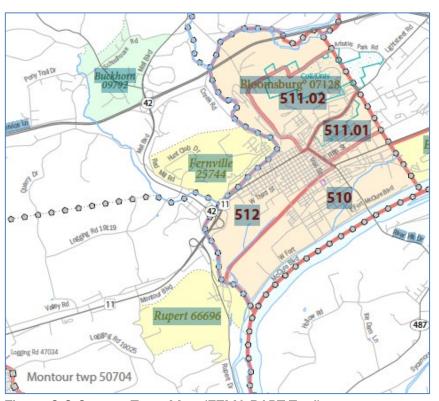


Figure 2.2 Census Tract Map (FEMA RAPT Tool)

A review of the Community Resilience Indicator Analysis (CRIA) Commonly Use indicators shows that the communities in the study area are ranked in the top three highest classifications representing an average to above average resilience.

Table 2.1 CRIA Indicators (FEMA RAPT Tool)

Population-Focused Indicators	Community-Focused Indicators		
CRIA Commonly Used	CRIA Commonly Used		
Indicators	Indicators		
% Population without Health	Connection to Civic/		
Insurance ^{a,b}	Social Organizations		
% Population Unemployed®,b	Hospital Capacity		
% Population without a High	Medical Professional		
School Education ^{e,b}	Capacity		
% Population with a	Affiliation with a		
Disability ^{a,b}	Religion		
% Population without	Presence of Mobile		
Access to a Vehicle ^{a,b}	Homes ^{e,b}		
% Population with Home	Public School		
Ownership ^{a,b}	Capacity		
% Population over 65a,b	Population Change		
% Population Single-Parent Households ^{a,b}	Hotel/Motel Capacity		
% Population with Limited	Rental Property		
English Proficiencya,b	Capacity ^{e,b}		
Median Household			
Income ^{a,b}			
Gini Index: Income			
Inequality			
CRIA Aggregate Resilience Indicatoro			

The Gini Index is a summary measure of income inequality. The Gini coefficient ranges from 0, indicating perfect equality (where everyone receives an equal share), to 1, perfect inequality (where only one recipient or group of recipients receives all the income).

Census Tract 503, Columbia County, Pennsylvania

Tract Population: 4,986

CRIA Indicators

Percent Age over 65: 17.99% Percent with a Disability: 10.54% Percent without HS Diploma: 8.38% Percent Unemployment: 3.50%

Percent Lacking Health Insurance: 2.40%

Percent HH with Limited English

Proficiency: 0.00%

Median HH Income: \$64,518 Percent of Mobile Homes: 8.15% Percent of Owner Occupied

Housing: 79.06%

Percent of Single Parent HH: 10.33%

Vacant Rental Rate: 0.00%

Percent of HH without a Vehicle: 2.04% Income Inequality (GINI Index): 0.42

Figure 2.3 Census Tract 503 Summary (FEMA RAPT Tool)

Census Tract 512, Columbia County, Pennsylvania

Tract Population: 4,204

CRIA Indicators

Percent Age over 65: 15.98% Percent with a Disability: 18.17% Percent without HS Diploma: 11.73% Percent Unemployment: 7.60%

Percent Lacking Health Insurance: 9.40%

Percent HH with Limited English

Proficiency: 0.00%

Median HH Income: \$32,318 Percent of Mobile Homes: 0.00% Percent of Owner Occupied

Housing: 20.06%

Percent of Single Parent HH: 26.50%

Vacant Rental Rate: 7.50%

Percent of HH without a Vehicle: 8.44% Income Inequiity (GINI Index): 0.54

Figure 2.4 Census Tract 512 Summary (FEMA RAPT Tool)

Columbia, Pennsylvania

County Population: 65,715

CRIA Indicators

Percent Age over 65: 18.93% Percent with a Disability: 13.91% Percent without HS Diploma: 9.74% Percent Unemployment: 4.60%

Percent Lacking Health Insurance: 4.40%

Percent HH with Limited English

Proficiency: 0.36%

Median HH Income: \$50,550 Percent of Mobile Homes: 8.70% Percent of Mobile Homes: 8.70% Percent of Owner Occupied

Housing: 60.51%

Percent of Single Parent HH: 18.35%

Vacant Rental Rate: 7.30%

Percent of HH without a Vehicle: 6.53% Income Inequality (GINI Index): 0.45 Percent of Religious Adherents: 46.50% Health Diagnosing and Treating Practitioners

per 1,000: 22.90

Public School per 5,000: 1.52 Hotels/Motels per 5,000: 0.53 Social and Civic Organizations per

10,000: 3.00

Hospitals per 10,000: 0.30

Population Change as a Standard

Deviation: 0.40

Aggregate Resilience Indicator: 0.17

Figure 2.5 Columbia County CRIA Summary (FEMA RAPT Tool)

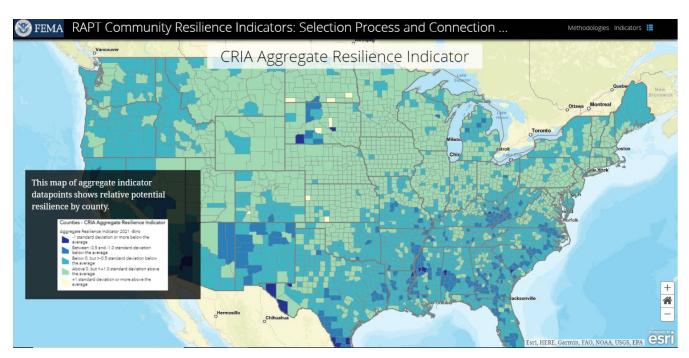


Figure 2.6 CRIA Aggregate Resilience Indicator (FEMA RAPT Tool)

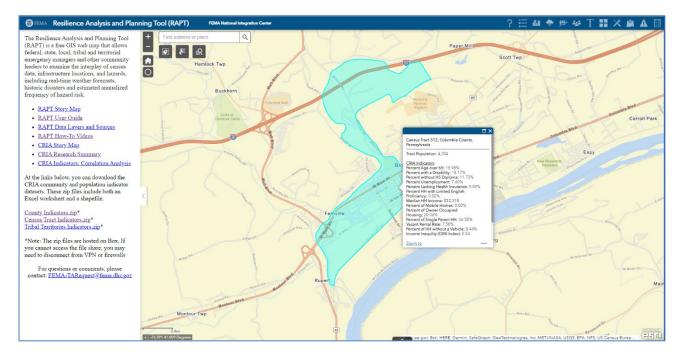


Figure 2.7 Census Tract 512 Location Map (FEMA RAPT Tool)

The second evaluation was the CDC's Social Vulnerability Index (SVI). The Montour/Hemlock Census tract (503) had a rating of 0.2376 (low level of vulnerability) and the Bloomsburg Census tract (512) had a rating of 0.3608 (low to moderate level of vulnerability). Details on the SVI are shown in Figures 2.8, 2.9 and 2.10 below.

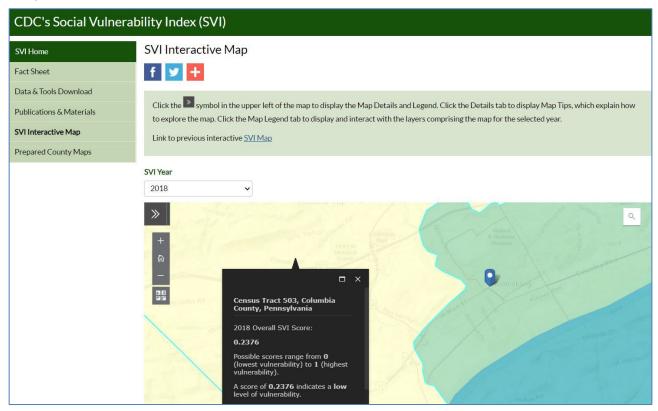


Figure 2.8 Census Tract 503 CDC Social Vulnerability Index (ATSDR CDC SVI)

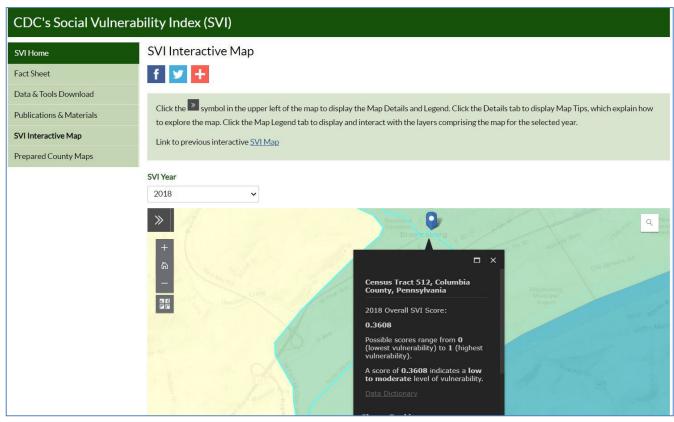


Figure 2.9 Census Tract 512 CDC Social Vulnerability Index (ATSDR CDC SVI)

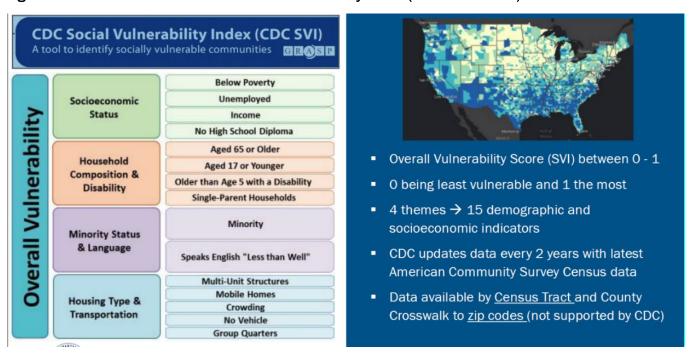


Figure 2.10 CDC Social Vulnerability Index Summary (CDC Schuylkill County PEMA HMGP)

A review of the FY 2021 ACS 5-Year 2011-2015 Low- and Moderate-Income Summary Data shows that the Town of Bloomsburg has a 59.14% Low-Moderate Income Percentage. The Community

Development Block Grant (CDBG) program requires that each CDBG funded activity must either principally benefit low- and moderate-income (LMI) persons, aid in the prevention or elimination of slums or blight, or meet a community development need having a particular urgency. Most activities funded by the CDBG program are designed to benefit low- and moderate-income (LMI) persons. This benefit may take the form of housing, jobs, and services. Additionally, activities may qualify for CDBG assistance if the activity will benefit all the residents of a primarily residential area where at least 51 percent of the residents are low- and moderate-income persons, i.e. area-benefit (LMA).

2.3 BASELINE CONDITIONS / AFFECTED ENVIRONMENT

In April 2005, "The Bloomsburg, Pennsylvania, Flood Damage Reduction Feasibility Study" was issued by the USACE. The study area for that study included generally the same area as this West End study. Data presented in the 2005 USACE study was utilized for this study, updated when necessary. The areal extent of lands that experienced flooding in 2011 is considered the study area. This section describes existing conditions and possible constraints on mitigation proposals.

The 2005 USACE Report is referenced and will not be re-written in this section for environmental conditions, which have not changed or for particular studies contained in that study which are not required for this study. Nearly two decades have elapsed since that study was completed and some environmental findings have changed since that time, and these new findings only are discussed in this section. The information below provides a baseline for measuring expected changes in the physical, environmental, cultural, social, and economic settings that would result from implementation of a flood damage reduction project in the study area.

Physical Setting (See 2005 USACE Report for Physiography, Geomorphology, and Soils)

Climate and Weather

Climate and weather patterns have changed over the last 20 years and so have some of the statistics for Bloomsburg since the 2005 USACE Report. In Bloomsburg, the summers remain warm and wet, while winters are cold and snowy, and it is partly cloudy year-round. Variations in temperatures and precipitation trends have changed over this period. Over the course of the year, the temperature typically varies from 21°F to 84°F and is rarely below 6°F or above 92°F. The warm season lasts for 3.7 months, from May 25 to September 15, with an average daily high temperature above 74°F. The hottest month of the year in Bloomsburg is July, with an average high of 83°F and low of 63°F. The cold season lasts for 3.2 months, from December 1 to March 6, with an average daily high temperature below 44°F. The coldest month of the year in Bloomsburg is January, with an average low of 22°F and high of 35°F.

A wet day in Bloomsburg is one with at least 0.04 inches of liquid or liquid-equivalent precipitation. The chance of wet days in Bloomsburg varies throughout the year. The wetter season lasts 4.8 months, from April 2 to August 29, with a greater than 30% chance of a given day being a wet day. The month with the most wet days in Bloomsburg is June, with an average of 11.5 days with at least 0.04 inches of precipitation. The drier season lasts 7.1 months, from August 29 to April 2. The month with the fewest wet days in Bloomsburg is January, with an average of 6.5 days with at least 0.04 inches of precipitation. The month with the most days of rain alone in Bloomsburg is June, with an average of 11.5 days.

Bloomsburg experiences *significant* seasonal variation in monthly rainfall. Rain falls throughout the year in Bloomsburg. The month with the most rain in Bloomsburg is *September*, with an average rainfall of 3.7 *inches*. The month with the least rain in Bloomsburg is *February*, with an average rainfall of 1.6 *inches*. Bloomsburg experiences significant seasonal variation in monthly snowfall as well. The snowy period of the year lasts for 5 months, from November to April, with a sliding 31-day snowfall of at least 1.0 inches. The month with the most snow in Bloomsburg is February, with an average snowfall of 7.1 inches. The snowless period of the year lasts for the other 7 months (weatherspark.com).

Water Resources

Below is a description of the existing water resources in the study area. State and federal surface water listings have changed some since the 2005 USACE Report and are discussed below. However, hydrogeology and groundwater studies were not part of this updated assessment and can be referenced in the 2005 USACE Report.

Surface Waters

Bloomsburg is within the Middle Susquehanna River subbasin. In the upper part of the subbasin, the Susquehanna River flows southeast through high, flat-topped plateaus separated by steep-sided valleys. Midway down the basin, the Lackawanna River joins the Susquehanna River before turning and flowing southwest toward Bloomsburg.

The Susquehanna River forms Bloomsburg's southern boundary and is the most prominent drainage feature, draining an area of approximately 10,576 square miles. Fishing Creek forms the northern and western boundary of the Town of Bloomsburg and drains an area of approximately 385 square miles at its confluence with the Susquehanna River. Fishing Creek and its tributaries - Huntington, Greene, Little Fishing, Spruce, and Hemlock Creeks - drain the northern nine townships of Columbia County southward to the bend of the Susquehanna River between Bloomsburg and Catawissa.

The middle Susquehanna River sub-basin is a mixture of urban and rural lands that include forest, agriculture, abandoned mines, and urban development. A section of this subbasin was heavily mined and remnants of mining activities (e.g., coal slag piles, abandoned mines, and acid mine drainage) still impact the water quality of many miles of streams and rivers throughout the Wyoming Valley (SRBC, 2002).

According to PADEP's eMAP website, Susquehanna River in this stretch of Bloomsburg also has an attaining use of "impaired" with the source cause being unknown with polychlorinated biphenyls (PCBs) and also having an unknown source of Mercury. Impairment status of Fishing Creek has changed for the better since the 2005 USACE Report. In the previous study, various reaches of Fishing Creek were listed on the PADEP 303(d) Impaired Streams and Rivers List (PADEP, 2002). Several reaches were listed for violations of Aquatic Life Use based on siltation from agriculture, road runoff, and removal of vegetation. Additionally, one reach of Fishing Creek (#20020111-1226-FIT) was listed for violations of Human Health Uses due to mercury. Little Fishing Creek, which flows into Fishing Creek at Bloomsburg, was also listed for violations related to Recreational Use due to pathogens. According to PADEP's eMAP website, Fishing Creek in the

stretch of Bloomsburg has an attained use of supporting aquatic life, potable water use, and fish consumption; and it is not listed as impaired.

Biological Resources

Vegetation (previously addressed in the 2005 USACE Report)

Wetlands (previously addressed in the 2005 USACE Report)

Wetlands were noted in the 2005 USACE Report in the study area. An updated wetland delineation will need to be completed for any projects identified for advancement to preliminary design. Permitting involving anticipated wetland and stream impacts by any proposed structural components of a levee within Fishing Creek and its floodway, as well as any channel modifications to Fishing Creek. Early coordination with agencies such as the USACE, PADEP and PA Fish and Boat Commission (PFBC) will be key to the success of this project in order to ensure all regulatory compliance requirements are met.

Field investigations were conducted along the project area in June 2003 by others to assess and determine the presence/absence of wetlands. The specific area investigated included the footprints and vicinities of two levee alignment corridors under consideration. The wetlands investigation was conducted in accordance with the "Corps of Engineers Wetland Delineation Manual," Technical Report Y-87-1, and specific regulatory guidance modifications subsequently issued.

Within the expected areas of disturbance, wetlands were identified only along the southeastern side of the Bloomsburg Fairgrounds property and delineated using a global positioning system unit. The 11 mapped wetlands (labeled A through K) are shown in Figure 2-3 of the 2005 USACE Report. The wetlands were further characterized as palustrine emergent wetland (PEM), palustrine shrub-scrub wetland (PSS), and palustrine forested wetland (PFO) characterized according to their cover type (Cowardin, 1979). The hydrologic source for these wetlands appears to be from local surface runoff (from parking lots and landfills) and a surface and groundwater connection to Snyder's Run.

In November 2004, a forested wetland system was identified along Fishing Creek's floodplain across the creek from the water treatment plant. This is a typical forested floodplain wetland (PFO) several acres in size with hydrology from both groundwater and overbank flooding from the Creek.

Wildlife (previously addressed in the 2005 USACE Report)

Fish

The previous 2005 USACE Report discussed the fish collected during a survey of Fishing Creek in 1998. The species list indicated that a cool/coldwater fishery existed at that time, and that the coldwater fish, (e.g., trout) were stocked (unknown if natural reproduction was occurring). According to the current PADEP eMapPA, Fishing Creek is listed as a Warm Water Fishery with no special trout listings in the project area by the PFBC. However, Fishing Creek is known for its great flyfishing and many public access areas north of Interstate 80 along Fishing Creek, where the stream inhabits both wild trout and stocked trout.

The proposed earthen/MSE/sheet pile levee would have a slight negative effect on Fishing Creek within the building footprint as it would eliminate the riparian corridor on the left bank of the stream, in turn affecting fish and other wildlife inhabiting this stretch. Mitigation assessment protocols regulated by the governing agencies will allow for compensation in the watershed to make up for this alteration.

Threatened and Endangered Species

Except for the occasional transient species, no Federally listed endangered, threatened, or candidate species under U.S. Fish and Wildlife Service (USFWS) jurisdiction are known to exist in the project area (USFWS, 2000). Therefore, no Biological Assessment or further Section 7 consultation under the Endangered Species Act is required with the USFWS.

However, the Pennsylvania Natural Diversity Inventory (PNDI) indicated that there are potential impacts to state regulated species of special concern within the project area (PNDI, 2022). According to the Pennsylvania Department of Conservation and Natural Resources (PA DCNR), further review of the project is necessary to resolve the potential impact to a "sensitive species" resource with a current status of Special Concern Resource and to the Fassett Jeweled Shooting Star (*Primula fassettii*), a flowering plant with a current status of Threatened.

It is anticipated that a botanical survey will be required for this species, which is time sensitive and would need to occur during its flowering period in late April to May. Further inquiry into the unidentified species is required to determine if a habitat survey will be required.

PFBC requires further review of the project to resolve the potential impact to the Triangle Floater (*Alasmidonta undulata*). If in-stream work is to occur as a result of this project, a mussel study may be required. The study period is not time of year sensitive, however, safety concerns for the malacologist would deter the study from being performed in the winter months.

Air Quality (See 2005 USACE Report for Air Quality)

Cultural Resources

Borton Lawson submitted a project review to the PA Historical and Museum Commission for the Columbia County - West End Flood Mitigation Study (ER Project # 2021PR06578.001) and received a summary letter on November 8, 2021 requesting more information for their environmental review due the high probability for archaeological resources.

It was PHMC's opinion that "a Phase IA archaeological study should be undertaken to assess this property's potential for National Register significant archaeological resources. This study should consist of a thorough review of all available historic through recent maps and other documentary sources which may provide information on past land use within the project area. A geomorphological assessment of the project area is recommended at this stage as it will provide useful information on the total depth and overall integrity of potential archaeological deposits. If this research suggests that potentially significant archaeological resources may be present, it will be our opinion that a Phase I archaeological testing plan should be developed to identify such resources."

The 2005 USACE Report has well documented findings from previous studies that will be utilized in the next phase of the project, as to not duplicate moneys and efforts. Historical and archaeological data does not expire and can be used for overlapping project areas. Additional studies outside of the initial APE are anticipated and will need to be addressed with similar studies. The next two sections below were taken from the 2005 USACE Report, addressing the actions that have been taken to date.

Archeological Investigations

Phase IA archaeological investigations were conducted by KAR in 1999 along the project area. The investigated portion runs from the Route 11 / Route 42 interchange, southeast across the Bloomsburg Fairgrounds parking area, and then generally northeast to the area adjacent to the now vacated Windsor Plant. KAR concluded that there was a high potential for significant archaeological resources in the tested area. The findings were reported to the PADEP and the State Historic Preservation Officer (SHPO) in a letter report, dated 16 July 1999 (KAR, 1999). The report recommended Phase IB testing of all undisturbed portions of the tested area.

The Phase IB investigation of the undisturbed portion of the Phase IA-tested area included a series of excavation units dug along two parallel transects within the project area in the vicinity of the Fairgrounds. Tests along each transect were spaced at 60-meter intervals and were staggered so that there was a test every 30 meters along the corridor. Additional test units were dug whenever suspected archaeological materials were identified.

Forty (40) units of the systematic sample were completed, plus five additional units to examine suspected archaeological materials. None of the latter has been found to meet minimum criteria for an archaeological site, as defined by the Bureau for Historic Preservation. The recovered materials include two chert flakes and one apparently worked piece of chert, found in the plow zones of three separate units in the systematic sample. None of the supplemental tests recovered any additional cultural material.

Further Phase I investigations of the remaining portions of the project area were proposed for spring 2005. The remaining portions to be tested include an area northeast of Windsor, and an area adjacent to the left descending bank of Fishing Creek.

Architectural Investigations

During the initial planning stages for this study, the USACE, PADEP and the Pennsylvania State Historic Preservation Office agreed that due to the uncertainty of the Area of Potential Effect (APE) for the project, it would be necessary to document, at least through a Phase I Level survey, all of the potentially affected historic properties up to a level of flooding equal to the 500-year event.

The following resources were identified within the original APE for this project:

The identification and documentation of National Register districts for the West Main Street portion of Bloomsburg, the Village of Fernville, and thirty individual structures located throughout the APE. Additionally, other new potential historic districts were identified, which consisted of the North Branch Canal workers housing district, a potential district of post-World War I housing, a potential district encompassing the village of Rupert, and individual forms to document the

bridges, rail, and canal resources, Bloomsburg Airport, the Irondale water treatment plant, and Bloomsburg Fairgrounds.

While most of the identified buildings and sites are not located within the project area, the Irondale water treatment plant (currently owned and operated by Suez Water Pennsylvania) is located immediately upstream of the project area.

Other Known Historic Sites

In addition to Bloomsburg's rich background in Native American history, as well as the industrial boom that lasted three-quarters of a century in the 1800's, all of which is discussed in the 2005 USACE Report, other very notable historic structures lie within or close to the project area.

Rupert's Covered Bridge, a historically significant bridge spanning Fishing Creek and located downstream of the project area on TR409, was added to the National Register of Historic Places in 1979 and is the oldest existing bridge in Columbia County. Leonard Rupert settled on Fishing Creek in 1788 and established a village and a ferry where the covered bridge was later built. At just over 185 feet in length, it is Columbia County's longest covered bridge. The bridge has Burr arches with multiple king-post trusses and vertical board siding. After 150 years of continuous use, the bridge was reinforced with steel I-beams and two concrete piers and is open to traffic with no restrictions.

One of the nonstructural mitigation options involves Fishing Creek channel modifications. A recent development is the proposed removal of Boone's Dam along Fishing Creek by its' current owner, Suez Water. Boone's Dam is not listed on PHMC's website as a landmark of historic significance. The dam was built in the 1850's to generate power to the mill that Samuel Boone constructed along Fishing Creek. The dam has been associated with the tranquil setting of the property and Boone's Dam Barn, which has been home to many families over the years, the most famous being artist David Armstrong. The current owners of The Barn at Boone's Dam own and operate a wedding venue. The removal of the dam would not impact the flood flows on Fishing Creek.

The study area is near the Delaware, Lackawanna & Western Railroad (also known as the DL&W or Lackawanna Railroad). This was a U.S. Class 1 railroad that connected Buffalo, New York, and Hoboken, New Jersey (and by ferry with New York City), a distance of about 400 miles (640 km). Incorporated in Pennsylvania in 1853 primarily for the purpose of providing a connection between the anthracite coal fields of Pennsylvania's Coal Region and the large markets for coal in New York City, the railroad gradually expanded both East and West, eventually linking Buffalo with New York City.

The Great Warrior Path is also a known historic resource within the project area, with its eligibility noted as undetermined. The Great Warrior Path travels from present day Athens (then known as Tioga) to Sunbury (then known as Shamokin). This path was used in both times of war and in times of peace. It was often frequented by Iroquois ambassadors who were traveling south.

Hazardous, Toxic and Radioactive Waste (HTRW) (see 2005 USACE Report for Hazardous Sites)

In previous studies within the project area, sites of potential concern were identified. In the URS 2003

report, sampling results revealed elevated concentrations of heavy metals in excess of applicable cleanup levels throughout the project area and volatile organics contamination within an area that passes through an inactive landfill (URS, 2003). Since the heavy metals that were detected are likely a local background condition and since much of the contaminated soil along the project area is considered historic fill, it is likely suitable for reuse during the construction of the flood protection elements from a regulatory perspective (URS, 2003).

Contaminated soil in the landfill area is unlike the material found elsewhere within the project area due to the presence of large amounts of debris and is unsuitable for reuse during construction.

The potential impact of underground storage tanks adjacent to the project area along Fishing Creek must be further defined to determine whether relocation or removal is necessary. There is little concern about potential human exposure to contaminants from drinking groundwater because nearly all residences near the proposed alignment are believed to utilize drinking water delivered by Suez Water Pennsylvania (USACE, 2003).

A Phase II Environmental Site Assessment (ESA) is recommended in the next phase of the project within the project limits in order to complete proper site characterization. The Phase II ESA would consist of a subsurface investigation to identify potential contamination sources that may affect the environmental integrity of the project. The results of the Phase II ESA may be used to ascertain the need for and extent of potential site remediation activities (i.e., Phase III ESA).

Socioeconomics

The Town of Bloomsburg is a rural and moderate density community characterized by attractive single-family residential neighborhoods, tree-lined streets and limited agricultural and industrial land use on the outskirts of town. Bloomsburg is the Columbia County seat and is the only incorporated town in Pennsylvania. The Town has a land area of 4.4 square miles and approximately 4,400 housing units. The Town of Bloomsburg had a population of 14,197 as of July 1, 2021. Bloomsburg ranks in the upper quartile for Population Density and Diversity Index when compared to the other cities, towns and Census Designated Places (CDPs) in Pennsylvania (HomeTownLocator.com).

The age distribution of Bloomsburg has a high proportion of persons in the 18- to 24-year-old category, which would be expected in a town with a moderately sized university. The median household income for Bloomsburg is \$32,217. The economy of Bloomsburg employs about 5,300 people. The largest industries in Bloomsburg are Health Care & Social Assistance, Accommodation & Food Services, and Educational Services, and the highest paying industries are Transportation & Warehousing, & Utilities, Public Administration, and Manufacturing.

Environmental Justice

As stated in the 2005 USACE Report, "Executive Order 12898, Federal Actions to Address Environmental Justice in Minority Population and Low-Income Populations (Executive Order, 1994), directs Federal agencies to identify and address, as appropriate, disproportionately high and adverse human health or environmental effects of their programs, policies, and activities on minority population and low- income populations." According to PADEP eMapPA, the project area is located within an Environmental Justice Area, Census Block Group 2015, Tract 512, Block Group 5 (eMapPA,

2022).

Noise (see 2005 USACE Report for Noise)

Traffic (see 2005 USACE Report for Traffic)

Aesthetics (see 2005 USACE Report for Aesthetics)

The proposed West End Flood Mitigation structures of earth levee, MSE levee with retaining wall, sheet pile levee, pump station, and gate closures, all can fit into the surrounding landscape of the Town of Bloomsburg with the proper design.

Land Use (see 2005 USACE Report for Land Use)

Parks and Recreation

Several state, local, and private park facilities are located near the study area and have been discussed in the 2005 USACE Report. But the most immediate park that the project will affect in a positive way is the Bloomsburg Fairgrounds. The fairgrounds is a 248-acre facility located within Bloomsburg's town limits and includes a grandstand with an 8,000-person seating capacity, 78,000 square feet of exhibition buildings, an indoor arena, a covered band shell, a half-mile racetrack, and other large outdoor event amenities. The Bloomsburg Fair begins the third Saturday after Labor Day and draws over 650,000 people (2003 estimate) from all along the Eastern Seaboard. The Fairgrounds also attracts many trade shows and conventions throughout the year. This project would mitigate the flood risk to the fairgrounds each year in September.

2.4 Existing Infrastructure / Storm and Sanitary Sewers

The three communities in the study area have storm and sanitary sewer systems and related pump stations for the sanitary sewers.

For Montour and Hemlock Townships, the biggest impacts from past flooding were related to the sanitary pump stations being flooding thereby impacting the operation of the pump units and electrical gear.

For Bloomsburg, the sanitary sewer system is extensive throughout the residential and commercial area of the West End. Flood events interrupt the normal flows to the Bloomsburg Municipal Authorities treatment plant located on the Susquehanna River on Fort McClure Boulevard. Past flooding damages essentially require cleanup and minor repairs.

Storm sewers for the residential area drain to Fishing Creek. A total of five (5) outfalls exist along the creek bank from Railroad Street to the Route 11 Entrance to the Fairgrounds near the historic Barton House. The largest outfall, an 84-inch pipe serves interior stormwater runoff from the town primarily east of the project area. These outfalls would need control structures to prevent backwater during high flows in the creek and during high Susquehanna River stages. As stated later in this report, the storm water would be diverted to a new pump station near 6th Street if a levee/floodwall system was built in Bloomsburg.

Storm sewers in the extensive Fairgrounds complex were reviewed with the Fairgrounds maintenance staff but they are not documented and will require extensive surveying to determine location, type, and size for analysis during preliminary design of a structural system is pursued.

2.5 Subsurface Conditions

The average soil thickness for the area is approximately 20 feet with bedrock depths highly variable over the entire project area. Bedrock was encountered as shallow as 8 feet, while it was not encountered at depths greater than 30 feet in several borings.

Along Fishing Creek from approximately, foundation soils are moderately pervious to very pervious with little to no impervious blanket above. A layer of dense gravel exists at a depth of approximately 10 feet. The soils had varying amounts of fines (material passing No. 200 sieve), but most of the soils were classified as sands and gravels. Also along Fishing Creek, bedrock was encountered between depths of 16 feet to 32 feet. Borings along the Bloomsburg Fairgrounds portion of the alignment show a silt/clay blanket (average thickness of 4 feet) overlying a sand/gravel layer. Beneath this sand/gravel layer, highly weathered bedrock was encountered at depths of 10 feet to 20 feet.

Groundwater varies from 4 feet to 20 feet below the surface. It varies on a seasonal basis and is greatly influenced by the river and creek flows. Any deep excavations should consider dewatering techniques in the wet periods of the construction season.

Details of the geotechnical investigations performed for the 2005 USACE Study are included in Appendix B Geotechnical Engineering.

SECTION 3.0 - STUDY DEVELOPMENT PROCESS

3.1 Study Process

Borton Lawson conducted this flood mitigation study under the oversight of SEDA-Council of Governments (SEDA-COG), the study administrator for Columbia County, Pennsylvania. The study was conducted to meet the All Hazard Plan requirements for flood hazards. As such, the recommendations and implementation of any projects should be compatible with community or regional plans for all hazards mitigation.

Assessment of adverse environmental impacts of each flood mitigation option was conducted in accordance with the requirements of Federal and Commonwealth of Pennsylvania regulatory and resource agencies, including: the U.S. Environmental Protection Agency (USEPA), USFWS, PADEP, the PFBC, and the SHPO.

The report was developed using the best available information obtained from a wide variety of sources. Throughout the plan development process, a concerted effort was made to gather information from participating municipal and county agencies, as well as, stakeholders, federal and state agencies, members of the local business and industry community, and the citizens of the Plan area. Thus, the flood mitigation strategies contained within this plan have been developed through an extensive planning process involving local jurisdictions, citizens, county, and state, regional and federal officials. The six steps in the iterative plan formulation process were:

- Specify water and related land resources problems and opportunities;
- Inventory of existing conditions;
- Formulate alternative plans;
- Evaluate alternative plans;
- Compare alternative plans; and
- Select the recommended plan.

The basis for selection of the recommended plans for each community is documented below, including the rationale used in plan formulation and plan selection.

3.2 Flooding Problem

Recurrent flooding that occurs in the study area is a result of the morphology of the Susquehanna River and the regional topography. In the vicinity of Bloomsburg, the river has very little slope and has shallow banks. As a result, the river flows more slowly in this reach. During heavy rainfall events (or rapid snowmelts), the river quickly swells and overflows its banks. Floods along Fishing Creek, as well as along the Susquehanna River, are slow to recede due to the flat topography, thereby isolating areas and exacerbating property damage.

When the Susquehanna River overflows its banks, it hinders normal discharge from Fishing Creek to the mainstem of the Susquehanna, resulting in backwater flooding on Fishing Creek. When the Susquehanna River and Fishing Creek simultaneously rise above flood stage, overbank flooding can cover up to 33 percent of the landmass within the Town of Bloomsburg's boundaries. Monitoring of existing stream gauges upstream of Bloomsburg typically provides at least 4-hours advance warning of potential Susquehanna River floods; however, flooding on

Fishing Creek can happen quickly with little or no warning.

The official flood stage (where flooding starts to cause property damage) is reached when the Susquehanna River water level at the Bloomsburg gauge on the Route 487 bridge exceeds a stage of 19 feet, which equates to 470 feet above mean sea level. The base flood (a flood that has at least a one in 100 chance of occurring in any given year (also called the 100-year flood) is reached at a stage of 30.74 feet, or 481.40 feet above mean sea level at the Route 487 gauge.

3.3 Review and Incorporation of Existing Information

Existing data was utilized to formulate an understanding of the existing flooding conditions. This information included previous studies and flood mitigation project designs. The data was utilized for the early meetings with stakeholders which were geared towards a listening session to gain a better understanding of the expectations of residents and business owners with regard to their flooding problems.

The following categories of existing data were researched and evaluated for use during the study:

Municipal plans and ordinances
Previous USACE Studies including Geotechnical Data
County Parcel Data - Property parcel information, flood zone classifications, etc.
Flood damage reports
Infrastructure mapping
FEMA data/Flood Insurance Studies
FEMA Flood Insurance Rate Maps (FIRMs)
Utilities/Sewers Mapping

3.4 Stakeholder Outreach

Meetings were held with municipal officials at the beginning of the study to understand the impacts of flooding to their communities, confirm past mitigation actions, review possible mitigation alternatives (structural and nonstructural), and to identify specific actions that would make the community more flood resilient.

Montour Township

Montour Township is located on the western side of Fishing Creek in the study area. It is bordered on the west by Montour County. The Susquehanna River and Fishing Creek form the southern and eastern boundaries. The unincorporated community of Rupert is located in the Township. The population (2010) was 1,344.

As part of the Map Modernization Project, FEMA estimated that the municipality has 915 structures with 80 located in the Special Flood Hazard Area (SFHA). Approximately 7% of the population lives in the flood high hazard area.

The study area consists of 63 properties located in the flood plain.

Following the 2011 Tropical Storm Lee flood event, the

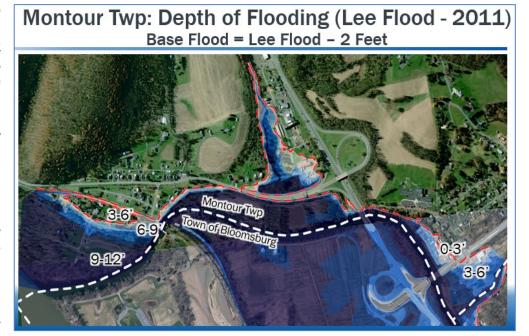


Figure 3.1 Lee Depth of Flooding in Montour Township

Township participated in the FEMA HMGP and acquired twelve properties, eleven of which were in the study area.

Additional properties are being acquired outside of the study area along Legion Road as part of the Department of Housing and Urban Development (HUD) Community Development Block Grant–Disaster Recovery (CDBG-DR) program.

Hemlock Township

Hemlock Township is located on the western side of Fishing Creek in the study area. Montour Township and Fishing Creek form the southern boundary and Mount Pleasant Township the eastern boundary. Madison Township forms the northern boundary. The population (2010) was 2,249. Fernville is located in the southeast corner abutting Fishing Creek.

Hemlock Twp: Depth of Flooding (Lee Flood - 2011) Base Flood = Lee Flood - 2 Feet



Figure 3.2 Lee Depth of Flooding in Hemlock Township

FEMA estimated that the municipality has 1,410 structures with 135 located in the SFHA. Approximately 10% of the population lives in the flood high hazard area. The study area consists of 126 properties located in the flood plain.

Hemlock Township has been active in the FEMA HMGP since 1983. Since the 2011 Flood event, the Township has acquired more than 40 properties using the FEMA HMGP program and the HUD CDBG-DR program. Future acquisitions are planned. Numerous properties have been elevated.

Town of Bloomsburg

The Town of Bloomsburg is located on the eastern side of Fishing Creek in the study area and is the county seat of Columbia County. It is bordered on the west and north by Fishing Creek and by the Susquehanna River on the south. Scott Township forms the eastern boundary. The population

Bloomsburg: Depth of River Flooding (2011)

Figure 3.3 Lee Depth of Flooding in the Town of Bloomsburg

(2010) was 14,855. Bloomsburg University is located in the town.

FEMA estimated that the municipality has 3,160 structures with 560 located in the SFHA. Approximately 8% of the population lives in the flood high hazard area.

The study area consists of 294 properties located in the flood plain, which includes 30 commercial properties and the Bloomsburg Fairgrounds.

The Town of Bloomsburg participated in FEMA HMGP buyouts following the 2011 flood when eleven properties were acquired and demolished. Several structures have been elevated since 2011. Recently additional properties have been identified for acquisition.

The Town participates in the FEMA Community Rating System (CRS) Program and currently is a Class 7 community which provides a 15% discount on flood insurance premiums.

Other Stakeholders

Meetings were held with community stakeholders to determine the impacts of flooding to their organizations and the overall area, learn of any mitigation actions completed since 2011, and identify

problem areas that still needed to be addressed. Meetings were held with the Bloomsburg Fairgrounds, Bloomsburg Municipal Authority, Bloomsburg University, Bloomsburg School District and the Geisinger Health System, which operates the Bloomsburg Hospital.

Bloomsburg Fairgrounds

The Columbia County Agricultural, Horticultural and Mechanical Association, owner of the fairgrounds, is the largest property owner in the study Their holdings area. include 227 acres with for 20.000 parking vehicles, RV Parking (no facilities), a large racetrack, one-half mile dirt racetrack, a grandstand with seating for 5,400 (under and roof)



Figure 3.4 Town of Bloomsburg Fairgrounds Parcel Location

numerous exhibit halls, restrooms and barns. Overall 54 structures are located on the property.

3.5 Public Participation

Three (3) Public Meetings were held as part of the Study.

The first public meeting introduced the public to the project and provided information related to the Public Outreach Plan. Maps of the project area were available for viewing. Valuable information was collected from residents related to unique features in the project area and their project-related concerns through oral comments and written questions submitted via the project website.

The second public meeting was held to review the progress of the study and future work to be accomplished. It provided an opportunity for the public to provide comments on the project immediately before completion of the study.

The final public meeting was held in March of 2022 to provide an overview of the study findings and recommendations for nonstructural and structural flood mitigation alternatives. The following items were discussed.

- A description of the study area and scope,
- Completed flood mitigation work by the communities,
- Options analyzed,
- Results of the hydrologic and hydraulic modeling,
- Flood Mitigation recommendations for each community,
- Adverse impacts and mitigation options.
- Funding opportunities,
- Draft opinion of probable construction costs,

Next Steps.

For further details of the meetings, see public meeting presentations in Appendix D.

3.6 Homeowner / Property Owner Surveys

The 2021 Floodplain Homeowner Survey was designed to capture input from property owners to inform the County's efforts and provide context to the Consultant's evaluation of flooding risks. Questions were developed to glean information on the following: attributes of the structures on study area properties, residents' "lived" experiences regarding flooding, damages experienced due to flooding, mitigation measures currently in place to reduce flooding damage, and impacts to daily life. In addition to collecting details regarding structure attributes and flooding history, a primary objective of the Homeowner Survey was to collect data to understand homeowners' plans or preferences for the future regarding relocation.

The Survey contained 19 questions and was designed to take 5-10 minutes to complete. The first four (4) included questions verifying the property owner's mailing address and the address of their property within the study area, to support tracking and documentation efforts. Questions five through nine (5-9) covered specific attributes of the structure on the property, including the use of the structure, the number of current inhabitants, the presence of a basement, the type of foundation on which the structure is built, and the number of stories. Questions 10 through 13 were designed to gather information on the property owner's past experiences with flooding, the types of property damage they have experienced due to flooding, and the types of measures they have put in place to prevent or reduce flooding. Questions 14 through 16 covered property owners' participation in flood insurance programs, the additional assistance needs of occupants in the case of flooding, and property owners' perceptions of the risk of flooding to the community. Questions 17 and 18 gauged respondents' interest in moving to a new location as a result of flooding, as well as any additional impacts to daily life they have experienced as a result of flooding. Lastly, Question 19 sought to identify what methods of communication would be most effective in reaching out to property owners regarding the West End Flood Mitigation Study in the future.

The Consultant Team identified 349 parcels in the Study Area on which a structure currently existed. A letter outlining the purpose of the survey and directions for its completion accompanied the survey. Each letter also included a Structure ID specific to each property that respondents were advised to include as the response to the first question of the survey, to support data analytics. The survey was kept open for approximately six weeks to allow property owners sufficient time to complete the survey and encourage a high response rate.

A total of 123 of the survey recipients returned a completed survey, which reflects a thirty-five percent (35%) response rate.

To better understand the history of flooding in the community, respondents were asked to identify if their properties have ever flooded from major storm events or nuisance flooding. Of the 122 respondents to this question, ninety-seven percent (97%) reported that their property has flooded in the past, and only three percent (3%) reported that their property has not flooded.

Survey Distribution

- Surveys were mailed on September 21, 2021, to the property owners of all 349 parcels in the Study Area. A letter outlining the purpose of the survey and directions for its completion accompanied the survey.
- Respondents could return their completed survey via mail or complete the survey online using the provided link and QR code.

Survey Response Rate

123 survey responses - Response Rate: ~35%

Figure 3.5 Survey Distribution and Response Information

Respondents were asked to identify the types of property damage that have been incurred to the structure on their property following flood events. Respondents were provided with the following list of types of property damage and were prompted to select all that applied:

- · Basement or below grade flooding
- Finished first floor flooding
- Finished second floor flooding
- No property damage experienced due to a flood event

Eighty-nine percent (89%) reported that the structure on their property experienced basement or below grade flooding, and seventy-nine percent (79%) reported that structure on their property experienced finished first floor flooding. Only three percent (3%) of the respondents reported that the structure on their property had never experienced property damage due to a flood event.

Upon review of the survey results, key trends and themes gleaned from the experiences and perspectives of property owners in the Study Area have been identified:

- Sixty-three percent (63%) of the respondents reported that flooding from Fishing Creek was
 of greater concern to them than flooding from the Susquehanna River. Thirty-one percent
 (31%) identified flooding from both Fishing Creek and Susquehanna River to be of major
 concern.
- While ninety-seven percent (97%) of the respondents reported that their property had experienced flooding in the past, only fifty-eight percent (58%) reported that their property was insured for flooding.
- Eighty-eight percent (88%) of respondents consider flooding to be either a serious or extreme challenge for the community.
- Forty percent (40%) of respondents reported that they do not have any measures in place to prevent or reduce flooding or flood-related damage to their property.

 Forty-five percent (45%) of respondents reported having considered moving to another location to avoid losses and damage due to flooding, demonstrating that a significant proportion of the community may be interested in relocation.

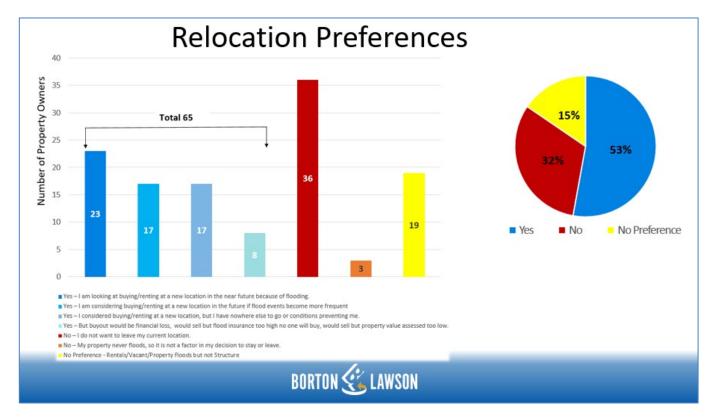


Figure 3.6 Summary of Responses from Relocation Survey Question

 The majority of respondents reported having witnessed a range of negative impacts to the community as a result of flooding, including loss of electricity, lack of clean drinking water, damage to personal possessions, and concerns for personal safety.

3.7 Summary of Stakeholder Meetings

The Study team Mitigation alternatives are classified into either structural (earthen levee/flood wall) or nonstructural (home acquisitions, elevation raisings, flood proofing, etc). The Study will evaluate induced flooding as a result of structural alternatives and financial impacts to the municipality as a result of nonstructural alternatives.

Municipal officials were provided a color-coded parcel map that identified approximate extents of Tropical Storm Lee flooding as well as vacant parcels, buyout parcels, and parcels located within the FEMA designated floodway and floodplain. Municipal officials were asked to provide feedback on the accuracy of the maps.

Montour Township

Study	Area Properties			
	Buyouts (FEMA)	10		
	Buyouts (Proposed)	1		
	Floodway	7		
	Floodplain (Zone AE)	24		
	Vacant	19		
	Mapped Out	2		
	Total	63		
	Commercial	6	9%	
	Residential	29	46%	
	Vacant	27	43%	
	No Land Use	1	2%	
	Total	63	2 /0	
	Iotal	03		
Proper	ty Values			
•	Fair Market Value (Assessment)	\$2.7 M		
	Assessed Value	\$1.4 M		
	Fair Market Value (CLR)	\$5.8 M		
		, c.c		
Taxes				
	Municipal	\$14,733		19%
	County	\$13,823		18%
	School	\$49,777		64%
	Total	\$78,333		
		,		

The following items were discussed at the meeting:

- 9 Perry Avenue was identified for acquisition.
- The County building located on Perry Avenue has experienced frequent flooding damage and is currently not used except for the rear of the building which is still utilized by the maintenance department.
- Most of the mobile/manufactured homes located within the mobile/manufactured homes park on Perry Avenue were flooded as a result of Tropical Storm Lee. The preliminary FEMA mapping shows the SFHA increasing on this property.
- The Montour Township ordinance regulates the 500-year floodplain by requiring permits for any development within this zone.
- An evacuation plan is required from the RV park by the township ordinance. Regulations
 are not followed and an evacuation plan has not been provided as of this time.
- The Township is interested in buying out a property along Hemlock Creek where inoperable vehicles are stored on the property and near the creek.
- There are three (3) sanitary pump stations located within the study area that are impacted by flooding.
 - Pump Station on Hock Road becomes inundated and needs to be raised.

- Pump Station on Perry Avenue has had electrical components raised.
- Design has been completed to raise the electrical components of the pump station located near the campground.

Hemlock Township

Study /	Area Properties			
	Buyouts (FEMA)	37		
	Buyouts (Proposed)	18		
	Floodway	12		
	Floodplain (Zone AE)	25		
	Vacant	25		
	Mapped Out	9		
	Total	126		
	Exempt	56	44%	
	Commercial	2	2%	
	Agricultural	1	1%	
	Residential	58	46%	
	Vacant	9	7%	
	Total	126		
Proper	ty Values			
	Fair Market Value (Assessment)	\$3.1 M		
	Assessed Value	\$1.5 M		
	Fair Market Value (CLR)	\$7.9 M		
Taxes				
	Municipal	\$14,894		15%
	County	\$17,705		18%
	School	\$63,755		66%
	Total	\$96,354		

The following items were discussed at the meeting:

 A large number of buyouts occurred as part of an HMGP Project (~2013) after Tropical Storm Lee in 2011. Properties that withdrew or were administratively withdrawn include:

24 William Street

270 William Street

- It was asked if the properties within the study area are renters or owners. The Township replied that properties are primarily owner occupied.
- It is noted that many of the homes located along the upper side of Drinker Street, though situated on higher ground, still experience significant basement flooding. 399 Drinker Street was highlighted as experiencing basement flooding to the floor joists during Tropical Storm Lee.

- Evacuation Routes and Planning are a priority for the Township as many properties become isolated when Fishing Creek flooding occurs. Red Mill Road floods blocking evacuation to the west and Bloom Street/Creek Road floods blocking evacuation to the east.
- A potential solution could be the construction of a gated stone road connecting Hassert Lane to Laurel Drive to serve as an emergency evacuation route. Hemlock Township officials replied that there is an existing field road from Red Mill Road that has been used by emergency services to reach otherwise inaccessible areas. A deep gully between Hassert Lane and the Ferncliff Road community would prevent these residents from utilizing this potential evacuation route if Bloom Street is flooded unless a bridge or culvert was constructed across the gully.
- A solution providing an alternative exit route does not solve the issue of flooding along Creek Road. Township officials are interested in a plan to raise the profile of Creek Road above the floodplain.
- The implementation of a structural flood mitigation solution in the West End of Bloomsburg
 would result in induced flooding on the opposite bank in the community of Fernville.
 Induced flooding could impact homes which are not currently impacted or homes which
 have already been elevated. A structural option such as a floodwall or earthen levee would
 be required to include a mitigation component for impacted communities upstream and
 downstream of the project.
- Hemlock Township has a sewer co-op. A sanitary pump station located at Red Mill Road and Drinker Street has been elevated.

Town of Bloomsburg

<u> </u>		_	
Study	Area	Pron	erties

Buyouts (FEMA)	11
Buyouts (Proposed)	1
Floodway	106
Floodplain (Zone AE)	118
Vacant	17
Mapped Out	0
Zone X	41
Total	294

Property Breakdown

Exempt	24	8%
Commercial	23	8%
Commercial Apartments	7	2%
Agricultural	1	
Residential	221	75%
Vacant	16	5%
No Land Use	2	
Total	294	

Property Values

Fair Market Value (Assessment)	\$17.4 M
Assessed Value	\$ 8.6 M
Fair Market Value (CLR)	\$44.7 M

Taxes		
Municipal	\$157,730	24%
County	\$110,278	17%
School	\$397,119	60%
Total	\$665,128	
Floodway	\$341,345	51%
Floodplain	\$242,283	36%
Zone X (Not in Total)	\$ 73,234	11%
Total	\$583.628	87%

The following items were discussed at the meeting:

- Bloomsburg differs from the other municipalities in that approximately 40 percent of the study area is located in the Floodway. In addition, the majority of the 226 acre Bloomsburg Fair parcel is located in the Floodway. No new construction or substantial improvement is allowed in the Floodway.
- The Town participates in the FEMA CRS program and is a Class 7 Community.
- The Town is very active in providing flood information to its citizens through its webpage, public meetings and mailings.
- The Town is concerned about the loss of tax revenue if properties are acquired and demolished.
- The Town expressed an interest in Mitigation Reconstruction for homes in the Floodplain.
- The Town indicated they would like a stream gauge on Fishing Creek to monitor stream flows and flood occurrences from Fishing Creek to the Town.

Bloomsburg Fairgrounds

The Fairgrounds leadership provided Economic studies held on the fairgrounds. The Bloomsburg Fair Assessment completed by the Bloomsburg University Center for Community Research and Consulting (2012) estimated the direct spending to the Fair was \$26.8 million dollars. Using the economic multiplier for Columbia / Montour region the total economic impact was \$30.5 million. The 2012 Covered Bridge Festival completed by the Research Media students at Bloomsburg University showed a direct economic impact of \$8.6 million and an overall economic impact of \$14.2 million dollars.

It was discussed that the depth of flooding was too deep to consider dry floodproofing methods. The Fairgrounds advised that the Exhibition Halls had the utilities relocated above the BFE.

Several of the newer buildings were constructed with flood vents and in compliance with the Town's floodplain regulations.

The Fairgrounds would provide insurance information since the county parcel data does not provide individual values.

Other Stakeholders

Virtual meetings were held with representatives of Bloomsburg University, Bloomsburg Area School District and the Geisinger Healthcare System.

Bloomsburg University

The University had one property located on Main Street acquired and demolished following the 2011 Lee Flood event.

Flood events impact the University in multiple ways. Staff and students cannot travel to the University nor can supplies be delivered.

Water supply and electrical power disruptions last for days after the water recedes. They noted that the water company relocated some of its facilities to make the system more disaster resistant. The electrical substation was being relocated out of the flood plain.

The University operated a gauge on Fishing Creek in prior years but the program is no longer active.

Bloomsburg Area School District

A meeting was held with the Bloomsburg school district administrative staff. Key feedback we received from the school district was their primary concern with a loss of school tax revenue with the implementation of the flood mitigation alternative for property acquisition and demolition. The school district high school and middle school property has a recently constructed flood risk mitigation system (i.e levee system) around the perimeter of the property.

Geisinger Health System

Similar to Bloomsburg University, the major impact of flood events is the ability to access Geisinger facilities. The hospital is located in Bloomsburg and the main Geisinger Hospital is located approximately ten miles away via Route 11.

Since 2011, Geisinger has upgraded the water distribution system at the Bloomsburg Hospital. Also, a mass notification system using emails and texts was implemented to keep staff informed of changing conditions.

In summary, the common concerns were:

- Access:
 - o Route 11 to Geisinger Danville
 - Staff
 - o Supplies
- Loss of Utilities:
 - o Electric
 - Water
- BASD and University Impact to students;
- Municipalities, BASD Loss of tax base;
- Fairgrounds Loss of revenue, loss of service to community.

Since 2011, the following mitigation actions have been completed:

- Drinking water Treatment Plant was rebuilt;
- Upgrades made to the PPL Substation / Distribution System;

2 Levee Systems have been constructed.

3.8 Study Webpage & Study Contacts

As part of the public outreach a Study Webpage was hosted by SEDA-COG at https://seda-cog.org/departments/flood-resiliency/columbia-county-flood-mitigtion-studies.

A study email was hosted by Borton Lawson at floodstudy@Borton Lawson.com.

The web site allowed users to obtain information on Public Meetings, the project schedule, surveys and the ability to contact the study team for questions and comments via email.

Next Study Update.... Final Public Meeting – February/ March 2022 FOR MORE PROJECT INFO... Study Webpage https://seda-cog.org/departments/flood-resiliency/columbia-county-flood-mitigation-studies Send Questions/ Comments floodstudy@borton-lawson.com BORTON ELAWSON

Figure 3.7 Study Webpage and Contact Information

SECTION 4 - FLOOD HAZARD IDENTIFICATION AND PROFILING

4.1 Location and Extent of the Flood Hazard

The preliminary (2022) FEMA FIRM for the West End study area shown below demonstrates the vast extents of the 100-year floodplain in this area. The floodplain shown is for a concurrent flooding event on the Susquehanna River and Fishing Creek. The wide floodway is due to Fishing Creek overbank flows at the base flood levels absent concurrent river flooding.

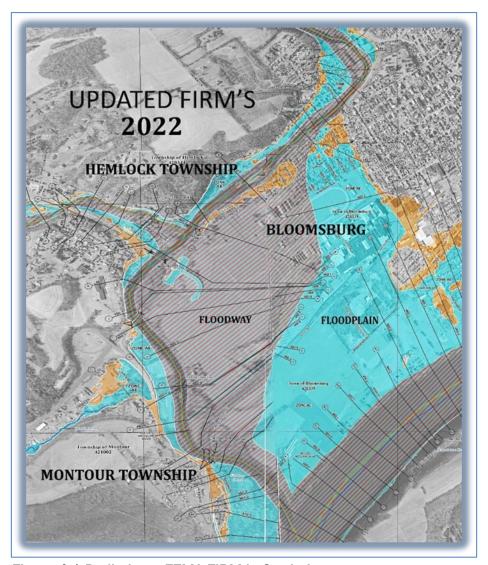


Figure 4.1 Preliminary FEMA FIRM in Study Area

4.2 Nature of the Flood Hazard / Types of Flooding

There are two sources of flooding in the West End study area of Bloomsburg. The first is backwater flooding from the Susquehanna River and the second is overbank flooding from Fishing Creek which tends to be a much more destructive flooding hazard due to the velocity of the floodwaters.

With the very large watershed of the river, over 10,500 square miles, the river usually lags by a day or two any flood events on Fishing Creek, which has a much smaller watershed of 355 square miles. In the FEMA Flood Insurance Study (FIS), the 100-year flood profile notes that BFE's in Fishing Creek are controlled by backwater from the Susquehanna River to approximately Leonard Street. Upstream of this point the FIS shows the BFE's on Fishing Creek exceed the BFE's on the Susquehanna River. Examination of the flooding data for the H&H analysis of this study revealed two recent cases when the flooding from Fishing Creek caused damages that were unrelated to the river level as the creek was cresting. The first was in the Storm Lee flooding of 2011. Fishing Creek flooded at record levels the day before the river crested. The overbank flows from Fishing Creek caused wide spread damage as shown in the History of Flooding section below. Severe damage at the Railroad Street bridge roadway approach (See Figure 4.2 below) and in the residential area of Fernville near and upstream of Railroad Street occurred a day before the river crested.



Figure 4.2 Fernville Side of Railroad Street Bridge - 2011 Tropical Storm Lee

In 2018, Fishing Creek recorded its fourth highest flooding level of all time. The Susquehanna River crested two days later but with little impact on the areas impacted by Fishing Creek.

These flood events, seven years apart, help explain why the residents of the West End fear flooding from Fishing Creek more so than flooding from the Susquehanna River, even though the Susquehanna River is responsible for 80% of the high stage flooding.

Any flood mitigation alternatives must consider both types of events, especially for high velocity out of bank creek flows as compared to the lake effect of river backwater.

4.3 History of Past Flooding

Communities along the Susquehanna River have long experienced floods of devastating proportions.

Native Americans first told of serious floods occurring about every 14 years along the Susquehanna River. Since the early 1800s the main stem Susquehanna River has flooded on average once every 20 years. Table 4.1 below ranks the top flood events for Fishing Creek and the Susquehanna River over the last 85 years.

Table 4.1 Ranking of Major Floods

Major Floods Ranked							
Fishing Creek @ West End of Town					Susquehanna River		
Return Period	COE Modelling Updated with Lee Event 2011	Rank	Date		Recurrenc (Floods Date Interval after 1920)		Date
500 yr	89,600				500 yr		
350	78,700	1	2011		250 yr		
250 yr	75,300					1	2011
100 yr	58,900					2	1972
95	57,900	2	2006		100 yr		
50 yr	48,200					3	2006
45	43,400	3	1972		50 yr		
35	42,000	4	2018			4	1936
30	41,300	5	1975			5	1975
25 yr	38,800					6	2004
14	29,900	6	1996			7	1996
10 yr	28,000					8	1940
		7	1976		25 yr		

Stream flow data covers past 85 years.

The top 5 major floods on Fishing Creek have all occurred in the last 50 years (1972, 1975, 2006, 2011, 2018).

Generally, river flooding occurs at the same time as the creek flooding, except in 2018.

Creek flooding can precede river flooding, which happened in 2011.

Figure 4.3 shows high water marks on a barn at the Fairgrounds to demonstrate the frequency of flooding.



Bloomsburg Fairgrounds

High water marks on barn behind grandstand

35 floods impacted Fairgrounds over last 120 years

1972 (Agnes Flood) 6 inches higher than Base Flood, has essentially become the new reference for the "100-Year" Flood

Figure 4.3 High Water Marks at The Bloomsburg Fairgrounds

Figure 4.4 indicates the five (5) most severe events on Fishing Creek, four (4) were accompanied by high Susquehanna River flood levels.

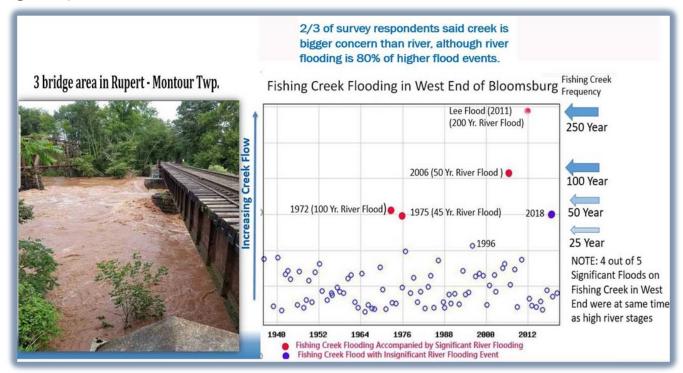


Figure 4.4 Fishing Creek Flooding Data

The Fishing Creek flooding of 2011 was devastating to the lower West End. Record Creek flooding preceded the river flooding. See Figure 4.5 below. The 2018 Creek flooding in the West End reinforced the residents' fears of creek flooding as their biggest concern. Water moves with a destructive velocity.



Figure 4.5 Year 2011 Fishing Creek Flood Damage at Route 11 near Route 42

4.4 Significant Historical Flood Events

The following is a summary of the most significant Susquehanna River and Fishing Creek floods that affected Bloomsburg and surrounding communities. The events are described in a time sequence, beginning with the most recent significant event.

August 2018 - Fishing Creek Flood

After several days of heavy precipitation in Columbia County and many other parts of Pennsylvania, Fishing Creek flowed over its banks in the West End of Bloomsburg. The creek flows were the fourth highest ever recorded and occurred only seven years after the record flooding of Tropical Storm Lee in 2011. Street flooding occurred in Bloomsburg and adjacent communities. Some properties below Railroad Street along Fishing Creek experienced basement flooding. Upstream of Railroad Street in Fernville, the water rose to within 3 feet of the 2011 flood levels.

The unique nature of this flood event on Fishing Creek was the relatively low level of the Susquehanna River flooding which crested at a 22.7 foot stage or 3 feet above flood activation stage. It was the 23rd highest crest on the river, two days after Fishing Creek crested at its 4th highest crest ever.

September 2011 - Storm Lee Flood

In September 2011, the remnants of Tropical Storm Lee dumped significant amounts of rain over nearly all central and eastern Pennsylvania resulting in some of the worst flooding in the region's history. The most severe flooding affected municipalities along the entire Susquehanna River including Bloomsburg, Danville, Wilkes-Barre, Sunbury, and Harrisburg. President Obama issued a major disaster declaration for the state of Pennsylvania on September 12, and it is estimated that over \$1 billion dollars in losses resulted from the impacts of Tropical Storm Lee.

The Town of Bloomsburg and surrounding communities experienced major flooding in areas along the Susquehanna River (south), Fishing Creek (north and west), and the West End at the confluence of the Susquehanna River and Fishing Creek. The Susquehanna River in Bloomsburg crested at over 32.75 feet making Tropical Storm Lee the highest flood on record. A Geographic Information Systems (GIS) analysis estimated that 2,400 structures may have been damaged by flood waters.

The flooding of Tropical Storm Lee created a groundswell of support for flood mitigation projects in Columbia County that has resulted in completion of two flood mitigation systems since that time.

January 1996 Flood

Torrential rains and massive snowmelt from the Blizzard of 1996 caused the Susquehanna River to crest at 26.76 feet at Bloomsburg in January. The blizzard covered much of Pennsylvania with several feet of snow by 13 January. All Pennsylvania counties were included in a Presidential Disaster declared on 21 January in response to flooding from rapid melting of the snow. The flooding forced hundreds of Bloomsburg and Fernville residents to be evacuated, and flooding of the water treatment plant left residents without water for several days. The Federal Emergency Management Agency (FEMA) estimated that the agency provided over \$2.2 million (1996 dollars) in aid to Columbia County as a result of the blizzard and subsequent flooding.

September 1975 - Storm Eloise Flood

The September 1975 flood was caused by Hurricane Eloise which was one of the deadliest Category 3 hurricanes ever recorded. The storm weakened rapidly after landfall and was downgraded to a tropical storm while over east central Alabama, and further downgraded to a tropical depression while

over eastern Tennessee. The storm was downgraded to an extratropical depression while located over West Virginia, but the remnants of the storm merged with a stationary front over New York, Pennsylvania and Maryland on 23 September, producing major flooding throughout the Susquehanna River Basin. Bloomsburg's gauge registered a crest of 27.50 feet on 27 September, and parts of Main Street were covered with two feet of water.

June 1972 - Tropical Storm Agnes

Devastating floods occurred across the Mid-Atlantic region due to the remnants of Hurricane Agnes in late June 1972. Hurricane Agnes came onshore over the Florida Panhandle during the afternoon of 19 June. The storm weakened to a tropical depression over the Carolinas only to re-intensify to tropical storm strength as it reached the Virginia coast on 21 June. The storm then moved north, weakening to extra-tropical strength as it passed just west of New York City, and before curving to the west across central New York. The storm then looped back to the east, crossing northern Pennsylvania before dissipating.

The remnants of the storm moved slowly across Pennsylvania. Rainfall amounts throughout central Pennsylvania for the four-day period of 20 June to 24 June typically ranged from 8 to 10 inches. The heaviest rain (12 to 16 inches) fell in a corridor from Williamsport, Pennsylvania, south through Harrisburg and York. The heaviest reported 24-hour rainfall was recorded at Harrisburg, Pennsylvania, where 12.53 inches fell between 8:00pm on 21 June and 8:00pm on 22 June. The heavy rains from Tropical Storm Agnes followed a relatively wet May, in which 3 to 4 inches of rain fell across the area, and grounds were nearly saturated. As a result, the Susquehanna River at Bloomsburg crested at 31.20 feet on 25 June, with an estimated discharge of 350,000 cubic feet per second (cfs).

Fifty deaths were attributed to Tropical Storm Agnes in Pennsylvania. In 1972 dollars, total damages from Tropical Storm Agnes reached over \$3 billion dollars nationwide, with over \$2 billion dollars in losses occurring in the Susquehanna River basin.

Agnes forced large-scale evacuations in Bloomsburg and produced widespread destruction of personal property. Residents returned to their homes one week after the flood crest to find flooded basements, saturated first and second floor drywall, ruined flooring and furnishings, no working utilities, raw sewage, and looming threats from electrical and natural gas fires. Curfews were in place, requiring the closure of some businesses. Fuel leakage and the threat of fire forced the Town to institute a smoking ban from the top of Scottown Hill to the 12th Street shopping area. Refuse disposal and burning was another storm-related problem that was compounded by flood-related closure of the Town's landfill.

March 1936 Flood

The March 1936 flood required massive rescue and relief efforts in the Bloomsburg region. Heavy snow accumulations melted rapidly as temperatures suddenly warmed in February. In addition to the rapid snowmelt and ice flows on the river, 17 March brought 24 hours of heavy rains. The flood crested at 27.8 feet on 19 March in Bloomsburg with an estimated peak flow of 232,000 cfs. Rail traffic was suspended. Magee Carpets was severely flooded, and damage was extensive, despite efforts to move more than 50 motors to the second floor and 24-hour operation of 14 large pumps.

Widespread flooding that caused major damage in several large river basins, including the Susquehanna and Ohio River basins in 1936, led Congress to pass the Flood Control Act of 1936, and later, the Flood Control Act of 1938.

March 1904 Flood (Ice Jam)

The 1904 March flood was a culmination of flooding events that began in January of that year. The river was clogged with ice in January. The rapid rise of water flooded lowlands all along the Susquehanna. Two weeks later, the river rose again. On 9 February, the Berwick Bridge was ripped away by floodwaters and portions were carried downstream to Mifflinville. Flood conditions eventually improved, and area residents believed that warm rains would help to disperse the ice and prevent further ice jam flooding. However, March gave rise to a third, and even more disastrous flood for the region. A notable impact of this flood was the deposition of multi-ton ice blocks in fields as far as one half-mile from the Susquehanna's banks.

Additional Flood Events

Other notable floods have been recorded at the Bloomsburg, Susquehanna River gauge in 1850, 1865, 1902, 1913, 1940, 1943, 1946, 1948, 1960, 1964, 1979, 1984, 2004 and 2005. Based on the magnitudes of the floods and the flood-prone areas within the Town, it is likely that the study area would have been impacted.

4.5 Future Without-Project (Flood Mitigation) Conditions

In the absence of flood mitigation actions in the study area, flooding problems associated with storms over the Susquehanna River and Fishing Creek watersheds are expected to worsen due to changing climate patterns.

The no-action alternative (future with no project) reflects the continuation of existing economic, social, and environmental conditions and trends within the affected area. Implicit in taking no action would be enforcement of local floodplain management ordinances, and the continuation of flood insurance coverage for properties within the 100-year floodplain as is currently available to property owners through the NFIP.

The Town of Bloomsburg also participates in the CRS, an incentive program within the NFIP that rewards communities with discounts on flood insurance policies based on pro-active steps the community takes to reduce or avoid flood damage and foster comprehensive floodplain management within its boundaries. For CRS participating communities, flood insurance premium rates are discounted in increments of 5 percent. For example, a Class 1 community would receive a 45 percent premium discount, while a Class 9 community would receive a 5 percent discount (a Class 10 is not participating in the CRS and receives no discount). The CRS classes for local communities are based on 18 creditable activities, organized under four categories: (1) Public Information, (2) Mapping and Regulations, (3) Flood Damage Reduction, and (4) Flood Preparedness. Bloomsburg is rated as a Class 7 community, and flood insurance policy holders receive a 15-percent premium discount.

Failure to provide flood mitigation measures could with the occurrence of a significant flood, contribute to the loss of life, as well as physical property and environmental damage. Significant

flooding can result in the overtopping of sewage treatment works, contamination of drinking water supplies, dispersion of HTRW and massive quantities of solid waste. Experience has shown that vast quantities of debris (homes, vehicles, mobile homes, etc.) and sediment must be removed from the floodplain after a flooding event. The physical removal of the debris from the floodplain typically involves large, heavy equipment and requires the removal of trees and vegetation to provide points of ingress and egress for the cleanup equipment. Hauling the collected debris to the local municipal landfill requires significant transportation resources, and involves huge quantities of solid waste that deplete available landfill space. In addition to debris removal, the preparation, placement, and removal of sandbags in attempts to reduce damages from flood events requires hundreds of volunteer and municipal man-hours at significant cost to the community.

Previous floods in Bloomsburg and its surrounding communities, especially the 2011 Lee Flooding from the Susquehanna River and Fishing Creek, have caused widespread damage to residential and commercial structures, industrial facilities, publicly owned facilities, municipal infrastructure, and vehicles. In areas with recurring flooding, homes tend to become more degraded over time because money that could have been used for general improvements is used for flood repairs. Over time, the market value of real estate property diminishes and negatively impacts local tax revenues. Recurring flooding also requires the expenditure of local tax revenues for flood-fighting, clean-up, infrastructure repair and emergency response. This diverts local revenues from infrastructure and recreation improvements from all of Bloomsburg, not just the flooded areas. Damage to commercial and industrial facilities ripple through the economy when businesses are forced to close, lay-off workers, and cease production for several weeks. In the long-run, permanent tax and employment losses will occur if owners of commercial and industrial facilities are no longer willing to endure recurrent flooding.

Existing conditions are not expected to undergo significant change during the period of analysis (2022-2072). The physical setting is expected to remain unchanged over the planning period, specifically: geology, physiography, topography, and soils. In addition, no significant changes are anticipated for cultural and historic resources, air quality, noise, HTRW, aesthetics, and infrastructure.

If flooding continues unmitigated, a change is expected in the density of housing and commercial establishments. This could have a significant impact on the tax base of each community, especially in Bloomsburg. Hemlock and Montour Townships have aggressively pursued buyouts and elevations to the point that future additional home buyouts will have a minor impact on the tax base for those municipalities.

4.6 Existing Conditions - Susquehanna River and Fishing Creek Flow Analysis

As the impacts of the Susquehanna River on the study area during Tropical Storm Lee and other historic floods are more documented and better understood, the development of the hydraulic model for the West End Flood Mitigation Study focused on the larger flood events caused by Fishing Creek with probabilities of occurrence of 1% or less. The FEMA Effective Hydraulic Model used to develop the regulatory FIRM and BFEs for Fishing Creek was created using HEC-2, which is a hydraulic modeling software developed by the USACE in 1968. This FEMA model was created in 1977 and has not been officially updated since.

Since the Effective Model of Fishing Creek was created by FEMA in 1977, additional data and

information has become available which was applied to the model to obtain a more accurate hydraulic analysis. The following adjustments were made to create a more accurate hydraulic model of Fishing Creek.

An existing conditions model was created for this study using the USACE Hydrologic Engineering Center River Analysis System (HEC-RAS) which superseded HEC-2 in 1995. The existing conditions model was created by transferring the original HEC-2 data into HEC-RAS and adding additional cross sections to the model at areas of interest. Cross section geomotries were revised using newly obtained aerial topography of the study area. Hydraulic parameters were adjusted to target high water marks identified from historical flood events, including Tropical Storm Lee as the flood of record.

Revisions to the existing model are outlined below.

Several iterations of proposed conditions modeling were performed with separate objectives:

- 1) Evaluate structural flood mitigation options (levees, floodwalls) for the West End of Bloomsburg which produce the greatest benefits to the community while resulting in the least amount of induced flooding in adjacent communities, and
- 2) Analyze mitigation actions aimed toward lowering any induced flooding to zero.

Each analysis is discussed below. A summary table containing the results of each alternative is provided in Appendix A-1.

1. SR 4003 Bridge Removal

The SR 4003 (Red Mill Road) Bridge incurred extensive damage in the Tropical Storm Lee Event and documentation obtained from the Pennsylvania Department of Transportation (PennDOT) regarding the damaged bridge indicates that the bridge collected substantial amounts of debris with an underwater inspection noting significant scour/erosion around the bridge's piers and footings.

Although the SR 4003 bridge over Fishing Creek was in place during Tropical Storm Lee, the bridge incurred significant structural damage such that the bridge was demolished by PennDOT after September 2011 and not replaced. Since the SR 4003 Bridge no longer exists, the bridge geometry was eliminated from the Existing Condition Model of Fishing Creek.

2. Railroad Street bridge Geometry Changes

The nearest upstream structure to the former location of the SR 4003 bridge is the SR 7210 Bridge, known locally as the Railroad Street Bridge. This structure was originally built in 1939 and replaced in 2010. The Effective FEMA Model includes the original structure consisting of two spans and one pier. The replacement structure consists of three spans with two piers and was modeled accordingly in the Existing Conditions Model.

3. Design Flows

The design flows used in the Effective FEMA Model were taken from the FEMA Flood Insurance Study (FIS) which has not been revised since the information was originally published in 1979. As a result, this data does not consider the Tropical Storm Lee flood of record, nor does it consider several other high flow events which occurred in the twenty years between 2000 and 2020. As discussed in detail in Appendix A of this report, a new hydrologic analysis was performed as part of the West End Flood Mitigation Study to ensure all recent flow events have been incorporated in determining present design flows. These newly computed flow rates were compared to flow rates derived by the USACE using similar methodologies following Tropical Storm Lee.

The flows selected for use in the Existing Conditions Model were taken from a USACE Study conducted in 2012 to incorporate data from the Tropical Storm Lee event. The flow value for the 100-year event at the confluence of Fishing Creek and the Susquehanna River differs from the FEMA effective flows by just 400 CFS. It is a more conservative value. This design flow is applied to the entirety of the model to avoid coding flow changes at Hemlock Creek and Montour Run and to maintain a constant, conservative design flow throughout the study area.

4. Ineffective Flow Areas

Ineffective flow areas are used to represent locations where water exists but there is no conveyance of flow due to an obstruction in the channel or floodplain. These were inserted into the Existing Conditions Model in those portions of the channel and floodplain that are blocked by railroad and/or bridge and roadway embankments. These areas were converted back to effective areas at a ratio of 1:1 upstream of the embankments and a ratio of 2:1 downstream of the embankments.

The stationing and elevations of ineffective flow areas around each of the bridge openings contained in the Existing Conditions Model were examined and adjusted to be consistent with the span of the bridge and the overtopping elevation where a significant amount of flow begins to overtop the bridge.

Ineffective flow areas are most prominent between the Route 42 bridge and the Route 11 Bridge due to the interchange situated in the floodway of Fishing Creek. This is also the point at which flow from Fishing Creek splits to either flow beneath Route 42 or across the fairgrounds property as shown in Figure 4.6.



Figure 4.6 Flow Vectors of Fishing Creek and Floodway

5. Contraction/Expansion Coefficients

Contraction/expansion coefficients are used in one-dimensional hydraulic modeling to account for energy losses that occur when flow must transition into or out of a narrower cross section. Adjustments of the contraction/expansion coefficients were made to calibrate the model to known United States Geological Survey (USGS) high water marks existing in the adjacent floodplain in Hemlock Township or because the presence of islands within the channel have already been accounted for by increasing the Manning's Roughness Coefficient.

6. Manning's Roughness Coefficients

The Manning's Roughness Coefficient is a variable within the Manning's Equation used in open channel flow hydraulics to represent resistance or friction applied to flow by the channel. Manning's Roughness Coefficients for the main channel of Fishing Creek were mostly retained as coded in the effective FEMA model (0.035), except for the channel downstream of the Railroad Street Bridge. Downstream of the Railroad Street Bridge, the channel roughness was increased to a maximum value of 0.045 to reflect the presence of large, vegetated islands within the channel cross section. Accounting for vegetated islands by increasing Manning's Coefficient is reasoned to be a more appropriate method than using contraction/expansion coefficients because the model only focuses on high flows during which the existing islands are fully submerged, thus the streamflow experiences the islands as additional resistance in the channel rather than having to maneuver around them.

Similar upward adjustments to the Manning's Roughness Coefficients were made in the overbank areas of the creek to reflect heavily forested areas and dense residential development such as the West End of Bloomsburg.

Manning's Roughness Coefficients in the right floodplain in the Fernville area were reduced to reflect the considerable number of home acquisition/demolitions that have occurred since Tropical Storm Lee in 2011. The lot on which a demolished home once stood is required to be maintained perpetually as green space by the municipality.

7. Floodplain Geometry

Light Detection and Ranging (LIDAR) topographic data, collected in 2021 to support the West End Study, was used to develop the revised geometry within the floodplain. Existing cross sections from the effective FEMA model as well as any new cross sections added in the existing conditions model were updated using the new topographic data. The topographic data obtained was produced at a resolution of 1' contours and is generally accurate to within 12" in open, unobstructed areas.

The water surface elevation (WSE) at the time the LIDAR was captured obstructed capture of channel topography below the water surface. A bathymetric survey was performed between Barton Street and Red Mill Road to capture more details of the existing island that exists within the channel at this location. No other adjustments to the geometry of the main channel or the right overbank of the floodplain of the Fishing Creek were made.

8. Bridge Geometry

In addition to the topographic survey received from the aerial LIDAR, survey crews performed traditional survey of all bridge structures along Fishing Creek within the study area specifically for this project. Data collected include abutment and pier locations, low chord elevations, and parapet and deck elevations. This data was used to ensure the structure data in the Existing Conditions Model reflects current field conditions.

9. Bridge Modeling Approach

The high flow calculation methods for each of the bridges were reviewed and adjusted to be consistent with the way water was either flowing through, or over and around the bridges, as computed by the model. If much of the flow was computed to be on the floodplain during high flow, the calculation method was adjusted to use the energy equation. This is observed to be the case at Railroad Street Bridge where a large volume of flow is conveyed in the right overbank through the Fernville community.

Conversely, if the flow in the section was computed to be primarily in the main channel of the stream, and the bridge was either partially or fully submerged, the pressure/weir calculations should be used to model the high flows through the bridges.

10. Vertical Datum

The Effective FEMA Model is referenced to the National Geodetic Vertical Datum of 1929 (NGVD 29). However, the LIDAR topographic data used to update the floodplain topography within the study area is referenced to the North American Vertical Datum of 1988 (NAVD 88). In order to use a consistent vertical datum or reference elevation, the elevation data used in the Existing Conditions Model was adjusted from NGVD 1929 to NAVD 1988 by subtracting 0.71 feet from all elevation data in the model, including all cross-section elevations, ineffective flow elevations, and bridge geometry elevations.

In addition to the geometric data used in the Existing Conditions Model, the model's boundary conditions that represent the starting downstream water surface elevation from the Susquehanna River as it acts on the Fishing Creek, were also adjusted to the NGVD 1988 vertical datum by – subtracting 0.71 feet from the Effective Model's boundary conditions.

Water Surface Elevations calculated by the Existing Conditions Model are notably higher than those calculated by the FEMA Model, especially in the portion of the model upstream of the Route 11 bridge. The increase is primarily attributed to the presence of large ineffective flow regions which were added in the Existing Conditions Model around the Route 11/Route 42 Interchange as well as revised topographic data in the floodplain. While the disparity between the FEMA Model and Existing Conditions Model is great, existing high-water marks along Fishing Creek correlate very well to the model results for both the 100-year and Tropical Storm Lee events. Appendix F provides a comparison of calculated WSEs to historical observed WSEs for the 100-year and Tropical Storm Lee events. WSEs reported below Washington Street (XS 18.649) may be exaggerated as the limitations of the one-dimensional model do not accurately predict the volume of flow exiting Fishing Creek and flowing across the fairgrounds.

4.7 Analysis of Structural Flood Mitigation Alternatives

Several iterations of proposed conditions modeling were performed with separate objectives:

- Evaluate structural flood mitigation options (levees, floodwalls) for the West End of Bloomsburg which produce the greatest benefits to the community while resulting in the least amount of induced flooding in adjacent communities, and
- 2) Analyze mitigation actions aimed toward lowering any induced flooding to zero.

Each analysis is discussed below. A summary table containing the results of each alternative is provided in Appendix A-1.

1. Levee Alternative A-1

Alternative A-1 consists of a levee system beginning at Railroad Street on the left bank of Fishing Creek. This conceptual alignment extends in a south-westerly direction along the bank of the creek before turning inland 90 degrees approximately 200 feet beyond Washington Street (see Figure 4.7 – Alternate 1 alignment is shown in red.). The alignment then proceeds across Gates 3, 4 and 5 of the Bloomsburg Fairgrounds and makes a second 90-degree bend at West 6th street where it ties

into the existing flood wall constructed around the Autoneum manufacturing facility. The total length of the Alternative A-1 alignment is 6,200 feet and is comprised of full earthen levee, MSE levee, and concrete-encased sheet pile wall.

Modeling of alternative A-1 reveals that induced flooding depths incurred for the 100-year flood flow reaches a maximum of 2.33 feet near Leonard Street. Induced flooding tapers to zero at the point where the alignment turns to cross the fairgrounds. Above Railroad Street, minimal induced flooding is expected for the 100-year event; this is because the existing backwater created by the Railroad Street Bridge is roughly equivalent to the backwater created by this levee alternative for this event.

Induced flooding occurs because of the alignment obstructing a substantial portion of the regulated floodway. By definition, the regulated floodway is that portion of the channel and overbank areas required to convey the 100-year flood flow with less than 1' of corresponding increase in water surface elevation. By constricting the floodway, water surface elevations are increased in the channel to compensate for lost conveyance in the floodway.

2. Levee Alternative A-2

Alternative A-2 is nearly identical to Alternative A-1 in every aspect except for that the levee turns approximately 350 feet before Washington Street to create a jog in the alignment prior to connecting to the original path across the Fairgrounds. This alternative is designed to minimize the encroachment into the floodway by turning inland from Fishing Creek sooner. Induced flooding under Alternative A-2 is decreased by 0.1 feet during the 100-year flood event (to be verified by 2D modeling during preliminary design).



Figure 4.7 Rendering for Levee Alignment Alternatives A-1 & A-2

3. Levee Alternative A-3

Alternative A-3, shown in below Figure 4.8, involves a shortened levee alignment intended to remove a portion of the floodway in Bloomsburg while providing meaningful reduction of overbank flows along Fishing Creek. This alternative alignment terminates near Barton Street and does not transect the Fairgrounds property to connect to the Phase 1 Autoneum system.

Because Alternative 3 does not tie into the existing floodwall, this alignment does not protect the West End against flooding from the Susquehanna River. However, this alignment does mitigate flood risk from Fishing Creek and brings many residential properties out of the regulatory floodway allowing those residents broader options for nonstructural flood mitigation alternatives such as home elevation or mitigation reconstruction options.

Modeling of alternative A-3 reveals that induced flood depths incurred for the 100-year flood reaches a maximum of 1.46 feet near Leonard Street. Induced flooding tapers to 1.16 feet immediately upstream of the Railroad Street Bridge and and quickly ties back to existing upstream of Fernville.

This alternative was dropped from further consideration due to potential permitting issues.



Figure 4.8 Depiction of Impacts on Floodway Resulting from Alternative A-3

4. Benched Floodplain Alternative A-4

Alternative A-4 considers construction of a benched floodplain and extension of the Railroad Street Bridge into Hemlock Township. This solution was evaluated as an alternative to a structural levee system along the left bank of Fishing Creek.

A benched floodplain approximately 80-feet wide and 10-feet deep was modeled with the intent of providing additional conveyance capacity in Fishing Creek so that the full extent of the floodway through the West End of Bloomsburg is not required. The Railroad Street Bridge was also lengthened for an additional span of 80-feet to increase the effective waterway opening of the bridge. The increased waterway opening is found to reduce backwater upstream of the bridge by 2.6-feet and significantly reduce the overbank conveyance in the Fernville approach of the bridge.

The positive hydraulic benefits of this alternative are limited to the Fernville community of Hemlock Township and do not extend downstream of Railroad Street to the West End Community. This is because multiple locations along Fishing Creek can be considered flow-controlling. Removing one point of constriction at Railroad Street solves a backwater problem upstream; however, increasing conveyance capacity simply moves flow to the next point of constriction downstream. As a result, the West End of Bloomsburg experiences little benefit from this alternative.

5. Fishing Creek Modifications Alternative A-5

Other structural mitigation alternatives along with Alternative 4 above were evaluated in lieu of a levee system in the West End of Bloomsburg. These options are presented in Table 4.2 and demonstrate the ineffectiveness of these options in reducing water surface elevations in the West End of Bloomsburg.

Table 4.2 Reduction in Existing 100-Year Flood Levels for Various Alternatives

Modification Alternatives	Near Hock Road	@ Route 42	@ Leonard Street	Above Railroad Street Bridge
Remove Covered Bridge & Railroad Bridge	2.1 FEET	0.0 FEET	0.0 FEET	0.0 FEET
Remove Route 11 & Route 42 Interchange Ramp Fill	0.0 FEET	0.0 FEET	0.0 FEET	0.0 FEET
Remove Existing Island	0.0 FEET	0.0 FEET	1.0 FEET	0.4 FEET
Excavate Benched Floodplain & Modify Railroad St Bridge (A-4)	0.0 FEET	0.0 FEET	0.0 FEET	2.6 FEET
Remove Railroad Street Bridge	0.0 FEET	0.0 FEET	0.0 FEET	2.3 FEET

6. Induced Flooding Mitigation Alternative A-6

Several options were evaluated for their effectiveness in reducing water surface elevations with a levee system in place. This analysis was only performed for those alternatives which produced the greatest results as a standalone option.

Because induced flooding is created by a levee system due to a reduction of conveyance rather than backwater from a downstream impediment to flow, an alternative to mitigate the induced flooding was evaluated. The focus of this analysis was on an alternative which provided greater conveyance in the channel adjacent to the proposed levee alignment, namely a benched floodplain on the right bank with an extension of the Railroad Street Bridge into Hemlock Township/Fernville.

Implementing this option in conjunction with a levee system along the left bank of Fishing Creek mitigates the induced flooding from a maximum of 2.22-feet to a maximum of approximately 1.1-feet near Leonard Street.

This alternative merits additional study if the structural flood mitigation option for Bloomsburg advances to the design stage.

4.8 Hydraulic Modeling - Risk & Uncertainty

One-dimensional hydraulic modeling of Fishing Creek in the West End of Bloomsburg carries significant uncertainty due to proximity to the Susquehanna River and because of the vast floodplain and complicated flow patterns which exist. One-dimensional modeling limitations include the following:

- 1-D Model only calculates flow in one direction perpendicular to the cross sections developed by the user. This is a poor assumption in a relatively flat floodplain where flow can easily change direction or pond in storage areas.
- 1-D Model assumes a constant water surface elevation along the entire length of the cross section and does not consider the great variation in water surface that occurs when a stream overtops its banks and flows across the terrain.
- 1-D Model does not effectively differentiate between flow through a bridge structure and flow around the structure in the overbank areas. This can be a significant source of error when selecting a bridge modeling approach.
- Gross assumptions are required when handling spatial changes in cover conditions and assignment of Manning's Roughness Coefficients in densely developed areas such as the West End of Bloomsburg.

Summary:

While 1-D modeling is capable of handling split flow conditions, these situations increase the complexity of the model and require an iterative process to balance energy. This modeling approach is only appropriate when there is a clear, defined flow path in the floodway. When a main channel spills into an unconfined floodplain where a single flow direction is not evident, a 2-D model is more appropriate. Such is the case with Fishing Creek.

4.9 Conclusions

Results of the one-dimensional hydraulic analysis of Fishing Creek indicate that a levee system in the West End will create induced flooding on the right bank of Fishing Creek opposite the proposed levee alignment. These results are expected as any levee alignment around the West End necessarily encroaches into the floodway of Fishing Creek and partially restricts conveyance of floodwaters in this area. Previous levee systems, such as the system around Autoneum, were constructed entirely outside the floodway where very little conveyance occurs resulting in little to no induced flooding.

An accurate determination of the magnitude of induced flooding caused by a levee system in the West End relies on a correct understanding of how much flow is moving through the floodway. That is, how much more flow must the channel convey when it is prevented from utilizing the floodway. The answer to this question determines the additional height of flooding, or induced flooding, that will occur in the channel.

Because a one-dimensional analysis assumes a constant water surface elevation for the channel

and the floodplain, it is possible that the amount of flow conveyed by the floodway is being over estimated in the one-dimensional model. If that is the case, obstructing this flow is also likely to overestimate the induced flooding. For this reason, a more detailed two-dimensional analysis of the Fishing Creek floodplain is recommended if a levee system is to be the preferred alternative for flood mitigation in the West End.

Two-dimensional hydraulic analyses utilize a digital terrain model of the ground surface with a user-defined grid size as opposed to linear cross sections used in one-dimensional analysis. The result of this is that flow is calculated in every direction into and out of each individual grid. Two-dimensional modeling requires fewer assumptions and offers much greater representation of actual conditions when working with streams having very wide floodplains, sharp bends, and complicated flow patterns or multiple channels.

Using more advanced modeling approaches is critical toward accurately identifying existing flow in the floodplain, induced flooding caused by a levee system, and the scope, magnitude, and cost of mitigation activities necessary to lower induced flooding.

SECTION 5 - RISK ASSESSMENT

5.1 Flooding Impacts

Several analysis tools were developed for analyzing the flood risk for the three communities. They are:

Base Flood Floodplain vs Storm Lee Flood Limits, Depth of Flooding Maps, First Floor Flood Impact Maps.

The base flood floodplain and Tropical Storm Lee Flood limit map is shown below for the West End study area. This mapping was utilized to develop a GIS based inventory of parcels to be evaluated for flooding impacts.

Once the parcels were identified, the depth of flooding of the 2011 Lee flooding and the depth of flooding above the first floor elevation for each parcel was developed with field survey data.

The map shown in Figure 5.1 of the Storm Lee flood level was utilized since it is the current flood of record and it is about 2 feet above the 2022 updated BFE. This mapping facilitated assessment of the flooding impacts for each structure which was directly converted to damages utilizing the FEMA Flood Assessment Structure Tool (FAST).

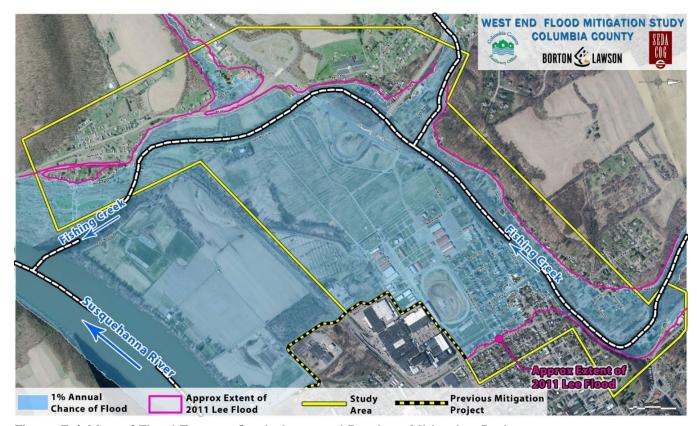


Figure 5.1 Map of Flood Extents, Study Area, and Previous Mitigation Projects



Fairgrounds impacted by deep water flooding.

Town residential area experiences significant first floor flooding.

Majority of deeper flooding in Fishing Creek floodway

Figure 5.2 Extents and Depth of Flooding in Study Area

Flooding impacts for each community are outlined below:

Montour Township

Montour Township is affected by flooding in three areas in the study area.

- South of Reading Street near Rupert (SFHA-floodplain)
- Between Fishing Creek and Perry Avenue near Route 42 (SFHA-floodplain)
- Between Route 42 and Hemlock Creek (SFHA-floodplain)

A total of twenty-four properties were evaluated for flooding impacts. Fifteen (15) of the properties did not experience any flooding, 5 had basement flooding and 4 properties were flooded on the first flood. The majority of the flooding was in the Rupert area.

Hemlock Township

Hemlock Township is affected by flooding at two locations in the study area.

- Drinker Street from Bloom Street to Red Mill Avenue (SFHA-floodplain)
- From the Railroad Street Bridge along the bend in Fishing Creek in the area of Drinker and Walnut Streets (SFHA-floodplain)

Thirty-five structures were reviewed. Six (6) properties had been elevated and 14 did not have flooding. Three structures experienced basement flooding and a 17 had approximately three feet of water on the first floor.

Town of Bloomsburg

The Bloomsburg study area is bounded by Railroad Street, West Fifth Street and Fishing Creek to the north and the west and includes the Bloomsburg Fairgrounds. The Bloomsburg area is bisected by the flood way and the floodplain with a small area adjoining Railroad Street that is located in Zone X.

Nearly 300 properties were reviewed with 17 not being flooded. Sixteen (16) properties experienced basement flooding; one hundred seventy-four (174) had between zero and four feet of water on the first floor and ninety (90) had greater than four feet of flooding on the first floor. Figure 5.3 below shows modeled depth of flooding in structures, relative to first floor elevations from the 2011 Flood Lee, in the West End of Bloomsburg area.



Figure 5.3 Modeled Depth of Flooding in Structures in West End of Bloomsburg from 2011 Flood Lee

Fairgrounds

The fairgrounds property is one of the most susceptible to flooding with a large area below elevation 472.00 which is 3 feet above activation stage for the existing Columbia County Flood Mitigation System. Approximately 35 floods have impacted the fairground over the past 120 years. The Fairgrounds has 54 buildings that are impacted by the base flood. Figure 5.3 above shows modeled depth of flooding in the Fairgrounds' structures from the 2011 Flood Lee.

5.2 Columbia County Hazard Mitigation Plan

The purpose of the Stafford Act, as amended by the Disaster Mitigation Act of 2000, is to reduce the loss of life and property, human suffering, economic disruption and disaster assistance costs resulting from natural disasters. Section 322 requires local governments to prepare a multi-hazard mitigation plan as a precondition for receiving FEMA mitigation project grants. The plans consist of a Community Profile, Planning Process, Capability Assessment, Risk Assessment, Mitigation Strategy and Plan Maintenance. The plans must be updated every five years. Columbia County last completed its Hazard Mitigation Plan in 2017. Work is underway to complete the 2022 Hazard Mitigation Plan.

The 2017 Plan included an analysis of ten natural hazards: drought, earthquake, flood/flash flood/ice jam, hurricane/tropical storm/nor'easter, pandemic, landslide, radon exposure, tornado/windstorm, wildfire, and winter storm and five human made hazards: dam failure, environmental hazards, levee failure, nuclear incidents, and utility interruption.

The 2017 plan generated 78 mitigation measures. The following actions are related to the communities in the study area. Work is underway to complete the 2022 Hazard Mitigation Plan. It is anticipated that the Plan will be completed later this year.

A Risk Factor ranking was completed for the fifteen identified hazards. The Risk Factor Values were developed by assigning varying degrees of risk to five categories for each of the hazards. The categories are probability, impact, special extent, warning time and duration. The table below shows the results. The Risk Factor value is based on the entire county. An evaluation of the three communities in the study area show that each has a greater risk than the county as a whole.

Table 5.1 Ranking of Hazard Types based on Risk Factor Methodology (Columbia County HMP)

Table 4.4-2: Ranking of hazard types based on Risk Factor methodology.								
HAZARD	HAZARD NATURAL (N) or MAN- MADE (M)	RISK ASSESSMENT CATEGORY						
RISK		PROBABILITY	IMPACT	SPATIAL EXTENT	WARNING TIME	DURATION	FACTOR	
	Flood, Flash Flood, Ice Jam (N)	4	3	3	2	3	3.2	
HBH	Environmental Hazards (M)	3	3	3	4	2	3.0	
主	Winter Storm (N)	4	2	4	1	2	2.9	
	Tornado, Windstorm (N)	4	2	3	2	1	2.7	
MODERATE	Nuclear Incident (M)	1	2	3	4	4	2.3	
	Dam Failure (M)	1	3	2	4	2	2.2	
10DE	Drought (N)	2	1	4	1	4	2.2	
2	Utility Interruption (M)	2	1	3	3	2	2.0	
	Hurricane, Tropical Storm, Nor'easter (N)	2	2	2	1	2	1.9	
	Landslide (N)	2	1	3	2	2	1.9	
>	Radon Exposure (N)	2	1	1	4	4	1.9	
ГОМ	Levee Failure (M)	1	2	1	4	3	1.8	
	Pandemic (N)	2	1	2	1	4	1.8	
	Wildfire (N)	2	1	2	3	1	1.7	
	Earthquake (N)	1	1	1	4	1	1.3	

5.3 Assessing Vulnerability (FAST Analysis)

A Scenario Analysis was completed for the study area. The analysis looks at the location of improvements in relation to the floodplain. Properties can be grouped into the following FEMA FIRM categories. The study evaluated the three main categories.

- Regulatory Floodway = High Vulnerability
- Floodplain (Zone A or AE) or SFHA = High Vulnerability
- Zone X (0.2%-annual-chance or "500-year" floodplain) = Moderate Vulnerability

The analysis was conducted using FEMA's Flood Assessment Structure Tool, or "FAST," which is an open source tool that can be used to rapidly analyze structure-level flood. For the analysis, structure data was obtained that included the following attributes: longitude and latitude, occupancy, building cost, building area, number of stories, foundation type, first floor elevation, depth of flooding.

Field surveys were conducted in October 2021 to obtain structure attributes for use in the FAST Tool. Approximately 350 structures were surveyed. Each structure was assigned a unique structure identification number. The data gathered included latitude and longitude, occupancy, building area, number of stories, foundation type and ground and first floor elevation. Assessment data provided additional data on the structure and a GIS analysis generated a depth of flooding model.

~350 Parcels with Structures in Study Area in Floodway & Floodplain

~ # of structures

- First Floor Elevations
 (accuracy to within +/- 2 inches)
- Location and elevation in front of structure (accuracy to within +/- 3/8 of an inch)
- · General Structure Information
 - ✓ Structure type
 - √ Basement
 - √ Number of stories
 - ✓ Detached Structures
 - ✓ Inhabited
 - ✓ Photo

Flood study responses needed

Official: Bloomsburg-area surveys to help determine mitigation options



DE WEBER, surveying crew chief, left, and Catrian Coppola, surveying assistant, document the property at the interion of West Third and Leonard streets this week. They were working in the west end of Bloomsburg, Resident survey of to be returned by Oct. 30.

Direct crees are on the stress of west Bloomsburg and the Blood-prone areas of Hemlock and Montour townships. They're take the blood prone areas of Hemlock and Montour townships. They're take the blood mitigation study officials say.

Meanwhile, the company doing the study berton Lawson, send area residents weeks ago. They're asking for measurements on their bomes, the flood his town of their property of

Those responses are mportant, said Jim Brozena. He's a consulant assisting Borton

Figure 5.4 Summary of Structure Field Data Collected in Flood Study (Press Enterprise, October 15, 2021)

The FAST Tool provides outputs for each structure that include the depth of flooding, building damage percent, building loss in USD, content loss percent, and content loss in USD. In the table below, building percentage and contents damage are the damage incurred on an average structure. Building loss and contents loss are the total costs for the entire study area. This table displays the results for each of the communities for a Tropical Storm Lee flood event.

Table 5.2 Summary of FEMA FAST Outputs

Location	Category	Building Damage %	Building Loss \$	Contents %	Contents \$
Montour	Residential (5)	23%	\$108,100	20%	\$44,600
Township	Commercial (4)	20%	\$556,400	40%	\$482,400
Hemlock	Residential (18)	20%	\$198,200	18%	\$90,300
Township	Commercial (3)	23%	\$26,300	46%	\$43,000
Town of	Residential (221)	23%	\$5,969,500	24%	\$3,069,900
Bloomsburg	Commercial (68)	28%	\$1,608,700	69%	\$3,474,900

Susquehanna Flood Warning System Update

In 2003 the Wyoming Valley Levee Raising Project developed a Flood Warning and Response System (FWRS) ArcGIS tool covering the five-county area (Luzerne, Columbia, Montour, Northumberland and Snyder) that was impacted by flooding from the Susquehanna River. The system became obsolete.

Through a cooperative effort of the USACE, PEMA, SRBC, and the Luzerne County Flood Protection Authority (LCFPA) a Silver Jackets Inter-agency Nonstructural Project was completed that updated the system to working condition, make the system sustainable for future iterations of software and make the applicability of the system more universal. The recently completed Wyoming Valley Susquehanna River Flood Inundation Mapping (FIM) is an exceptional tool for emergency managers and updating this outdated GIS tool to use the FIM data will provide even more information to better identify flood hazards, prepare and execute flood response measures, alleviate loss of life and mitigate structure and contents damage. The tool will generate Flood Response/Action Tables that are customizable by the user, develop a query tool for flood impacts to specific buildings or infrastructure (such as structures with 4 feet or more of flooding, critical structures, etc.). The tool will include structure values and can estimate damages for the various flood stages on a structure-by-structure basis using finished floor elevations (FFE) or aggregated by county or municipality for damage assessment purposes. The tool can be used for "What-if" scenarios and assist floodplain managers administering its Flood Plain Ordinance (determining probable substantially damaged properties) after flood events.

Unfortunately, the system is using the original datasets from the original program with the exception of West Pittston, Luzerne County, which served as a pilot project for updating the field data. The data developed by the surveys has been provided to the SRBC for inclusion in the model so that current information is available for the study area.

5.4 Analysis of Repetitive Loss Properties

Repetitive Loss and Severe Repetitive Loss properties are those properties that meet the definitions below.

- RL property: Any insurable building for which the NFIP paid two or more claims of more than \$1,000 within any rolling 10-year period, since 1978. A RL property may or may not be currently insured by the NFIP.
- SRL property: Has at least four losses each exceeding \$5,000, or when there are two or more losses where the building payments exceed the property value.

An inspection of the community records indicates the number of Repetitive Loss and Severe Repetitive Loss properties in each of the municipalities within the Study Area, summarized in the Table 5.3 below.

Table 5.3 Repetitive Loss, Severe Repetitive Loss, and Mitigated Properties (FEMA 2019 and 2017 data)

Community	Repetitive Loss	Severe Repetitive Loss	Mitigated
Montour Township	0	0	0
Hemlock Township	10	0	4
Town of Bloomsburg	84	3	15

All three communities have been active in the FEMA HMGP and the HUD CDBG-DR programs following the 2011 Lee Flood Event completing multiple acquisition/demolition and a limited number of elevation projects. Hemlock Township completed several HMGP acquisition projects in the 1980's.

5.5 Economic Analysis

The phrase "100-Year Flood" is a cause of confusion among the public, government officials, and insurers. Many continue to believe it is a description of a flood that occurs only once every 100 years. In fact, "100- Year Flood" is an abbreviated way of describing a flood of such magnitude that has a 1-percent (or 1 in 100) statistical probability of being equaled or exceeded in any given year. By definition, more than one 100-year flood event or base flood can occur within the span of a single year or one might not be witnessed during a 100-year timeframe.

Housing values in the floodplain are impacted by flood insurance requirements which consider the following: Based on probability theory, a building in the SFHA has a 26 % (or 1 in 4) chance of experiencing a 100-year flood over the entire life of a 30-year mortgage.

An economic analysis of the technically feasible alternatives was completed utilizing the FEMA Benefit-Cost Analysis (BCA) Tool to determine if the benefits of implementing the alternatives outweighed the costs.

BCA is a method that determines the future risk reduction benefits of a hazard mitigation project and compares those benefits to its costs. The result is a Benefit-Cost Ratio (BCR). A project is considered cost-effective when the BCR is 1.0 or greater.

Table 5.4 Chance of Flooding Over a Period of Years (FEMA)

Time				
Period	10-year	25-year	50-year	100-year
1 year	10%	4%	2%	1%
10 years	65%	34%	18%	10%
20 years	88%	56%	33%	18%
30 years	96%	71%	45%	26%
50 years	99%	87%	64%	39%

The analysis has been completed using the FEMA BCA Toolkit, Version 6.0. Data inputs include, latitude and longitude, hazard type mitigation type, project useful life, FIS data including return intervals discharges, and SFHA information. structure building size. elevations. building replacement values,

building characteristics including number of stories, basement and foundation type. FEMA Standard Values were used for Building Depth-Damage Functions.

Box A: Benefit-Cost Analysis

The Stafford Act requires every project funded by HMGP to be cost effective, as demonstrated by a Benefit-Cost Analysis (BCA). BCA involves estimating and comparing the expected costs and future benefits of a project; dividing a project's total net benefits by its total cost results in the benefit-cost ratio (BCR). A project is considered cost-effective when its BCR is greater or equal to 1.0.

Mitigation project "benefits" typically include avoided damage to structures, avoided deaths or injuries, and other quantifiable losses. Historically, ecosystem-wide environmental benefits were not included in the scope of BCA. However, in 2013, FEMA changed its BCA methodology for acquisition projects to facilitate and promote ecosystem-based management. Under the new methodology, environmental benefits can be added to a project's total net benefits if (and only if) the project in question already has a BCR of 0.75 or greater using traditional benefits. In other words, environmental benefits currently may be considered to "tip the scale" in favor of approval.

The environmental benefits of open space are estimated according to rates based on land area: green space is valued at \$2.57/ft2/year; and riparian open space is valued at \$12.29/ft2/year.

Sources: 44 C.F.R. 206.434(c)(5); FEMA, Benefit-Cost Analysis, http://www.fema.gov/benefit-cost-analysis (March 16, 2015); FEMA, Mitigation Policy FP-108-024-01, Consideration of Environmental Benefits in the Evaluation of Acquisition Projects under the Hazard Mitigation Assistance (HMA) Programs (June 18, 2013), available at: https://www.fema.gov/media-library-data/20130726-1920-25045-4319/environmental_benefits_policy_june_18_2013_mitigation_policy_fp_108_024_01.pdf

H(c)(5); FEMA, Benefit-Cost Analysis, http://www.fema.gov/benefit-cost-analysis
Mitigation Policy FP-108-024-01, Consideration of Environmental Benefits in the
Projects under the Hazard Mitigation Assistance (HMA) Programs (June 18)

Figure 5.5 Summary of Benefit Cost Analysis (FEMA)

The updated values for use of pre-calculated benefits to determine cost effectiveness of elevations and acquisitions in SFHA are:

- Acquisitions: \$323,000 per structure.
- Elevations (and Mitigation Reconstruction): \$205,000 per structure.

In addition to the Benefit Cost
Analysis, FEMA issued a
Memorandum in 2013 titled
"Cost-Effectiveness
Determinations for
Acquisitions and Elevations
in Special Flood Hazard
Areas Using Pre-Calculated
Benefits." The memo was
recently updated to adjust
the values for inflation.

SECTION 6 - TYPES OF FLOOD MITIGATION ALTERNATIVES

6.1 Strategy / Mitigation Categories

Nonstructural mitigation projects include:

- Residential Structures in Floodway Acquisition / Demolition,
- Residential Structures in Floodplain Acquisition / Demolition, Elevations or Mitigation Reconstruction,
- Commercial Buildings Wet Floodproofing,
- Other Emergency Access Roads, Floodproofing Wastewater / Utility Systems, Emergency Action Plans, Additional Stream Gauges, Ordinances.

Structural Mitigation Projects include:

- Levee / Floodwall Systems,
- Channel / Floodplain Modifications.

6.2 Nonstructural Flood Risk Management Measures

Nonstructural flood risk management measures are proven methods and techniques for reducing flood risk and flood damages. Effective for both short and long term flood risk and flood damage reduction, nonstructural measures can be very cost effective when compared to structural measures. An advantage of nonstructural measures is the ability of nonstructural measures to be sustainable over the long term with minimal costs while structural solutions have higher costs for the operation, maintenance, repair, rehabilitation, and replacement of the built infrastructure.

The following nonstructural measures are techniques used in reducing flood risk and the damages associated with flooding. The measures vary from removing an entire structure from the floodplain to purchase flood insurance for a structure which is located within the floodplain. The costs associated with implementing a measure vary. An example would be acquisition / demolition will eliminate all future damages associated with flooding while flood insurance will assist in the costs to repair a structure after a flood event but does not eliminate future flood damages to that structure.

Tables 6.1 and 6.2 are included at the end this section as references when assessing the options for mitigation projects.

Acquisition

Acquisition consists of buying the structure and the land. The structure is demolished and the land is deed restricted to prevent any future development of the parcel.

Elevation

Elevation raises an existing structure to an elevation where the first floor is equal to or greater than the BFE. In Pennsylvania, an additional eighteen inches (18") is required above the BFE. The cost of elevating a structure beyond the minimum requirements is less expensive than the original lift due to the cost incurred for mobilizing equipment. Elevation can be performed using fill material, on

extended foundation walls, on piers, post, piles and columns. Elevation can be done for slab on grade structures.

Relocation

Relocation requires physically moving the at-risk structure and buying the land upon which the structure is located. It makes sense when structures can be easily relocated from a high flood hazard area to an area that is located out of the floodplain.

Mitigation Reconstruction

Mitigation Reconstruction is the demolition of a flood damaged structure and reconstructing a new floodplain compliant home on the existing parcel. In some instances, the reconstruction takes place on a new site located outside of the floodplain.

Wet Floodproofing

Wet floodproofing is applicable as either a stand-alone measure or as a measure combined with other measures such elevation. As a stand-alone measure, all construction materials and finishing materials need to be water resistant and all utilities must be elevated above the BFE.

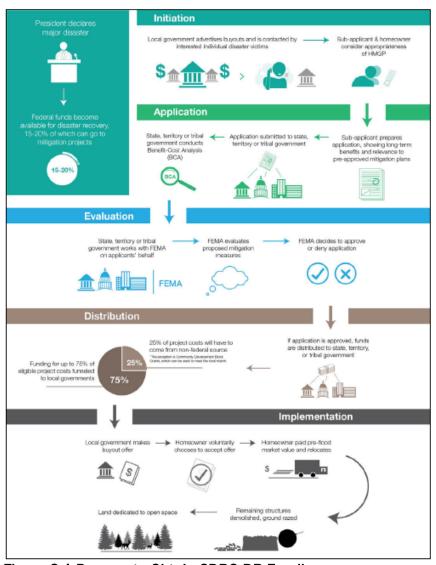


Figure 6.1 Process to Obtain CDBG-DR Funding

Wet floodproofing is applicable to commercial and industrial structures when combined with a flood warning and flood preparedness plan. This measure is generally not applicable to deep flood depths and high velocity flows.

Dry Floodproofing

Dry floodproofing consists of waterproofing the structure. This option is limited to commercial and industrial structures. This measure achieves flood risk reduction but it is not recognized by the NFIP for any flood insurance premium rate reduction since human interaction is required. Laboratory tests show that a "conventionally" built structure can generally only be dry flood proofed up to 3-feet in elevation. A structural analysis of the wall strength would be required if it was desired to achieve

higher protection. A sump pump should be installed as part of the measure. Closure panels are used at openings. This concept does not work with basements or crawl spaces.

Flood Warning System

Flood Warning Systems rely upon stream gauge, rain gauges, and hydrologic computer modeling to determine the impacts of flooding for areas of potential flood risk. A flood warning system is able to identify the amount of time available for residents to implement emergency measures to protect valuables or to evacuate the area during serious flood events.

Land Use Regulations

Land use regulations within a designated floodplain effective tools in reducing flood risk and flood damage newly constructed substantially improved structures. The requirements are based on the NFIP. For example, land use regulations identify where may development can and cannot occur, or to what elevation structures should locate their lowest habitable floor.

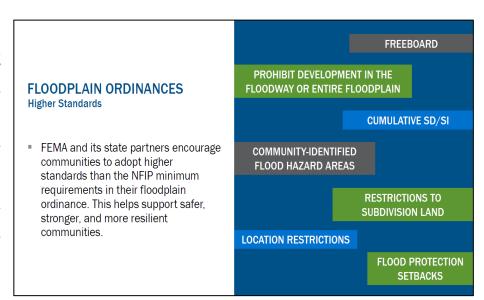


Figure 6.2 Floodplain Ordinances Overview (FEMA)

6.3 Guiding Principles

- Preserve and restore floodplains where possible to recognize, preserve and restore the beneficial functions of floodplains for hazard reduction, water quality enhancement, wetland protection, wildlife habitat, riparian corridors, recreation, environmental relief, aesthetics and greenway areas.
- 2. Be prepared for floods by developing advanced floodplain mapping, detailed risk assessments, enhanced early warning systems, multiple emergency notification measures, understandable response plans, workable recovery plans, and ongoing storm monitoring.
- 3. Help people protect themselves from flood hazards through public interaction and involvement, available flood information, community outreach and education, self-help measures, flood proofing options, affordable flood insurance, and emergency preparedness.
- 4. Prevent adverse impacts and unwise uses in the floodplain through appropriate regulation and land use, open land preservation, acquisition of structures and relocation assistance programs, relocation of infrastructure (such as wastewater disposal plants), multi- objective

planning, prohibiting unacceptable encroachments, and establishing ongoing maintenance practices that preserve and enhance environmental functions.

- 5. Prevent adverse impacts from development and redevelopment by preparing regional stormwater management plans, adopting appropriate engineering standards into local ordinances, consistently administering and enforcing ordinances and providing long-term maintenance of facilities.
- 6. Acknowledge the values of structural flood control measures after a careful analysis of the ecological, economic, long-term operation and maintenance, and social costs and benefits of all mitigation options; identify those situations where a combination of structural solutions, structural modifications, and nonstructural solutions is the most beneficial option.

6.4 Economic Analysis

Economic impacts of flooding affect households, businesses and communities. The losses to households include personal items, household goods, vehicles, homes, and in some cases, lost wages or even lost jobs. Local businesses experience lost inventory, lost sales, and lost productivity and profits. Even firms not directly affected by flooding might lose sales if they were suppliers of goods and services to affected businesses or households. All aspects of public service delivery are affected. In some communities, wastewater and water facilities are compromised and must be restored. Affected municipalities need to repair roads and bridges, public lighting, public parks, and public buildings.

The community fiscal effects of infrastructure losses depend primarily on the amount of federal and state disaster assistance they obtain. Federal and state disaster assistance programs take the form of direct payments, grants, and no-interest or low-interest loans to individuals, businesses and communities. Under the Public Assistance Grant Program, FEMA awards grants to assist state and local governments and certain private nonprofit organizations with the response to and recovery from disasters. The program provides funding for debris removal, implementation of emergency protective measures and permanent restoration of infrastructure. The Individuals and Households Program can assist those affected flooding by providing temporary help with alternative housing and/or financial assistance with other disaster-related needs. Individual assistance can also be in the form of low-interest disaster loans from the U.S. Small Business Administration for homeowners, renters, businesses of all sizes, and non-profit organizations. Future studies may be able to begin to evaluate the economic impacts of past flood events to municipalities by tracking and comparing awarded Public Assistance, Individual Assistance and Small Business Loans by municipality.

In considering economic impacts of flooding, it would be remiss not to mention the impact to a community's tax base. Local property tax revenues decline if properties remain vacant, property values decline or affected properties are mitigated through acquisition.

6.5 Structural Systems

Structural systems are defined as flood mitigation features that change the physical environment. Examples are floodwalls, earth levees, and stream channel modifications.

Structural flood mitigation systems were considered in the 2005 USACE study; however, the study area, especially the West End and the Fernville areas, have changed since that timeframe. The 2011 Lee record flood and the subsequent 2018 Fishing Creek flood added a sense of urgency to review structural systems even though homes and businesses were acquired and removed from the floodplain after the 2011 Storm Lee event, especially near the Route 42 interchange and on the Hemlock Township (Fernville) side of the creek.

Hemlock Township and Montour Township

In Hemlock Township, on the Fernville side of Fishing Creek, a structural system (Floodwall) is not viable from an economic standpoint. The successful buyout program removed many repetitive loss properties. With far fewer homes along the creek, the benefit to cost ratio for any structural project would not exceed 1.0. During discussions with Hemlock Township, they indicated their focus was on continuing the buyout program and elevations, not structural system such as a levee or floodwall.

In Montour Township, the density of structures is not sufficient to justify a structural system.

For Bloomsburg general levee/floodwall alignment alternatives were developed based on the number of structures in the floodplain that would be located behind the alignment and the physical constraints imposed by structures. The Fishing Creek floodway will be encroached upon in a significant way for any alignment thus, the alignment of the levee is impacted by the flow area required for the floodway. Adjustments were made to minimize the induced flooding from the levee system, however, other forms of mitigation such as modification of the creek channel may be required to reduce the induced flooding to zero for permitting the project.

The floodwall or levee system alternative for the West End of Bloomsburg considered impacts to the Town tax base and the community fabric, present and future. Two (2) alignments were considered as shown and outlined below.

Alignment 1 shown in Figure 6.3 would be a levee and floodwall system extending along the left bank of the creek from the Railroad Street Bridge westward, then south to a point where it would turn east resulting in a U-shaped system tying out to high ground near Scott Avenue and W. Anthony Street. This alignment would avoid the Fairgrounds minimize disruption to access points and the general operation of the facility. It was also thought to be more economical. Right-of Way constraints limited the type of system options to an H-pile or sheetpile floodwall from Route 11 to high ground near Railroad Street.

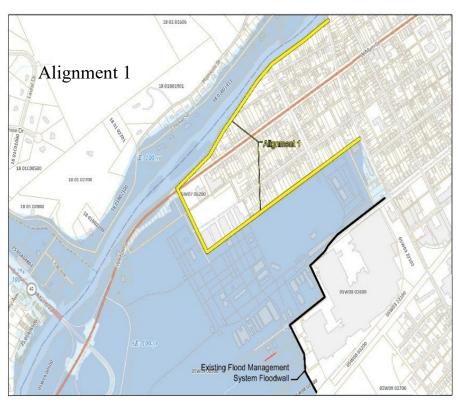


Figure 6.3 Proposed Levee Alignment 1

Alignment 2 (pictured right) extends through the Fairgrounds to tie into the first floodwall system in the vicinity of 6th Street. The Fairgrounds expressed interest in participating in this alignment due to the repeated flooding on their large parcel with 54 structures.

This alignment was not as limited as Alignment 1 with regard to right-of-way thus permitting the use of more economical earth and MSE levees.

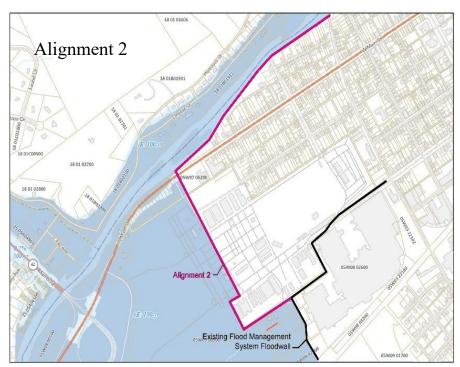


Figure 6.4 Proposed Levee Alignment 2

Opportunities to deal with interior stormwater runoff was considered more difficult with Alignment 1 since ponding areas are not available in the dense residential area. Alignment 2 has large relatively flat areas ideal for storing storm runoff to reduce the cost of pump facilities.

Unlike the previous two flood mitigation projects constructed nearby, utilities such as gas, water, communications, and electric do not pose any major challenges, including sanitary sewer systems or sanitary pump stations. Minor relocations may be necessary along the system alignments.

Prioritization Process

Prioritizing structural system alignments usually depends on the number and type of structures behind the system, available real estate, community support, permitting issues, and the total project cost.

Alignment #1 Considerations:

- 1. Restricted rights-of-way require sheet pile or H-pile floodwalls for significant length along the alignment. This increases the cost significantly.
- 2. Stormwater issues are more difficult to deal with since the Fairgrounds large land area is not available for management of stormwater flows.
- 3. Constructability issues along the restricted rights-of-way will increase cost.
- 4. The Fairgrounds has expressed a desire to be included behind the line of protection.
- 5. The benefit to cost ratio will be lower than 1.0.

Alignment #2 Considerations:

- 1. Less restricted rights-of-way reduce costs and eliminate most constructability issues.
- 2. Stormwater can be managed during flood events with one pump station versus two for Alternative #1.
- 3. The Fairgrounds buildings will be included in the project protection.
- 4. The benefit to cost ration is greater than 1.0.
- 5. The general community supports the proposal.

Based on the above considerations, Alternative 2 was chosen as the preferred alignment.

Fishing Creek Channel Modifications

Modifications to the Fishing Creek channel were considered a standalone structural project or a part of Alternative 2 for reduction of induced flooding along Fishing Creek.

General considerations:

 The Lee Flood is considered a 350-Year Flood on the Creek and a 200-Year Flood on the Susquehanna River.

- Modifications to the Fishing Creek channel cannot reduce the Base Flood and Storm Lee Flood Elevations to the degree necessary for Bloomsburg or Hemlock Township flood mitigation without a levee system, which is not economically feasible.
- Modifications to the approach roadway to the Railroad Street Bridge and a benched floodplain
 provide significant reduction for Fernville flooding in that reach of the stream. These
 modifications can also be utilized to mitigate some induced flooding from the levee on the
 Bloomsburg side.
- Dredging is not feasible. Rock in streambed prevents adequate excavation.

Figures 6.5 and 6.6 below show the bridge and channel modifications that are recommended for further study as structural systems for mitigation of induced flooding related to Alignment 2 (levee/floodwall system).

FEMA must provide an approved map revision and PADEP must issue a permit for any structural system impacting the floodplain or floodway.

This channel modification would be required along with community outreach to all impacted property owners to ensure that all induced flooding impacts are addressed to their satisfaction.

A detailed 2D H&H study is recommended to examine in detail the channel work necessary to maximize the reduction in the induced flooding along Fishing Creek.

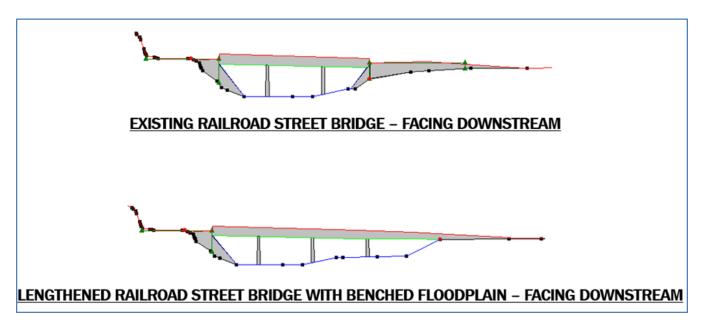


Figure 6.5 Existing Railroad Street Bridge and Proposed Modifications

BENCHED FLOODPLAIN BENEFITS:

- Compensates for lost conveyance in Bloomsburg Floodplain with levee option
- Allows more flow through RR St Bridge rather than through <u>Fernville</u>
- Environmental benefits of creek to Floodplain during lower flood flows.

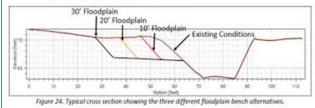




Figure 6.6 Benefits of Benched Floodplains

Table 6.1 Nonstructural Flood Risk Management Matrix (USACE, https://www.usace.army.mil/Missions/Civil-Works/Project-Planning/nnc)

Eng	Mational Nonstructural Committee	e									
	May 2019	- 1	PHYSIC	CAL NO	NSTRU	CTURA	AL MITI	GATIO	N MEA	SURES	
	NONSTRUCTURAL FLOOD RISK MANAGEMENT MATRIX	Extend	Piers	Posts Posts	Columns	Piles	Fill (Compacted)	Relocation	Acquisition	Dry Flood Proofing	Wet Flood Proofing
	Flood Depth										
	Shallow (less than 3 ft)	Y	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
	Moderate (3 to 6 feet)	Y	Υ	Υ	Y	Υ	Υ	Υ	Y	N	Y
	Deep (6 to 12 feet)	Υ	Υ	Y	Υ	Υ	Y	Υ	Υ	N	Y
tics	Very Deep (more than 12 feet)	N	N	N	N	N	N	Υ	Υ	N	N
eris	Flood Velocity	200	12 1		25 13			78			
gc	Low (less than 3 feet per second)	Y	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
Flooding Characteristics	Moderate (3 to 6 feet per second)	N	Y	Y	Y	Y	Y	Y	Y	N	N
Ď.	High (more than 6 feet per second)	N	Υ	N	N	Y	N	Υ	Y	N	N
din	Flash Flooding		072E 0			-		2 100		100	SECTION .
8	Yes (less than 1 hour warning)	Y	Υ	Y	Υ	Υ	Υ	Υ	Υ	N	N
ш.	No (more than 1 hour warning)	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
	Debris / Ice Flow										
	Yes	N	Υ	N	N	Υ	Y	Υ	Υ	N	N
	No	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
50	Site Location		() S		4 4			4 40			
stic	Coastal Beach Front	N	N	N	N	Υ	N	Υ	Υ	N	N
teri	Coastal Interior (Low Velocity)	Y	Υ	Y	Υ	Y	Υ	Υ	Υ	Υ	Υ
Site Characteristics	Riverine Flood Plain	Y	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
hai	Soil Type	- 10 m	ti (V S	<i>a</i>	4	4 44	di s		4 1
te	Permeable	Y	Υ	Υ	Υ	Υ	Υ	Υ	Υ	N	Υ
275	Impermeable	Y	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
	Structure Foundation					-					
	Slab on Grade (reinforced)	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
8	Crawl Space	N	N	N	N	N	Υ	Υ	Υ	N	Υ
sti	Basement	N	N	N	N	N	Υ	Υ	Υ	N	Υ
ter	Abandonment of Crawl space / Basement	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
M 30	Structure Construction	- 150 - 150	ala	•	to 18		•	9 99			
£	Concrete, Stone, or Masonry	Y	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
200	Metal	Υ	Υ	Y	Y	Υ	Υ	Y	Υ	Υ	Υ
Building Characteristics	Wood	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ
Bu	Overall Structure Condition		A 1000	•			•				
	Excellent to Fair	Υ	Υ	Υ	Υ	γ	Υ	Υ	γ	γ	Υ
	Fair to Poor	N	N	N	N	N	N	N	Υ	N	N
	Economics	32 33	3 3						31 3		
	Insurance Premium Reduction (Residential)	Υ	Υ	Y	Υ	Υ	Υ	Υ	Υ	N	N
(00)	Insurance Premium Reduction (Non-Residential)	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	Υ	N
ect An	Avoids Adverse Impact on Adjacent Property	Y	Υ	Υ	Υ	Υ	N	Υ	Υ	Υ	Υ
	Reduction in Admin Costs of NFIP	N	N	N	N	N	Υ	Υ	Υ	N	N
	Reduction in Emergency Costs	N	N	N	N	N	N	Υ	Υ	N	N
Benefits	Public Infrastructure Damage Reduced	N	N	N	N	N	N	Υ	Υ	N	N
80	Intangible Benefits		10000		Stor House				allo e		No. of London
	Ecosystem Restoration Potential	N	N	N	N	N	N	Υ	Υ	N	N
5	Recreation Potential	N	N	N	N	N	N	Y	Y	N	N
-	Community (Project Are) Cohesion	Y	Y	Y	Y	Y	Y	N	N	Y	Y
	Communicat in twice tweet come worth	N	N	<u> </u>	N	-		-11	Y	-	

Table 6.2 Comparison of Structural & Nonstructural Flood Protection Approaches (USACE, Local Flood Proofing Programs, February 2005)

Comparison of Flood Protection Approaches							
Structural Flood Control	Acquisition/Relocation	Flood Proofing					
Protects development without disrupting existing buildings or patterns of development	Disruptive: successful only if owners willing to sell and leave	Protects development with minimal disruption to existing buildings and development					
Can disrupt natural water flows and/or destroy wildlife habitat	Does not disrupt natural water flows or damage wildlife habitat; can improve habitat	Does not disrupt natural water flows or damage wildlife habitat, but may affect local drainage					
Can protect to any flood level	Generally most cost-effective for deep flooding and/or high velocity flooding	Some measures are only appropriate for low flood hazards					
Can be the most cost-effective and practical solution for areas already densely developed.	Can be the most cost-effective solution in areas of damaged or low-cost buildings	Can be the most cost-effective solution in areas with low flood depths					
Large capital expenditures often make this approach cost prohibitive or dependent on state or Federal assistance	Cost depends on property values, often done with state or Federal assistance	Many approaches can be afforded by the property owner					
Protects streets and land in addition to buildings	Can remove all types of property that need protection from floods	Focuses on protecting buildings					
Publicly owned, operated, and maintained, so more dependable over the long run	No operation and maintenance needed to keep flood protection benefits	Operation and maintenance dependent on every current and future occupant					
Built to a certain flood protection level that can be exceeded by larger floods, causing extensive damage	Only properties outside the cleared area are subject to damage from larger floods	Built to a certain flood protection level that can be exceeded by larger floods, causing extensive damage					
Can create a false sense of security as people protected by a project often believe that no flood can ever reach them	Damage level does not increase if flood levels increase	Can create false sense of security, especially if mainten- ance neglected or new owners not familiar with operation					
May improve property values and encourage more development	Communities lose some tax base and utility customers (may be offset by using vacated land for parks or other assets)	Preserves tax base and may improve property values					
Water supply and recreational uses can be incorporated into some projects' designs	Cleared out area can be converted to recreational, educational or ecosystem restoration uses	Preserves existing buildings and land uses. Compatible with existing ecosystem					
Although it may be unintended, can promote more intensive development in the flood plain	May encourage more intensive development in adjacent areas as people want to be near parks that were created on vacated land	Should encourage property maintenance and preservation of existing development					
Can have adverse flood plain and ecosystem impacts, e.g., higher flood stages and degraded ecosystem	May have positive flood plain and ecosystem impacts	Usually no change to flood plain or ecosystem					

SECTION 7 - FLOOD MITIGATION ALTERNATIVES EVALUATED FOR EACH MUNICIPALITY

7.1 Montour Township

A total of twenty-four (24) properties were evaluated for flooding impacts utilizing first floor elevations, topography, and a flood depth model developed for the 2011 flood.

Fifteen (15) of the properties were projected to not experience any flooding, 5 projected for basement flooding and 4 properties were projected to flood on the first flood. The majority of the flooding was in the Rupert area.

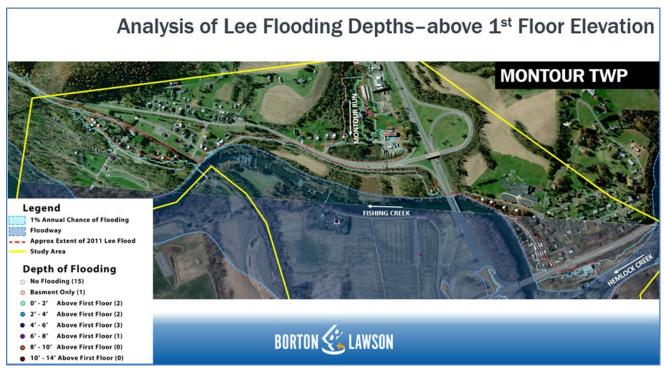


Figure 7.1 Modeled Depth of 2011 Lee Flooding in Structures in Montour Township

Mitigation Options

- Levees Not Feasible
- Buyouts Voluntary
- Elevations Voluntary
- RV Park Develop Flooding Emergency Action Plan
- Sanitary Pump Stations Dry Floodproofing Township recommendation
- Evaluate County Building for Floodproofing
- Ordinance Revisions Floodplain Management
- Construct Emergency Access Route from Reading St to Jackson St across RR Montour Township. Provides evacuation and access route when floods at base flood or higher occur. See Figure 7.2 below.

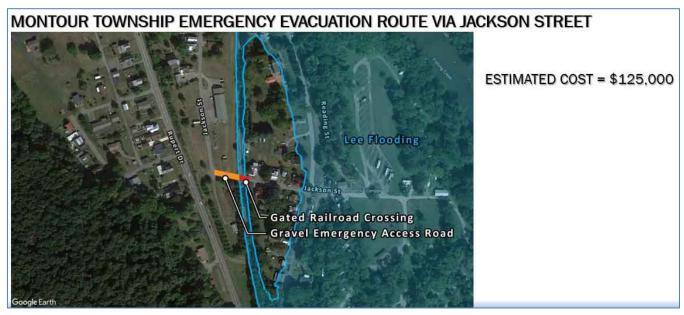


Figure 7.2 Montour Township Proposed Emergency Evacuation Route

Permits Required

Permits will be required for each project per Township ordinance. No large projects are proposed which would require larger more complex permitting.

Rights-of-way / Easements

The emergency access road on Jackson Street will require standard project permits and also an operating agreement between the Township and railroad authority.

7.2 Hemlock Township

Thirty-five (35) structures were evaluated for flooding impacts utilizing first floor elevations, topography, and a flood depth model developed for the 2011 flood.

Six (6) properties have been elevated and 14 did not have flooding. Three (3) structures were projected to experience basement flooding and 17 were projected to have approximately three feet of water on the first floor.

Mitigation Options

- Buyouts Voluntary
- Elevations Voluntary
- Emergency Access Road Hassert to Laurel Street The Township recommended reconstruction of Creek Road to provide an access during a flood event. An alternative was developed for access by connecting Hassert to Laurel Street (see Figure 7.3).
- Ordinance Revisions

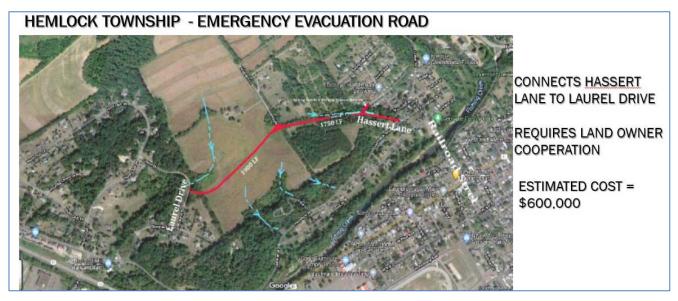


Figure 7.3 Proposed Emergency Evacuation Road for Hemlock Township

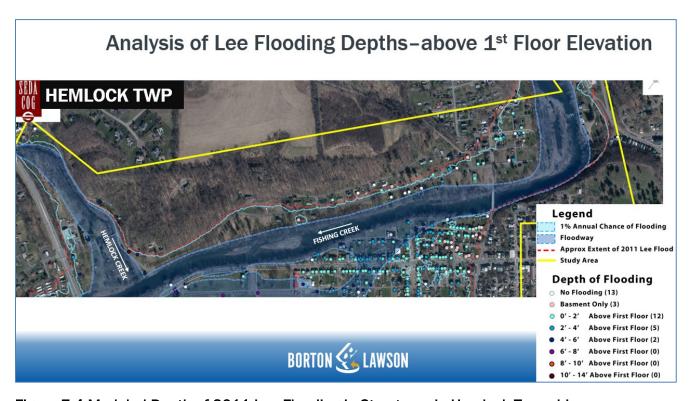


Figure 7.4 Modeled Depth of 2011 Lee Flooding in Structures in Hemlock Township

Structural Alternatives

Channel modifications to Fishing Creek in the area of Railroad Street, such as outlined in Section 6, could benefit homes in Fernville if further 2D H&H analysis is performed to verify and refine the

conclusions reached in this study. If reduction of flooding levels up to two (2) feet can be achieved, it may be cost effective to consider this option. The benefits would accrue for the higher level flood events such as the base flood and events similar to the 2011 flooding.

7.3 Town of Bloomsburg

Nearly 300 properties were evaluated for flooding impacts utilizing first floor elevations, topography, and a flood depth model developed for the 2011 flood.

Evaluation projected the following:

- Seventeen (17) of the properties were not flooded;
- Sixteen (16) properties experienced basement flooding;
- One hundred seventy-four (174) had between zero (0') and four feet (4') of water on the first floor, and
- Ninety (90) had greater than four feet (4') of flooding on the first floor.

Mitigation Options - Nonstructural Alternatives

- Buyouts Voluntary
- Elevations Voluntary
- Mitigation Reconstruction
- Managed Retreat Rebuild offsite
- Wet Floodproofing Commercial Properties
- Utility Relocations
- Fishing Creek Gauge Town recommendation: Requested the installation of additional stream gauge to enhance early notification for Fishing Creek flooding
- One (1) Emergency Siren Addition in the residential area closest to Fishing Creek

Bloomsburg Fairgrounds

- Wet Floodproofing
- Utility Relocation
- Emergency Action Plan

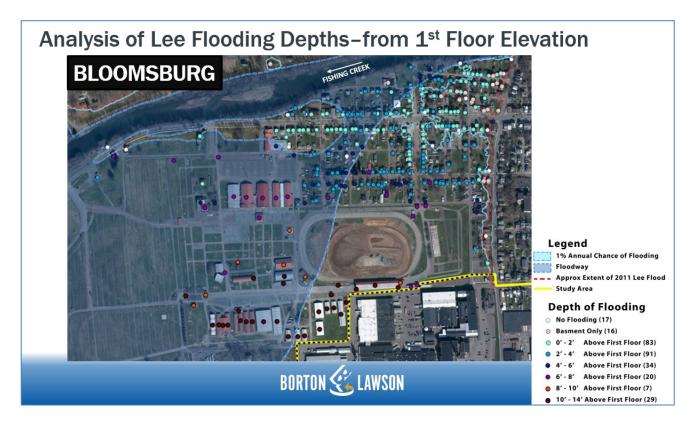


Figure 7.5 Modeled Depth of 2011 Lee Flooding in Structures in the Town of Bloomsburg

Structural Alternative

The recommended structural alternative is a flood mitigation system consisting of earth levees and a floodwall with a top of system elevation based on the Storm Lee flood levels plus approximately three (3) feet of freeboard which satisfies the FEMA requirements for the NFIP. The plan considered community requirements for minimizing the impacts from a system which would change the visual aesthetics in the community. To mitigate the visual impacts, the concept plans show various types of levees.

The overall system concept plan and various enlarged segments of the system are shown below. The system consists of the following components:

- Earth levee 6,200 feet (1.2 miles)
- Concrete capped sheet pile wall 1,700 feet (0.3 miles)
- Roadway closure structures (6)
 - o Route 11 5' Height
 - o Gates 2 and 2A Fairgrounds access 7' Height
 - Gate 3 Fairgrounds 10' Height
 - Gate 4 and 5 Fairgrounds -10' Height
- Pump Station

- o Fairgrounds at 6th Street Stormwater pump station
- Induced flooding impacts:
 - Upstream of Railroad Street Negligible
 - Downstream of Railroad Street along levee length 1.8 Feet

Note: For permitting of project, induced flooding must be mitigated to zero increase or impacted structures must be provided flood protection.

Fishing Creek Channel Modifications for induced flooding mitigation

Concept Drawings

Proposed concept drawings and levee sections are shown below in Figures 7.6 and 7.7. See Appendix E for larger scale plans.



Figure 7.6 Concept Design Plan

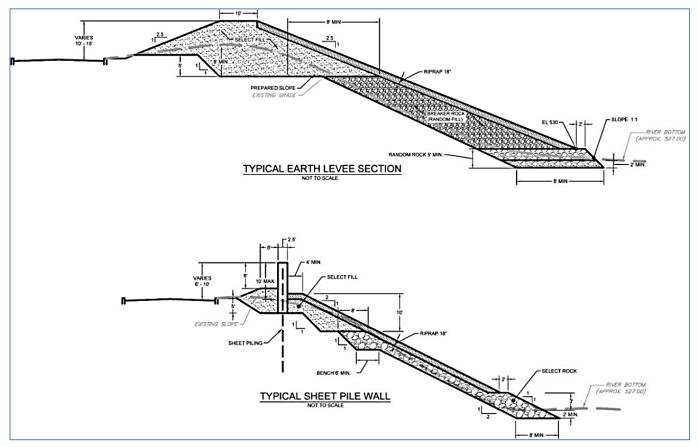


Figure 7.7 Concept Drawings of Typical Levee Sections

The proposed alignment is a schematic level concept without the benefit of detailed design documentation and analysis.

The Fishing Creek floodway will be encroached upon in a significant way. The flow depths through the floodway area are shallow however, a conveyance analysis performed to verify the induced flooding impacts resulted in about two (2) feet of increase in the base flood levels. This must be decreased through mitigation efforts to zero feet.

The alignment minimizes property takes, however, several properties will need to be acquired and as many as nine other properties will require partial takes for removal of garages and sheds along the levee alignment. Arriving at the proposed alignment considered the construction cost and the impact of reducing the tax base with property takes.

The system features represent the proper mix of context sensitive floodwall and levees on the most cost effective alignment for flood mitigation. A cost estimate for the proposed alignment was developed for the economic analysis. A summary of the estimate is included at the end of this section.

Levee / Floodwall System Description

The recommended project will consist of a system of earthen levees, MSE levees, concrete floodwalls, sheet pile floodwalls, road closure structures, and a storm water pump station. Earthen and MSE

levees are proposed for the majority of the flood protection alignment. Riprap will be utilized to protect the waterside slopes of the system along Fishing Creek.

The system begins immediately to the East of Railroad Street where the earthen levee ties into high ground. The top of the system at this location is Elevation 491.00. The alignment proceeds westward across Railroad Street which is at Elev. 490.0 +/-. The roadway would be raised approximately one foot. The top of protection elevation descends from Elev. 491.00 at Railroad Street to Elev. 485.00 at the Route 11 closure structure.

On the west side of Railroad Street, an earthen levee with a landside toe drain extends downstream to Station 11+50. Through this reach the levee crest is 10' wide with a land side slope of 2.5 Horizontal to 1 Vertical (2.5H:1V) and a riverside side slope of 2H:1V. This reach of the system is through a residential area. The riverside toe will extend into the bed of the creek since severe erosion since the 2011 Lee Flood has caused loss of the bank along this reach of the creek. The riverside levee slope will be protected by 18 to 24" riprap.

A MSE levee then extends westward adjacent to Fishing Creek from Station (Sta.) 11+50 to 14+50. The MSE levee has a 12' wide crest with vertical wall faces, fall protection railings and a landside toe drain. The MSE levee will have a riverside slope of 2H:1V. This reach of the system is also through a residential area. The riverside toe will extend into the bed of the creek

Starting at Sta. 14+50 a sheet pile wall is proposed 4 feet from the top of bank to Sta. 22+50. A concrete cap can be added to the sheet piling for additional strength and aesthetics.

This reach of the line of protection is on an alignment with minimal lateral clearance through the residential area. The riverside levee slope will be protected by 18 to 24" riprap.



Figure 7.8 Proposed Levee Design from Railroad Street to West 1st Street



Figure 7.9 Proposed Levee Design Near Route 11 Closure Structure

Beginning at Sta. 22+50, an earth levee will extend to the Route 11 road closure structure abutment at Sta. 25+70. The stop log closure across route 11 is approximately 6 feet in height if the roadway is not raised. Being a state highway and also being in the floodplain, it was determined that the road should not be raised to lower the activation frequency.

On the south side of the closure, an earth levee begins at Sta. 26+50 extending to the Fairgrounds road closure structures 2 and 2A. The top of levee is at Elevation 485.00, about 6 to 7 feet in height. Flow velocities from the creek overbank flows during higher level flood events requires 24" riprap on the levee slope.

Closures 2 and 2A are proposed to be automatic Floodbreak type of closures since the creek flows in this area are fast rising compared to the river backwater which is also a source of flooding in the West End of Bloomsburg. To minimize the activation frequency, the ground level would be raised to elevation 478.00 as indicated on the concept plans.



Figure 7.10 Proposed Levee Design from Route 11 Closure to Gate 3 Closure

An MSE levee of varying heights is proposed from the abutment of closure 2A at Sta. 31+30 to the tie-in to a concrete floodwall at Sta. 59+95. The tie-in location is near Closure 5 of the Columbia County Levee System #1. This location is also the lowest ground elevation, approximately Elev. 470.5. With a top of system elevation of 485.00, the MSE levee would be about 14 feet in height. Extensive investigation of the embankment stability and underseepage potential will be required to determine the final width of the crest of the levee and the riverside earth slope which is assumed to be 3:1. Underseepage may require a deeper base trench (See MSE levee cross section in concept plans). Other options would be a slurry cutoff trench or sheeting.

The above stretch of MSE levee has three access road closure structures located at Sta. 40+35, Sta. 46+10, and Sta. 47+25. They are proposed stop log closures 10 feet in height. To minimize the erection time for each flood event, it is assumed most of the approximately 10 foot segments of stop

logs between the steel column supports can remain in place until a major Fairgrounds event which would require removal to fully open the access points.



Figure 7.11 Proposed Levee Design from Gates 4 and 5 Closure to Tie-in Location

Interior Flooding

A stormwater pump station is proposed at approximately Sta. 51+25 to collect and discharge interior stormwater draining towards the levee from the Fairgrounds and the residential and commercial areas of the West End behind the levee system. Detailed drainage calculations will be required to develop a conveyance system which will collect the drainage which now exits to Fishing Creek via several storm sewers along to creek. These sewers extend along town streets from the edge of the Fairgrounds to Fishing Creek.

Connections to the systems would convey the excess flows during high rainfall periods to the combined overland and subsurface system directing the flows to the pump station at Sta. 51+25. The pump station is estimated to be a 20,000 gallons per minute (GPM) capacity if the very low area of the main promenade of the fairgrounds is utilized for storage at a 2 foot depth.

Other features consist of stormwater control structures at each storm sewer penetration of the system along Fishing Creek and at the Route 11 storm sewer system.

Geotechnical Conditions

The USACE report of 2005 provides a good understanding of the geotechnical conditions along the proposed levee / floodwall system alignment.

Several items such as recommendations for seepage control features, types of suitable floodwall systems along the bank of Fishing Creek, material sourcing, and soil parameters for engineering design are a few items to be determined by geotechnical engineers during the during the preliminary engineering and design phase.

Additional subsurface investigations should be undertaken to refine the design features and to identify any unknown foundation conditions. Seepage potential along the MSE levee has to be confirmed. Previously identified pervious subsurface soil strata along to bank of Fishing Creek will require testing and geotechnical recommendations. Also, subsurface conditions along the reach of the proposed sheet pile wall require additional investigation and analysis for acceptable driving conditions for PZ piling to the depths required for stability and seepage control.

The future investigations will consist of additional soil borings, soil testing, rock coring, test pits, and permeability tests. Samples recovered will be tested as required. Design of the recommended plan will be refined during design based on the additional information from the investigations.

Environmental Impacts

Impacts resulting from implementation of the recommended plan have been assessed as outlined in Section 2. Key environmental impacts include those related to biological resources (aquatic habitat), cultural resources, and visual resources. In general, the project would introduce a large-scale built element to the natural environment, potentially affecting view from and towards Fishing Creek.

The floodwalls can be designed with aesthetically pleasing architectural treatments. Design details that would minimize impacts, include the use of architectural construction materials and/or landscaping to blend the structures into the surrounding environment.

The project would involve placement of fill material in jurisdictional waters of the U.S. In addition, excavation in the creek would also be required for construction of the levee slopes. A joint permit will be required from the USACE for the project.

With the project still in the feasibility phase, there are still a number of unknown variables that may result in adverse effects through the future planning, design, and construction phases, however, the environmental investigations for this Study conclude those to be minimal and easily addressed through the design process. Permitting requirements are detailed in Section 8.0.

Mitigation of Adverse Flooding Impacts

Adverse impacts were outlined in Section 4.0. Fishing Creek channel modifications for elimination of induced flooding to meet FEMA requirements for a zero increase in the BFE after construction of the levee and floodwall system. The system alignment configured for this report is preliminary and would

be refined in the design phase for the project. Opportunities for mitigation of impacts suggested below were deemed possible but not fully pursued during the modeling of the system due to the study level effort. The modeling results for Fishing Creek provided enough insight into the sensitivity of the creek levels to the alignment of the levee to provide a level of confidence that the possible mitigation levels below are realistic.

The following mitigation considerations for flood level reduction measures could be incorporated into the design of the recommended system.

- 1. Adjustment in Levee Alignment along Fishing Creek.
- 2. Expand floodplain channel along right descending bank of Fishing Creek (Fernville side) up and downstream of Railroad Street.
- 3. Railroad Street Bridge and approach roadway modifications.

Residual Damages

Although the recommended plan eliminates the 1-percent floodplain throughout the West End of the community, it would not entirely eliminate every flood risk. Nonstructural solutions can be evaluated as a means of providing additional mitigation measures since structural flood mitigation systems can be overtopped by future record flooding.

The flood warning system which has been included in the recommended plan as a nonstructural measure will allow residents of the community to evacuate in a timely manner to avoid loss of life during a catostrphic flood event.

Another residual risk associated with the recommended plan is the risk related to the severity of local rainfall induced street flooding during a flood event. A 10 year rainfall was utilized for this Study to determine the pump station capacities. Further evaluation of the interior drainage system is recommended during project design.

Risk and Uncertainty

Risk and uncertainty is fundamental to all water resource planning projects. There is some project performance uncertainty in all studies, even with the risk assessment procedures.

This Study incorporated risk management framework principles and risk-informed planning into the plan formulation process. Specific examples include the following:

- As previously described, the probability of a flood occurring at the same time as a major rain storm is low. The hydraulic analysis for the Study included the evaluation of a 10 year rainfall event over the study area while the river is at flood stage.
- Other risks include unknowns that will be addressed in more detail during future design efforts, such as field investigations of geotechnical information, cultural resources, biological resources, and updates of available information about construction costs and property values for economic analyses. Subsequent technical, agency, and public reviews aid in identifying and assessing concerns regarding related project risks, and will assist in identifying ways to reduce them to acceptable levels during the design phase of the project. Opportunities for

value engineering should be considered during design to reduce the risks of missed opportunities for identifying more cost efficient project features, designs, and/or construction methods.

Resiliency, Overtopping

Under the risk-based framework, the top of the proposed system would be designed for the Lee flooding level plus three feet. Resiliency refers to how well the system performs in case of capacity exceedance or overtopping of the system. Resiliency of the system can be incorporated as a structural measure into a levee and floodwall design by eliminating features on the protected side of the levee or floodwall that would erode easily during flood events that exceed the top of levee / wall elevation. It can also address how well the community can recover from an overtopping event by limiting the destructive impacts from an overtopping event.

If the recommended system was constructed, a unique outcome would be its connection and relationship to the first and second levee systems built in Bloomsburg. It would create a three cell combined system.

From a resiliency standpoint, each cell would be independent of the other two systems. If one system failed during a flood event, the other two systems should not be impacted unless a sudden and catastrophic failure mode would result in a destructive flood wave.

See Figure 7.12 for the configuration of the combined systems. Each of the systems has a common leg with another system. This creates three (3) separate cells or systems for flood mitigation resiliency.

Levee superiority should be included in the design of the system top of protection elevations to facilitate overtopping at the extreme downstream location within the system limits. The overtopping reach is to provide a known initial exceedance location and to provide some warning or evacuation time before total system exceedance.

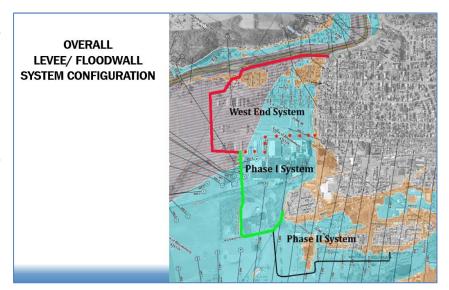


Figure 7.12 Overall System Configuration

Materials for Construction

Suitable borrow materials (including rip-rap) and soil fill material required for project construction are expected to be available from existing commercial sources. Excavated materials from project construction are expected to be reusable for random fill in the levee system. Soil and rock waste would be hauled off site for disposal at an approved waste facility. Haul routes are expected to consist

primarily of existing public roads. Some roadway improvements and localized access roads would be required in addition to staging areas for contractor equipment and materials storage.

Consideration should also be given to utilization of excavated material from any Fishing Creek channel modification work.

Project Costs and Benefits

The project cost estimate (2022 price level) for the recommended system is summarized below. Additional detail is provided in Appendix D. The project first cost serves as the basis for providing the cost of the project for which funding is sought. It includes costs associated with engineering and design, construction, lands, easements, rights-of-way, utility relocations, sewer and road modifications, and a 25% contingency.

The BCR for the levee and floodwall system was calculated to be 1.05 to 1.17. There are additional benefits that could be added to this evaluation to increase the BCR including:

- damage costs to roadways and utilities that would be prevented with the construction of the levee system, and
- loss of income from commercial properties that could be prevented with the construction of the levee system.

Possible cost reduction opportunities are listed below:

- Further refinement of sewer system consolidations and pump statio;
- Funding of project elements that can be completed separate from the Levee construction (e.g. sanitary and storm sewers and utilities);
- Economical slope protection meeting USACE requirements versus riprap.

The benefits of constructing a levee as a structural mitigation option are:

- Protects approximately 300 structures, including the Fairground Buildings, in the Floodway, Floodplain, and Zone X. Total protected property value is estimated at \$44.7 Million (utilizing Columbia County assessed values multiplied by the Common Level Ratio factor published by the State for Columbia County).
- Maintaining tax base approximately \$657,000 in taxes.

Table 7.1 Total Project Cost Estimate

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ITEM	COST					
Construction – Levee & Floodwall System	\$22,000,000					
Induced Flooding Mitigation – Stream Benched Floodplain & Property Elevations	\$3,000,000					
Environmental / Cultural Resources	\$500,000					
Legal & Administration of Grant	\$275,000					
Engineering / Geotechnical	\$2,300,000					
Permitting	\$300,000					
Construction Inspection	\$675,000					
TOTAL	\$29,050,000					

Performance

Future impacts of climate change on hydrologic conditions such as the frequency and severity of flooding is the subject of much debate nationwide. It is prudent to assume the recent events warrant a system design which would mitigate a flood of record (2011 Lee flood).

The 1972 Agnes flood was estimated after the event to be a 350-year flood. It is now estimated to be close to the 100-year flood forty years later. The 2011 Lee flood (Flood of Record) is considered a 125 to 200 year flood, approximately 2 feet higher than the updated 100 year flood. Existing conditions and damages that have occurred in the recent past confirm the flooding problem would likely persist and possibly get worse in the future.

The concept levee was developed with estimated top of protection elevations set to mitigate risk for a recurrence of the preliminary (2022) BFE for the Susquehanna River and for USGS high water marks for the record Tropical Storm Lee flood (2011) along Fishing Creek. The top of protection profile was established by adding a minimum of four feet to the updated base flood surface profile after adjustments to reasonably reflect the impact of river channel features.

Operation and Maintenance

All structures and equipment constructed, erected, or installed by or with the help of the Federal and State Government or private entities would be the property of Columbia County. The County Water Mitigation Authority was established by Columbia County to operate, maintain, and replace any County flood mitigation project features when necessary.

Real Estate Requirements

Several properties along the alignment will require full takes to accommodate the levee and access easements. Two are located on West First Street between Barton Avenue and Leonard Street. Another is located at the top of the Fishing Creek bank opposite Orchard Street.

Other takes will be partial for accessory type structures such as garages and sheds.

Permits Required.

Permits required to construct the flood risk management system are anticipated to be the following:

- USACE / PADEP Joint Permit
- PADEP Sewage Planning
- PADEP Water Quality Management Permit
- PADEP Air Pollution Permit
- Town of Bloomsburg Zoning
- Town of Bloomsburg Building Permit

7.4 Benefit Cost Analysis

The FEMA BCA Tool was utilized to evaluate the cost effectiveness of the flood mitigation alternatives including acquisitions, elevations, mitigation reconstruction, and for the proposed levee/floodwall system.

Montour Township & Hemlock Township

The mitigation alternatives evaluated for Montour and Hemlock Townships included acquisition/demolition, elevations and mitigation reconstruction (demolish and rebuild).

Due to the low density of structures that remain in the floodway/floodplains in both municipalities, combined with the high cost of implementing a structural levee/floodwall system in this area, a structural option is not economically feasible.

Town of Bloomsburg

The mitigation alternatives evaluated for the Town of Bloomsburg included acquisition/demolition, elevations, mitigation reconstruction and the construction of a Levee/Floodwall system.

Acquisitions

FEMA will fund an acquisition/demolition on structures that meet certain criteria. This type of program is voluntary for property owners. The structure must be located in a SFHA (Floodway or Floodplain) or, if located outside of a SFHA, be classified as a RL or SRL property.

For Acquisitions, FEMA has a defined Pre-Calculated Benefit of \$323,000 per structure. If the total cost for the acquisition/demolition project is less than \$323,000, the project is considered cost effective and qualifies for FEMA funding. In this case, a BCA is <u>not</u> required to be completed to obtain FEMA funding.

If acquisition/demolition project costs for a structure are estimated to be greater than \$323,000, FEMA funding may still be utilized; however, a BCR must be calculated utilizing FEMA's BCA Tool, and the BCR must be shown to be greater than 1 to qualify for FEMA funding.

Based on evaluation of County assessed property values and estimated administration and demolitions costs that would factor into the acquisition/demolition process, greater than 95% of properties, evaluated in aggregate, within the SFHAs within Montour, Hemlock and Bloomsburg would qualify for the FEMA Pre-Calculated Benefit for an acquisition/ demolition project.

There is a 25% local match required for utilizing FEMA funding through the FMA and BRIC programs, but no match required if HMGP funding is utilized.

In summary,

Acquistions/Demolition FEMA Pre-Calculated Benefit: \$323,000.
 Project deemed eligible when project cost is less than \$323,000.

- If project cost is greater than \$323,000 need to complete BCA and show BCR > 1.
- >90% Residential Properties in Floodway/Floodplain are estimated to qualify under FEMA Pre-Calculated Benefits.
- 25% Local Share required with FEMA FMA and BRIC programs; HMGP no local share.

Elevations/ Mitigation Reconstructions

FEMA will fund elevations and mitigation reconstruction on structures that meet certain criteria. Mitigation Reconstruction involves demolition of a structure with a complete rebuild, at an elevation above the PA Higher Regulatory Standard. The structure must be located in a SFHA (Floodway or Floodplain) or, if located outside of a SFHA, be classified as a RL or SRL property. This type of program is voluntary for property owners.

For elevations and mitigation reconstructions, FEMA has a defined Pre-Calculated Benefit of \$205,000 per structure. If the total cost for the elevation or mitigation reconstruction project is less than \$205,000, the project is considered cost effective and qualifies for FEMA funding. In this case, a BCA is <u>not</u> required to be completed to obtain FEMA funding.

If the elevation or mitigation reconstruction costs for a structure are estimated to be greater than \$205,000, FEMA funding may still be utilized; however, a BCR must be calculated utilizing FEMA's BCA Tool, and the BCR must be shown to be greater than 1 to qualify for FEMA funding.

Elevations and mitigation reconstruction projects have a number of variables that have a direct impact on the cost of the project, such as the type and size of the home's existing foundation, the condition of the foundation, the required height for the elevation, and the size and finished detail of the re-built home (for mitigation reconstruction). Subsequently, due to the number of variables that impact cost for these types of projects, each home would need to be evaluated on a case-by-case to determine if it would qualify for the FEMA Pre-Calculated Benefit.

There is a 25% local match required for utilizing FEMA funding with the FMA and BRIC programs, but no match required if HMGP funding is utilized. With elevations and mitigation reconstruction, additional funding outside of FEMA programs is required if the homeowner desires a higher elevated home than FEMA will fund resulting in greater costs than covered by FEMA. FEMA will fund an elevation to the height of the BFE + 1.5 feet (PA Higher Regulatory Standard) or to the height of Best Available Data (Flood of Record Elevation).

In summary,

- Elevations & Mitigation Reconstruction, FEMA Pre-Calculated Benefit: \$205,000 per structure.
 - Project deemed eligible when project cost is less than \$205,000.
- If project cost is greater than \$205,000 need to complete BCA and show BCR > 1.

• 25% Local Share required with FEMA FMA and BRIC programs; HMGP no local share.

Levee/Floodwall System

A FEMA BCA was completed for the proposed levee and floodwall system to be located in the West End of Bloomsburg. The analysis showed the levee to be cost effective.

The following key data/criteria were utilized in the FEMA BCA Tool for this evaluation:

- Levee was modeled as a "Floodproofing" Mitigation Alternative.
- Levee Total Project Costs = \$29 million (includes construction, design, real estate costs, permitting and induced flooding mitigation costs).
- Levee useful life = 75 years.
- Levee Estimated Annual Operating & Maintenance Costs = \$75,000 per year.
- Residential Building Replacement Value (BRV) = \$150/ square foot (SF).
- Commercial BRV = \$150/ SF (with the exception of the Fairgrounds' buildings).
- Fairgrounds Buildings BRV = \$100/ SF.
- Non-Residential Garages BRV = \$100/ SF.
- Lowest Finished Floor Elevations (all Basements were entered as unfinished).

The BCR for the proposed levee using above criteria was calculated to be 1.05.

A number of benefits* (costs that would be prevented during a flood with the construction of a levee system) were <u>not</u> included in this BCA, but could be entered into the BCA for the levee project if needed or for future funding applications, include the following:

- Damage costs to roadways and utilities (sanitary, storm, gas, water, electric, traffic signals, etc.).
- Loss of income from commercial properties there are 19 commercial properties located within the floodway & floodplain in Bloomsburg, with the Fairgrounds having the largest number of structures (54) impacted.
- Finished basements in residential or commercial properties.
- Volunteer efforts and expenses.

*Utilization of these benefits in the BCA requires submission to FEMA of supporting documentation. Adding benefits to the BCA should increase the BCR value for the proposed project assuming project costs are not increased.

A BCA for the proposed levee system was also completed using the same above criteria but with a reduced total project cost of \$26 million, assuming engineering and permitting could be completed as a separate phase of the project, and therefore these costs could be subtracted from the \$29 million. This produced a BCR of 1.17.

If FEMA BRIC funding were to be utilized for a levee project, a 25% local share would be required.

7.5 Flood Insurance

In October 2021 FEMA overhauled the NFIP to include a new pricing methodology. The new program is known as Risk Rating 2.0 – Equity in Action. The intent of the program is to allow policyholders to make more informed decisions on the purchase of flood insurance. The new program incorporates improved technology to develop individualized actuarial rates based on multiple flood risk variables.

National Flood Insurance Program

NFIP Risk Rating 2.0

Changes

- Changes from Zone to Individual Rating
- Zone changes smaller difference in costs
- Replacement cost is part of premium calculation
- No elevation certificates needed
- Premiums reflect unique flood risk

Staying the Same

- Statutory rate caps on annual premium increases
- Availability of premium discounts
- Transfer of policy discounts to new owners
- FIRM's used for mandatory purchase and Floodplain Management
- FEMA Community Rating System discounts (all flood zones)



Figure 7.13 Summary of NFIP Risk Rating 2.0

SECTION 8 - STUDY FINDINGS

8.1 Study Summary

- Nonstructural flood mitigation is feasible for the three communities, Montour Township, Hemlock Township, and the Town of Bloomsburg.
- Structural flood mitigation is feasible for the West End of the Town of Bloomsburg. Benefit to Cost Ratio greater than 1.0.
- Flood Insurance As of Summer 2022, all existing policies will be renewed under NFIP's Risk Rating 2.0 program.
- Flood Mitigation Alternatives Nonstructural and Structural (Levee) Alternatives are cost effective when BCR>1.0. Some nonstructural alternatives will require individual analysis; this is more applicable for higher value properties.
- County and Municipalities will determine the mitigation alternatives that will be implemented.
- Challenges:
 - o Acquisitions / Elevations / Mitigation-Reconstruction Voluntary Program
 - Commercial Properties Funding Options
 - Levee System
 - Further Analysis of flooding Impacts with 2D analysis
 - Mitigation of Induced Flooding
 - Permitting of levee in Floodway
 - Property takes on voluntary basis

8.2 Municipal Review

Adoption of any of the alternatives outlined in this study should be in line with current and future planning initiatives including the County Hazard Mitigation Plan. Funding opportunities for the larger projects may require community action to facilitate the grant application process.

8.3 Municipal Adoption Process

Adoption of any of the alternatives outlined in this study should be in line with current and future planning initiatives including the County Hazard Mitigation Plan. Funding opportunities for the larger projects may require community action to facilitate the grant application process.

8.4 Incorporation into Existing Planning Mechanisms

This report and its recommendations can in part or in its' entirety be adopted for incorporation into the County Hazard Mitigation Plan or community land use planning documents

8.5 Opportunities

- Recent progress towards flood mitigation in Columbia County provides momentum and optimism for future flood mitigation. Proven success helps with pursuit of funding.
- Community supports action.
- County committed to flood resiliency utilizing cost effective approach based on best practices.

Timing for federal infrastructure funding requires near term action – Schedule is important.

8.6 Challenges

Community Actions - Each community has made significant progress with property acquisitions and demolition of flood prone properties. Hemlock and Montour Townships are expected to continue to prioritize acquisitions in the study area.

Small projects mentioned in this report, such as emergency access roads, require community action and funding.

Any modifications to the Fishing Creek channel to mitigate current flooding and mitigation of induced flooding related to the levee alternative for the Town of Bloomsburg will require coordinated actions to obtain state and federal stream encroachment permits.

Due to the significant amount of structures in the West End of Bloomsburg, a successful flood mitigation program will require voluntary participation in the program by a sufficient number of property owners.

Next Phase - Design - The next phase of design will be the preliminary engineering and design (PED) phase. Final design for the levee, MSE walls, floodwall, closure structures, roadway revisions, drainage control structures, and the stormwater pump station will be performed based on the additional new data and the information collected to date.

8.7 Next Steps

Nonstructural Alternatives

- Compare possible alternatives to current priorities
- Prioritize all alternatives
- Review chosen alternatives with legislative leaders for inclusion in local and county planning documents
- Secure funding (some may be continuation of current programs)

Structural Alternatives

- Perform 2D analysis of Fishing Creek to determine options for mitigation of stream flooding and permitting of levee in floodway.
- Consider funding for preliminary engineering to verify project details and cost.
- Coordinate with local and state legislators for funding of levee system in Bloomsburg.

8.8 Funding Opportunities

FEMA Grant Programs

Hazard Mitigation Grant Program (HMGP)

FEMA's HMGP provides funding to state and local governments to develop Hazard Mitigation Plans and rebuild in a way that reduces, or mitigates, future disaster losses in their communities. HMGP funding is available after a presidentially declared disaster. Total funding for the HMGP program is allocated based on the percentage of funds spent on Public and Individual Assistance for each Presidentially declared disaster.

The projects are cost shared 75% federal and 25% local. In Pennsylvania, the Commonwealth provides the non-federal share.

Homeowners cannot apply for a grant. The local community may apply for funding on their behalf.

To qualify for HMGP funding, state and local governments must develop and adopt hazard mitigation plans. The plans are required to be updated every five years.

Eligible Projects

Planning & Enforcement

- Developing and adopting hazard mitigation plans, which are required for state, local, tribal and territorial governments to receive funding for their hazard mitigation projects.
- Acquisition of hazard prone homes which enables owners to relocate to safer areas (acquisition).
- Post-disaster code enforcement.

Flood Protection

- Protecting homes and businesses with permanent barriers to prevent floodwater from entering (levees, floodwalls, floodproofing).
- Elevating structures above known flood levels to prevent and reduce losses (elevation).
- Reconstructing a damaged dwelling on an elevated foundation to prevent and reduce future flood losses. (Mitigation Reconstruction).
- Drainage improvement projects to reduce flooding (flood risk reduction projects).

Flood Mitigation Assistance (FMA) Grant

The FMA Program is a competitive grant program that provides funding to states and local communities. Funds can be used for projects that reduce or eliminate the risk of repetitive flood damage to buildings insured by the NFIP.

The projects are cost shared 75% federal and a 25% local share. For Severe Repetitive Loss Properties (SRL) the funding is 100% federal and for Repetitive Loss (RL) properties, the funding is 90%federal. Generally, between \$160 million and \$200 million is available in Flood Mitigation Assistance funding each year.

FEMA chooses recipients based on the applicant's ranking of the project and the eligibility and costeffectiveness of the project. FEMA requires state and local governments to develop and adopt Hazard Mitigation Plans as a condition for receiving certain types of non-emergency disaster assistance, including funding for hazard mitigation assistance projects. The plans are required to be updated every five years.

Communities must be participating in the NFIP and must be insured under the NFIP.

The BRIC program is available annually and the grant period opens on September 30. Applications are due by January 28 of the following year. Awards are made on October 1.

Eligible Projects

Eligible individual flood mitigation projects include the following project types:

- Priority 1 (Project scoping, previously referred to as advanced assistance): conducting
 meetings, outreach, and coordination with subapplicants and community residents;
 developing or conducting engineering, environmental feasibility, and/or Benefit-Cost
 Analyses (BCA); undertaking activities that lead to development of project applications;
 evaluating facilities to identify mitigation actions; and using staff or resources to develop cost
 share strategies.
- Priority 2 (Community flood mitigation projects): eligible projects that benefit NFIP insured properties include, but are not limited to, localized flood control, floodwater storage and diversion, floodplain and stream restoration, stormwater management, and wetland restoration/creation.
- Priority 3 (Technical assistance): technical assistance to maintain a viable FMA program over time; to be eligible for technical assistance, the applicant must have received an prior FMA award of at least \$1 million.
- Priority 4 (Flood hazard mitigation planning): Planning grants for the flood hazard component of State, Local, Territory, and Tribal (SLTT) Hazard Mitigation Plans and plan updates.
- Priority 5 (Individual flood mitigation projects): property acquisition and structure demolition/relocation; structure elevation; dry floodproofing of historical residential structures or nonresidential structures; nonstructural retrofitting of existing buildings and facilities; mitigation reconstruction; structural retrofitting of existing buildings.

Building Resilient Infrastructure and Communities (BRIC) Program

FEMA's new BRIC program provides funding for public infrastructure projects and mitigation efforts that bolster a community's flood resilience before a disaster strikes. In the FY2021 cycle, BRIC will award \$1 billion in funding, split into 3 categories: State/Territory Allocation, Tribal Set-Aside, and a National Competition. BRIC replaces FEMA's Pre-Disaster Mitigation (PDM) program.

Mitigation projects that were eligible under PDM are still eligible under BRIC. While BRIC requires states to have had a Presidential Disaster Declaration issued in the last seven years in order to be eligible for funding, numerous major disaster declarations in recent years have led to Declarations being issued for all 50 states, therefore communities in all states and territories meet this eligibility requirement.

Communities must be participating in the NFIP.

The projects are cost shared 75% federal and a 25% local share.

The FMA BRIC program is available annually and the grant period opens on September 30. Applications are due by January 28 of the following year. Awards are made on October 1.

Eligible Projects

FEMA provides the following uses of assistance through the BRIC program:

Capability and capacity-building (C&CB) activities: Activities that enable recipients to identify mitigation actions and implement projects that reduce risks posed by natural hazards. Eligible activities include project scoping, partnerships, mitigation planning and planning-related activities, and adoption and implementation of building codes.

Mitigation projects: Projects designed to increase resilience and public safety, reduce injuries and loss of life, and reduce damage to property, critical services, facilities, and infrastructure from flooding. Examples include property acquisition and structure relocation, structure elevation, mitigation reconstruction, dry floodproofing of historic residential structures, dry floodproofing of non-residential structures, generators, and structural and nonstructural retrofitting of existing buildings.

HUD Grant Programs

Community Development Block Grant - Disaster Recovery (CDBG-DR)

CDBG-DR funding is particularly useful for small municipalities because of its broad list of eligible projects. Small municipalities needing funds to recover from a debilitating disaster may benefit from HUD Disaster Recovery grants. A subset of the CDBG Program, these grants provide crucial seed money and address the long-term recovery and restoration of infrastructure, housing, and economic activity, including mitigation and mitigation planning activities intended to reduce or eliminate damage from future disasters.

Requires Presidential Disaster Declaration.

Funding amount: Varies. In response to a natural disaster, Congress appropriates funds to HUD, which then allocates funds to eligible states and municipalities based on unmet recovery needs.

Cost share: This program has no cost share requirements.

Eligible activities: There are 27 eligible activities. Flood-related activities include open space acquisition; construction, repair, replacement, or relocation of public facilities; and improvements, such as dams or levees.

American Flood Coalition Funding Tool

The American Flood Coalition is a nonpartisan group organization consisting of cities, elected officials, military leaders, businesses, and civic groups that have come together to drive adaptation to the reality of higher seas, stronger storms, and more frequent flooding through national solutions

that support flood-affected communities and protect our nation's residents, economy, and military installations.

The American Flood Coalition created the Flood Funding Finder—a first-of-its-kind, interactive website—to simplify the complex federal grants system and to help small communities identify and prioritize opportunities to fund flood resilience.

Hundreds of programs across 26 federal agencies were reviewed and the American Flood Coalition identified a set of federal funding opportunities that will provide assistance to projects in small communities that address flooding. This interactive tool is primarily targeted toward communities with populations of 50,000 or fewer, but communities of all sizes may find its information helpful.

The Flood Funding Finder also includes a set of filters to highlight specific program characteristics that are of interest to smaller communities:

- Gives special consideration for small communities
- Does not require a cost share or matching funds from smaller communities
- Allows in-kind services to contribute toward nonfederal cost share requirements
- Focuses on environmental restoration
- Requires a Presidential Disaster Declaration

The tool can be used by connecting to the following location: https://floodcoalition.org/resources/floodfundingfinder/

Nonstructural Funding Opportunities

Funding opportunites for nonstructural mitigation options include:

- FEMA Grant programs
 - Hazard Mitigation Grant Program HGMP
 - Flood Mitigation Assistance FMA
 - Building Resilient Infrastructure and Communities BRIC
- US Department of Housing and Urban Development HUD CDBG-DR
- American Flood Coalition Resources for flood mitigation funding information

Funding for structural mitigation options include:

- Building Resilient Infrastructure and Communities BRIC
- Flood Mitigation Assistance FMA
- Federal Infrastructure Bill large amount of money avialable for flood mitigation and coastal restoration projects from storms
- State funding opportunities

COLUMBIA COUNTY

West End Flood Mitigation Study APPENDICES

June 2022



VOLUME II

Prepared for: Columbia County

11 West Main Street County Annex

Bloomsburg, PA 17815

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BL Project #: 2021-5134-001









VOLUME II

APPENDICES

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- B. GEOTECHNICAL ENGINEERING
- C. ENVIRONMENTAL AND REGULATORY COMPLIANCE
- D. PUBLIC AND STAKEHOLDER OUTREACH
- E. MITIGATION ALTERNATIVES CONCEPT DRAWINGS
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WEST END FLOOD MITIGATION STUDY

Appendix A Hydrologic and Hydraulic Analysis

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A. Reference Materials

West End Mitigation Study Reference Materials

Fishing Creek in the vicinity of Town of Bloomsburg has been the topic of several flood studies over the last 20 years. Many of these studies and the reference data used to complete these analyses were reviewed as part of the hydraulic analysis for the flood protection proposed for this project and were incorporated into this study to improve the accuracy of the analysis. This study used data collected from the following sources to complete the analysis:

- 1. Reference: Columbia County Flood Insurance Study (Community Number 42037CV001A)

 Description: A report that documents how the regulatory floodplain was established using the regulatory floodplain model, how flows were developed for use in the model and how the flow changes in the river or stream based on location along the stream.
- 2. Reference: Columbia County Digital Flood Insurance Rate Maps (Map Numbers 42037C0240E, 42037C0243E, 42037C0330E, 42037C0335E,)
 - Description: Maps showing the location, extent and in some cases the elevations of regulatory flooding (flooding that has a 1% probability of occurring in any given year) that occurs in a certain geographic area. In addition to regulatory flood elevations the map may also identify the floodway (that portion of the floodplain that must not be filled so as to not create a significant increase in the regulatory flood elevation). When provided in a digital format, the location of the floodplain and floodway is very accurate and the map is referred to as a D-FIRM.
- 3. Reference: Preliminary Columbia County Flood Insurance Study (Community Number 42037CV001B Version Number 2.3.3.3.)
 - Description: A preliminary report that documents how the preliminary regulatory floodplain was proposed using the preliminary regulatory floodplain model, how preliminary flows were developed for use in the model and how the flow changes in the river or stream based on location along the stream.
- 4. Reference: Preliminary Columbia County Flood Insurance Rate Maps (Map Numbers 42037C0238F, 42037C0239F, 42037C0326F, 42037C0327F, Version Number 2.3.3.3)
 - Description: Preliminary maps showing the location, extent and in some cases the elevations of the preliminary regulatory flooding (flooding that has a 1% probability of occurring in any given year) that occurs in a certain geographic area. In addition to the preliminary regulatory flood elevations the map may also identify the floodway (that portion of the floodplain that must not be filled so as to not create a significant increase in the regulatory flood elevation).
- 5. Reference: History Flood Insurance Study for Town of Bloomsburg, Columbia County, PA (Community Number 420339)
- 6. Reference: Susquehanna River Regulatory Floodplain Model

Description: A hydraulic model of the Susquehanna River developed using the river geometry (e.g. width, depth, shape and slope of the channel and floodplain) and bridge geometries to determine flood elevations for various flows in the river that are statistically projected to occur at a defined frequency.

7. Reference: Fishing Creek Regulatory Floodplain Model

Description: A hydraulic model of the Fishing Creek developed using the stream geometry (e.g. width, depth, shape and slope of the channel and floodplain) and bridge geometries to determine flood elevations for various flows in the river that are statistically projected to occur at a defined frequency.

8. Reference: Bloomsburg, PA Flood Risk Management Study (FRMS) Update of Hydrology and Hydraulic for Inclusion of Tropical Storm Lee Event, June 2012

Description: This report documents the process of the update, the results and how Tropical Storm Lee affected the H&H for the Bloomsburg FRMS.

9. Reference: National Weather Service Advanced Hydrologic Prediction Service

Description: Plots and data identifying flood stages on the Susquehanna River at Danville, Bloomsburg and Wilkes-Barre, Pennsylvania. The data provides a graphic representation of river flows plotted by time and is used to predict high water elevations on the river in order to initiate appropriate actions to protect the public, such as warning and evacuation notices.

10. Reference: The Towns of Bloomsburg, Columbia County, Pennsylvania, Flood Damage Reduction Project Report, August 2005;

Description: A report evaluating the feasibility of and environmental consequences of constructing a flood protection system in Bloomsburg, Pennsylvania. Several alternatives were investigated and evaluated to provide protection Hurricane Agnes level protection on the Susquehanna River and 100-year protection on the Fishing Creek.

11. Reference: Susquehanna River Flood Warning and Response System (PR 56), July 2003;

Description: A report describing the development of the Flood Warning Response System (FWRS) for 110 miles of the main stem of the Susquehanna River. The purpose of the FWRS is to provide an early warning system that maximizes response time to residents and emergency responders to flood conditions on the river.

12. Reference: Flood Recovery Report-Tropical Storm Lee-Wyoming Valley, June 2013

Description: A report documenting hydrologic and hydraulic changes to the models used to develop the 2003 FWRS. The FWRS was revised based on geometric changes that occurred along the river basin since the development of the FWRS, errors identified in the hydraulic model since the development of the FWRS and potential impacts to base flood elevations resulting from application of the hydrologic data collected for Tropical Storm Lee.

- 13. Reference: Fishing Creek near Bloomsburg, PA (Gage Number 01539000)
- 14. Reference: Fishing Creek-Orangeville, PA (Gage Number 01539008)

Description: Devices placed into streams which are used to measure the height (stages) of floodwaters in rivers and streams, and are able to correlate the height of the water to a flow in a stream or river. Several of these gages stopped functioning during Tropical Storm Lee or could not be used to accurately determine the flow since the elevations occurred at a height that was not encountered previously and as such were too high to accurately equate to a flow. For this analysis the stage (height of water at the gage) was given precedence or considered accurate. Streamflow was considered provisional or potentially not accurate. In addition to the elevation of the floodwaters, these gages were used to establish the timing of peak flows in the Susquehanna River and Fishing Creek.

B. Figures

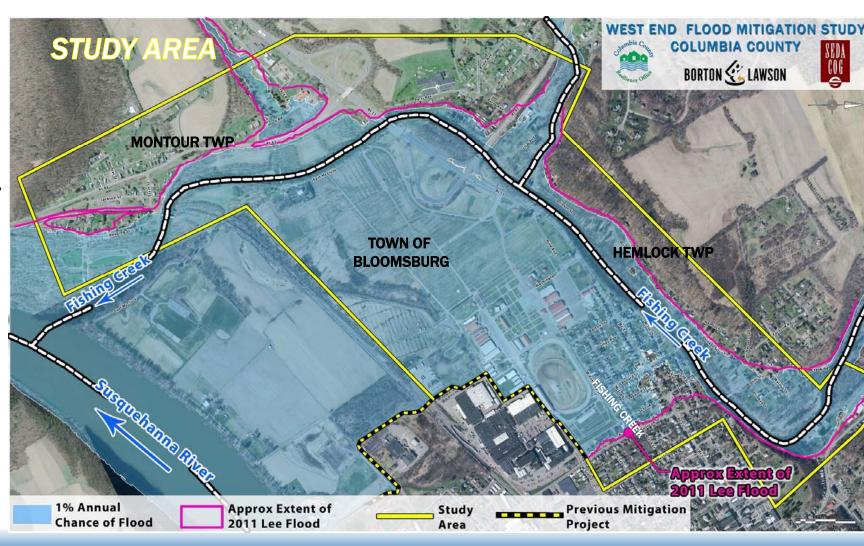
B.1 Location Map

West End Flood Study Area

Floodplains of Fishing Creek in Town of Bloomsburg, Hemlock Twp & Montour Twp

~500 parcels

~350 structures





B.2 Effective Flood Insurance Rate Map (FIRM)

To obtain more detailed information in areas where **Base Flood Elevation** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for filood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevation (BFEs) shown on this map apply only land-ward of 0.0" North American Vertical Datum (NAVD). Users of this FIRM should be aware that coastal flood elevations may also be provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this community. Elevations shown in the Summary of Stillwater Elevations table should be used for construction, and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood** control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures in this jurisdiction.

The **projection** used in the preparation of this map is Universal Tranverse Mercator (UTM) zone 18. The **horizontal datum** is NAD83, GRS1980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of the FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at www.ngs.noaa.gov or contact the National Geodetic Survey website at www.ngs.noaa.gov or contact the National Geodetic Survey at the following address:

Spatial Reference System Division National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3242

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Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

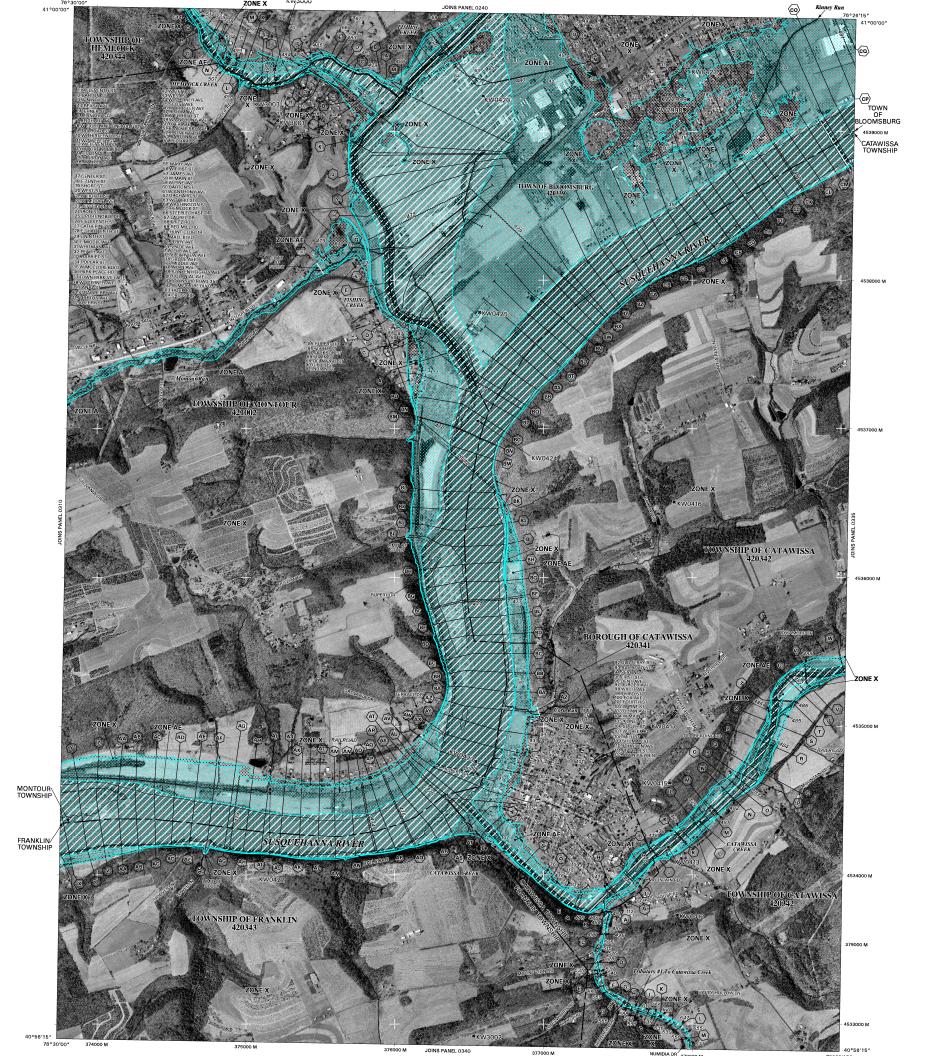
Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each

An accompanying Flood Insurance Study report, Letters of Map Revision or Letters of Map Amendment revising portions of this panel, and digital versions of this PANEL may be available. Contact the FEMA Map Service Center at the following phone numbers and Internet address for infomation on all related products available from FEMA;

Phone: 800-358-9616 FAX: 800-358-9620

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-ERMA-MAP (1-877-336-2627) or visit the FEMA website at http://wwww.fema.gov/business/nfip/

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report may reflect stream channel distances that differ from what is shown on this map.



that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual ohance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Sase Flood Elevation is the water surface elevation of the 1% annual chance flood.

ZONE A No base flood elevations determined.

Flood depths of 1 to 3 feet (usually areas of ponding); base flood elevations determined.

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

Area to be protected from 1% annual chance flood event by a Federal flood protection system under construction; no base flood elevations

Coastal flood zone with velocity hazard (wave action); no base flood elevations determined.

FLOODWAY AREAS IN ZONE AE

is the channel of a stream plus any adjacent floodplain areas that must be ancroachment so that the 1% annual chance flood can be carried without reases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance floodplain ZONE D Areas in which flood hazards are undetermined, but possible.

.....

4276000N

M1.5

ZONE X

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas

1% annual chance floodplain boundary

Floodway boundary Zone D boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or velocities. -----513------Base Flood Elevation line and value: elevation in feet*

Base Flood Elevation value where uniform within zone elevation in feet* (EL 987)

 $\langle A \rangle$ $-\langle A \rangle$ Cross Section Line 23-----23

Transect Line

97°07'30", 32°22'30"

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid values, zone 18 600000 FT 5000-foot grid ticks

DX5510 X Bench mark (see explanation in Notes to Users section of this FIRM panel).

River Mile

Refer to Repository Listing on Index Map

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

AUGUST 19, 2008

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

To determine if flood insurance is available in this community, contact agent or call the National Flood insurance Program at (800) 638-6620.



MAP SCALE 1" = 1000'

500 0 1000 2000 FEET

rrr

FIRM

PANEL 0330E

FLOOD INSURANCE RATE MAP COLUMBIA COUNTY,

PENNSYLVANIA (ALL JURISDICTIONS)

PANEL 330 OF 470

420344 420338 420342 421002 420341 420343



EFFECTIVE DATE:

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Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood** control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures in this jurisdiction.

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Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each

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Phone: 800-358-9616 FAX: 800-358-9620 http://msc.fema.gov/

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that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual ohance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Sase Flood Elevation is the water surface elevation of the 1% annual chance flood. No base flood elevations determined. Flood depths of 1 to 3 feet (usually areas of ponding); base flood elevations determined. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

Area to be protected from 1% annual chance flood event by a Federal flood protection system under construction; no base flood elevations

Coastal flood zone with velocity hazard (wave action); no base flood Coastal flood zone with velocity hazard (wave action); base flood elevation

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

FLOODWAY AREAS IN ZONE AE

OTHER FLOOD AREAS

OTHER AREAS

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights

Areas determined to be outside the 0.2% annual chance floodplain

Areas in which flood hazards are undetermined, but possible. COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

Floodway boundary Zone D boundary

Cross Section Line

5000-foot grid ticks

Refer to Repository Listing on Index Map

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

AUGUST 19, 2008 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

FIRM

River Mile

To determine if flood insurance is available in this community, contact agent or call the National Flood Insurance Program at (800) 638-6620. MAP SCALE 1" = 1000' 500 0 1000 2000 FEET

rrr

سيس

Transect Line

CBRS and OPA boundary

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas

1% annual chance floodplain boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or velocities.

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)

1000-meter Universal Transverse Mercator grid values, zone 18

Bench mark (see explanation in Notes to Users section of this FIRM panel).

PANEL 0240E

FLOOD INSURANCE RATE MAP

COLUMBIA COUNTY,

(ALL JURISDICTIONS)

421042 420344 421004 420339 0240 0240 0240 0240

MAP NUMBER 42037C0240E

EFFECTIVE DATE:

PENNSYLVANIA

PANEL 240 OF 470

COMMUNITY

Base Flood Elevation line and value: elevation in feet* Base Flood Elevation value where uniform within zone; elevation in feet*

ZONE A

ZONE AH

ZONE X

ZONE X

ZONE D

.....

-----513------

—⟨A⟩

(EL 987)

23-----23

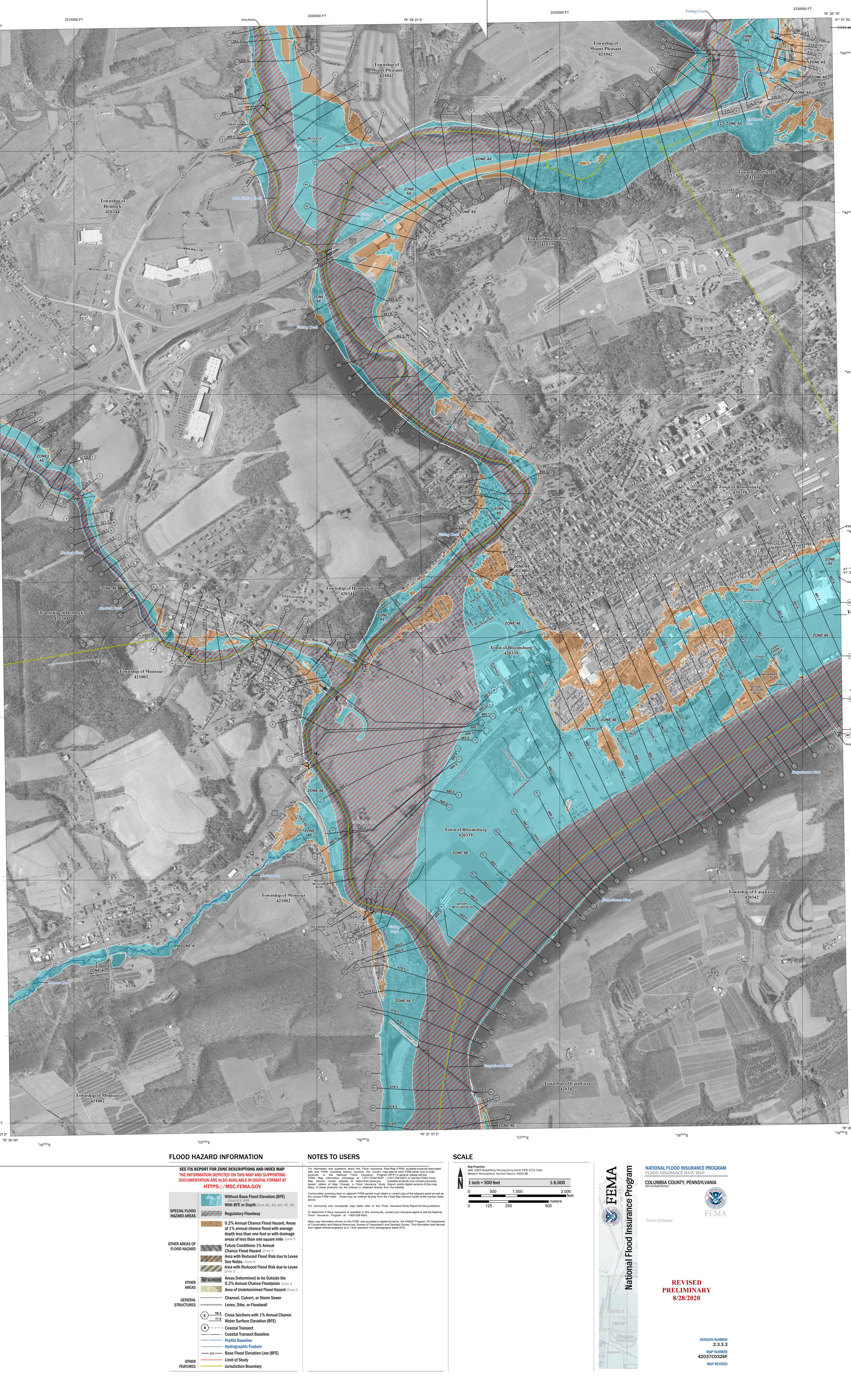
97°07'30", 32°22'30"

4276000N 600000 FT

DX5510 X M1.5

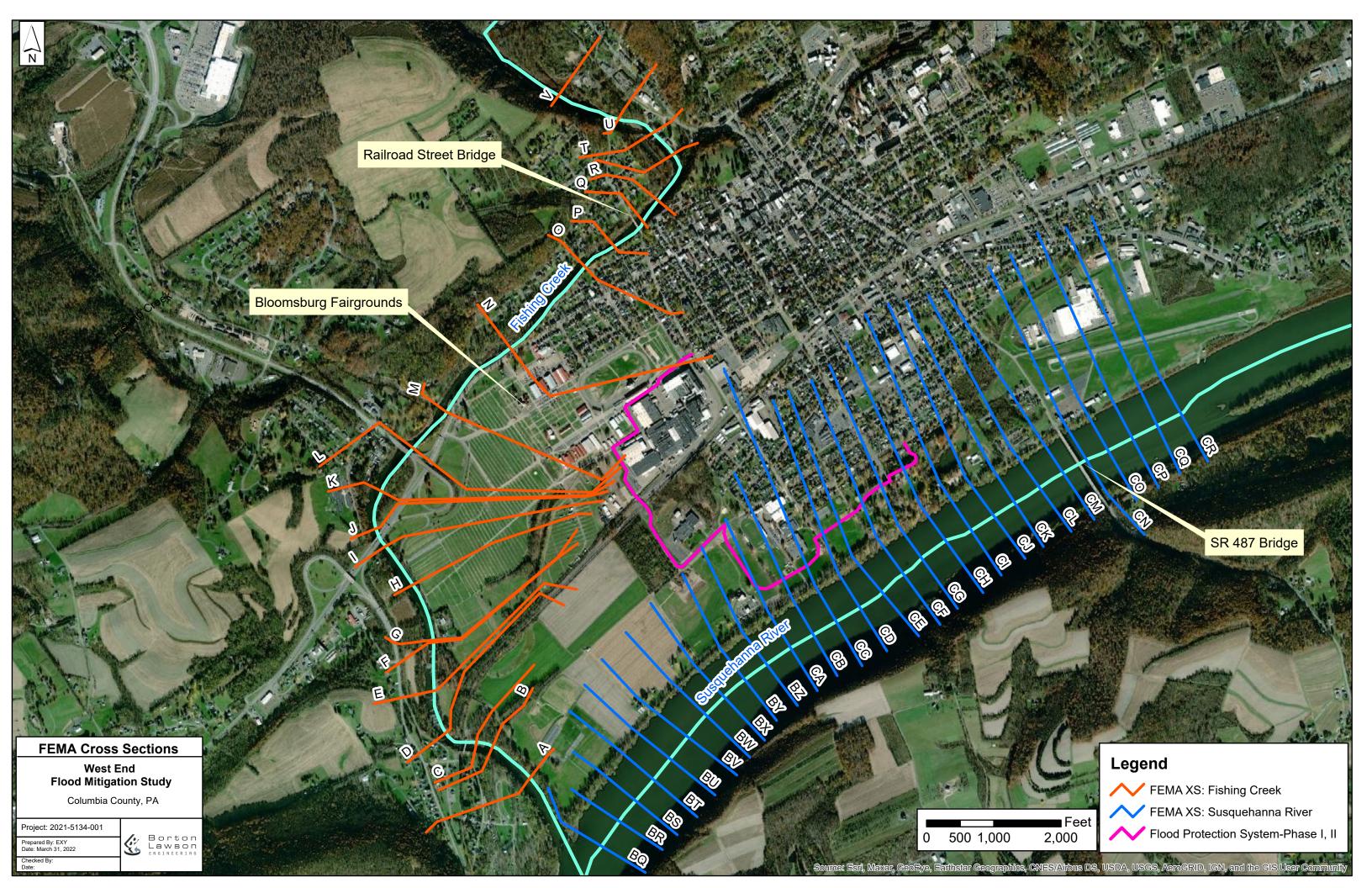
 $\langle A \rangle$

B.3 Preliminary Flood Insurance Rate Map (FIRM)

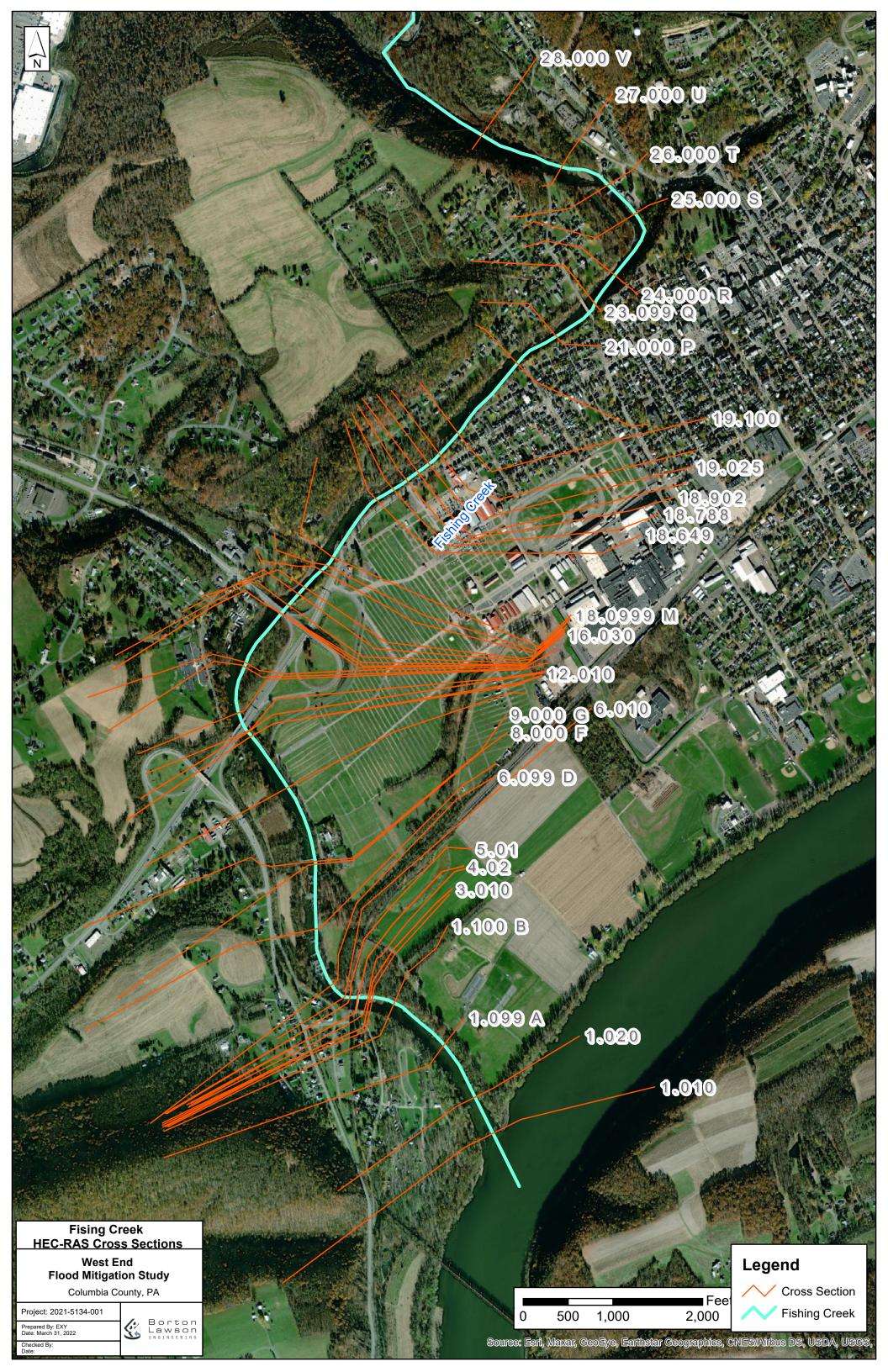


B.4 Susquehanna River and Fishing Creek Cross Section

B.4.a Susquehanna River and Fishing Creek FEMA Cross Section Map



B.4.b Fishing Creek HEC-RAS Cross Section Map



B.5 Levee Alignment Figure (Alternative A-2)

Full Floodwall/ Levee System Bloomsburg 6,200 LF

Total Estimated
Cost
\$29 million



C. Supporting Hydrologic Analysis

C.1 Summary of Hydrologic Analysis

Columbia County West End Flood Study Recommendations for Analysis of Fishing Creek Flows

1. FEMA FIS Report

The preliminary Flood Insurance Study (FIS) for Columbia County, Pennsylvania was issued by FEMA in August 2020. FEMA conducted detailed hydrologic analyses for select areas along Fishing Creek in Columbia County; the results of these analyses are presented in the FIS. Annual peak flow data from the nearest stream gage on Fishing Creek (gage 01539000) located 5.5 miles upstream of the Town of Bloomsburg provided the basis for determining flood flow frequencies at these select areas. This stream gage has a drainage area of 274 square miles and has been active since 1939. The Hydrologic analysis of Fishing Creek determined flood flow frequency data by applying the standard Log-Pearson Type III statistical analysis (WRC) method to available gage data (37 years of record) or by utilizing regional regression equations for ungagged sites. The peak discharges at the confluence of Fishing Creek and the Susquehanna River for the 10-, 50-, 100- and 500-year events are included in Table 2.

The locations and peak discharges reported for Fishing Creek in the original FIS (1979) remain equivalent to the peak discharges reported in the Effective FIS (2008) and the Preliminary FIS (2020). FEMA has not performed a hydrologic study of Fishing Creek since the original FIS was published in 1979. The related pages from the 1979 FIS, 2008 Effective FIS, and 2020 Preliminary FIS are provided in Appendix A1, A2 and A3, respectively.

2. 2005 US Army Corps of Engineers (USACE) Flood Damage Reduction Feasibility Study

In 2005, the USACE conducted a Flood Damage Reduction Feasibility Study to evaluate a series of flood mitigation alternatives and determine environmental impacts. An H&H analysis performed as part of this study also relied on statistical analysis of the same Fishing Creek stream gage with the additional years of record included since the 1979 FEMA analysis was performed. USACE performed the statistical analysis of the peak flow data using their Hydrologic Engineering Center — Flood Frequency Analysis (HEC-FFA) program. The computed flows for the 2-, 5-, 10-, 25-, 50-, 100-, and 500-year events are included in Table 2. The period of record available at the time of this study (61 years of record) did not include the events of 2006 or the 2011 flood of record. Details of the analysis from the 2005 study are provided in Appendix A4.

3. 2012 US Army Corps of Engineers (USACE) Flood Risk Management Study

In 2012, the USACE prepared a Flood Risk Management Study (FRMS) for the purpose of updating the hydrology and hydraulics of Fishing Creek and the Susquehanna River to include the 2011 Tropical Storm Lee event. In this report, the peak discharge frequency analysis for Fishing Creek is presented. This analysis utilized the active USGS stream gage (# 01539000) of Fishing Creek (75 years of record). Additionally, the 2012 USACE study incorporated data from a non-active historical gage (# 01540000) formerly located at the Railroad Street Bridge in Bloomsburg. This historical stream gage monitored a drainage area of 355 square miles and was active from 1914 to 1931 (18-years). Both sets of gage data were used to analyze the peak discharge frequency on Fishing Creek at the project area. The gage data was analyzed using the

Hydraulic Engineering Center – Statistical Software Package (HEC-SSP) with regional skew; the results were then transposed to the project location using a direct drainage area relationship. The development of the peak discharges are presented in Table 2. Details of the analysis can be found in the extracted UASCE report in Appendix 5.

4. Project Evaluation

The active stream gage (# 01539000) on Fishing Creek upstream of the project area recorded an additional 8 years of data since the most recent USACE analysis was performed in 2012. Due to the gage having a longer period of record and USGS SIR 2019-5094 providing updated guidance for analysis of gaged streams, a revised analysis was performed to determine stream flows and recurrence intervals within the project area. USGS PeakFQ was used to evaluate the peak discharges using the data from 1936 to 2020 with weighted skew as recommended in USGS SIR 2019-5094. The results were then transposed to both Railroad Street and the confluence with the Susquehanna River using the procedure outlined in USGS SIR 2019-5094. The results are presented in Table 2 and the detailed PeakFQ output is provided in Appendix 6

The differences between the USACE analysis performed in 2012 and the current PeakFQ analysis are noted below:

Source	Software	Data	Equation	Skew Factors	
USACE Flood Risk Management Study (June 2012)	HEC-SSP	Gage # 01540000 Peak Annual Flows (1914-1931) & Gage # 01539000 Peak Annual Flows (1936-2012)	$\frac{Q_{US}}{Q_{DS}} = \frac{DA_{US}}{DA_{DS}}$	Regional Skew	
Current Project Evaluation (July 2021)	Evaluation Peak FO		$\frac{Q_{DS}}{Q_{US}} = \left(\frac{DA_{DS}}{DA_{US}}\right)^{B}$	Weighted Skew	

Table 1 – Method Comparison

5. **Conclusion**

A comparison of the peak discharges from the FEMA FIS, the 2005 USACE Flood Damage Reduction Feasibility Study, the 2012 USACE Flood Risk Management Study, and the current project analysis utilizing the USGS PeakFQ software are presented in Table 2. The results of the comparison reveal strong consistencies for all events analyzed. The absence of historic flood events of 2011 and 2006 from the 2005 USACE FRMS period of record accounts for the difference in results between the 2005 study and the 2012 study.

B - Basin Characteristics Coefficient from USGS SIR 2019-5094 Table 3

Results of the current project evaluation using PeakFQ reveal that the flows calculated at Railroad Street vs. flows calculated at the confluence with the Susquehanna River differ by approximately 6%, which would not significantly alter the hydraulics within the project area. Therefore, flows determined at the confluence with the River should be applied through the subject reach in the West End of the Town of Bloomsburg.

Whereas the flows calculated at the confluence of the Susquehanna River utilizing PeakFQ are nearly identical to the flows presented in the 2012 USACE FRMS at the same location, the recommendation is to utilize these flows developed by the 2012 USACE FRMS as the project flows in the hydraulic analysis of Fishing Creek for analyses occurring between the confluence of Little Fishing Creek and the Susquehanna River. The following points are made as further justification for selection of the 2012 USACE flows:

- USACE 2012 study includes a greater period of record (98 years) and data from two gaging stations including a historic gaging station within the study area at Railroad Street.
- USACE 2012 flows are marginally larger than all other flows and thus are more conservative.
- USACE 2012 flows are published and available for use by others.
- USACE 2012 flows were produced by a Federal Agency giving them more credence when seeking eventual LOMR approval from FEMA.

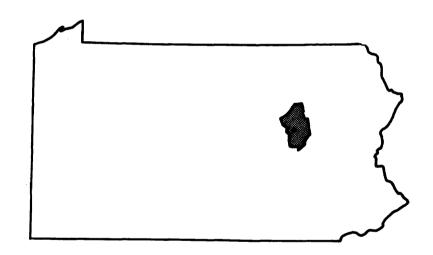
Table 2 – Summary of Flow Calculations

Source	Software	Location /	Peak Discharge (cfs)						
		Drainage Area (SM)	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	500-yr
FEMA FIS* (1979, 2008, 2020)	Unknown	Confluence Susquehanna River / 385	-	-	24,300	-	45,700	58,500	102,000
USACE Flood Damage Reduction Feasibility Study (2005)	HEC-FFA	Confluence Susquehanna River / 385	10,700	17,600	23,300	31,800	39,100	47,400	71,600
USACE Flood Risk Management Study (June 2012)	HEC-SSP	Confluence Susquehanna River / 385	12,400	21,000	28,100	38,800	48,200	58,900	89,600
Current Project Evaluation (July 2021)	USGS Peak FQ	Confluence Susquehanna River / 385	11,300	19,300	26,300	37,200	47,000	58,600	93,500
	USGS Peak FQ	At Railroad St. Br. / 355	10,500	18,100	24,600	34,900	44,200	55,100	88,000

APPENDIX A1 Extracted from Historic FIS - 1979



TOWN OF BLOOMSBURG, PENNSYLVANIA COLUMBIA COUNTY



NOVEMBER 1979

FEDERAL EMERGENCY MANAGEMENT AGENCY FEDERAL INSURANCE ADMINISTRATION

COMMUNITY NUMBER -420339

TABLE 1 - SUMMARY OF DISCHARGES

	DRAINAGE AREA		PEAK DISC	HARGES (cf	s)
FLOODING SOURCE AND LOCATION	(sq. miles)	10-YEAR	50-YEAR	100-YEAR	500-YEAR
SUSQUEHANNA RIVER At mouth of Fishing Creek (western boundary of Town of Bloomsburg)	10,576	173,000	243,000	274,000	356 000
or rown or broomsburg)	10,576	173,000	243,000	274,000	356,000
FISHING CREEK					
At mouth At mouth of Little	385	24,300	45,700	58 , 500	102,000
Fishing Creek	292	20,000	38,000	48,800	87,000
KINNEY RUN					
At mouth	2.74	246	285	297	*

*Not computed

Susquehanna River were computed from a downstream study; Fishing Creek and Kinney Run were computed by the critical depth method.

Cross sections were located at regular intervals along the stream length and at significant changes in ground relief, land use and land cover. Ground elevations for the cross sections were photogrammetrically obtained as the 1:2,400 scale base maps were compiled (Reference 11). The channel bottom elevations were taken from field-surveyed cross sections at an interval distance of not more than 1,000 feet. Flood profiles were drawn showing computed watersurface elevations to an accuracy of 0.5 foot for floods of the selected recurrence intervals. Locations of selected cross sections used in the hydraulic analyses are shown on the Flood Profiles (Exhibit 1). For stream segments for which a floodway is computed (Section 4.2), selected cross-section locations are also shown on the Flood Boundary and Floodway Map (Exhibit 2).

Reach lengths for the stream channels were measured along the centerline of the channel and between cross sections as scaled from the 1:2,400 maps (Reference 11). The overbank reach lengths were measured along the approximate centerline of the effective out-of-channel area as scaled from the 1:2,400 maps (Reference 11).

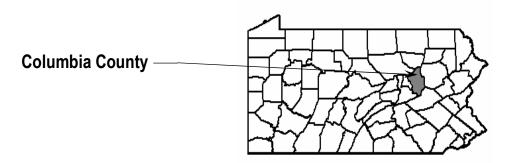
APPENDIX A2

Extracted of Effective FIS - 2008



COLUMBIA COUNTY, PENNSYLVANIA ALL JURISDICTIONS

COMMUNITY NAME	COMMUNITY NUMBER	COMMUNITY NAME	COMMUNITY NUMBER
BEAVER, TOWNSHIP OF	421547	JACKSON, TOWNSHIP OF	421552
BENTON, BOROUGH OF	421543	LOCUST, TOWNSHIP OF	421001
BENTON, TOWNSHIP OF	421037	MADISON, TOWNSHIP OF	421553
BERWICK, BOROUGH OF	420338	MAIN, TOWNSHIP OF	421554
BLOOMSBURG, TOWN OF	420339	MIFFLIN, TOWNSHIP OF	421167
BRIAR CREEK, BOROUGH OF	420340	MILLVILLE, BOROUGH OF	421545
BRIAR CREEK, TOWNSHIP OF	421548	MONTOUR, TOWNSHIP OF	421002
CATAWISSA, BOROUGH OF	420341	MOUNT PLEASANT, TOWNSHIP OF	421042
CATAWISSA, TOWNSHIP OF	420342	NORTH CENTRE, TOWNSHIP OF	421555
CENTRALIA, BOROUGH OF	421544	ORANGE, TOWNSHIP OF	421003
CLEVELAND, TOWNSHIP OF	421000	ORANGEVILLE, BOROUGH OF	420345
CONYNGHAM, TOWNSHIP OF	421549	PINE, TOWNSHIP OF	421556
FISHING CREEK, TOWNSHIP OF	421550	ROARING CREEK, TOWNSHIP OF	421557
FRANKLIN, TOWNSHIP OF	420343	SCOTT, TOWNSHIP OF	421004
GREENWOOD, TOWNSHIP OF	421551	SOUTH CENTRE, TOWNSHIP OF	421137
HEMLOCK, TOWNSHIP OF	420344	STILLWATER, BOROUGH OF	421546
		SUGARLOAF, TOWNSHIP OF	421558



EFFECTIVE DATE: AUGUST 19, 2008



Federal Emergency Management Agency FLOOD INSURANCE STUDY NUMBER 42037CV001A

Table 3 "Summary of Discharges"

		Peak Discharges (cubic feet per second)			
Flooding Source and Location	Drainage Area	10 Percent	2 Percent	1 Percent	0.2 Percent
	(Square Miles)	Annual Chance	Annual Chance	Annual Chance	Annual Chance
Appleman's Run					
at ponding area upstream of New Route 487in Scott Township	1.7	1,078	1,568	1,938	2,641
at the confluence with Fishing Creek	2.4	390	470	510	630
Briar Creek					
at the confluence with East Branch Briar Creek	16.7	2,590	5,267	6,712	11,200
at the confluence with Susquehanna River	33.0	3,252	6,520	8,312	14,000
Catawissa Creek					
at the confluence with Susquehanna River	153.0	8,300	16,000	20,800	37,800
Catawissa Creek, Tributary No. 1					
at Legislative Route 19087 in Catawissa Township	1.2	365	900	1,300	3,000
at the confluence with Catawissa Creek	2.3	520	1,290	1,800	4,000
East Branch Briar Creek					
at upstream corporate limits of Berwick Borough	13.9	*	*	4,330	*
at the end of Eaton Street	14.2	*	*	4,415	*
at the downstream corporate limits of Berwick Borough	15.0	*	*	4,500	*
at the lower corporate limits of East Branch Briar Creek	15.1	*	*	4,500	*
at the confluence with Briar Creek	15.5	1,822	3,730	4,500	8,000
East Branch Fishing Creek					
at Jamison City in Sugarloaf Township	18.0	*	*	5,200	*
Fishing Creek					
at Grassmere Park in Sugarloaf Township	52.3	*	*	11,400	*
at the confluence with West Creek	71.1	7,080	12,900	16,200	24,400
at the upstream limits of Stillwater Borough	92.0	*	*	18,800	*
at the downstream corporate limits of Benton Township	93.2	8,510	15,100	18,600	27,400
above Raven Creek	93.5	*	*	19,000	*
at Zaher Bridge	109.0	*	*	23,900	*
at the downstream corporate limits of Stillwater Borough	109.0	*	*	23,900	*
above Confluence of Huntington Creek	114.0	*	*	24,900	*
at the downstream corporate limits of Fishing Creek Township	225.0	*	*	41,500	*
at western corporate limits of Orangeville Borough	236.4	17,200	32,900	42,400	77,000
at the confluence with Susquehanna River LITTLE FISHING CREEK	292.0	20,000	38,000	48,800	87,000
at the confluence with Hemlock Creek SUSQUEHANNA RIVER	385.0	24,300	45,700	58,500	102,000
Glen Brook					
at the downstream corporate limits of Berwick Borough	4.9	*	*	2,080	*
at the confluence with East Branch Briar Creek	5.0	*	*	2,080	*

APPENDIX A3

Extracted of Preliminary FIS - 2020

FLOOD INSURANCE STUDY

FEDERAL EMERGENCY MANAGEMENT AGENCY

VOLUME 1 OF 3



COLUMBIA COUNTY, PENNSYLVANIA

ALL JURISDICTIONS

COMMUNITY NAME	NUMBER	COMMUNITY NAME	NUMBER
BEAVER, TOWNSHIP OF	421547	LOCUST, TOWNSHIP OF	421001
BENTON, BOROUGH OF	421543	MADISON, TOWNSHIP OF	421553
BENTON, TOWNSHIP OF	421037	MAIN, TOWNSHIP OF	421554
BERWICK, BOROUGH OF	420338	MIFFLIN, TOWNSHIP OF	421167
BLOOMSBURG, TOWN OF	420339	MILLVILLE, BOROUGH OF	421545
BRIAR CREEK, BOROUGH OF	420340	MONTOUR, TOWNSHIP OF	421002
BRIAR CREEK, TOWNSHIP OF	421548	MOUNT PLEASANT, TOWNSHIP OF	421042
CATAWISSA, BOROUGH OF	420341	NORTH CENTRE, TOWNSHIP OF	421555
CATAWISSA, TOWNSHIP OF	420342	ORANGE, TOWNSHIP OF	421003
CENTRALIA, BOROUGH OF*	421544	ORANGEVILLE, BOROUGH OF	420345
CLEVELAND, TOWNSHIP OF	421000	PINE, TOWNSHIP OF	421556
CONYNGHAM, TOWNSHIP OF	421549	ROARING CREEK, TOWNSHIP OF	421557
FISHING CREEK, TOWNSHIP OF	421550	SCOTT, TOWNSHIP OF	421004
FRANKLIN, TOWNSHIP OF	420343	SOUTH CENTRE, TOWNSHIP OF	421137
GREENWOOD, TOWNSHIP OF	421551	STILLWATER, BOROUGH OF	421546
HEMLOCK, TOWNSHIP OF	420344	SUGARLOAF, TOWNSHIP OF	421558
JACKSON, TOWNSHIP OF	421552		

^{*}No Special Flood Hazards Identified

Revised Preliminary August 28, 2020

REVISED: TBD

FLOOD INSURANCE STUDY NUMBER 42037CV001B

Version Number 2.3.3.3



Table 9: Summary of Discharges (continued)

			Peak Discharge (cfs)				
Flooding Source	Location	Drainage Area (Square Miles)	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance
Fishing Creek	Above confluence of Huntington Creek	114.0	*	*	*	24,900	*
Fishing Creek	At the downstream corporate limits of Fishing Creek Township	225.0	*	*	*	41,500	*
Fishing Creek	At western corporate limits of Orangeville Borough	236.4	17,200	*	*	42,400	77,000
Fishing Creek	At the confluence with Little Fishing Creek	292.0	20,000	*	38,000	48,800	87,000
Fishing Creek	At the confluence with Susquehanna River	385.0	24,300	*	45,700	58,500	102,000
Glen Brook	At the downstream corporate limits of Berwick Borough	4.9	*	*	*	2,080	*
Glen Brook	At the confluence with East Branch Briar Creek	5.0	*	*	*	2,080	*
Green Creek	Above confluence of Little Green Creek	10.3	*	*	*	3,000	*
Green Creek	At the confluence with Fishing Creek	36.8	4,950	*	10,400	14,000	27,900

^{*}Not calculated for this Flood Risk Project

APPENDIX A4

Extracted of Corps Flood Damage Reduction Project Draft Integrated Feasibility Report & Environmental Impact Statement - 2005



US ARMY CORPS OF ENGINEERS BALTIMORE DISTRICT

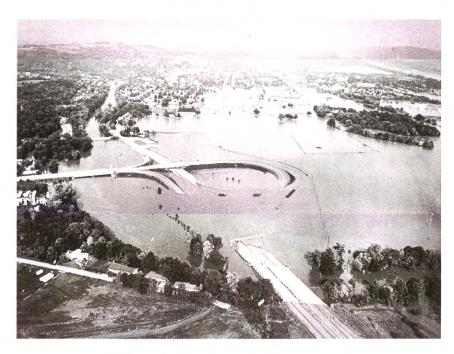


PENNSYLVANIA

THE TOWN OF BLOOMSBURG, COLUMBIA COUNTY, PENNSYLVANIA FLOOD DAMAGE REDUCTION PROJECT

DRAFT INTEGRATED FEASIBILITY REPORT & ENVIRONMENTAL IMPACT STATEMENT

Volume 1



April 2005

The differing recurrence interval assigned to the June 1972 (Agnes) flood event on the Susquehanna River at Bloomsburg (440-year) as compared to Fishing Creek at Bloomsburg (53-year) was a key consideration as the Corps completed this feasibility evaluation. Assignment of the different recurrence intervals is discussed in greater detail in the Hydrology & Hydraulics Attachment to the Engineering Appendix. The difference in recurrence intervals also is incorporated into the formulation of alternative protection levels, and formulation of the recommended plan presented in Sections 4 and 6 of this report.

3.3.2 Existing Conditions Flow Frequency

The Corps Hydrologic Engineering Center – Flood Frequency Analysis (HEC-FFA) program was used to estimate flood frequencies for Fishing Creek at Bloomsburg and for the Susquehanna River above the confluence with Fishing Creek at Bloomsburg. HEC-FFA is a standard Corps computer model that is used to compute flood frequencies in accordance with Corps guidelines. The flood frequencies that were produced are comparable to those shown in other agency studies. The HEC-FFA model results are shown in Tables 3-1 and 3-2. To check validity of the model results, they were compared to estimated flood flows computed by other agencies for three other studies:

- Flood Insurance Study, Town of Bloomsburg, Pennsylvania. FEMA, 1979. Methodology is based on flood flow statistics.
- Comparison of Methods for Computing Streamflow Statistics for Pennsylvania Streams. U.S. Geological Survey (USGS), 1999. Methodology is based on flood flow statistics.
- Techniques for Estimating Magnitude and Frequency of Peak Flows for Pennsylvania Streams. USGS, 2000. Methodology is based regression equations.

Because methods for estimating flood peaks vary based on numerous factors, including methodology and completeness of data, the various studies do not yield the same results. However, in each case, the estimated flows from other agencies were within the 5 percent and 95 percent confidence limits associated with the current HEC-FFA results.

Table 3-1
Comparison of Estimated Peak Discharges (cfs)
for Fishing Creek at Bloomsburg

Recurrence Interval	Current Corps Analysis (385 sq. mi. drainage area)	1999 USGS Report (355 sq. mi. drainage area)	2000 USGS Report (355 sq. mi. drainage area)	1979 FEMA FIS (385 sq. mi. drainage area)
2 years	10,700	-	•	-
5 years	17,600	•	-	-
10 years	23,300	22,400	22,100	24,300
25 years	31,800	28,400	29,600	-
50 years	39,100	33,000	36,000	45,700
100 years	47,400	37,800	43,300	58,500
500 years	71,600	49,300	64,000	102,000

APPENDIX A5

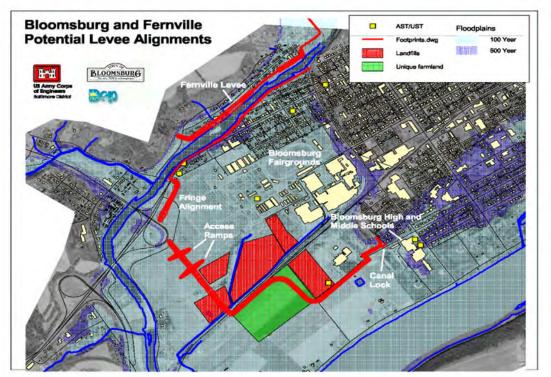
Extracted of Corps
Flood Risk Management Study (FRMS)
Update of Hydrology and Hydraulics for Inclusion of
Tropical Storm Lee Event - 2012

Bloomsburg, PA Flood Risk Management Study (FRMS) Update of Hydrology and Hydraulics for Inclusion of Tropical Storm Lee Event June 2012

Introduction:

The Bloomsburg flood risk management project is in the pre-construction engineering and design (PED) phase of design. The feasibility study evaluated an array of alternative plans based on reducing the flood damages in Bloomsburg along Fishing Creek and the Susquehanna River. To help in intermediate PED design decisions, the hydrology and hydraulics (H&H) portion of a risk and uncertainty (R&U) analysis was performed in October 2010 for the line of protection along Fishing Creek and the Susquehanna River. Since the completion of the risk and uncertainty analysis, Tropical Storm Lee (TSLee) occurred in September 2011, producing record breaking peak flows. The hydrology was updated to include the period of record up to this event to determine its effect on peak flow frequency on the Susquehanna River and Fishing Creek at Bloomsburg. The revised peak discharges were used to update the water surface profiles along the Susquehanna River and Fishing Creek in the project area. This report documents the process of the update, the results and how Tropical Storm Lee affected the H&H for the Bloomsburg FRMS. See Figure 1 for a map presenting the Bloomsburg line of protection (LOP).

FIGURE 1
Bloomsburg Flood Risk Management Project Line of Protection



Hydrology:

The subsequent years of record since the completion of the R&UA were added to the period of record for the applicable gage locations. Gage data were not directly available at Bloomsburg. The nearest gages on the Susquehanna River are at Danville, PA, approximately 10.3 miles downstream of the project area with a drainage area of 11220 square miles (sq mi) and at Wilkes-Barre, PA, approximately 39.5 miles upstream of the project area with a drainage area of 9960 sq mi. The period of record for the Danville gage was increased to 1900-2011 (112 years). The historic period of record for the Wilkes-Barre gage was increased to 1865-2011 (147 years). These gages were used to develop a peak flow frequency curve for the Susquehanna River at the Bloomsburg project area (drainage area = 10560 sq mi). Fishing Creek has a gage located 5.5 miles north of Bloomsburg with a drainage area of 274 sq mi. The period of record for the gage was increased by two years to 1936, 1939-2011 (75 years). A discontinued gage also existed on Fishing Creek from 1914-1931 (18 years). It was located near the Railroad Street Bridge in Bloomsburg with a drainage area of 355 sq mi. Both sets of gage data were used to analyze the peak flow frequency on Fishing Creek at the Bloomsburg project area (drainage area = 385 sq mi).

Fishing Creek Peak Flow Frequency Analysis:

The peak flow values for the entire period of record from both of the U.S. Geological Survey (USGS) gages on Fishing Creek were transposed to the project location downstream (385 sq mi) by using a drainage area relationship as presented in equation (Eq.) 1.

$$Q_{U/S}/Q_{D/S} = (DA_{U/S}/DA_{D/S})$$
 (Eq. 1)

The peak flow data is presented in Table 1.

TABLE 1

Fishing Creek at Bloomsburg, PA
at USGS gages # 01539000 (DA=274 mi²) and # 01540000 (DA=355 mi²)
and at Bloomsburg FRMS Project Site (DA=385 mi²)
Years of Record 1914-1931, 1936, 1939-2011

		ol Record 1914-	1331, 1330, 1		l
	Peak Discharge	Peak Discharge		Peak Discharge	Peak Discharge
Dete	at USGS gage	at Project Site	Data	at USGS gage	at Project Site
Date	$DA = 355 \text{ mi}^2$	$DA = 385 \text{ mi}^2$	Date	$DA = 274 \text{ mi}^2$	$DA = 385 \text{ mi}^2$
0/00/4044	(cfs)	(cfs)	0/40/4004	(cfs)	(cfs)
3/28/1914	10600	11500	3/10/1964	13600	19100
2/25/1915	14000	15200	2/8/1965	2860	4020
7/26/1916	19700	21400	2/14/1966	4760	6690
3/28/1917	6920	7500	3/15/1967	3900	5480
10/30/1917	16700	18100	11/3/1967	3730	5240
7/21/1919	4770	5170	6/16/1969	15300	21500
3/13/1920	11800	12800	4/3/1970	9100	12800
12/14/1920	10000	10800	2/27/1971	3650	5130
6/6/1922	13000	14100	6/22/1972	30900	43400
7/29/1923	13200	14300	12/6/1972	5520	7760
9/30/1924	23000	24900	12/21/1973	5250	7380
2/12/1925	15000	16300	9/26/1975	29400	41300
11/13/1925	6380	6920	10/18/1975	9700	13600
11/16/1926	21500	23300	10/9/1976	19700	27700
7/6/1928	16900	18300	3/27/1978	8120	11400
5/3/1929	17100	18500	3/5/1979	12300	17300
11/18/1929	5630	6110	3/21/1980	5550	7800
3/29/1931	3720	4030	2/2/1981	8430	11800
	Peak Discharge	Peak Discharge	6/6/1982	3980	5590
	at USGS gage	at Project Site	4/16/1983	9920	13900
Date	$DA = 274 \text{ mi}^2$	$DA = 385 \text{ mi}^2$	12/13/1983	13000	18300
	(cfs)	(cfs)	11/29/1984	4040	5680
3/18/1936	17600	24700	3/15/1986	17200	24200
12/10/1938	4420	6210	9/13/1987	5720	8040
3/31/1940	18100	25400	2/2/1988	4030	5660
4/6/1941	3340	4690	5/7/1989	7680	10800
5/23/1942	13400	18800	10/20/1989	5220	7330
12/30/1942	14300	20100	12/4/1990	7960	11200
11/9/1943	12000	16900	3/27/1992	5070	7120
9/19/1945	4790	6730	4/11/1993	14300	20100
5/28/1946	14200	20000	11/28/1993	7660	10800
7/22/1947	4150	5830	11/28/1994	8270	11600
4/15/1948	6120	8600	1/19/1996	21300	29900
12/30/1948	11700	16400	12/2/1996	12700	17800
1/7/1950	5560	7810	1/9/1998	13600	19100
12/4/1950	14000	19700	1/24/1999	13000	18300
3/11/1952	16200	22800	2/28/2000	4860	6830
11/22/1952	8660	12200	12/17/2000	10200	14300
4/17/1954	6140	8630	5/14/2002	13200	18500
8/19/1955	8070	11300	10/12/2002	8600	12100
10/16/1955	7540	10600	9/18/2004	15200	21400
4/6/1957	9610	13500	4/3/2005	16300	22900
12/21/1957	8430	11800	6/28/2006	41200	57900
1/22/1959	8130	11400	11/16/2006	10400	14600
4/4/1960	12200	17100	3/5/2008	14800	20800
2/26/1961	13200	18500	12/12/2008	4330	6080
4/8/1962	5540	7780	1/25/2010	17500	24600
3/27/1963	4050	5690	9/8/2011	56000	78700
0/21/1900	1 000	0000	3/3/2011	30000	10100

A peak flow frequency curve was developed for Fishing Creek at the FRMS project site using the program HEC-SSP (Hydraulic Engineering Center – Statistical Software Package) version 1.1. Since Fishing Creek is unaffected by regulation, the Log-Pearson Type III distribution was used. The regional skew coefficient was determined from a map developed for the North Atlantic Division for a study of the affects of Tropical Storm Agnes in the Susquehanna and Potomac River Basins in June 1972. The study report is titled "Hydrologic Study, Tropical Storm Agnes, North Atlantic Division, December 1975".

The regional skew for Fishing Creek at the Bloomsburg FRMS project site is 0.45, with the mean square error of the map equal to 0.2. These values along with the natural flows were input into HEC-SSP to determine a peak flow frequency curve. The resulting statistics are presented in Table 2. The peak flow frequency curve is presented in Figure 2. Table 3 presents a comparison of the peak flow frequency with and without the additional two years of record which includes Tropical Storm Lee. The addition of these 2 events to the period of record caused a 17.8% increase in the 100 year discharge.

TABLE 2 HEC-SSP Results

Fishing Creek at Bloomsburg, PA FRMS Project Site DA = 385 sq mi						
Computed		Percent	Confidence	o Limito		
Computed	Expected		Confidenc			
Curve	Probability	Chance	0.05	0.95		
Flow, cfs		Exceedance	Flow,	cfs		
89578		0.2	119989	70928		
75305		0.4	98657	60646		
58902		1	74828	48558		
48225		2	59791	40491		
38822		4	46928	33215		
28064		10	32761	24620		
20956		20	23830	18707		
12379		50	13733	11148		
7622		80	8545	6693		
6011		90	6834	5168		
4981		95	5740	4201		
3569		99	4229	2899		
Log Transfo	rm:					
Flow, cfs		Number of Events				
Mean	4.105	Historic events		0		
Standard Dev	0.262	High Outliers		0		
Station Skew	0.239	Low Outliers		0		
Regional Skew	0.450	Zero or Missing		0		
Weighted Skew	0.291	Systemic Events		92		
Adopted Skew	0.291	Historic Period		98		

FIGURE 2

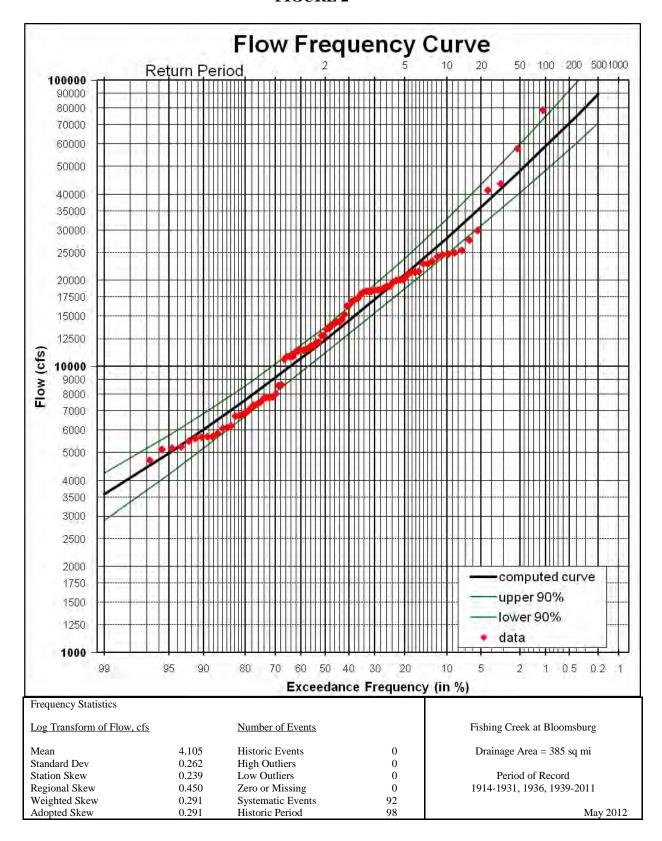


TABLE 3

Fishing Creek at Bloomsburg, PA					
	FRMS Project	t Site DA = 385 sq mi			
Flood	Percent Chance	Q from Oct 2010	Q with		
Event	Exceedance	R&U - No TSLee	TSLee (cfs)		
500 yr	0.2	71300	89600		
250 yr	0.4	61600	75300		
100 yr	1	50000	58900		
50 yr	2	42000	48200		
25 yr	4	34800	38800		
10 yr	10	26100	28100		
5 yr	20	20000	21000		
2 yr	50	12200	12400		

Susquehanna River Peak Flow Frequency Analysis:

The stream gage at Wilkes-Barre, PA is located on the Susquehanna River upstream of Bloomsburg and the gage at Danville, PA is located downstream of Bloomsburg. These gages were used to develop a peak flow frequency curve on the Susquehanna River at the Bloomsburg project area. Additional years of record since the October 2010 R&U analysis were added to the gage data. However, the gage at Wilkes-Barre malfunctioned and a peak for the TSLee event was not recorded. The discharge for TSLee at Wilkes-Barre was estimated by the Corps of Engineers (COE) using the rating curve at the gage derived from the Wyoming Valley LFP HEC-2 model. The USGS published a provisional discharge that is still being evaluated as of the date of this analysis. The peak flow frequency analysis for the Susquehanna River at Wilkes-Barre and Bloomsburg was performed with both the USGS provisional discharge and the COE estimated discharge. Both sets of results will be presented. When the TSLee discharge is finalized, this analysis may need to be recomputed. The gage data for these gages is presented in Tables 4 and 5.

APPENDIX A6

Project Evaluations - 2021

Program PeakFq Version 7.3 10/25/2019 U. S. GEOLOGICAL SURVEY Annual peak flow frequency analysis Seq.002.000
Run Date / Time
07/21/2021 09:09

--- PROCESSING OPTIONS ---

Plot option = Graphics device

Basin char output = None
Print option = Yes
Debug print = No
Input peaks listing = Long

Input peaks format = WATSTORE peak file

Input files used:

peaks (ascii) - C:\Users\exy\PKFQ\USGS 01539000.TXT

specifications - C:\Users\exy\PKFQ\PKFQWPSF.TMP

Output file(s):

main - C:\Users\exy\PKFQ\USGS 01539000.PRT

*** User responsible for assessment and interpretation of the following analysis ***

1

Program PeakFq Version 7.3 10/25/2019 U. S. GEOLOGICAL SURVEY Annual peak flow frequency analysis Seq.001.001 Run Date / Time 07/21/2021 09:09

Station - 01539000 Fishing Creek near Bloomsburg, PA

TABLE 1 - INPUT DATA SUMMARY

Number of peaks in record 83 Peaks not used in analysis = 0 Gaged peaks in analysis 82 = Historic peaks in analysis 1 Beginning Year 1936 Ending Year 2020 Historical Period Length 85 = Skew option WEIGHTED = Regional skew = 0.350 Standard error 0.425 = Mean Square error 0.181

Gage base discharge = 0.0
User supplied high outlier threshold = -User supplied PILF (LO) criterion = -Plotting position parameter = 0.00
Type of analysis EMA
PILF (LO) Test Method MGBT
Perceptible Ranges:

Start Year End Year Lower Bound Upper Bound
1936 2020 0.0 INF DEFAULT

1936 1938 17600.0 INF HISTORIC 1

TABLE 2 - DIAGNOSTIC MESSAGE AND PILF RESULTS

WCF002J-CALCS COMPLETED. RETURN CODE = 2 EMA002W-CONFIDENCE INTERVALS ARE NOT EXACT IF HISTORIC PERIOD > 0

MULTIPLE GRUBBS-BECK TEST RESULTS
MULTIPLE GRUBBS-BECK PILF THRESHOLD N/A
NUMBER OF PILFS IDENTIFIED 0

Kendall's Tau Parameters

		TAU	P-VALUE	MEDIAN SLOPE	
GAGED	PEAKS	0.064	0.398	15.800	82

1

Program PeakFq U. S. GEOLOGICAL SURVEY Seq.001.002
Version 7.3 Annual peak flow frequency analysis Run Date / Time 07/21/2021 09:09

Station - 01539000 Fishing Creek near Bloomsburg, PA

TABLE 3 - ANNUAL FREQUENCY CURVE PARAMETERS -- LOG-PEARSON TYPE III

LOGARITHMIC

	MEAN	STANDARD DEVIATION	SKEW	
EMA WITHOUT REG SKEW EMA WITH REG SKEW	3.9478 3.9478	0.2691 0.2691	0.454 0.419	
EMA ESTIMATE OF MSE OF EMA ESTIMATE OF MSE OF			(AT-SITE)	0.0898 0.0902

TABLE 4 - ANNUAL FREQUENCY CURVE -- DISCHARGES AT SELECTED EXCEEDANCE PROBABILITIES

ANNUAL EXCEEDANCE	<- EMA ES WITH	TIMATE -> WITHOUT	<- FOR EMA ES LOG VARIANCE	TIMATE WITH F	
PROBABILITY	REG SKEW	REG SKEW	OF EST.	5.0% LOWER	95.0% UPPER
0.9950	2292.	2339.	0.0046	1697.0	2870.0
0.9900	2544.	2585.	0.0034	1962.0	3086.0
0.9500	3463.	3487.	0.0015	2912.0	3958.0
0.9000	4142.	4155.	0.0011	3594.0	4670.0
0.8000	5219.	5217.	0.0009	4625.0	5853.0
0.6667	6570.	6553.	0.0009	5851.0	7375.0
0.5000	8492.	8462.	0.0010	7546.0	9590.0
0.4292	9489.	9455.	0.0010	8416.0	10760.0
0.2000	14690.	14670.	0.0014	12830.0	17240.0
0.1000	20070.	20090.	0.0022	17110.0	24770.0
0.0400	28530.	28710.	0.0039	23350.0	38580.0
0.0200	36210.	36600.	0.0058	28590.0	53050.0
0.0100	45210.	45890.	0.0082	34320.0	72200.0
0.0050	55730.	56840.	0.0112	40600.0	97470.0
0.0020	72400.	74310.	0.0160	49820.0	143500.0

^{*}Note: If Station Skew option is selected then EMA ESTIMATE WITH REG SKEW will display values for and be equal to EMA ESTIMATE WITHOUT REG SKEW.

1

Program PeakFq	U. S. GEOLOGICAL SURVEY	Seq.001.003
Version 7.3	Annual peak flow frequency analysis	Run Date / Time
10/25/2019		07/21/2021 09:09

Station - 01539000 Fishing Creek near Bloomsburg, PA

TABLE 5 - INPUT DATA LISTING

WATER PEAK PEAKFQ FLOW INTERVALS (WHERE LOWER BOUND NOT = UPPER BOUND)

YEAR	VALUE	CODES	LOWER	BOUND	UPPER	BOUND	REMARKS
-1936	17600.0	Н					
1939	4420.0						
1940	18100.0						
1941	3340.0						
1942	13400.0						
1943	14300.0						
1944	12000.0						
1945	4790.0						
1946	14200.0						
1947	4150.0						
1948	6120.0						
1949	11700.0						
1950	5560.0						
1951	14000.0						
1952	16200.0						
1953	8660.0						
1954	6140.0						
1955	8070.0						
1956	7540.0						
1957	9610.0						
1958	8430.0						
1959	8130.0						
1960	12200.0						
1961	13200.0						
1962	5540.0						
1963	4050.0						
1964	13600.0						
1965	2860.0						
1966	4760.0						
1967	3900.0						
1968	3730.0						
1969	15300.0						
1970	9100.0						
1971	3650.0						
1972	30900.0						
1973	5520.0						
1974	5250.0						
1975	29400.0						
1976	9700.0						
1977	19700.0						
1978	8120.0						
1979	12300.0						
1980	5550.0						
1981	8430.0						
1982	3980.0						
1983	9920.0						
1984	13000.0						
1985	4040.0						
1986	17200.0						

1987	5720.0
1988	4030.0
1989	7680.0
1990	5220.0
1991	7960.0
1992	5070.0
1993	14300.0
1994	7660.0
1995	8270.0
1996	21300.0
1997	12700.0
1998	13600.0
1999	13000.0
2000	4860.0
2001	10200.0
2002	13200.0
2003	8600.0
2004	15200.0
2005	16300.0
2006	41200.0
2007	10400.0
2008	14800.0
2009	4330.0
2010	17500.0
2011	56000.0
2012	6590.0
2013	4630.0
2014	4340.0
2015	5860.0
2016	3580.0
2017	9000.0
2018	29900.0
2019	7150.0
2020	8190.0

Explanation of peak discharge qualification codes

NWIS	
CODE	DEFINITION
3	Dam failure, non-recurrent flow anomaly
8	Discharge greater than stated value
3+8	Both of the above
4	Discharge less than stated value
6 OR C	Known effect of regulation or urbanization
0	Opportunistic peak
7	Historic peak
	CODE 3 8 3+8 4 6 OR C

- Minus-flagged discharge -- Not used in computation

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Program PeakFq U. S. GEOLOGICAL SURVEY Seq.001.004
Version 7.3 Annual peak flow frequency analysis Run Date / Time
10/25/2019 07/21/2021 09:09

Station - 01539000 Fishing Creek near Bloomsburg, PA

TABLE 6 - EMPIRICAL FREQUENCY CURVES -- HIRSCH-STEDINGER PLOTTING POSITIONS

		-	
WATER	RANKED	EMA	FLOW INTERVALS (WHERE LOWER BOUND NOT = UPPER
BOUND)			
YEAR	DISCHARGE	ESTIMATE	LOWER BOUND UPPER BOUND
2011	56000.0	0.0106	
2006	41200.0	0.0212	
1972	30900.0	0.0318	
2018	29900.0	0.0423	
1975	29400.0	0.0529	
1996	21300.0	0.0635	
1977	19700.0	0.0741	
1940	18100.0	0.0847	
-1936	17600.0	0.0953	
2010	17500.0	0.1178	
1986	17200.0	0.1297	
2005	16300.0	0.1416	
1952	16200.0	0.1535	
1969	15300.0	0.1655	
2004	15200.0	0.1774	
2008	14800.0	0.1893	
1943	14300.0	0.2132	
1993	14300.0	0.2012	
1946	14200.0	0.2251	
1951	14000.0	0.2370	
1964	13600.0	0.2608	
1998	13600.0	0.2489	
1942	13400.0	0.2728	
1961	13200.0	0.2966	
2002	13200.0	0.2847	
1984	13000.0	0.3205	
1999	13000.0	0.3085	
1997	12700.0	0.3324	
1979	12300.0	0.3443	
1960	12200.0	0.3562	

1944	12000.0	0.3681
1949	11700.0	0.3801
2007	10400.0	0.3920
	10200.0	0.4039
2001		
1983	9920.0	0.4158
1976	9700.0	0.4278
1957	9610.0	0.4397
1970	9100.0	0.4516
2017	9000.0	0.4635
1953	8660.0	0.4754
2003	8600.0	0.4874
		0.5112
1958	8430.0	
1981	8430.0	0.4993
1995	8270.0	0.5231
2020	8190.0	0.5351
1959	8130.0	0.5470
1978	8120.0	0.5589
1955	8070.0	0.5708
1991	7960.0	0.5827
1989	7680.0	0.5947
1994	7660.0	0.6066
1956	7540.0	
		0.6185
2019	7150.0	0.6304
2012	6590.0	0.6424
1954	6140.0	0.6543
1948	6120.0	0.6662
2015	5860.0	0.6781
1987	5720.0	0.6900
1950	5560.0	0.7020
1980	5550.0	0.7139
1962	5540.0	0.7258
1973	5520.0	0.7377
1974	5250.0	0.7497
1990	5220.0	0.7616
1992	5070.0	0.7735
2000	4860.0	0.7854
1945	4790.0	0.7974
1966	4760.0	0.8093
2013	4630.0	0.8212
1939	4420.0	0.8331
2014	4340.0	0.8450
2009	4330.0	0.8570
1947	4150.0	0.8689
1963	4050.0	0.8808
1985	4040.0	0.8927
1988	4030.0	0.9047
1982	3980.0	0.9166
1967	3900.0	0.9285
1968	3730.0	0.9404
1971	3650.0	0.9523

2016	3580.0	0.9643
1941	3340.0	0.9762
1965	2860.0	0.9881

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Program PeakFq	U. S. GEOLOGICAL SURVEY	Seq.001.005
Version 7.3	Annual peak flow frequency analysis	Run Date / Time
10/25/2019		07/21/2021 09:09

Station - 01539000 Fishing Creek near Bloomsburg, PA

TABLE 7 - EMA REPRESENTATION OF DATA

<---- USER-ENTERED ----><----- FINAL -----> WATER <---- OBSERVED ----><---- EMA -----><- PERCEPTIBLE RANGES -><-PERCEPTIBLE RANGES -> YEAR Q_LOWER Q_UPPER Q_LOWER Q_UPPER LOWER **UPPER** LOWER UPPER 1936 17600.0 17600.0 17600.0 17600.0 17600.0 INF 17600.0 INF 0.0 1937 0.0 17600.0 17600.0 17600.0 INF 17600.0 INF 0.0 1938 0.0 17600.0 17600.0 17600.0 INF 17600.0 INF 4420.0 1939 4420.0 4420.0 4420.0 0.0 INF 0.0 INF 18100.0 18100.0 18100.0 18100.0 0.0 INF 1940 0.0 INF 1941 3340.0 3340.0 3340.0 3340.0 0.0 INF 0.0 INF 1942 13400.0 13400.0 13400.0 13400.0 0.0 INF 0.0 INF 1943 14300.0 14300.0 14300.0 14300.0 0.0 INF 0.0 INF 1944 12000.0 12000.0 12000.0 0.0 INF 12000.0 0.0 INF 0.0 1945 4790.0 4790.0 4790.0 4790.0 INF 0.0 INF 1946 14200.0 14200.0 14200.0 14200.0 0.0 INF 0.0 INF 4150.0 4150.0 0.0 1947 4150.0 4150.0 INF 0.0 INF 1948 6120.0 6120.0 6120.0 6120.0 0.0 INF 0.0 INF 1949 11700.0 11700.0 11700.0 11700.0 0.0 INF 0.0 INF 0.0 1950 5560.0 5560.0 5560.0 5560.0 INF

0.0	INF					
1951	14000.0	14000.0	14000.0	14000.0	0.0	INF
0.0	INF					
1952	16200.0	16200.0	16200.0	16200.0	0.0	INF
0.0	INF					
1953	8660.0	8660.0	8660.0	8660.0	0.0	INF
0.0	INF	6140.0	(140.0	C140 0	0.0	TNIC
1954 0.0	6140.0 INF	6140.0	6140.0	6140.0	0.0	INF
1955	8070.0	8070.0	8070.0	8070.0	0.0	INF
0.0	INF	0070.0	0070.0	0070.0	0.0	2111
1956	7540.0	7540.0	7540.0	7540.0	0.0	INF
0.0	INF					
1957	9610.0	9610.0	9610.0	9610.0	0.0	INF
0.0	INF	0.430	0.100	0.400.0		
1958	8430.0	8430.0	8430.0	8430.0	0.0	INF
0.0 1959	INF 8130.0	8130.0	8130.0	8130.0	0.0	INF
0.0	INF	0150.0	0130.0	0150.0	0.0	TIMI
1960	12200.0	12200.0	12200.0	12200.0	0.0	INF
0.0	INF					
1961	13200.0	13200.0	13200.0	13200.0	0.0	INF
0.0	INF					
1962	5540.0	5540.0	5540.0	5540.0	0.0	INF
0.0	INF	4050 0	4050 0	4050 0	0.0	TNIF
1963 0.0	4050.0 INF	4050.0	4050.0	4050.0	0.0	INF
1964	13600.0	13600.0	13600.0	13600.0	0.0	INF
0.0	INF					
1965	2860.0	2860.0	2860.0	2860.0	0.0	INF
0.0	INF					
1966	4760.0	4760.0	4760.0	4760.0	0.0	INF
0.0	INF	2000 0	2000 0	3900.0	0.0	TNE
1967 0.0	3900.0 INF	3900.0	3900.0	3900.0	0.0	INF
1968		3730.0	3730.0	3730.0	0.0	INF
0.0	INF	27200	27200	27200		
1969	15300.0	15300.0	15300.0	15300.0	0.0	INF
0.0	INF					
1970	9100.0	9100.0	9100.0	9100.0	0.0	INF
0.0	INF	2650.0	2650.0	2650.0	0.0	TNE
1971 0.0	3650.0 INF	3030.0	3650.0	3650.0	0.0	INF
1972	30900.0	30900.0	30900.0	30900.0	0.0	INF
0.0	INF	502000	302000	202000		
1973	5520.0	5520.0	5520.0	5520.0	0.0	INF
0.0	INF					
1974	5250.0	5250.0	5250.0	5250.0	0.0	INF
0.0	INF	20400 0	20400 0	20460 0	0.0	TNIF
1975	29400.0	29400.0	29400.0	29400.0	0.0	INF

0.0	INF					
1976	9700.0	9700.0	9700.0	9700.0	0.0	INF
0.0	INF					
1977	19700.0	19700.0	19700.0	19700.0	0.0	INF
0.0	INF					
1978	8120.0	8120.0	8120.0	8120.0	0.0	INF
0.0	INF					
1979	12300.0	12300.0	12300.0	12300.0	0.0	INF
0.0	INF					
1980	5550.0	5550.0	5550.0	5550.0	0.0	INF
0.0	INF	9420 0	0420 0	9420 0	0.0	TNIC
1981 0.0	8430.0 INF	8430.0	8430.0	8430.0	0.0	INF
1982	3980.0	3980.0	3980.0	3980.0	0.0	INF
0.0	INF	3300.0	3300.0	3300.0	0.0	TIM
1983	9920.0	9920.0	9920.0	9920.0	0.0	INF
0.0	INF	22200	22_313	22_010		
1984	13000.0	13000.0	13000.0	13000.0	0.0	INF
0.0	INF					
1985	4040.0	4040.0	4040.0	4040.0	0.0	INF
0.0	INF					
1986	17200.0	17200.0	17200.0	17200.0	0.0	INF
0.0	INF					
1987	5720.0	5720.0	5720.0	5720.0	0.0	INF
0.0	INF					
1988	4030.0	4030.0	4030.0	4030.0	0.0	INF
0.0	INF	7690 0	7600 0	7690 0	0.0	TNIC
1989 0.0	7680.0	7680.0	7680.0	7680.0	0.0	INF
1990	INF 5220.0	5220.0	5220.0	5220.0	0.0	INF
0.0	INF	3220.0	3220.0	3220.0	0.0	TIM
1991	7960.0	7960.0	7960.0	7960.0	0.0	INF
0.0	INF	7200.0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	7500.0	0.0	
1992	5070.0	5070.0	5070.0	5070.0	0.0	INF
0.0	INF					
1993	14300.0	14300.0	14300.0	14300.0	0.0	INF
0.0	INF					
1994	7660.0	7660.0	7660.0	7660.0	0.0	INF
0.0	INF					
1995	8270.0	8270.0	8270.0	8270.0	0.0	INF
0.0	INF	04000	04000	04000		
1996	21300.0	21300.0	21300.0	21300.0	0.0	INF
0.0	INF	12700 0	12700 0	12700 0	0.0	TNI
1997 0.0	12700.0 INF	12700.0	12700.0	12700.0	0.0	INF
1998	13600.0	13600.0	13600.0	13600.0	0.0	INF
0.0	INF	15000.0	15000.0	15000.0	0.0	TIMI
1999	13000.0	13000.0	13000.0	13000.0	0.0	INF
0.0	INF					
2000	4860.0	4860.0	4860.0	4860.0	0.0	INF

0.0	INF					
2001	10200.0	10200.0	10200.0	10200.0	0.0	INF
0.0	INF					
2002	13200.0	13200.0	13200.0	13200.0	0.0	INF
0.0	INF					
2003	8600.0	8600.0	8600.0	8600.0	0.0	INF
0.0	INF					
2004	15200.0	15200.0	15200.0	15200.0	0.0	INF
0.0	INF					
2005	16300.0	16300.0	16300.0	16300.0	0.0	INF
0.0	INF					
2006	41200.0	41200.0	41200.0	41200.0	0.0	INF
0.0	INF					
2007	10400.0	10400.0	10400.0	10400.0	0.0	INF
0.0	INF	44000	1.000	4.4000		
2008	14800.0	14800.0	14800.0	14800.0	0.0	INF
0.0	INF	4220.0	4220.0	4220.0	0.0	TNE
2009	4330.0	4330.0	4330.0	4330.0	0.0	INF
0.0 2010	INF 17500.0	17500.0	17500.0	17500.0	0.0	INF
0.0	INF	17300.0	17300.0	17300.0	0.0	TIME
2011	56000.0	56000.0	56000.0	56000.0	0.0	INF
0.0	INF	30000.0	30000.0	30000.0	0.0	TIMI
2012	6590.0	6590.0	6590.0	6590.0	0.0	INF
0.0	INF					
2013	4630.0	4630.0	4630.0	4630.0	0.0	INF
0.0	INF					
2014	4340.0	4340.0	4340.0	4340.0	0.0	INF
0.0	INF					
2015	5860.0	5860.0	5860.0	5860.0	0.0	INF
0.0	INF					
2016	3580.0	3580.0	3580.0	3580.0	0.0	INF
0.0	INF	0000	0000	0000	0.0	T.1.E
2017	9000.0	9000.0	9000.0	9000.0	0.0	INF
0.0	INF	20000 0	20000 0	20000	0.0	TNE
2018	29900.0	29900.0	29900.0	29900.0	0.0	INF
0.0 2019	INF 7150.0	7150.0	7150 0	7150.0	0.0	INF
0.0	INF	7130.0	7150.0	ש.שכד/	0. 0	TINL
2020	8190.0	8190.0	8190.0	8190.0	0.0	INF
0.0	INF	0170.0	0170.0	0170.0	0.0	TIMI
1	TIM					
-						

End PeakFQ analysis. Stations processed : 1 Number of errors : 0 Stations skipped : Station years : 0 83

Data records may have been ignored for the stations listed below. (Card type must be Y, Z, N, H, I, 2, 3, 4, or *.) (2, 4, and * records are ignored.)

For the station below, the following records were ignored:

FINISHED PROCESSING STATION: 01539000 USGS Fishing Creek near Bloomsburg

For the station below, the following records were ignored:

FINISHED PROCESSING STATION:



BORTON-LAWSON 3897 Adler Place Bethlehem, PA 18107 (484) 821-0470 - Fax (484) 821-0474 www.borton-lawson.com JOB <u>2021-5134-002</u>

SHEET NO $\underline{1}$ OF $\underline{1}$ CALCULATED BY \underline{EXY} DATE $\underline{7/21/2021}$

CHECKED BY DATE

SCALE <u>NTS</u>

		TF	RANS	POS	ED:	STF	REA	M F	LO	W	FRO	MC	US	GS	GA	GE T	O PI	ROJI	EC1	Γ LC)CA	TION	1																																																					
JSG	SS S1	REA	M GAG	E PRC	PER	TIES												Freau	enc	v Coe	effici	ents fr	om																																																					
Gag	e Nu	mbe	er 0	15390	000	Fish	ing (Creek	nea	r Bl	oom	sbur	g PA				'	-				19-509																																																						
Yea	rs Da	ita R	ecorde	d	193	6-20	20																																																																					
Gag	e Dr	aina	ge Area	(SM)		2	74											2	2			0.836	6																																																					
USG	is sii	R 201	L9-5094	Regi	on	F	Regio	n	3									5	5			0.805	8																																																					
																		1	0			0.791	6																																																					
LOC	ATIC	N -	CONFL	JENCI	WI	TH S	USQ	UEHA	NN	A RI	VER							2.	5			0.778	2																																																					
Drai	inage	e Are	a (SM)	3	85													5	0			0.770	7																																																					
Drai	inage	e Are	a Ratio	(Proj	ect D	A/ga	age [DA)		1.	.41							10	00			0.764	4																																																					
Acc	epta	ble D	Prainage	e Area	Rati	o (B	etwe	en 0.	.5 ar	nd 1	.5)	Υ	es					20	00			0.759																																																						
																		50	00		ı	0.753	1																																																					
We	ight	ed S	kew																		ı																																																							
			ction 10	0.6.C 8	& SIR	201	9-50	94			De	sigr	sto	rm	Ex	Annua ceeda obabi	nce			t Ga n 17	_	Pı	ow at roject cation																																																					
												(ye	ars)			(%)			(c	fs)			(cfs)																																																					
													1			0.995	0		2,2	92		3	3,046																																																					
Wh	ere:											1.	.01			0.990	0		2,5	44		3	3,381																																																					
	Q	=	Peak d	ischar	ge at	t pro	project site		project site		project site		ite			1.	.05			0.950	0		3,4	163		4	1,603																																																	
	Α	=	Basin a	rea al	bove	project site				project site			ct site			project site				project site			project site			project site			oroject site			project site				project site			project site						1.	.11			0.900	0		4,1	.42		5	5,505																				
	Q_G	=	Peak d	ischar	arge at stream gage			charge at stream gage	at stream gage				t stream gage			it stream gage				at stream gage				at stream gage			stream gage				stream gage			tream gage			stream gage				stream gage				am gage			stream gage				stream gage			stream gage			stream gage			stream gage		tream gage		1.	.25			0.800	0		5,2	19		(5,937
	A_{G}	=			ea above stream gage						1.	.50			0.666	7		6,5	70		8	3,733																																																						
	В	=	Freque 2019-5	-			cient from SIR						2			0.500	0		8,4	192		1	1,287																																																					
				1U34 I	avie	3	ı					2.	.33			0.429	2	<u> </u>	9,4	189		1	2,481																																																					
													5			0.200	0	<u> </u>	14,	690		1	9,322																																																					
												1	LO			0.100	0		20,	070		2	6,271																																																					
												2	25			0.040	0		28,	530		3	7,175																																																					
												5	50			0.020	0		36,	210		4	7,062																																																					
												1	00			0.010	0		45,	210		5	8,633																																																					
												2	00			0.005	0		55,	730		7	2,149																																																					
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BORTON-LAWSON
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JOB <u>2021-5134-002</u>

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<u>USC</u>	GS S1	TREA	M G/	4GE	PRC	PER	TIES											╛,	Frague	ncy Coef	ficio	nts from
Gag	ge Nu	ımbe	er	01	5390	000	Fish	ing	Cree	k nea	ar Bl	oom	sbur	g PA				_ '	•	3 of SIR		
Yea	rs Da	ata R	ecord	ded		193	6-20	20														
Gag	ge Dr	aina	ge Ar	ea (SM)		2	74											2		(0.8366
USG	GS SII	R 20	19-50	94 F	Regio	on	F	Regio	on	3									5		(0.8058
																			10		(0.7916
LOC	CATIO	<u> NC</u>	RAILE	ROA	D ST	REE	T BR	IDG	E										25		(0.7782
Dra	inag	e Are	ea (SN	/ 1)	3.	55													50		(0.7707
Dra	inag	e Are	ea Rat	tio (Proje	ect D	A/ga	age I	DA)		1.	.30						-	100)	(0.7644
Acc	epta	ble [Draina	age /	Area	Rati	o (B	etw	een ().5 a	nd 1	.5)	Υ	es					200)		0.7592
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			kew																			
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Per	DM-	2 Se	ction	10.6	6.C 8	k SIR	201	9-50)94			De	sign	Sto	rm	Exce				v at Gag		Project
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wn	ere:		D I	1! -	_l				-:					01			9900			2,544		3,159
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C.2 Drainage Area Map

D. Fishing Creek Hydraulic Analysis

D.1 HEC-2 Data of Fishing Creek

******************************* SEPT 1971 VERSTON. UPDATED JUNE 1974 * * THIS PROGRAM IS OWNED BY THE UNITED STATES GOVERNMENT ERROR CORRECTIONS 01 THRU 09R2 * AND IS USED BY PERMISSION OF THE CORPS OF ENGINEERS. * DEPARTMENT OF THE ARMY. MODIFICATIONS 52 THRU 58 * THE PROGRAM HAS BEEN REVISED BY MICHAEL BAKER. JR. . INC. * MBJ UPDATED 07/20/76 0830 * ONLY AS REQUIRED FOR USE ON THEIR COMPUTER AND EXECUTES * TODAYS DATE IS 02/28/77 * CORRECTLY THE STANDARD TEST SERIES AS PUBLISHED BY THE * 16.58 * CORPS OF ENGINEERS. HYDROLOGIC ENGINEERING CENTER. ************************* 2.723 SECONDS FISHING CREEK SUSQUEHANNA RIVER BASIN COMMISSION TI MULTIPLE PROFILES : TZ BLOOMSBURG-BERWICK-SHICKSHINNY REACH T3 FISHING CREEK 10 YEAR FLOOD WSEL J1 ICHECK TNO NINY TOTA STRT METRIC HVINS 0.0 0.0 0. 456.100 Known WSEL for 10-yr flow Michael Baker, Jr., Inc. CHNIM NPROF TPI OT PREVS XSECV XSECH FN ALLDC IBW 2763 N. Fourth St. 0.0 0.0 1.000 0.0 -1.000 0.0 0.0 0.0 0.0 0.0 Box 3225 0.0 Harrisburg, Pa. 17105 34.000 27.000 28.000 9.000 0.0 0.0 1.000 3.000 4.000 0.0 0.0 OT 24300.000 45700.000 58500.000 58500.000 102000,000 0.0 0.0 5.000 0.0 0.300 0.0 0.0 0.0 0.0 NC 0.050 0.070 0.035 0.100 9.100 0.0 4900.000 5243.000 0.0 0.0 FT 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 XI 1.010 94.000 4960.000 5243.000 473.300 1030.000 474.000 1040.000 474.300 1059.000 GR 480.000 1000.000 479.800 1010.000 1239.000 474.100 1347.000 GR 474.300 1077.000 473.900 1100.000 473.600 1159.000 473.800 470.700 468.400 1712.000 GR 473.500 1450.000 473.800 1539.000 473.900 1613.000 1652.000 GP 468.300 1729.000 468.800 1752.000 469.700 1798.000 470.200 1846.000 472.500 1863.000 GR 473.700 471.800 1951.000 471.500 2037.000 472.100 2122.000 1895.000 472.200 1908.000 GR 468.000 2285.000 469.000 2325.000 471.500 2388.000 471.800 2176.000 469.900 2221.000 472.500 2790.000 473.000 2852.000 GR 472.100 2466.000 472,500 2555.000 471.700 2658,000 3114.000 470.200 3194.000 471.300 3278.000 GP 471.200 472.400 3079.000 472.100 3001.000 471-800 3745.000 GR 471,300 3546.000 471.700 3662.000 470.800 3350.000 471.500 3464.000 474.100 4421.000 4090.000 472.000 4114.000 GR 472.600 3859.000 472.300 3979.000 471.800 4685.000 465.900 4746.000 GR 474.000 4498.000 470.300 4561.000 469.800 4636.000 467.200 459.900 4891.000 GR 464.600 4798.000 463.000 4844.000 463.700 4857.000 463.700 4874.000 4979.000 5089.000 448.200 5089.000 CD 455.800 4924.000 455.500 4960.000 454.500 448.200 457.000 5217.000 461.300 5243.000 465,300 5283.000 GR 448.200 5181.000 454.500 5207.000 5499.000 468.100 5597.000 470.100 5657.000 GR 5317.000 466.800 5415.000 467.300 466.000 5827.000 GR 471.800 5732.000 473.600 5760.000 470.500 5791.000 470.700 5807.000 475.100 484.800 5995.000 482.400 5932.000 485.500 5973.000 GR 475.400 5851.000 477.200 5885.000 483.900 6122.000 483.700 6177.000 481.100 6187.000 GR 484.600 6022.000 485.100 6053.000 0.0 GR 481.100 6198.000 483.100 6210.000 484.900 6228,000 486.900 6272.000 0.0 0.0 0.0 9.100 0.0 0.0 0.0 4830.000 5283.000 0.0 0.0 0.0 450.000 450.000 450.000 0.0 0.0 0.0 1.020 0.0 0.0 0.0 0.0 4656.000 5285.000 ET 0.0 9.100 0.0 0.0 0.0 630.000 680.000 0.0 0.0 0.0 0.0 670,000 X1 1.000 0.0 0.0 0.0 0.0 0.0 4530.000 5509.000 0.0 9.100 0.0 0.0 0.0 0.0 700.000 0.0 0.0 650.000 510.000 X1 1.100 94.000 5236.000 5509.000 1637.000 473.000 1417.000 474.100 1484.000 473.000 GR 486.000 1.000 473.200 1000.000 473.300 2039.000 2024.000 472.000 1729.000 471.600 1805.000 471.400 1931.000 471.800 471.600 3043.000 470.400 2053.000 469.400 2647.000 470.700 2737.000 471.500 2875.000 471.500 3306.000 472.800 3319.000 473.400 3338.000 GR 470.400 3208.000 470.100 3247.000 470.400 3567.000 469.900 3669.000 470.100 3368.000 469.800 3432.000 469.800 3481.000

3834.000

469.900

3873.000

469.900

3714.000

468.300

3787.000

469.900

3906.000

468.700

	GR	-66.300	3975.00C	465.200	4037.000	465.600	4143.000	466.000	4228.000	468.600	4541.000	
9	GR	465.900	4833.000	467.300	4871.000	467.800	4919.000	473.500	4938.000	474.100	4947.000	<u> </u>
	GR	474.100	4957.000	474.000	4968.000	472.100	4997.000	470.500	5050.000	470.200	5118.000	
	GR	469.700	5189,000	466.800	5236.000	460.700	5263.000	449.400	5265.000	449.400	5282.000	
	GR	479.400	5282.000	479.400	5290.000	449.400	5290.000	449.400	5325.000	479.400	5325.000	
	GR	479.400	5333.000	449.400	5333.000	449.400	5368.000	479.400	5368.000	479.400	5376.000	
4	GR	449.400	5376.000	449.400	5411.000	479.400	5411.000	479.400	5419.000	449-400	5419.000	
	GR	449.400	5454.000	479.400	5454.000	479.400	5462.000	449.400	5462.000	449.400	5488.000	' • i
	GR	454.800	5493.000	462.900	5501.000	466.300	5509.000	469.900	5549.000	468.600	5605.000	7 - 2
	GR	475.100	5757.000	477.800	5896.000	482.500	5973.000	483.900	6022.000	484.300	6036.000	
	GR	482.700	6046.000	482.900	6062.000	483.900	6105.000	486.300	6153.000	485.500	6157.000	
. 4	GR	485.800	6181.000	487,200	6204.000	488.600	6235.000	490.800	6254.000	490.800	6275.000	•
	GR	493.700	6297.000	496.400	6403.000	496.400	6443.000	495.800	6448.000	0.0	0.0	
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4160.000	5545.000	
1			ر									
18	X1	2.000	95.000	5349.000	5545.000	350.000	170.000	230.000	0.0	0.0	0.0	
1 11	GR	485.000	1.000	468.500	1000.000	471.100	1126.000	470.800	1178.000	470.200	1216.000	
12	GR	470.700	1265.000	473.000	1339.000	473.500	1405.000	473.900	1470.000	474.800	1548.000	A
13	GR	475.400	1624.000	476.000	1663.000	477.400	1714.000	476.200	1764.000	474.900	1810.000	
P 14	GR	473.600	1835.000	473.400	1863.000	472.800	1984.000	471.100	2159.000	471.400	2295.000	
15	GR	471.900	2382.000	471.800	2491.000	471.400	2572.000	470.400	2664.000	469.400	2754.000	149
10	GR	468.100	2873.000	468.700	2978.000	468.200	3088.000	468.200	3204.000	467.800	3316.000	n_
	GR	467.800	3434.000	469.400	3553.000	468.500	3660.000	468.200	3791.000	469.300	3914.000	
18	GR	468.100	4059.000	467.300	4189.000	466,800	4338.000	465.900	4478.000	466.800	4596.000	11
19	GR	466.400	4721.000	466.900	4769.000	467.900	4799.000	467.200	4826.000	467.100	4834.000	u_
9 16	GR	465.000	4857.000	455.400	4886.000	461.700	4906.000	465.400	4941.000	469.200	4958.000	
21	GR	469.200	4972.000	467.000	4988.000	466.300	5049.000	466.300	5127.000	466.400	5207.000	J*
12 m	GR	466.400	5259.000	465.900	5308.000	460.600	5349.000	456.800	5361.000	454.800	5368.000	15_
E 19 17	GR	446.000	5397.000	446.000	5451.000	446.000	5516.000	454.800	5533.000	460.900	5545.000	
	GR	470.600	5560.000	473.700	5610.000	474.800	5661.000	475.400	5703.000	475.400	5726.000	
	GR	475.400	5741.000	476.600	5785.000	480.000	5840.000	481.300	5888.000	481.700	5926.000	17.
	GR GR	482.400	5959.000	484.900	5972.000	485.100	5987.000	485.100	6012.000	484.900	6020.000	
	CONTRACTOR OF THE PARTY OF	485.700	6038.000	489.600	6072.000	490.400	6110.000	491.100	6129.000	491.900	6155.000	1" 2
	GR GR	492.600	6203.000	498.500	6239.000	499.000	6271.000	499.700	6308.000	499.700	6323.000	17.00
	NC	496.800	6343.000	496.800	6356.000	496.800	6362.000	504.900	6376.000	510.200	6388.000	
23		0.0	0.0	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0	
(n	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4140.000	5689.000	in
	X1 .	3.010	68.000	5527.000	5689.000	50.000	125.000	125.000	0.0	0.0	0.0	11
14	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	464.500	476.100	0.0	
25	GR	485.000	1.000	467.100	1032.000	465.600	1048.000	467.200	1062.000	468.400	1128.000	и.
3	GR	469.600	1200.000	468.300	1256.000	470.100	1276.000	471.800	1335.000	472.700	1362.000	
37	GR	473.700	1407.000	472.700	1461.000	472.800	1521.000	473.800	1562.000	475.300	1623.000	
(9 38	GR	475.700	1663.000	476.000	1726.000	475.200	1778.000	474.800	1861.000	468.700	1880.000	•
19	GP	468.800	1898.000	469.200	1941.000	470.100	2019.000	471.500	2111.000	470.900	2199.000	26
62	GR	470.800	2307.000	471.700	2432.000	471.700	2533.000	471.600	2629.000	470.200	2740.000	
94	GR	469.800	2835.000	469.900	2959.000	467.600	3084.000	469.000	3183.000	469.400	3303.000	
47	GR	468.400	3399.000	468.600	3482.000	468.700	3588.000	468.700	3754.000	468.900	3909.000	/ H
42	GR	466.400	4042,000	464.500	4136.000	464.900	4204.000	465.800	4296.000	466.200	4427.000	
94	GR	466.700	4547.000	467.300	4681.000	467.300	4776.000	466.800	4807.000	466.600	4839.000	. •
45	GR	466.500	4863.000	466.500	4882.000	466.500	4925.000	466.600	4983.000	466.900	5065.000	100
46	GR	466.300	5140.000	466.600	5223.000	465,400	5239.000	467.600	5387.000	466.000	5439.000	
00	GR	458.000	5486.000	449.500	5527.000	449.500	5527.000	449.500	5689.000	449.500	5689.000	
48	GR	455.000	5700.000	476.100	5761.000	485.400	6002.000	0.0	0.0	0.0	0.0	W =
49	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4140.000	5689.000	
€ 50					10.00							
51	X1	3.020	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0	34 J
. 52	RT	9.000	5387.000	467.600	467.600	5439.000	469.600	466.000	5486.000	474.500	458.000	
() so	RT	5527.000	478.600	449.500	5527.000	478.600	473.500	5689.000	479.000	473.500	5689.000	
54	AT	479.000	449,500	5700.000	479.000	455.000	5761.000	476.100	476.100	0.0	0.0	A I
25	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4140.000	5689.000	1, 2
95												01
57	X1	3.100	0.0	0.0	0.0	21.000	21.000	21.000	0.0	0.0	0.0	3a *
12	XS	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0	9 200
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4140.000	5689.000	
					10 10 10 may 12 mg	154704 1445	11/0/5/0				100000000000000000000000000000000000000	To the second se

	XI	3.200	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0	3
	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	464.500	476.100	0.0	
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3850.000	6100.000	
•	×ı	4.010	39.000	5880.000	6100.000	400.000	10.000	30.000	0.0	0.0	0.0	o
	GR	480.000	1.000	466.000	1000.000	470.000	1530.000	471.000	3025.000	470.000	3525.000	
1	GR	470.000	4330.000	474.000	4500.000	470.000	4590.000	465.000	4820.000	465.000	4920.000	
9 7	GR '	464.000	5000.000	460.000	5150.000	460.500	5160.000	460.000	5165.000	459.000	5180.000	
业	GR	460.000	5195.000	460.000	5300.000	457.000	5380.000	460.000	5700.000	466.100	5765.000	
	GR	466.100	5785.000	465.000 475.000	5805.000 6100.000	460.000 463.000	5880.000 6200.000	448.300 485.000	5920.000 6305.000	448.300 486.500	6075.000 6330.000	'
	GR GR	455.000	6082.000	495.000	6460.000	500.000	6520.000	501.000	6580.000	500.000	6638.000	
1	GR	504.900	6650.000	505.000	6690.000	510.000	6800.000	515.000	6875.000	0.0	0.0	
	⊝ FT	0.0	0.0	0.0	0.0	9.100	0.0	0.5	0.0	3850.000	6100.000	•
10	X1	4.020	0.0	0.0	0.0	15.000	15.000	15.000	0.0	0.0	0.0	
1 1	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	470.000	475.000	0.0	
12	FT	0.0	0.0	0.0	0.0	9,100	0.0	0.	0.0	3850.000	6100.000	
13	SB	1.250	1.500	3.000	0.0	133.000	16.000	4100.000	1.900	451.000	451.000	•
15	X1	4.100	0.0	0.0	0.0	17.000	17.000	17.000	0.0	0.0	0.0	
16	XS	0.0	0.0	1.000	476.000	474.100	0.0	0.0	0.0	0.0	0.0	
100	X3 BT	10.000	0.0	0.0	0.0	1000.000	0.0 475.500	0.0	474.200 1785.000	475.000 474.700	0.0	
14	BT	29.000	1.000	480.000	2141.000	474.600	0.0	2473.000	474.200	0.0	4029.000	
₽ 70	BT	475.300	0.0	4554.000	478.100	0.0	4758.000	478.500	0.0	4813.000	479.300	30
21	BT	0.0	4887.000	479.800	0.0	4941.000	480.200	0.0	5018.000	480.500	0.0	Ju J
22	BT	5053.000	480.700	0.0	5140.000	480.900	0.0	5243.000	481.000	0.0	5333.000	15 mg
(P) 13	BT	481.200	0.0	5415.000	481.500	0.0	5525.000	482.100	0.0	5551.000	482.600	•
74	BT	0.0	5581.000	482.500	0.0	5676.000	482.900	0.0 6064.000	5878.000 483.300	482.900	0.0 6099.000	*
D 176	BT BT	5885.000 483.900	483.000	0.0 6118.000	6028.000 484.100	483.000	0.0 6134,000	485.200	0.0	0.0	0.0	. 100
27	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3850.000	6100.000	18
20	X1	4.200	0.0	0.0	0.0	66.000	66.000	66.000	0.0	0.0	0.0	"•
n	хз	10.000	0.0	0.0	0.0	0.0	0.0	0.0	471.000	475.000	0.0	10
31 • 129	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3540.000	5918.000	no
n	X1	5.010	70.000	5603.000	5918.000	5.000	5.000	5.000	0.0	0.0	0.0	n
34	BT	12.000	5603.000	482.200	482.200	5603.000	482.200	479.400	5625.000	482.300	479.500	n
2 225.	вт	5625.000	482.300	482.300	5718.000	483.200	483.200	5718.000	483.200	478.200	5815.000	•
24	BT	483.800	478.800	5815.000	483.800	483.800	5821.000	483.800	483.800	5821.000	483.800	14
37	BT	478.800	5918.000	484.300	479.300	5918.000	484.300	484.300	0.0	0.0	0.0	"0
23	GR GR	480.000	1.000	471.000	1000.000	471.000 475.100	3536.000 4779.000	471.100 475.700	3683.000 4979.000	471.200 476.400	3987.000 5054.000	26
0	GR	472.960 476.500	4580.000 5055.000	474.000 477.000	4696.000 5095.000	477.500	5157.000	478.600	5240.000	479.300	5295.000	
9 41	GR	479.900	5358.000	480.300	5401.000	481.400	5467.000	481.900	5511.000	482.000	5572.000	"•)
42	GR	482.200	5603.000	467.000	5603.000	467.000	5603.000	467.000	5625.000	467.000	5625.000	
- 6	GR	482.300	5625.000	483.200	5718.000	456.100	5718.000	456.100	5718.000	453.100	5750.000	19
C4	GR	448.400	5783.000	443.400	5815.000	443.400	5815.000	483.800	5815.000	483.800	5821.000	
45	GR	442.800	5821.000	442.800	5821.000	448.600	5853.000	450.200	5886.000	466.100	5918.000 6068.000	
947	GR GR	466.100	5918.000 6093.000	484.300 485.500	5918.000 6119.000	483.400 487.200	6009.000	479.200 490.100	6028.000 6180.000	481.200	6209.000	n _n O
45	GR	496.600	6241.000	496.600	6260.000	501.500	6287.000	501.500	6341.000	502.300	6388.000	n n
45	GR	500.300	6406.000	498.600	6423.000	498.600	6441.000	505.000	6460.000	506.300	6473.000	13
€"a	GR	506.300	6495.000	507.100	6525.000	509.500	6587.000	511.200	6633.000	514.400	6652.000	•
Я	GR	515.400	6668.000	516.300	6719.000	521.300	6794.000	525.200	6844.000	531.000	6889.000	²⁴ g
F 12	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3540.000	5918.000	80
. 44	X1	5.100	0.0	0.0	0.0	18.000	18.000	18.000	0.0	0.0	0.0	
35	XS	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0	n_
O 36	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2980.000	5821.000	,
12 7	X1	6.010	94.000	5593.000	5821.000	5.000	5.000	5.000	0.0	0.0	0.0	76
0	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	467.200	475.000	0.0	•
	GR	480.000	1.000	471.500	1000.000	471.400	1152.000	471.800	1242.000	471.800	7.327.000	

							Service Control					798
	GR	470.400	1483.000	469.000	1604.000	467.500	1724.000	467.900	1842.000	465.300	1944,000	4
	GR	469.600	2079.000	468.600	2256.000	469.200	2444.000	469.300	2587.000	468.500	2684.000	
	GR	467.500	2745.000	466.500	2758.000	465.800	2764.000	460.600	2808.000	465.800	2834.000	
	GR	467.700	2843.000	472.000	2866.000	471.400	2923.000	470.700	3042.000	464.100	3074.000	
	GR	464.200	3084.000	467.300	3101.000	468.300	3141.000	469.700	3191.000	468.800	3265.000	
	GR	467.400	3316.000	466.200	3336.000	466.200	3392.000	466.200	3465.000	469.000	3516.000	
	GR GR	469.500	3594.000 4221.000	468.700 468.000	3675.000	468,800	3845.000	469.100	3977.000	469.000	4107.000	6
	GR	466.300	4674.000	465.900	4370.000 4721.000	467.900	4483.000 4756.000	467.800 462.200	4567.000	467.600	4625.000	
	GR	465.700	4800.000	466.400	4832.000	466.600	4880.000	467.000	4772.000	464.800 467.400	4787.000 5013.000	2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
	GR	467.400	5090.000	467.100	5179.000	467.500	5250.000	467.700	5292.000	468.000	5378.000	1
	GR	468.100	5443.000	468.400	5486.000	467.900	5496.000	467.900	5519.000	468.300	5537.000	
7	GR	467.100	5574.000	465.800	5593.000	459.400	5602.000	455.800	5608.000	454.800	5614,000	
	GR	451.500	5632.000	451.500	5685.000	451.500	5685.000	454.800	5751.000	455.100	5758.000	•
4	GR	455.100	5770.000	454.800	5778.000	452.600	5791.000	454.800	5804.000	456.100	5811.000	
16	GR	472.700	5821.000	478.800	5835.000	478.800	5851.000	478.200	5863.000	479.500	5870.000	
● 11 ··	GR	482.500	5905.000	488.300	5953.000	492.800	5993.000	495.200	6023.000	497.100	6057.000	•
1	GR	499.300	6071.000	499,300	6083,000	496.800	6088.000	502.000	6108,000	0.0	0.0	
_ 3	NC	0.050	0.070	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
	ET .	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2980.000	5821.000	
	X1	6.000	0.0	0 0	0.0	110 000	200 000	305 000				10
	FT	0.0	0.0	0.0	0.0	9.100	290.000	205.000	0.0	0.0	0.0	· · · · · · · · · · · · · · · · · · ·
14		0.	12.00	V• U	0.0	7.100	0.0	0.0	0.0	2840.000	5394.000	
m[X1	7.000	95.000	5136.000	5394.000	80,000	780.000	680.000	0.0	0.0	0.0	
Ø 10	GR	480.000	1.000	471.500	1000.000	471.000	1211.000	471.400	1323.000	470.400	1455.000	13
n	GR	469.900	1556.000	469.300	1640.000	469.200	1654.000	467.200	1672.000	466.700	1728.000	14
27	GR	466.300	1861.000	469.100	1977.000	469.800	2101.000	468.700	2200.000	468.900	2308.000	
Ø 173	GR	469.100	2429.000	467.600	2538.000	468.200	2660.000	466.900	2720.000	466.200	2745.000	
",_	GR	465.800	2763.000	467.500	2785.000	472.300	2816.000	472.100	2856.000	470.600	2929.000	18
25	GR	470.300	2978.000	469.500	3024.000	463.300	3045.000	465.300	3058.000	467.000	3093.000	u_
23	GR	467.700	3145.000	468.100	3195.000	468.800	3274.000	467.200	3304.000	466.200	3315.000	•
	GR	459.100	3393.000	466.200	3511.000	467.200	3527.000	467.200	3570.000	467.300	3597.000	1 ¹⁶ 1
	GR GR	466.600	3605.000	464.000	37.000	466.600	3661.000	467.200	3666.000	467.800	3730.000	10
30	GR	467.900	3836.000 4330.000	468.500 468.200	3936.000 4409.000	469.400 468.100	4021.000 4486.000	469.900	4108.000 4597.000	467.800	4225.000	
n	GR	465.100	4706.000	460.500	4725.000	465.300	4740.000	466.500	4793.000	466.900	4663.000	
Ø- 12	GR	467.100	4861.000	465.400	4886.000	465.300	4924.000	467.800	4945.000	467.500	4825.000 5026.000	21
33	GR	468.300	5074.000	468.700	5112.000	468.800	5136.000	460.600	5151.000	456.300	5157.000	2
34	GR ·	454.900	5166.000	454.300	5170.000	454.300	5246.000	454.300	5314.000	454.900	5319.000	
9-15	GR	455.700	5325.000	457.100	5343.000	460.500	5360.000	468.400	5394.000	467.500	5439.000	0
34	GR	465.900	5457.000	464.500	5475.000	465.300	5495.000	465.800	5531.000	470.200	5554.000	
37	GR	473.700	5592.000	481.600	5613.000	482.900	5636.000	483.300	5686.000	484.800	5703.000	
W 38	GR	487.600	5724.000	492.600	5756.000	497.400	5777.000	503.600	5802.000	503.600	5823.000	
34	ET	0.0	0.0	0.0	0.0	9,100	0.0	0.0	0.0	2480.000	5042.000	124
	v 1	0 000	66 000	4717 000	E0/2 000	270 000	740	705				4
41	X1 GR	8.000 480.000	66.000	4717.000	5042.000	270.000	740.000	725.000	0.0	0.0	0.0	
0	GR	469.600	1.000	471.500	1000.000	471.400	1220.000	471.000	1339.000	470.300	1423.000	
Ø=11	GR	467.700	2068,000	468.300	1623.000 2233.000	468.400 467.600	1667.000 2370.000	468.400	1772.000	467.800	1925.000	"6
45	GR	470.700	2651.000	471.000	2719.000	471.200	2819.000	464.500	2480.000 2871.000	470.100 465.100	2552.000 2884.000	30
46	GR	465.500	2949.000	465.500	3019.000	465.900	3127.000	465.900	3252.000	465.200	3372.000	
9	GR	464.800	3449.000	465.300	3500.000	466.200	3603.000	466.900	3715.000	466.800	3873.000	33
45	GR	466.300	4018.000	466.200	4129.000	466.300	4205.000	466.400	4240.000	466.500	4285.000	27
45	GR	466.500	4335.000	468.000	4381.000	468.500	4435.000	469.500	4498.000	470.500	4571.000	n d
10	GR	470.700	4653.000	470.500	4678.000	470.300	4691.000	464.500	4708.000	464.500	4717.000	(0)
я	GR	457.700	4719.000	456.900	4729.000	456.000	4740.000	456.000	4850.000	456.000	4979.000	2
5) 600 mm	GR	456.900	4983.000	459.000	4992.000	464.300	5009.000	467.600	5042.000	467.800	5103.000	35
	GR	466.100	5160.000	464.900	5201.000	461.400	5233.000	460.300	5246.000	458.700	5264.000	•
40	GR	460.300	5265.000	470.300	5270.000	475.900	5282.000	483.000	5299.000	484.400	5309.000	*
0 4	GR ET	484.700	5331.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	W.
57	• 1	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2465.000	5042.000	
50	X1	9.000	66.000	4680.000	4999.000	20 000	30.000	30 000			0.0	
Ø 99	GR	480.000	1.000	471.500	1000.000	20.000 471.300	1222.000	30.000 471.000	0.0 1339.000	0.0 470.400	0.0 1422.000	"
	GR	469.600	1570.000	469.200	1622.000	468.500	1668.000	468.300	1772.000	467.700	1924.000	W

GR								4						
Column C			467.600	2052.000		2216,000	467.500	2376.000	468.100	2486,000	470,100	2552.000	E	
62 464,380 3459,000 465,200 1950,000 466,220 1005,000 466,520 373,000 467,000 373,000 467,000 373,000 467,000 373,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 477,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 466,520 427,000 467,000	•					CONTRACTOR DESCRIPTION OF THE PROPERTY OF THE		2815.000	464.700	2855.000	465.400		U	
60							466.100	3123.000	465.800	3250.000				
## 646-320 #278-800 #458-800 #456-100 #128-000 #66-100 #266-000 #66-400 #248-000 #257-000 #25					465.400	3508.000	466.200	3605.000	466.700	3719.000	467.000			
Section Color Co						4128.000	466.200	4206.000	466.400	4244.000				•
62 46, 100 400, 100 400, 100 400, 100 470, 100 4	_			4326.000	468.400	4387.000	468.800	4449.000	469.900					
Beta 461,700 4700,000 461,500 470,000 461,700 460,000 470,000 450,000 4718,000 461,000 470,400 566,000 470,400 566,000 470,400 566,000 470,400 576,000 576,000 470,400 576,0				4612.000	470.700	4647.000	470.500	4656.000	470.500	4680.000				
62 455.000 4940.000 490.700 3577.000 461.400 4074.000 466.200 5275.000 467.200 5275.000 667.000 5187.000 466.200 5275.000 467.000 5275.000 667.000 5275.000 667.000 5275.000 667.000 5275.000 667.000 5275.000 677				4700.000	461.800	4700.000	460.700	4704.000	460.060	4707.000				
Column C		CONTRACTOR OF THE PARTY.		4940.000	460.700	4957.000	461,400	4974.000	466.000					, 1
## 85.500 \$542.000 \$76.400 \$76.400 \$76.600 \$47.400 \$526.000 \$47.400 \$526.000 \$47.400 \$526.000 \$47.400 \$526.000 \$47.400 \$60.00 \$47.400					466.900	5143.000	466.200	5187.000	466.200	5223.000				- ;
## 485.100 5223.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	•				470.400	5266.000	474.600	5276.000	479.700	5286.000				
## 10.00 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	-						0.0	0.0	0.0					4
## 10.000		ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1830.000			
GR	•						2.5				0.0	6.4		
68 459,600 1448,000 466,200 1556,000 477,000 1651,000 466,700 1792,000 446,000 2251,000 464,000 2251,000 464,000 2251,000 464,000 2251,000 464,000 2251,000 464,000 2251,000 464,000 2251,000 464,400 2245,000 2269,000 88 464,400 2313,000 465,400 2326,000 464,400 2346,000 2269,000 88 464,400 2313,000 465,400 2355,000 467,400 2655,000 467,400 467,400 2655,000 467,400										0.0	0.0	0.0		
68										1222.000	470.600	1316.000		
GR	•									1792.000	466.000	1867.000		
GR		THE PROPERTY OF THE PARTY OF TH									464.800	2269.000		
GR	- LI											2446.000		
GR 467,700 3131,000 466,500 3207,000 467,500 3258,000 467,500 3346,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 378,000 467,500 477,500 468,000 4120,000 467,600 378,000 467,500 478,000 467,500 478,000 467,500 478,000 467,500 478,000 467,500 478,000 467,500 478,000 467,500 478,000 468,000 4120,000 468,000 4120,000 468,000 4120,000 468,000 4120,000 468,400 478,000 478,000 468,000 456,700 458,000 468,000 478,000 468,000 478,000 468,000 456,700 458,000 468,000 478,000 468,000 478,000 468,000 478,000 478,000 468,000 47	•													•
GR 467,700 3573,000 466,000 3648,000 467,500 3710,000 467,400 3776,000 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 3828,000 467,200 468,200 4120,000 468,200 4120,000 468,200 4120,000 468,200 470,000 468,200 4120,000 468,200 4120,000 468,200 4120,000 468,200 4120,000 468,200 4120,000 468,200 4705,000 468,200 4705,000 468,200 4705,000 468,200 4705,000 468,200 4705,000 468,200 4705,000 468,200 4705,000 468,200 5132,000 468,200 5132,000 468,200 5132,000 468,200 5132,000 468,200 5132,000 468,200 4705,000 468,200 5132,000 468,200 4705,000 468,200 5132,000 468,	14	CONTROL MANAGEMENT OF THE PARTY		BEING AND THE RESIDENCE OF STREET AND STREET AND STREET										10
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6R 467.500 4497.000 465.800 4501.000 461.000 460.900 462.800 4756.000 469.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 464.900 466.900 687.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 465.600 5072.000 494.500 5193.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	19		Manager State Committee of the Committee											17
GR 456,700 4609,000 456,700 4679,000 469,900 468,400 469,400 468,400 468,400 468,400 468,400 468,400 468,400 468,400 468,400 5093,000 468,400 5093,000 468,400 5093,000 468,400 5093,000 468,400 5093,000 468,400 5093,000 468,400 5093,000 476,000 5102,000 469,500 5172,000 469,400 5093,000 476,500 5103,000 485,100 5131,000 491,000 5172,000 476,500 5193,000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	20													
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	GR ·	470.700	2827.000	471.000	2942.000	471.000	3022.000	470.800	3079.000	470.300	3153.000	6	
	GR	470.500	3182.000	470.800	3200.000	470.100	3213.000	469.000	3292.000	469.200	3385.000	6	
	GR	469.700	3473.000	469.900	3553.000	470.700	3631.000	474.000	3648.000	474.000	3692.000		
	GR	471.700	3715.000	472.100	3736.000	475.100	3766.000	476.700	3827.000	478.000	3866.000		
	GR GR	477.200	3907.000	475.000	3986.000	473.300	4061.000	473.300	4154.000	472.900	4238.000		
į.		472.200	4317.000	471.800	4404.000	471.800	4470.000	471.600	4516.000	472.100	4530.000		
9	GR GR	472.100 461.700	4547.000	480.000	4900.000	460.000	4900.000	452.900	4940.000	454.900	4992.000		To Base
	GR	484.200	4992.000	461.700	4998.000 5425.000	461.700	4998.000	456.900	5040.000	463.300	5092.000		
	GR	490.900	5629.000	497.700	5654.000	502.400	5448.000	485.700	5507.000	488.400	5577.000		2
	ET	0.0	0.0	0.0	0.0	9.100	5677.000	507:400	5709.000	507.400	5731.000		
		0.0	0.0	0.0	20, 16, 200	9.100	0.0	0.0	0.0	1670.000	5092.000		
1	X1	12.100	0.0	0.0	0.0	110.000	110.000	110.000	0.0	0.0	0.0		
	XS	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0		
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	469.000	0.0	0.0		1.
iv	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1650.000	5148.000		
o ⊘ n						/468,858		451,295	44.69, 398		10 0 A A A A A RADIO 10 A A A A A A A A A A A A A A A A A A		•
17_	X1	13.100	95.000	4937.000	5148.000	5.000	5.000	5.000	0.0	0.0	0.0		1
n	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	469.000	0.0	0.0		
14	GR	485.000	1.000	471.300	1084.000	470.800	1185.000	470.200	1277.000	468.900	1359.000		
15	GR	467.300	1402.000	465.700	1423.000	466.800	1448.000	467.000	1469.000	465.500	1489.000		110
16	GR	464.300	1505.000	465.500	1537.000	466.000	1551.000	466.200	1576.000	465.900	1618.000		11
11	GR GR	465.700	1690.000	465.700	1758.000	466.000	1841.000	465.800	1869.000	466.000	1909.000		
	GR	465.700	1948.000	464.700	1974.000	464.600	2028.000	464.800	2037.000	464.300	2055.000		
(D) 20	GR	464.500	2069.000	464.400	2131.000	464.900	2151.000	465.000	2215.000	465.100	2247.000		13
	GR	470.000	2626.000	470.000	2748.000	470.300	2367.000	470.700 470.800	2419.000 2934.000	470.000 471.000	2470.000 3003.000		
27	GR	471.100	3038.000	470.700	3071.000	470.700	3137.000	470.800	3176.000	470.700	3216.000		
(7n	GR	470.300	3263.000	469.600	3326.000	469.300	3347.000	469.800	3382.000	470.100	3488.000		
и	GR	471.500	3551.000	474.200	3563.000	474.200	3586.000	473.700	3590.000	474.800	3606.000		la constitución
25	GR	473.000	3620.000	474.600	3645.000	486,600	3683.000	486.600	3710.000	485.000	3726.000		
26	GR	480.700	3756.000	476.900	3798.000	474.900	3826.000	472.800	3885.000	472.700	3965.000		. 0
77	GR	472.900	4063.000	474.000	4125.000	475.400	4146.000	476.000	4163.000	474.800	4186.000		13 (N
70	GR	473.400	4237.000	472.800	4301.000	472.800	4345.000	473.600	4370.000	473.200	4417.000		Vasa
(D) 77	GR	472.800	4472.000	472.000	4503.000	471.800	4554.000	470.200	4640.000	469.700	4768.000		00
30	GR	470.100	4852.000	469.500	4902.000	463.300	4937.000	465.400	4952.000	460.500	4961.000		78
21	GR	460.000	4962.000	460.000	5046.000	460.000	5128.000	460.500	5129.000	463.100	5133.000		21
W 12	GR	474.600	5148.000	495.300	5182.000	499.200	5208.000	500.600	5378.000	512.500	5551.000		0
*E	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1630.000	5148.000		17
25	× 1	12 200			• •	100 000	105 000	115 000					23
- 14	X3	13.200	0.0	0.0	0.0	100.000	195.000	115.000	0.0	0.0	0.0		74
97	NC	0.050	0.0	0.0	0.0	0.0	0.0	0.0	469.000	0.0	0.0		
(D) 12	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1620.000	4976.000		D'
39			EREN NAMES	1982, 540		7.100			7.0	1020.000	47.0.000		24
6	X1	14.000	95.000	4717.000	4967.000	20.000	720.000	635.000	0.0	0.0	0.0		
9 10	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	469.000	0.0	0.0		
47	GR	485.000	1.000	471.200	1094.000	470.800	1227.000	469.300	1325.000	466.900	1405.000		23
43	GR	465.500	1423.000	466.600	1445.000	466.900	1466.000	465.700	1482.000	465.500	1512.000		39
(3 14)	GR	466.100	1558.000	466.100	1617.000	466.200	1678.000	466.000	1741.000	466.200	1796.000		0
45	GR	465.400	1876.000	465.200	1935.000	464.900	1960.000	464.700	1996.000	464.100	2010.000		38
19.00	GR	464.300	2026.000	464.300	2087.000	464.600	2149.000	464.800	2197.000	465.700	2551.000		n
13/41	GR	468.300	2269.000	470.400	2315.000	470.500	2387.000	470.200	2428.000	469.900	2522.000		
- ETS	GR	469.800	2629.000	469.900	2748.000	470.100	2826.000	470.600	2919.000	470.700	2993.000		11
1000	GR	470.700	3028.000	471.000	3108.000	470.600	3174.000	470.300	3274.000	469.500	3385.000		n n
51	GR GR	471.500	3450.000	472.000	3530.000	474.600	3545.000	474.600	3570.000	473.800	3577.000		
57	GR	474.600	3585.000 3709.000	473.100	3599.000	474.500	3612.000	476.400	3633.000	487.600	3658.000		, ş
£ 51	GR	471.000	4019.000	479.200 472.600	3737.000	474.400 474.100	3800.000	472.200	3865.000	471.100	3939.000		35 8
54	GR	473.100	4238.000	474.400	4103.000		4139.000	475.800	4169.000	473.400	4199.000		11
35 (GR	472.900	4496.000	471.800	4284.000 4541.000	474.700	4317.000 4642.000	474.400	4370.000	474.200 465.500	4424.000 4717.000		
9 11	GR	464.900	4722.000	460.700	4730.000	456.000	4739.000	456.000	4824.000	456.000	4893.000		17 60 9
9/	GR	460.800	4913.000	463.400	4923.000	465.700	4967.000	466.500	5035.000	475.200	5062.000		35
16	GR	490.400	5097.000	488.200	5113.000	491.200	5140.000	489.200	5154.000	488.000	5172.000		
(1) to	68	500.800	5194.000	508.900	5234.000	510.000	5273.000	511.500	5284.000	511.500	5310.000		0
CONTRACTOR OF STREET	GR	512.500	5364.000	512.900	5492.000	512,900	5562.000	509.700	5599.000	513.300	5668.000		

	10.0												
6	NC	0.060	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	7	O PARKSIA
0	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1545.000	4621.000		0
	X1	16.010	00 000	4430 000									
6	X3	10.000	90.000	4430.000	4621.000	44.000	714.000	684.000	0.0	0.0	0.0		
	GR	485.000	1.000	471.300	1070.000	0.0 470.900	0.0	0.0	474.000	480.700	0.0		OI
	GR	466.200	1395.000	468.700	1411.000	466.600	1175.000	469.100 465.300	1287.000	466.200	1367.000		
	GR	467.100	1475.000	467.400	1506.000	466.900	1533.000	466.900	1438.000 1589.000	467.000	1454.000		0
	GR	465.700	1801.000	465.900	1870.000	466.100	1901.000	465.400	1921.000	466.200 464.700	1664.000		1 4 劉
	GR	464.700	1974.000	466.400	1995.000	469.300	2034.000	469.900	2110.000	469.700	2150.000		
• 4	GR	468.700	2196.000	469.500	2223.000	470.200	2257.000	470.500	2323.000	470.200	2360.000		0
	GR	470.100	2440.000	469.600	2538.000	469.600	2634.000	469.800	2765.000	470.000	2842.000		
	GR	470.906	2914.000	471.400	2955.000	471.700	3098.000	472.400	3244.000	471.500	3306.000		
	GR GR	471.000	3370.000	471.500	3425.000	471.006	3454.000	471.500	3473.000	472.600	3492.000		
10	GR	475.300 476.100	3521.000	475.300	3547.000	475.300	3700.000	475.200	4053.000	476.100	4073.000		
_ n.	GR	471.000	4143.000	479.600 469.300	4198.000	485.200	4243,000	485.500	4261.000	475.200	4299.000		
11	GR	458.000	4538.000	458.000	4392.000 4621.000	465.000 461.200	4425.000	461.200	4428.000	458.000	4430.000		•
13	GR	466.000	4741.000	466.500	4800.000	471.800	4636.000 4883.000	463.200	4643.000	465.400	4661.000		1
. 14	GR	477.200	5119.000	477.200	5138.000	480.500	5197.000	482.700	4957.000 5262.000	475.500	5038.000		1
15	GR	479.700	5308.000	482.100	5350.000	484.800	5472.000	489.600	5509.000	482.200 501.000	5286.000 5543.000		10
16	GR	506.400	5565.000	506,600	5667.000	505.400	5694.000	505.700	5707,000	510.700	5730.000		4"
• "	GR	512.000	5784.000	512.600	5847.000	514.000	5887.000	515.500	5954.000	517.700	6033.000		11
18	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1645.000	4721.000		12
201	X1	16.020	02 000	4530 000						10.70 16.6			1.
71	X3	10.000	92.000	4530.000	4721.000	10.000	10.000	10.000	0.0	0.0	0.0		"•)
n	RT	12.000	4115.000	494.600	0.0 494.600	0.0	0.0	0.0	474.000	0.0	0.0		IN .
12	BT	4210.000	493.100	493.100	4530.000	4115,000 488,500	494.600	491.500	4210.000	493.100	490.000		15
74	BT	487.100	483.300	4624.000	487.100	487.100	4627.000	4530.000 487.000	488.500 487.000	484.600	4624.000		19
15	BT	483.200	4721.000	485.700	481.800	4721.000	. 485.700	485.700	0.0	4627.000	487.000		14
(→ ²⁴	GR	485.000	1.000	471.300	1070.000	470.900	1175.000	469.100	1287.000	466.200	0.0 1367.000		17
n	GR	466.200	1396.000	468.700	1411.000	466.600	1427.000	465.300	1438.000	467.000	1454.000		E 2
26	GR	467.100	1475.000	467.400	1506.000	466.900	1533.000	466.900	1589.000	466.200	1664.000		, 15 F1
•	GR	465.700	1801.000	465.900	1870.000	466.100	1901.000	465.400	1921.000	464.700	1939.000		10 A
	GR GR	464.700	1974.000	466.400	1995.000	469.300	2034.000	469.900	2110.000	469.700	2150.000		70
	GR	468.700	2196.000	469.500	2223.000	470.200	2257.000	470.500	2323.000	470.200	2360.000		
33	GR	470.900	2440.000	469.600 471.400	2538.000	469.600	2634.000	469.800	2765.000	470.000	2842.000		•
	GR	471.000	3370.000	471.500	2955.000 3425.000	471.700 471.000	3098.000	472.400	3244,000	471.500	3306.000		72
6 15	GR	475.800	3521.000	475.300	3547.000	472.300	3454.000 3578.000	471.500 472.300	3473.000	472.600	3492.000		B .
14	GR	481.000	3691.000	493.700	3769.000	494.900	3795.000	495.400	3653.000 3872.000	477.100 496.100	3669.000 3993.000		
37	GR	495.200	4096.000	494.600	4115.000	475.400	4115.000	475.400	4210.000	493.100	4210.000		
• 12	GR	488.500	4530.000	458.000	4530.000	458.000	4624.000	487.100	4624.000	487.000	4627.000		25
39	GR	458.000	4627.000	458.000	4721.000	485.700	4721.000	484.600	4849.000	484.300	5134.000		20
40	GR	484.100	5192.000	480.900	5241.000	481.200	5272.000	482.900	5353.000	484.700	5440.000		
•	GR GR	489.200	5463.000	501.300	5520.000	504.100	5560.000	505.700	5599.000	504.000	5619.000		
a l	GR	504.000 516.000	5639.000	510.400	5658.000	513.800	5793.000	514.000	5879.000	515,200	5940.000		A
4	GR	520.500	5965.000 6232.000	516.000	5982.000	516.500	6021.000	517.500	6114.000	518.600	6156.000		79
45	ET	0.0	0.0	525.100	6325.000	0.0	0.0	0.0	0.0	0.0	0.0		9
46			•	V. V	0.0	9.100	0.0	0.0	0.0	1645.000	4721.000		30
→ 0	X1	16.030	0.0	0.0	0.0	76.000	76.000	76.000	0.0	0 0	0 0		31
46	XS	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0		, ,
41	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.000	0.0	0.0		1 2
● 50	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1545.000	4621.000		33
4							/						34
N/L W	X1	16.040	90.000	4430.000	4621.000	10.000	10.000	10.000	0.0	0.0	0.0		Ugro
	X3 GR	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.200	480.900	0.0		92
55	GR	485.000	1.000	471.300	1070.000	470.900	1175.000	469.100	1287.000	466.200	1367.000		24 . 1
	GR	466.200	1396.000	468,700	1411.000	466.600	1427.000	465.300	1438.000	467.000	1454.000		27 . 7
37	GR	465.700	1475.000	467.400	1506.000	466.900	1533.000	466.900	1589.000	466.200	1664.000		9
и	GR	464.700	1974.000	465.900	1870.000	466.100	1901.000	465.400	1921.000	464.700	1939.000		30
6	GR	468.700	2196.000	469.500	1995.000	469.300 470.200	2034.000	469.900	2110.000	469.700	2150.000		27
	GR	470.100	2440.000	469.600	2538.000	469.600	2257.000 2634.000	470.500	2323.000	470.200	2360.000		
	***	* M & M M M M M M M	A STATE OF THE STA		2000,000	107.000	7034.000	469.800	2765.000	470,000	2842.000	√ ,	

	GR	470.900	2914.000	471.400	2955.000	471.700	3098,000	472.400	3244.000	471.500	3306.000		
	GR	471.000	3370.000	471.500	3425.000	471.000	3454.000	471.500	3473.000	472.600	3492.000	8	
	GR	475.300	3521.000	475.300	3547.000	475.300	3700.000	475.200	4053.000	476.100	4073.000		
	GR	476.100	4143.000	479.600	4198.000	485.200	4243.000	485.500	4261.000	475.200	4299.000		
	GR	471.000	4344.000	469.300	4392.000	465,000	4425.000	461.200	4428.000	458.000	4430.000		
	GR	458.000	4538.000	458.000	4621.000	461.200	4636.000	463.200	4643.000	465.400	4661.000		
1	GR	466.000	4741.000	466.500	4800.000	471.800	4883.000	473.300	4957.000	475,500	5038.000		
0 2	GR	477.200	5119.000	477.200	5138.000	480,500	5197.000	482.700	5262.000	482.200	5286.000		101
	GR	479.700	5308.000	482.100	5350.000	484.800	5472.000	489.600	5509.000	501.000	5543.000		
4	GR	506.400	5565.000	506.600	5667.000	505.400	5694.000	505.700	5707.000	510,700	5730.000		
	GR	512.000	5784.000	512.600	5847.000	514.000	5887.000	515.500	5954.000	517.700	6033.000		'
	NC	0.060	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0			
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1585.000	0.0		
								0.0	0.0	1363.000	4661.000		150
	X1	16.000	95.000	4392.000	4661.000	60.000	60.000	60.000	0.0	0.0	0.0		
Solito III	хз	10.000	0.0	0.0	0.0	0.0	0.0						
	GR	485.000	1.000	471.300	1070.000	470.900	1175.000	0.0 469.100	474.200 1287.000	0.0	0.0		7
	GR	466.200	1396.000	468.700	1411.000	466.600	1427.000	465.300		466.200	1367.000		
11	GR	467.100	1475.000	467.400	1506.000	466.900			1438.000	467.000	1454.000		
	GR	465.700	1801.000				1533.000	466.900	1589.000	466.200	1664.000		
15	GR	464.700	1974.000	465.900	1870.000	466.100	1901.000	465.400	1921.000	464.700	1939.000		
	GR	468.700			1995.000	469.300	2034.000	469.900	2110.000	469.700	2150.000		14
	GR		2196.000	469.500	2223.000	470.200	2257.000	470.500	2323.000	470.200	2360.000		U.
	GR	470.100 470.900	2440.000	469.600 471.400	2538.000	469.600	2634.000	469.800	2765.000	470.000	2842.000		•
			PRODUCTION OF THE PROPERTY OF		2955.000	471.700	3098.000	472.400	3244.000	471.500	3306.000		17
	GR	471.000	3370.000	471.500	3425.000	471.000	3454.000	471.500	3473.000	472.600	3492.000		u i
	GR	475.300	3521.000	475.300	3547.000	472.300	3578.000	472.300	3653.000	471.600	3743.000		
		470.500	3832.000	469.800	3914.000	469.700	3993.000	475.200	4053.000	476.100	4073.000		14
	GR	476.100	4143.000	479.600	4198.000	485.200	4243.000	485.500	4261.000	475.200	4299.000		
•	GR	471.000	4344.000	469.300	4392.000	465.000	4425.000	461.200	4436.000	459.000	4442.000		•
4	GR	459.000	4538.000	459.000	4628.000	461.200	4636.000	463.200	4642.000	465.400	4661.000		la
25	GR	466.000	4741.000	466.500	4800.000	471.800	4883.000	473.300	4957.000	475.500	5038.000		
\$ 26	GR	477.200	5119.000	477.200	5138.000	480.500	5197.000	482.700	5262.000	482.200	5286.000		● pg
11	GR	479.700	5308.000	482.100	5350.000	484.800	5472.000	489.600	5509.000	501.000	5543.000		18 2
11	GR	506.400	5565.000	506.600	5667.000	505.400	5694.000	505.700	5707.000	510.700	5730.000		20 A
9 7	GR	512.000	5784.000	512.600	5847.000	514.000	5887.000	515.500	5954.000	517.700	6033.000		0 0
30	F7	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000		20
31													
12	X1	18.010	67.000	3984.000	4154.000	758.000	678.000	738.000	0.0	0.0	0.0		
23	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.600	472.200	0.0		22
34	GR	485.000	1.000	471.300	1039.000	470.700	1095.000	470.200	1179.000	469.900	1234.000		297
● :35	EB	468.300	1317.000	468.400	1424.000	467.100	1467.000	467.500	1517.000	470.800	1551.000		•
4.	GR	473.300	1572.000	474.700	1629.000	473.700	1688.000	472.800	1758.000	469.900	1811.000		24
37	GR	468,900	1872.000	. 468.700	1949.000	468.500	2033.000	468.800	2162.000	468.700	2264.000		
9 .4	GR	468.800	2343.000	469.700	2393.000	470.600	2480.000	471.100	2582.000	471.200	2724.000		•
39	GR	471.500	2851.000	471.900	2953.000	472.000	3003.000	472.100	3043.000	472.100	3083.000		25
40	GR	472.100	3100.000	472.200	3111.000	471.000	3243.000	470.700	3362.000	470.400	3504.000		
	GR	470.300	3632.000	471.100	3700.000	472.600	3780.000	474.700	3849.000	478.500	3894.000		•
4	GR	478.500	3917.000	465.900	3984.000	465.900	3984.000	459.000	4001.000	459.000	4038.000		25
43	GR	459.000	4033.000	459.000	4042.000	459.000	4042.000	459.000	4096.000	459.000	4096.000		
10,11	GR	459.000	4100.000	459.000	4100.000	459.000	4145.000	464.300	4154.000	464.300	4154.000		(0)
45	GR	473.500	4200.000	473.500	4221.000	473.100	4257.000	473.300	4299.000	474.500	4359.000		30
46	GR	479.700	4396.000	484.100	4432.000	486.700	4446.000	491.600	4485.000	499.600	4508.000	and the second s	
1941	GR	512.900	4530.000	525.000	4556.000	0.0	0.0	0.0	0.0	0.0	0.0		•
42	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000		0 8
41						200				1,75.000	1131000		
(€ ,056	X1	18.020	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0		•
- 43	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.600	0.0	0.0		11
- 17	BT	18.000	3917.000	478.500	478.500	3984.000	478.800	465.900	3984.000	478.800	474.000		- Car
(0.51	BT	4001.000	478.900	474.000	4038.000	479.000	474.000						
34	BT	479.000	459.000	4042.000	479.000	475.500	4096.000	4038.000	479.000	459.000	4042.000		
35 🖟	BT	459.000	4100,000	479.300	459.000	4100.000		479.300	475.500	4096.000	479.300		
600	BT	4154.000	479.500				479.300	474.000	4145.000	479.500	474.000		
9	PT	474.300		474.000	4154.000	479.500	464.300	4200.000	475,000	473.500	4221.000		
9	FT		473.500	4257.000	473.100	473.100	0.0	0.0	0.0	0.0	0.0		
(and		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000		
	X1	18.030	0 0	0.0	. \.	27 000	27 000						
Manage of the last	-	10,000	0.0	0.0	0.0	27.000	27.000		0.0	0.0	0.0		

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FT 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	9			474.700								X3	
X1				0.0									
X3	•	4154.000	1490.000	0.0	0.0	0.0	9.100	0.0	0.0	0.0	0.0	ΕT	
X3		0.0	0.0	0.0	10.000	10.000	10-000	0.0	0.0	0.0	18.040	XI	
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GP 470,300 3632,000 471,100 3700,000 472,600 3784,000 474,700 3844,000 478,500 3917,000 465,900 3984,000 459,000 4094,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 4096,000 459,000 474,500 464,300 4154,000 474,500 484,000 473,500 4299,000 474,500 484,000 474,500 489,600 488,000 499,600 45	- A							BOOK STATE OF THE BOOK STATE OF THE STATE OF					13
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GR	18												18
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X1 19.000 80.000 4140.000 4525.000 1750.000 1500.000 1283.000 0.0				THE SAN THE SAN THE PROPERTY OF THE PROPERTY O		0.0	9.100	0.0	0.0	0.0	0.0	FT.	27
X3 10.000 0.	•		444.334						. 186,665				● 23
GR	14	0.0	0.0	0.0	1283.000	1500.000	AND COMPANY OF THE PROPERTY OF						28
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GR 474.200 1870.000 474.200 1991.000 474.400 2084.000 474.800 2248.000 474.800 2447.000 6R 473.200 2622.000 471.600 2660.000 472.600 7758.000 473.400 2821.000 471.600 2850.000 7758.000 473.400 2821.000 471.600 2850.000 7758.000 473.400 2821.000 471.600 2850.000 7758.000 472.100 3324.000 472.000 3274.000 7758.000 472.400 3349.000 472.100 3566.000 472.600 3610.000 474.800 3689.000 475.700 3772.000 6R 476.500 3867.000 478.000 3975.000 479.000 4096.000 470.000 410.000 474.900 4162.000 474.9	18 X	It was not a separate of the second of the s										ASSESSMENT OF THE PROPERTY.	44
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GR 476.500 3867.000 478.000 3975.000 479.000 4096.000 479.000 4140.000 474.900 4162.000 GR 470.700 4174.000 465.600 4187.000 465.500 4317.000 462.100 4199.000 462.100 4252.000 GR 462.100 4309.000 462.500 4310.000 465.000 4317.000 465.900 4327.000 465.500 4349.000 GR 462.500 4360.000 462.100 4361.000 462.100 4370.000 462.100 4370.000 465.500 4349.000 GR 462.800 4392.000 462.500 4401.000 460.700 4447.000 460.700 4447.000 460.700 477.000 GR 462.500 4884.000 465.000 4495.000 473.700 4525.000 473.800 4588.000 474.700 4607.000 GR 475.900 4641.000 476.900 4687.000 473.700 4525.000 473.800 4588.000 474.700 4607.000 GR 475.400 4779.000 477.200 4804.000 477.700 4823.000 485.200 4866.000 491.200 4889.000 GR 491.200 4906.000 500.200 4916.000 510.000 4932.000 517.200 4949.000 526.200 4972.000 FT 0.0 0.0 0.0 0.0 0.0 0.0 9.100 0.0 0.0 0.0 0.0 0.0 0.0 0.0 X1 19.100 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	n = 1												1937
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GR 475.400 4779.000 477.200 4804.000 477.700 4823.000 485.200 4866.000 491.200 4889.000 GR 491.200 4906.000 500.200 4916.000 510.000 4932.000 517.200 4949.000 526.200 4972.000 FT 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	а									4641.000	475.900		29
FT 0.0 0.0 0.0 0.0 9.100 0.0 0.0 0.0 0.0 3291.000 X1 19.100 0.0 0.0 0.0 0.0 750.000 800.000 805.000 0.650 1.200 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0			491.200	4866.000	485.200	4823,000	477.700	4804.000	477.200	4779.000	475.400		40
X1 19.100 0.0 0.0 0.0 750.000 800.000 0.650 1.200 0.0 0.0 X3 10.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0						4932.000							€41
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GR 490.700 1306.000 487.000 1348.000 486.600 1371.000 485.200 1383.000 483.700 1410.000 GR 479.700 1450.000 477.800 1570.000 477.400 1622.000 478.600 1663.000 480.500 1730.000	20												9 58
GR 479.700 1450.000 477.800 1570.000 477.400 1622.000 478.600 1663.000 480.500 1730.000	и												a a
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GR 479.100 2029.000 479.700 2094.000 480.400 2181.000 480.200 2240.000 480.200 2269.000	W.											GR	51
GR 480.300 2360.000 480.500 2458.000 480.500 2521.000 480.500 2578.000 480.800 2649.000	. 3										480.300		55
GR 480.100 2719.000 479.300 2793.000 477.800 2858.000 477.100 2935.000 477.700 2976.000	1.0								479.300	2719.000			266
GR 480.500 2998.000 475.700 3049.000 465.200 3067.000 463.200 3076.000 461.400 3084.000	33 3			3076.000									51
GR 461.400 3142.000 461.400 3197.000 463.200 3211.000 464.600 3222.000 469.800 3257.000	7					3211.000							
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GR 482.500 3469.000 485.900 3495.000 489.700 3527.000 497.300 3564.000 498.500 3587.000		3587.000	498.500	3564.000	497.300	3527.000	489.700	3495.000	485.900	3469.000	482.500	GR	

	GR	500.100	3596.000	514.500	3619.000	525.600	3641.000	0.0	0.0	0.0	0.0	
	NC	0.070	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	10
	ET	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	
	X1	21.000	54.000	2225.000	2592.000	600.000	600.000	525.000	0.0	0.0	0.0	•
	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	GR	523.900	1000.000	524.000	1050.000	523.700	1124.000	523.400	1182.000	520.100	1223.000	/3
D ,	GR	517.900	1244.000	510.600	1277.000	500.700	1302.000	498.600	1315.000	494.800	1342.000	/ • 5
	GR	490.500	1354.000	489.700	1398.000	488.800	1439.000	485.200	1462.000	483.500	1543.000	1 3
	GR	482.900	1650.000	482.900	1713.000	482.700	1744.000	482.200	1846.000	481.800	1953.000	
	GR	481.000	2033.000	480.100	2077.000	479.600	2111.000	479.000	2174.000	480.100	5505.000	
1	GR	480.300	2225.000	475.500	2236.000	465.400	2247.000	463.800	2257.000	462.800	2263.000	4
	GR	462.800	2314.000	462.800	2360.000	463.800	2376.000	464.800	2391.000	464.900	2414.000	
	GR	467.500	2443.000	472.300	2481.000	474.000	2527.000	477.700	2592.000	477.700	2673.000	
9	GR	478.700	2712.000	478.900	2734.000	479.400	2778.000	481.100	2819.000	482,800	2855.000	·
W 10	GR	489.600	2889.000	493.800	2931.000	499.400	2966.000	499.400	3006.000	500.200	3046.000	1-
9 n	GR	501.500	3106.000	505.500	3138.000	515.200	3177.000	525.300	3203.000	0.0	0.0	
12	NC	0.0	0.0	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0	
13 18	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1299.000	1575.000	'•
15	X1	23.010	39.000	1299.000	1497.000	600.000	455.000	445.000	0.0	0.0	0.0	
16	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	488.000	481.500	0.0	n_
11	GR	542.800	1000.000	542.100	1020.000	540.000	1060.000	536.900	1119.000	526.400	1139.000	
18	GR	520.500	1169.000	512.700	1198.000	510.400	1225.000	500.600	1267.000	490.800	1283.000 1353.000	organization and " " " " " " " " " " " " " " " " " " "
19	GR	480.200	1299.000	471.500	1318.000	466.200	1324.000	464.200	1331.000	458.300	1516.000	8.
23	GR	458.300	1416.000	458.300	1442.000	464.200	1488.000	455.300	1497.000	473.500 482.800	1764.000	
21	GR	479.100	1569.000	480.100	1593.000	482.300	1647.000	482.700 483.800	1720.000 2001.000	484.200	2075.000	
v	GR	482.800	1788.000	483.000	1876.000	483.200	1943.000	498.000	2235.000	499.860	2250.000	15
n n	GR	484.600	2124.000	488.600	2164.000	491.000	2205.000		2437.000	0.0	0.0	
14	GR	505.200	2286.000	514.900	2330.000	524,200 131,000	2390,000 5,000	525.000 4200.000	1.200	459.000	459.000	
75	SB	0.900	1.500	2.600	0.0	9.100	0.0	0.0	0.0	1299.000	1575.000	10 m
1/	C)	0.0	0.0									18 25
29	X1	23.020	0.0	0.0	0.0	30.000	30.000	30.000	0.0	0.0	0.0	11
(C) 21	XS	0.0	0.0	1.000	485.000	482.500	0.0	0.0	0.0	0.0	0.0	
30	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	489.000	482.500	0.0	
31	BT	6.000	1285.000	489.000	0.0	1590.000	488.000	0.0	1720.000	482.500	0.0	21
n () n	BT	1940.000	483.000	0.0	2120.000	484.500	0.0	2200.000	491.000	0.0	0.0	, O
33	NC	0.070	0.080	0.035	0.300	0.500	0.0	0.0	0.0	0.0	0.0	
# 1 35	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1299.000	1575.000	" \$
36	X1	23.000	39.000	1299.000	1569.000	55.000	55.000	55.000	0.0	0.0	0.0	24
y.	GR	542.800	1000.000	542.100	1020.000	540.000	1060.000	536.900	1119.000	526.400	1139.000	В
19 18	GR	520.500	1169.000	512.700	1198.000	510.400	1225.000	500.600	1267.000	490.800	1283.000	•
39	GR	480.200	1299.000	471.500	1318.000	466.200	1324.000	464.200	1331.000	458.300	1353.000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
46	GR	458.300	1416.000	458.300	1442.000	464.200	1488.000	465.300	1497.000	473.500	1516.000	u 🔏
(*) 41	GR	479.100	1569.000	480.100	1593.000	482.300	1647.000	482.700	1720.000	482.800	1764.000	· ·
42	GR	482.800	1788.000	483.000	1876.000	483.200	1943.000	483.800	2001.000	484.200	2075.000	
- 13	GR	484.600	2124.000	488.600	2164.000	491.000	2205.000	498.000	2235.000	499.800	2250.000	n a
100	GR	505.200	2286.000	514.900	2330.000	524.200	2390.000	525.000	2437.000	0.0	0.0	.0
45	NC	0.070	0.080	0.035	.0.100	0.300	0.0	0.0	0.0	0.0	0.0	
• 0	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1239.000	1472.000	30
45	X1	24.000	46.000	1239.000	1472.000	380.000	280.000	370.000	0.0	0.0	0.0	
49	GR	549.400	1000.000	549.600	1016.000	556.500	1046.000	. 564.400	1097.000	569.200	1128.000	, and the second of the second
● 56	GR	573.800	1148.000	570.700	1166.000	559.900	1185.000	550.700	1205.000	525.200	1216.000	•
51	GR	499.600	1227.000	487.000	1239.000	486.300	1248.000	473.700	1259.000	470.000	1267.000	#
57	GR	465.200	1279.000	462.800	1285.000	462.800	1346.000	462.800	1405.000	465.200	1416.000	. и 2
(P)53		467.300	1426.000	470.000	1446.000	474.900	1472.000	475.900	1500.000	479.800	1539.000	0
я	GR	483.100	1598.000	483.100	1639.000	483.900	1689.000	484.200	1745.000	484.000	1789.000	14
55	GR	484.100	1808.000	484.200	1845.000	484.200	1874.000	484.400	1906.000	484.400	1970.000	91 . 9
9 16	GR	484.600	2032.000	484.600	2121.000	484.900	2167.000	485.800	2550.000	485.800	2240.000	•
57	GR.	489.400	2260.000	492.300	2326.000	497.100	2358.000	509.000	2394.000	515.300	2415.000	
. 51	GR	525.100	2445.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	19
(P)51	NC	0.080	0.080	0.035	0.500	0.700	0.0	0.0	0.0	0.0	0.0	•
	EL	0.0	0.0	0.0	0.0	9,100	0.0	0.0	0.0	1365.000	1890,000	

				Control of the second									
9	Xl	25.000	44.000	1394.000	1624.000	920.000	250.000	750.000	0.0	0.0	0.0	- 11	•
	GR	574.600	1000.000	550.300	1035,000	525.000	1066.000	499.800	1094.000	488.300	1116.000		
	SP	488.300	1132.000	486.300	1144.000	479.700	1164.000	477.500	1180.000	477.600	1256.000		
	GR	479.300	1278.000	476.500	1316.000	475.700	1377.000	474.700	1394.000	469.200	1401.000		1
	GR	467.000	1413.000	465.200	1423.000	465.200	1470.000	465.200	1515.000	467.000	1521.000		
	6R	469.700	1530.000	473.200	1557.000	475.200	1610.000	477.800	1624.000	478.000	1803.000		1
	GR	478.000	1817.000	474.000	1830.000	474.000	1895.000	480.700	1924.000	480.700	1936.000		(0) 8
	GR	482.400	1979.000	483.100	2085,000	484.100	2160.000	484.200	2273.000	484.400	2372.000		7 7
	GR	484.400	2410.000	484.800	2460.000	486.600	2476.000	486.600	2492.000	491.700	2511.000		
	6R FT	493.000	2528.000	500.100	2549.000	511.500	2573.000	524.900	2599.000	0.0	0.0		(4)
		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1445.000	1940.000		4
	×1	26.000	44.000	1462.000	1634.000	440.000	450.000	450 000		W. T. C. (2000)			3.
	SR	525.000	1000.000	514.300	1038.000	514.000		450.000	0.0	0.0	0.0		
	6R	504.700	1113.000	502.200	1125.000	502.200	1058.000	507.300 495.300	1077.000	507.300	1099.000		
	GR	490.500	1206.000	484.800	1216.000	484.200	1245.000	481.800	1286.000	491.600 483.000	1185.000 1324.000		1
	GR	485.500	1339.000	486.700	1398.000	487.000	1408.000	484.200	1420.000	480.900	1438.000		
	GR	475.800	1462.000	472.100	1469.000	468.000	1479.000	465.500	1485.000	465.500	1530.000		
● (84)	SP	465.500	1561.000	468.000	1584.000	469.400	1596.000	474.100	1613.000	477.200	1634.000		'o .
	GR	477.600	1817.000	475.300	1833.000	474.000	1850.000	474.000	1910.000	475.300	1919.000		16
	GR	484.300	2003.000	484.400	2046.000	484.600	2120.000	489.400	2154.000	489.400	2173.000		
	GR	490.000	2183.000	500.000	2202.000	509.900	2220.000	524.300	2253.000	0.0	0.0		
	NC	0.0	0.0	0.0	0.100	0.300	0.0	0.0	0.0	0.0	0.0		12
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	1830.000		12
		27 200				407.73							
	X1	27.000	34.000	1602.000	1830.000	600.000	325.000	540.000	0.0	0.0	0.0		14
•	GR.	521.000	1000.000	521.000	1016.000	517.300	1033.000	505.100	1071.000	499.100	1099.000		15
	GP	498.700 485.900	1135.000	492.600	1173.000	487.400	1235.000	487.500	1267.000	487.500	1306.000		
	GR	475.300	1320.000	476.600	1337.000	476.600	1474.000	476.000	1514.000	475.700	1561.000	sample in the second state of the second state	18
	SP.	467.800	1719.000	473.700 467.800	1621.000 1791.000	469.800 468.900	1633.000	468.900	1641.000	467.800	1652.000		17
	GR	480.400	1858.000	482.300	1879.000	484.200	1798.000	470.500 485.700	1808.000 1913.000	474.900	1830.000		-/19
20	GR	489.600	1940.000	499.500	1967.000	513.100	1989.000	525.100	2012.000	485.700 0.0	1932.000		
•	NC	0.080	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		17 6
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1780.000	2100.000		
				1000000	108 5 660	47. No. 10. No. 1	1185,565	A COLUMN TO		4.0 12 1, 1/10/05			
•	X1	28.000	38.000	1877.000	2095.000	915.000	950.000	940.000	0.0	0.0	0.0		"•)
2	GR	525.100	1000.000	516.600	1051.000	506.500	1080.000	499.900	1107.000	496.200	1147.000		n = 1
36	GR	493.000	1199.000	490.400	1226.000	490.400	1245.000	490.400	1258.000	490.100	1323.000		
	GP	488.700	1365.000	485.700	1397.000	499.400	1416.000	502.300	1444.000	505.800	1484.000		
	GR	510.700	1542.000	515.700	1586.000	515.000	1604.000	500.500	1661.000	500.000	1678.000		14
	GR CS	481.000	1716.000	477.700	1747.000	474.900	1804.000	472.500	1835.000	475.500	1877.000		75
	GR GR	472.700	1921.000	471.200	1943.000	470.500	1951.000	468.500	1974.000	468.500	2004.000		
	6P	485.700	2044.000	470.500	2056.000	471.900	2065.000	475.500	2076.000	485.700	2095.000		76
	NC	0.080	0.080	500.500 0.035	2124.000	524.900	2140.000	0.0	0.0	0.0	0.0		77.
-6	ET	0.0	0.0	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
400				0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		
	X1	29.000	46.000	2154.000	2293.000	730.000	800.000	790.000	0.0	0.0	0.0		25
	GP	529.700	1000.000	525.700	1032.000	521.900	1062.000	520.100	1100.000	517.100	1157.000		39
160	GR	514.800	1212.000	496.000	1246.000	496.000	1258.000	500.800	1282.000	490.800	1311.000		
•	GR	490.800	1324.000	484.600	1337.000	484.200	1375.000	485.300	1420.000	485.000	1460.000		"•)
	GR	485.500	1478.000	484.900	1493.000	485.500	1512.000	482.200	1538.000	478.700	1599.000		32 - 2
40.5	GP	478.600	1658.000	481.200	1707.000	481.500	1758.000	480.600	1787.000	478.200	1839.000		*
•	GR	477.000	1908.000	476.600	2020.000	476.600	2073.000	474.400	2092.000	475.100	2119.000		10
	6B	474.800	2154.000	473.100	2171.000	472.000	2185.000	470.100	2208.000	470.100	2232.000		я "
	GR	470.100	2281.000	472.000	2288,000	473.100	2293.000	480.400	2306.000	488.300	2323.000		Jare 1
	GR	488.500	2338.000	499.400	2355.000	512.700	2369.000	524.400	2382.000	535.400	2400.000		9)2
	GR	549.700	2418.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		36
	EI	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		17 . 2
-	X]	30.000	34 000	1000 000	2221 222	250 200							9
3	6R	524.800	36.000	1923.000	2321.000	350.000	420.000	410.000	0.0	0.0	0.0		
	GR	494.600	1000.000	521.400 490.600	1090.000	512.600	1188.000	499.000	1228.000	497.700	1257.000		79.
-Files	GR	478.000	1518.000	482.700	1310.000	490.200	1329.000	485.800	1370.000	482.000	1431.000		V
		710000	1310.000	702.100	1633.000	480,100	1694.000	477.900	1751,000	481.300	1799.000		

	GR	481.900	1859.000	482.000	1923.000	480,500	1967.000	476.800	2013.000	475.600	2057.000	40	
	GR	474.000	2099.000	473.900	2119.000	475.200	2159.000	475.500	2181.000	474.400	2201.000	12	
	GR	474.000	2210.000	471.000	2246.000	474.000	2281.000	475.000	2296.000	496.300	2321.000		
	GR	496.300	2339.000	497.100	2345.000	500.200	2348.000	524.400	2370.000	541.200	2389.000		
	GR	550.700	2407.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		•
	NC					0.500	0.0	0.0	0.0	0.0	0.0		
F	NC	0.0	0.0	0.0	0.300	0,300	0.0	. 0.0	0.0		0.0		3
	XI	31.000	49,000	1765.000	2007.000	310.000	620,000	575.000	0.0	0.0	0.0		(A) 100 M
	GR	524.500	1000.000	520.500	1080.000	513.100	1145.000	501.200	1188.000	500.000	1227.000		7 2
	GR	497.300	1254.000	491.700	1284.000	490.800	1306.000	485.600	1353.000	481.800	1385.000		
	GR	478.800	1447.000	480.200	1485.000	482.200	1537.000	481.600	1635.000	481.400	1716.000		36
	GR			474.900	1789.000	474.900	1805.000	475.400	1816.000	476.600	1628.000		
	GR	480.200	1765.000	475.100	1865.000	472.900	1906.000	472.900	1918.000	472.900	1943.000		
9	GR	475.800	1852.000		1985.000	480.900	2007.000	480.900	2046.000	480.500	2095.000		66
3		475.100	1972.000	476.100					2265.000	486.100	2309.000		
1	GR	478.700	2135.000	480.500	2160.000	481.600	2203.000	484.300		476.100	2433.000		
	GR	487.000	2334.000	485.400	2354.000	483.200	2384.000	478.700	2423.000				16
	GR	477.400	2443.000	480,200	2466.000	486.100	2488.000	487.900	2499.000	487.900	2518.000		
u u	GR	489.800	2524.000	500.300	2536.000	524.500	2566.000	550.000	2604.000	0.0	0.0	ANGELIN PROPERTY.	
	NC	0.0	0:070	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0		3
, i	X1	32,000	53.000	1313.000	1427.000	770.000	350.000	630.000	0.0	0.0	0.0		in
io E	GR GR	524.900	1000.000	518.300	1055.000	514.200	1111.000	505.100	1157.000	501.000	1198.000		
	GR	499.900		499.000		499.400	1240.000	502.200	1250.000	492.300	1273.000		17
U	GR	492.300	1207.000	486.200	1222.000	478.300	1313.000	474.500	1323.000	470.800	1333.000		12
10	Service against Reported that the		1280.000					CONTRACTOR OF THE PROPERTY OF	1427.000	480.800	1459.000		
	GR GR	470.800	1367.000	470.800	1407.000	474.500	1418.000 1552.000	477.600 480.800	1563.000	482.900	1580.000		13
		482.200	1506.000	481.900	1526.000	481.100	1694.000	485.800	1721.000	485.400	1746.000		14
AL.	GR	483.500	1608.000	483.900	1640.000	485.400				488.500	1846.000		
•	GR	483.900	1769.000	481.900	1788.000	481.600	1799.000	485.600	1814.000 1987.000	482.400	2006.000		
	GR	486.200	1860.000	485.300	1910.000	483.900	1969.000	480.400 479.200	2099.000	480.500	2121.000		u de
5		482.400	2023.000	480.300	2042.006	495.200		499.700	2219.000	515.000	2242.000		
	GP	482.100	2158.000	494.600	2187.000		2210.000			0.0	0.0		17
200	GR	529.600	2263.000	539.000	2289.000	550.700	2318.000	0.0	0.0	0.0	0.0		18 20
27	NC	0.0	. 0.0	0.0	0.100	0.300	0.0	0.0	0.0	1280.000	2246.000		WE SE
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1280.000	2240.000		16 AB
30	×1	33.000	57.000	1403.000	1581.000	475.000	175.000	380.000	0.0	0.0	0.0		20
31	6R	526.200	1000.000	516.800	1063.000	511.800	1111.000	503.200	1151.000	499.100	1193.000		
9 12	GR	491.700	1208.000	491.700	1227.000	485.700	1248.000	480.700	1258.000	483.100	1269.000		
33	GR	483.500	1298.000	483.500	1337.000	482.500	1353.000	482.200	1387.000	480.200	1403.000		22
34	GR	476.800	1408.000	475.200	1416.000	469.000	1446.000	469.000	1480.000	469.000	1500.000		
1 15 15	GR	475.200	1553.000	476.600	1565.000	480.400	1581.000	482.400	1607.000	482.300	1630.000		•
	GR	481.900	1649.000	485.400	1683.000	485.800	1718.000	486.000	1813.000	485.800	1831.000		74
w.F	GR	484.200	1856.000	482.900	1873.000	483.000	1891.000	485.800	1904.000	488.400	1931.000		
Ø3, 33	GR	485.900	1955.000	484.900	1969.000	484.700	1985.000	483.100	1999.000	480.900	2028.000		
	GR	481.700	2059.000	480.800	2082.000	480.300	2114.000	480.000	2131.000	482.300	2157.000		24
49	GR	480.700	2175.000	484.900	2198.000	484.900	2222.000	485.500	2277.000	485.700	2320.000		
9 941	GR	485.900	2342.000	496.900	2370.000	497.000	2396.000	499.200	2407.000	524.100	2440.000		
41	GR	535.100	2466.000	550.700	2509.000	0.0	0.0	0.0	0.0	0.0	0.0		28
af	NC	0.0	0.060	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
919.42	FT.	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		
6				1.0									N
44	×1	34.000	50.000	1764.000	1977.000	250.000	525.000	480.000	0.0	0.0	0.0		31_
● 0.47	GR	530.400	1000.000	526.400	1071.000	522,900	1129.000	514.500	1170.000	500.600	1189.000		
- 41	GR	497.200	1218.000	499.900	1229.000	492.300	1250.000	492.300	1274.000	484.100	1290.000		11
44	GR	480.700	1301.000	482.600	1320.000	483.600	1389.000	483.700	1468.000	483.500	1540.000		
● 2 50	GR	483.900	1566.000	480.800	1586.000	480.600	1604.000	484.200	1616.000	483.600	1649.000		•
51	GR	483.900	1689.000	484.200	1720.000	484,200	1747.000	483.900	1764.000	480.700	1782.000		34
	GR	477.000	1793.000	475.400	1797.000	475.400	1864.000	475.400	1932.000	477.000	1938.000		larco
● 453	GR	479.100	1945.000	486.100	1962.000	488.500	1977.000	486.800	1985.000	486.600	2010.000		9 9
54	GR	484.800	2021.000	485.100	2047.000	485.500	2078.000	486.300	2130.000	486.600	2211.000		N. A.
55	GR	487.100	2243.000	490.500	2270.000	490.500	2288.000	494.100	2299.000	504.700	2321.000		77 6
(Fa 56	GR	505.300	2341.000	509.000	2356.000	525.100	2379.000	535.500	2397.000	550.000	2428.000		91
51	OT	5.000	24300.000	45700.000	58500.000	58500.000	102000.000	0.0	0.0	0.0	0.0		18
58	NC-	0.080	0.060	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		11-
(Plan	FT	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		9
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* X3 10.000 0.0 0.0 0.0 0.0 0.0	
* X3 10.000 0.0 0.0 0.0 0.0 0.0	0.0 2629.000 3130.000
	0.0 2629.000 3130.000
16 0.049 0.000 0.009 0.000 0.00 0.0	0.0 2629.000 3130.000
* FT 0.0 0.0 0.0 0.0 9.100 0.0 0.0	0.0 2629.000 3130.000 0.0 0.0 0.0 494.100 532.000 0.0
•	0.0 2629.000 3130.000 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0
×1 38.000 22.000 2265.000 2624.000 65.000 75.000 100.0	0.0 2629.000 3130.000 0.0 0.0 0.0 494.100 532.000 0.0
GR 520.000 2200.000 495.500 2265.000 495.500 2265.000 490.6	0.0 2629.000 3130.000 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000
• GR 479.400 2328.000 477.500 2337.000 476.500 2342.000 476.5	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 2265.000 2630.000
9 GR 477.500 2585.000 479.000 2589.000 480.100 2593.000 482.9	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 481.600 2322.000 0.0 2473.000 476.500 2582.000
GR 499.200 2650.000 512.400 2678.000 509.200 2702.000 514.8	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 481.600 2322.000 0.0 2473.000 476.500 2582.000 0.0 2605.000 486.600 2624.000
GR 534.200 2752.000 549.400 2775.000 0.0 0.0 0.0	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 481.600 2322.000 0.0 2473.000 476.500 2582.000 0.0 2605.000 486.600 2624.000
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• X1 39.000 39.000 2151.000 2391.000 200.000 150.000 315.0	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 481.500 2322.000 0.0 2473.000 476.500 2582.000 0.0 2605.000 486.600 2624.000 0.0 2713.000 524.800 2735.000
7 X1 39.000 39.000 2151.000 2391.000 200.000 150.000 315.0 6R 520.000 1960.000 490.000 2035.000 486.500 2090.000 486.9	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 481.600 2322.000 0.0 2473.000 476.500 2582.000 0.0 2605.000 486.600 2624.000 0.0 2713.000 524.800 2735.000 0.0 0.0 0.0 0.0 0.0 2151.000 2850.000
GR 487.100 2169.000 483.700 2191.000 479.500 2203.000 479.0	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 481.600 2322.000 0.0 2473.000 486.600 2582.000 0.0 2605.000 486.600 2624.000 0.0 2713.000 524.800 2735.000 0.0 0.0 0.0 0.0 0.0 2151.000 2850.000
GR 478.500 2271.000 478.500 2335.000 479.000 2337.000 480.4	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 491.600 2322.000 0.0 2473.000 476.500 2582.000 0.0 2605.000 486.600 2624.000 0.0 2713.000 524.800 2735.000 0.0 0.0 0.0 0.0 0.0 2151.000 2850.000
GR 485.500 2391.000 484.800 2432.000 484.300 2455.000 483.5	0.0 2629.000 3130.000 0.0 0.0 0.0 0.0 494.100 532.000 0.0 0.0 0.0 0.0 0.0 0.0 2265.000 2630.000 0.0 2300.000 481.600 2322.000 0.0 2473.000 476.500 2582.000 0.0 2605.000 486.600 2624.000 0.0 2713.000 524.800 2735.000 0.0 0.0 0.0 0.0 0.0 2122.000 489.200 2151.000

												continuent Consention of the Consent Consent	and the second
- 1	GR	484.400	2618.000	483.800	2677.000	483,200	2717.000	481.100	2739.000	478.400	2747.000	14	
	GR	477.600	2749.000	477.600	2776.000	477.600	2800.000	478.400	2803.000	479.600	2809.000	! -	
	GR	485.900	2837.000	499.300	2863.000	514.700	2890.000	513.000	2913.000	516.100	2917.000		
	GR	520.500	2931.000	530.400	2952.000	539.600	2974.000	549.400	2991.000	0.0	0.0		6
•	QT	5.000	24300.000	45700.000	.58500.000	48800.000	102000.000	0.0	0.0	0.0	0.0		
	NC	0.0	0.045	0.0	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1780.000	2465.000		· ·
9 7			10 TO 40 1676	1005 000	2072 000	415.000	380.000	410.000	0.0	0.0	0.0		1 141
4	X1	40.000	49.000	1905.000	2072.000	487.900	1725.000	488.100	1732.000	488.100	1732.000		
	GR	520.000	1405.000	490.000	1851.000	485.800	1905.000	484.300	1916.000	480.200	1930.000		
	GR GR	487.700	1786.000	478.600	1942.000	478.600	1986.000	478.600	2035.000	479.300	2042.000		4
	GR	480.200	2051.000	485.400	2072.000	487.300	2114.000	486.900	2181.000	487.100	2249.000		
	GR	487.400	2346.000	488.100	2415.000	487.700	2506.000	486.500	2583.000	486.000	2710.000		•
	GR	485.400	2829.000	485.300	2882.000	486.300	2933.000	485.200	2991.000	484.500	3032.000		
10 to	GR	485.800	3096.000	486.800	3128.000	485.400	3152.000	481.100	3165.000	479.500	3173.000		
• 1 n	GR	478.900	3176.000	478.900	3208.000	478.900	3240.000	479.500	3244.000	480.300	3248.000		•
12	GR	489.300	3259.000	500.800	3273.000	519.800	3292.000	521.000	3301.000	521.000	3319.000	THE ARMS THE TAXABLE PROPERTY.	
13	GR	523.000	3328.000	531.200	3341.000	540.100	3359.000	549.600	3371.000	0.0	0.0		2
● 11.24	OT	5.000	24300.000	45700.000	58500.000	48800.000	102000.000	0.0	0.0	0.0	0.0		15
15	NC	0.045	0.045	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
16	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1525.000	2730.000		11
O WH	ONG			1004 000	2006 000	470 000	300 000	460 000	0.0	0.0	0.0		12
19	XI	41.000	57.000	1904.000	2096.000	470.000	390.000 1500.000	460.000	1654.000	492.400	1740.000		
A 20 -	GR	510.000	1250.000	495.000	1856.000	485.800	1875.000	485.100	1904.000	483.700	1921.000		13
V ** 8	GR GR	489.500	1928.000	488.200 479.400	1932.000	478.800	1934.000	478.800	1998.000	478.800	2058.000		14
	GR	479.400	2063.000	480.300	2071.000	490.000	2096.000	485.700	2114.000	487.000	2130.000		15
02n	GR	487.500	2214.000	488.700	2298.000	488.100	2367.000	488.000	2423.000	485.800	2583.000		•
76	GR	488.000	2712.000	498.700	2835.000	488.500	2925.000	488.100	3009.000	487.600	3108.000		16 18
25	GR	487.000	3185,000	485.300	3220.000	486.400	3256.000	486.900	3343.000	486.600	3432.000		172
11 26	GR	486.300	3552.000	486.600	3637.000	486.600	3705.000	487.200	3801.000	487.200	3839.000		• m
η	GR	487.500	3861.000	484.600	3876.000	482.000	3886.000	478.800	3897.000	478.000	3899.000		18 19
18	GR	478.000	3923.000	478.000	3942.000	478.800	3946.000	480.100	3953.000	490.200	3974.000		1 2
€# B	GR	502.100	3995.000	520.900	4011.000	520.900	4027.000	522.000	4036.000	527.300	4047.000		. 0
10	GR	537.600	4068.000	551.200	4087.000	0.0	0.0	0.0	0.0	0.0	0.0		
35	NC	0.0	0.0	0.042	0.500	0.700	0.0	0.0	0.0	0.0	0.0		27
●10 I2	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	2760.000		n
33	CASE C	0.075.0404		1055 . 222	2125 000	100 000	250 000	250.000	0.0	0.0	0.0		
94 (************************************	X1	42.010	37.000	1955.000	2125.000	100.000	250.000 1042.000	509.800	1053.000	505.400	1073.000		•
A 20 B	GR GR	511.600	1000.000	511.800 494.000	1027.000 1113.000	510.800	1125.000	494.000	1145.000	494.000	1218.000		21
l vil	GR	492.600	1100.000	494.000	1413.000	494.000	1543.000	494.700	1582.000	495.200	1640.000		
Ø 75 v	GR	495.400	1695.000	495.700	1771.000	495.800	1815.000	482.200	1955.000	482.200	1955.000		•
35	GR	484.200	1988.000	477.000	2073.000	479.200	2106.000	479.200	2106.000	494.600	2125.000		24
40	GR	492.000	2400.000	490.000	2905.000	492.500	3330.000	490.000	3570.000	485.000	3580.000		11,
(4) 4)	GR	481.900	3585.000	481.900	3640.000	484.000	3690.000	485.000	3785.000	490.000	3860.000		•
47	GR	500.000	3980.000	520.200	4005.000	0.0	0.0	0.0	0.0	0.0	0.0		
6	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	2760.000		79
● 20 24		and a property							This said	977 346	4-1-24-1		•
6	X1	42.020	37.000	1955.000	2106.000	25.000	25.000	25.000	0.0	0.0	0.0		
46	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	492.500	491.900	0.0		11
♦ 47.4)	GR	511.600	1000.000	511.800	1027.000	510.800	1042.000	509.800	1053.000	505.400	1073.000		32 2
9	GR	492.600	1100.000	494.000	1113.000	494.000	1125.000	494.000	1145.000	494.000	1218.000		
49	GR	494.000	1308.000	494.000	1413.000	494.000	1543.000	494.700	1582,000	495.200	1640.000 1955.000		
Q 50 35	GR	495.400	1695.000	495.700	1771.000	495.800	1815.000	482.200	1955.000	494.600	2125.000		и
10	GR	484.200	1988.000	477.000	2073.000	479.200	2106.000	479.200	3570.000	485.000	3580.000		986
21	GR	492.000	2400.000	490.000	2905.000	492.500	3690.000	485.000	3785.000	490.000	3860.000		* DE 10
	GR GR	481.900	3585.000	520.200	3640.000 4005.000	0.0	0.0	0.0	0.0	0.0	0.0		35
		500.000	3980.000	0.0	0.0	9.100	v.0	0.0	0.0	1490.000	2760.000		17 9
€ 54.56	ET SB	0.0	1.500	2.500	6.0	151.000	0.0	1786.000	0.0	0.0	0.0		10
s	36	0.0	1.300	2.300	0.0	209,889		1000	1440,535	1000			13
58	X1	42.100	0.0	0.0	0.0	25.000	25.000	25.000	0.0	0.0	0.0		n
	X2	0.0	0.0	1.000	493,000	492.000	0.0	0.0	0.0	0.0	0.0		•
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	492,600	492,000	0.0		

	Anneal or the Control of the Control												
	RT	34.000	1000.000	511.600	0.0	1027.000	511.800	0.0	1042.000	510.800	0.0	15	
	BT	1053.000	509.800	0.0	1073.000	505.400	0.0	1100.000	492.600	0.0	1113.000	10	
	BT	494.000	0.0	1125.000	494.000	0.0	1145.000	494.000	0.0	1218.000	. 494.000		
	BT	0.0	1308.000	494.000	0.0	1413.000	494.000	0.0	1543.000	494.000	0.0		
•	BT	1582.000	494.700	0.0	1640.000	495.200	0.0	1695.000	495.400	0.0	1771.000		•
	BT	495.700	0.0	1815.000	495.800	0.0	1955.000	496.000	482.200	1955.000	496.000		
100	RT	493.000	2106.000	494.900	491.900	2106.000	494.900	479.200	2125.000	494.600	0.0		
	BT	2400.000	492.000	0.0	2905.000	490.000	0.0	3330.000	492.500	0.0	3570.000		10
	BT			3580.000									
		490.000	0.0		485.000	0.0	3585.000	481.900	0.0	3640.000	481.900		
	BT	0.0	3690.000	484.000	0.0	3785.000	485.000	0.0	3860.000	490.000	0.0		
	RT	3980.000	500.000	0.0	4005.000	520.200	0.0	0.0	0.0	0.0	0.0		
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	2760.000		
									54.51				300
•	X1	42.200	37.000	1955.000	2125.000	50.000	50.000	50.000	0.0	0.0	0.0		
	GR	511.600	1000.000	511.800	1027.000	510.800	1042.000	509.800	1053.000	505.400	1073.000		
10	GR	492.600	1100.000	494.000	1113.000	494.000	1125.000	494.000	1145.000	494.000	1218.000		1
6)11	GR	494.000	1308.000	494.000	1413.000	494.000	1543.000	494.700	1582.000	495.200	1640.000		
17	GR	495.400	1695.000	495.700	1771.000	495.800	1815.000	482.200	1955.000	482.200	1955.000		
0	GR	484.200	1988.000	477.000	2073.000	479.200	2106.000	479.200	2106.000	494.600	2125.000		
▼ 14	GR	492.000	2400.000	490.000	2905.000	492.500	3330.000	490.000	3570.000	485.000	3580.000		
15	GR	481.900	3585.000	481.900	3640.000	484.000	3690.000	485.000	3785.000	490.000	3960.000		10
16	GR	500.000	3980.000	520.200	4005.000	0.0	0.0	0.0	0.0	0.0	0.0		
₩ ¥ tr	NC	0.050	0.045	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		1.20
18	OT	5.000	24300.000	45700.000	58500.000	48800.000	102000.000	0.0	0.0	0.0	0.0		
191	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1520.000	2980.000		
9 26		A 10 (9 (9 ())		4 17 4 17									
21	X.1	43.000	59.000	2146.000	2442.000	230.000	230.000	230.000	0.0	0.0	0.0		и
21	GR	509.500	1000.000	509.500	1010.000	508,500	1023.000	504.600	1043.000	506.700	1064.000		
● 473	GR	509.500	1073.000	509.500	1098.000	507.200	1108.000	500.400	1124.000	492.800	1159.000		13
75-	GR	492.900	1183.000	493.300	1263.000	493.700	1324.000	493.900	1384.000	493.700	1463.000		16
25	GR	493.700	1535.000	493.100	1607.000	493.500	1677.000	493.900	1744.000	494.100	1829.000		
0716	GR	493.400	1902.000	492.900	1937.000	493.600	1965.000	493.100	2011.000	487.000	2023.000		17
27	GR	487.000	2059.000	486.500	2085.000	484.800	2112.000	486.900	2138.000	486.900	2146.000		10 19
28	GR	484.500	2159.000	482.800	2202.000	481,600	2217.000	481.000	2224.000	481.000	2279.000		READ ON A
● 1.94	GR	481.000	2333.000	481.700	2335.000	484.300	2342.000	485.200	2373.000	486.300	2419.000		* · · · · · · · · · · · · · · · · · · ·
	GR	487.500	2442.000	487.400	2468.000	487.200	2475.000	490.000	3020.000	493.000	3040.000		20
	GR	493.000	3065.000	490.000	3085.000	488.000	3150.000	486.500	3550.000	485.000	4030.000		
(Day)	GR	482.500	4085.000	482.500	4115.000	485.000	4135.000	490.000	4400.000	495.000	4450.000		11 🕶
	GR	505.000	4475.000	507.000	4480.000	507.000	4495.000	510.000	4510.000	0.0	0.0		11
	QT	6.000	20000.000	38000.000	48800.000	48800.000	87000.000	0.0	0.0	0.0	0.0		
9	NC									0.0	0.0		23
		0.0	0.050	0.0	0.600	0.800	0.0	0.0	0.0				24
, .	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1495.000	2540.000	•	
● 131					2255 222	275 000	700 000	() 5 000					25 👡
	XI	44.000	61.000	2114.000	2355.000	275.000	700.000	415.000	0.0	0.0	0.0		76
	GR	507.800	1000.000	507.800	1013.000	506.700	1024.000	503.100	1050.000	506.200	1065.000		
•	GR	507.800	1073.000	507.800	1098.000	507.000	1112.000	491.000	1149.000	492.000	1163.000		27
	GR	495.200	1190.000	495.400	1277.000	495.700	1342.000	495.700	1407.000	495.800	1518.000		
	GR	496.200	1596.000	495.600	1649.000	493.900	1711.000	493.300	1807.000	493.600	1875.000		
43	GR	494.600	1933.000	495.300	1974.000	495.300	2008.000	495.500	2064.000	494.700	2088.000		76
***	GR	494.900	2088.000	488.900	2114.000	485.600	2141.000	483.400	2160.000	482.000	2173.000		10
	GR	480.600	2186.000	480.600	2231.000	480.600	2259.000	482.006	2288.000	482.700	2303.000		
- 44	GR	482.000	2312.000	481.500	2319.000	481.500	2321.000	481.500	2330.000	482.000	2332.000		B 👞)
Air.	GR	483.700	2337.000	490.300	2355.000	490.900	2403.000	491.200	2491.000	491.700	2570.000		J.
- 45	GR	492.700	2611.000	494.200	2623.000	495.300	2635.000	495.300	2661.000	495.700	2682.000		
- 67	GR	498.300	2703,000	498.300	2731.000	501.300	2759.000	501.300	2803.000	506.500	2828.000		131 2 1
₽8 ₉	GR	509.100	2860.000	522.000	2881.000	511.300	2921.000	512.200	2970.000	513.500	3010.000		10
51	GR	525.200	3031.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		H .
ii .	NC	0.0	0.095	0.0	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
P ₅₃	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1780.000	2674.000		0
54 8 a	X1	45.000	40.000	2431.000	2674.000	395.000	425.000	420.000	0.0	0.0	0.0		
	GR	535.200	1000.000	520.700	1031.000	509.200	1060.000	506.500	1065.000	506.500	1305.000		7
9	GR	506.500	1386.000	506.500	1411.000	505.600	1422.000	492.300	1461.000	493.300	1495.000		23. 2
9	GR	495.400	1536.000	495.800	1608.000	495.900	1701.000	496.100	1790.000	495.800	1874.000		
· ()								495.500					31
	GR	495.500	1931.000	494.600	1985.000	495.200	2040.000		2113.000	495.700	2201.000		
	GR	496.100	2318.000	496,100	2379.000	495,800	2431.000	493,500	2444.000	487.800	2463.000		

	GR	485.200	2470.000	483.000	2478.000	481,500	2483.000	481,500	2545.000	481,500	2602.000	16	
•	GR	483.000	2608.000	484.000	2612.000	486.300	2631.000	489.300	2652.000	499.4.00	2674.000	IO	0)
	GR	505.400	2683.000	505.400	2704.000	516.200	2729.000	525.800	2773.000	531.500	2851.000		
	NC	0.040	0.100	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
•	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1645.000	2560.000		•
	X1	46,000	35.000	2374.000	2560.000	530.000	570.000	565.000	0.0	0.0	0.0		1 8
	GR	535.200	1000.000	504.600	1085.000	504.500	1342.000	500.900	1358.000	495.600	1405.000		() 3
	GR	495.700	1470.000	496.100	1522.000	496.200	1626.000	496.400	1725.000	496.500	1805.000		2 2
	entropy and the second section of the second	496.800	1866.000	496.300	1935.000	495.600	1993.000	494.700	2102.000	493.800	2187.000		
	GR GR	492.700		491.700	2321.000	490.600	2374.000	488.700	2391.000	484.700	2399.000		•
	GR		2255.000	482.200	2433.000	482.200	2467.000	482.200	2503.000	483.800	2530.000		1
		483.800	2411.000		2553.000	490.300	2560.000	497.800	2581.000	497.800	2592.000		
	GR	484.100	2535.000	488.100	2633.000	520.200	2638.000	529.900	2651.000	535.200	2660.000		•
	GR	519.200	2611.000	519.200	0.100	0.300	0.0	0.0	0.0	0.0	0.0		08 6 8
	NC	0.060	0.100	0.042	0.100	9.100	0.0	0.0	0.0	1570.000	2350.000		
•	FT	0.0	0.0	0.0	0.0	9.100	0.0			13/0.000			•
12	X1	47.000	48.000	2160.000	2327.000	325.000	660.000	630.000	0.0	0.0	0.0		
13	GR	535.200	1000.000	520,500	1031.000	510.000	1055.000	503.800	1072.000	503.800	1200.000		1
- 6 14 14	GR	503.800	1282.000	501.800	1298.000	497.200	1317.000	497.200	1364.000	497.100	1434.000		•
13	GR	497.000	1519.000	496.700	1600.000	496.800	1680.000	496.100	1749.000	495.600	1835.000		10
14	GR	495.000	1913.000	494.100	1940.000	491.300	1997.000	485.800	2010.000	485.200	2018.000		11_
● 11 17	GR	484.900	2022.000	484.900	2024.000	484.900	2027.000	485.200	2031.000	486.900	2051.000	specification in the	
	GR	488.600	2071.000	490.900	2095.000	489.200	2124.000	487.900	2160.000	485.500	2191.000	Of Toursell St.	12
19	GR	485.300	2203.000	484.900	2212.000	484.000	2234,000	484.000	2250.000	484.000	2283.000		
●A 20	GR	484.900	2296.000	485.900	2310.000	492.300	2327.000	491.500	2344.000	488.000	2359.000		
21	GR	484.600	2382.000	485.900	2400.000	492.400	2418.000	498.300	2440.000	498.300	2460.000		
27	GR	521.300	2480.000	521.300	2509.000	535.500	2528.000	0.0	0.0	0.0	0.0		
● 7421	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1580.000	2175.000		•
24	X1	48.000	38.000	1994.000	2172.000	570,000	620.000	610.000	0.0	0.0	0.0		
Ana	GR	535.400	1000.000	526.200	1021.000	512.500	1049.000	503.500	1067.000	503.500	1279.000		
	GR	501.400	1289.000	497.800	1313.000	499.000	1354.000	498.300	1397.000	498.100	1479.000		18 64
	GR	498.600	1563.000	496.700	1625.000	494.100	1704.000	492.300	1767.000	492,500	1843.000		
● 19.00	GR	491.900	1871.000	487.500	1893.000	488.000	1914.000	487.400	1928.000	489.400	1942.000		990
	GR	491.600	1969.000	489.900	1994.000	487.900	2001.000	486.800	2009.000	486.000	2014.000		20
	GR	486.000	2076.000	486.000	2133.000	486.800	2138.000	488.200	2148.000	489.100	2172.000		
●n n	GR	496.600	2190.000	497.000	2211.000	499.500	2219.000	514.200	2234.000	530.900	2251.000		0
	GR	530.900	2266.000	531.700	2276.000	534.700	2284.000	0.0	0.0	0.0	0.0		n
	FT		0.0	0.0	0.0	15.400	0.0	0.0	0.0	0.0	0.0		
9 39 35		0.0	0.0	0.0	0.0	13.400	ÿ . 0						0
14	X1	49.000	40.000	1781.000	1998.000	549.000	555.000	555.000	0.0	0.0	0.0		A
17	GR	534.700	1000.000	520.300	1028.000	503.900	1069.000	503.900	1100.000	503.900	1200.000		25
935 35	GR	503.900	1294.000	503.900	1315.000	501.200	1333.000	497.600	1361.000	494.000	1378.000		0
31	GR	492.400	1401.000	492.000	1455.000	491.100	1482.000	491.300	1510.000	495.300	1522.000		10
40	GR	495.800	1532.000	495.200	1544.000	491.900	1557.000	489.800	1571.000	491.000	1593.000		27
((1) (a)	GR	491.900	1635.000	492.900	1695.000	494.700	1739.000	493.000	1781.000	491.100	1810.000		0
47	GR	488.500	1835.000	487.000	1846.000	486.300	1850.000	486.300	1913.000	486.300	1974.000		16
45	GR	487.000	1978.000	488.100	1985.000	492.600	1998.000	499.200	2015.000	499.200	2034.000		n
9 60, 64	GR	514.300	2061.000	514.500	2081.000	516.100	2099.000	524.800	2122.000	535.300	2179.000		"0
- 45	NC	0.080	0.095	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		3) •
45	ET	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		31
0.0					2122 222	430 000	460 000	465.000	0.0	0.0	0.0		32
48	X1	50.000	32.000	1987.000	2190.000	420.000	468.000			505.500	1500.000		
49	GR	525.000	1555.000	505.500	1262.000	505.500	1300.000	505.500	1400.000	490.000	1813.000		11
50 35	GR	505.500	1675.000	505.000	1680.000	495.000	1703.000	494.000	1778.000		1948.000		34
51	GR	487.000	1828.000	487.000	1848.000	490.000	1869.000	492.600	1910.000	492.100			
57	GR	492.800	1968.000	490.200	1987.000	488.900	2020.000	488.400	2043.000	487.500	2059.000		35
21 52	GR	486.200	2081.000	486.200	2106.000	486.200	2150.000	487.500	2155.000	489.100	2163.000		34
50	GR	491.000	2190.000	500.800	2218.000	500.800	2233.000	522.100	2258.000	522.100	2276.000		
55	GR	535.000	2292.000	550.900	2310.000	0.0	0.0	0.0	0.0	0.0	0.0		"0
27	EJ	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		31
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****** SEPT 1971 VERSION. UPDATED JUNE 1974 * THIS PROGRAM IS OWNED BY THE UNITED STATES GOVERNMENT * AND IS USED BY PERMISSION OF THE CORPS OF ENGINEERS. FRROR CORRECTIONS 01 THRU 09R2 * DEPARTMENT OF THE ARMY. MODIFICATIONS 52 THRU 58 * THE PROGRAM HAS BEEN REVISED BY MICHAEL BAKER, JR., INC. * MBJ UPDATED 07/20/76 0830 * ONLY AS REQUIRED FOR USE ON THEIR COMPUTER AND EXECUTES * * CORRECTLY THE STANDARD TEST SERIES AS PUBLISHED BY THE * TODAYS DATE IS 03/01/77 18.13 * CORPS OF ENGINEERS. HYDROLOGIC ENGINEERING CENTER. ******************************** 2.857 SECONDS TI SUSQUEHANNA RIVER BASIN COMMISSION TP DI DOMCDIDO-DEDUTCK-CHTCKCHTNNY REACH T3 FISHING CREEK 10 YEAR FLOOD IDIR STRT METRIC HVINS WSEL FQ TCHECK TNO NTNV JI 0.0 499.023 0.0 0. 0.0 0.0 0. Michael Baker, Jr., Inc. CHNIM ITRACE NPROF TPI OT PREVS XSECV **XSECH** FN ALLDC IBW 2763 N. Fourth St. -1.000 0.0 0.0 0.0 0.0 0.0 1.000 0.0 0.0 0.0 Box 3225 27,000 28.000 9.000 0.0 0.0 0.0 Harrisburg, Pa. 17105 **j3** 1.000 34.000 3.000 4.000 0.0 20000.000 48800.000 87000.000 0.0 0.0 0.0 OT 5.000 38000.000 48800.000 0.095 0.100 0.300 0.0 0.0 0.0 0.0 0.039 0.0 NIC 0.080 0.0 0.0 0.0 10.400 0.0 0.0 FT 0.0 0.0 0.0 0.0 2190.000 420.000 468.000 465.000 0.0 0.0 0.0 X1 50.000 32.000 1987.000 1262,000 1400.000 505.500 1500.000 GP 525.000 1222.000 505.500 505.500 1300.000 505.500 1778.000 490.000 1813.000 GR 505.500 1675.000 505.000 1680.000 495.000 1703.000 494.000 492.100 1948.000 GR 487.000 1828.000 487.000 1848.000 490.000 1869.000 492.600 1910.000 2059.000 GR 492.800 1968.000 490.200 1987.000 488.900 2020.000 488.400 2043.000 487.500 486.200 2106.000 486.200 2150.000 487.500 2155.000 489.100 2163.000 CD 486.200 2081.000 500.800 2233.000 522.100 2258.000 522.100 2276.000 GR 491.000 2190.000 500.800 2218.000 0.0 0.0 0.0 GR 550.900 2310.000 0.0 0.0 0.0 535.000 2292.000 NH 1657.000 0.055 1914.000 0.036 2052.000 0.095 2234.000 0.0 4.000 0.085 205.000 225.000 0.0 0.0 0.0 X1 51.000 34.000 1914.000 2052.000 230.000 1024.000 506.000 1039.000 506.000 1300.000 506.000 1633.000 GR 535.000 1000.000 521,200 GR 504.100 1670,000 495.300 1691.000 493.100 1711.000 492.700 1744.000 506.000 1657.000 GR 490.200 1779.000 491.500 1801.000 490.200 1823.000 490.300 1759.000 488.400 1766.000 488.500 1935.000 488.000 1963.000 490.100 1914.000 GR 490.200 1848.000 490.300 1876.000 492.500 2098.000 GR 2042.000 490.000 2052.000 492.500 2078.000 486.100 2003.000 488.000 516.000 2185.000 500.700 516.000 2168.000 GR 491.100 2112.000 500.700 2134.000 2146.000 535.100 2212.000 550.000 2234.000 0.0 0.0 GP 518.900 2190.000 527.400 2200.000 0.0 0.0 0.0 NC 0.060 0.060 0.060 0.100 0.500 0.0 0.0 2421.000 2297.000 0.085 0.0 NH 4.000 0.085 1925.000 0.060 2051.000 0.036 FT 0.0 0.0 9.400 0.0 0.0 0.0 0.0 0.0 0.0 0.0 X1 29.000 2051.000 2297.000 223.000 217.000 225.000 0.0 0.0 0.0 52.000 506.500 1925.000 GP 535.400 1000.000 525.800 1042.000 510.000 1064.000 506.500 1073.000 2017.000 491.200 2032.000 GR 505.800 494.900 1963.000 493.300 1982.000 492.400 1937.000 2091.000 489.300 2101.000 GR 490.100 2085.000 489.800 492.800 491.100 2068.000 2051.000 492.300 2253.000 2238.000 GR 489.300 489.300 2232.000 489.800 2234.000 490.900 2164.000 512.100 2347.000 501.900 2314.000 501.900 2328.000 GR 492.900 2278.000 497.900 2297.000 GP 2379.000 535.400 2398.000 550.200 2421.000 0.0 0.0 512.100 2365.000 524.400 0.700 0.0 0.0 0.0 0.060 0.100 0.0 0.0 NC 0.060 0.060 0.0 0.0 0.0 FT 0.0 0.0 0.0 4.400 0.0 0.0 0.0 0.085 0.050 2147.000 0.080 2265.000 0.0 NH 4.000 1897.000 1952.000 0.036

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		MARKET AND										ACTION OF THE PARTY OF THE PART
	GR	495.000	1952.000	489.600	1971.000	489.600	2136.000	495.000	2147.000	500.000	2177.000	18
•	GR	505.000	2217.000	509.000	2227.000	509.000	2246.000	510.000	2247.000	515.000	2248.000	. •
	GR	520.000	2255.000	525.000	2265.000	0.0	0.0	0.0	0.0	0.0	0.0	
	NH	4.000	0.085	2057.000	0.040	2107.000	0.036	2309.000	0.070	2466.000	0.0	6
•	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	0
, I	Xì	53,000	27.000	2107.000	2309.000	298.000	252,000	275.000	0.0	0.0	0.0	
	GR	550.100	1000.000	524.900	1019.000	508.400	1030.000	508.400	1080.000	508.400	2000.000	
	GR	508.400	2035.000	508.400	2057.000	507.500	2068.000	504.400	2084.000	501.200	2107.000	1,
	GR	492.500	2125.000	491.000	2131.000	489.900	2135.000	489.900	2206.000	489.900	2270.000	1.0
6	GR	491.000	2276.000	492.200	2283.000	500.400	2309.000	501.600	2330.000	502.700	2351.000	•
	GR	502.700	2358.000	506.300	2374.000	506.300	2393.000	509.100	2400.000	525.300	2419.000	4
, F	GR	534.100	2437.000	549.900	2466.000	0.0	0.0	0.0	0.0	0.0	0.0	
0	NH	4.000	0.100	2088.000	0.050	2148.000	0.038	2343.000	0.080	2520.000	0.0	0
9				10 (15 . 15 . 15 . 15 . 15 . 15 . 15 . 15	CONTROL CONTROL					994,490	100000000000000000000000000000000000000	··
to.	X1	54.000	56.000	2146.000	2343.000	813.000	797.000	805.000	0.0	0.0	0.0	1
0111	GR	549.800	1000.000	526.300	1013.000	512.600	1028.000	512.300	1029.000	512.300	2088.000	•
R.	GR	510.800	2097.000	507.700	2117.000	504.900	2148.000	495.600	2156.000	493.500	2163.000	
13	GR	491.500	2169.000	491.500	2239.000	491.500	2312.000	493.500	2317.000	495.800	2323.000	1
€ 16	GR	502,300	2343.000	505.000	2368.000	505.700	2383.000	505.700	2396.000	514.400	2409.000	
15	GR	514.400	2426.000	524.300	2454.000	527.000	2467.000	535.200	2483.000	544.600	2507.000	
li.	GR	550.100	2520.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	H _C
1 38	NC	0.050	0.055	0.030	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
18	NH	4.000	0.085	1802.000	0.040	1848.000	0.036	2043.000	0.070	2229.000	0.0	"
19		EE 000	20 000	1949 000	2043.000	659.000	662,000	655.000	0.0	0.0	0.0	13
	X1	55.000	29.000	1848.000 525.800	1014.000	513.800	1028.000	513.800	1100.000	513.800	1500.000	и
"[GR	550.000	1771.000	513.800	1802.000	512.500	1812.000	507.300	1831.000	504.100	1848.000	
A 2	GR	513.800		497.000	1868.000	495.300	1875.000	491.800	1889.000	491.800	1947.000	, B
		497.600	1863.000			496.900	2026.000	502.700	2043.000	504.700	2068.000	14
	GR GR	491.800	2013.000	495.300 505.500	2022.000	508.600	2135.000	508.500	2146.000	515.100	2157.000	
•	GR	505.500	2094.000	526.000	2197.000	537.300	2209.000	549.900	2229.000	0.0	0.0	
4	NC	526.000		0.030	0.100	0.300	0.0	0.0	0.0	0.0	0.0	10
28	NH	0.055 4.000	0.095	1645.000	0.100	1668.000	0.036	1865.000	0.070	2218.000	0.0	10
1 1/2		4.000	0.003	1040-000	, , , ,							(b)
30	Xl	56.000	32.000	1668.000	1865.000	374.000	368.000	380.000	0.0	0.0	0.0	ere constituent and according
31 -	GR	549.800	1000.000	525.100	1012.000	516.300	1019.000	516.300	1300.000	516.300	1617.000	
9 32 32	GR	516.300	1645.000	515.800	1651.000	510.200	1668.000	499.700	1702.000	498.700	1706.000	0
53	GR	496.000	1712.000	491.700	1738.000	496.000	1763.000	496.400	1770.000	496.000	1776.000	A _B
St.	GR	491.700	1806.000	496.000	1836.000	497.400	1852.000	502.400	1865.000	506.100	1890.000	и
● # 25	GR	505.800	1932.000	505.400	1968.000	505.900	2010.000	506.400	2054.000	506.700	2102.000	
36	GR	510.700	2115.000	510.700	2131.000	515.600	2147.000	515.600	2164.000	525.700	2172.000	
37	GR	540.200	2196.000	550.500	2218.000	0.0	0.0	0.0	0.0	0.0	0.0	P ₁
€ 55 €	FT	0.0	0.0	0.0	0.0	8.400	0.0	0.0	0.0	0.0	0.0	
37	NH	4.000	0.085	1406.000	0.060	1529.000	0.036	1774.000	0.060	2339.000	0.0	
- 6	Heles	4 500 600	2.75		1777 586.	E20 000	500 000	E00 000	0.0	0.0	0.0	n
41.41	×1	57.000	35.000	1529.000	1774.000	530.000	500.000	500.000	0.0	520.500	1406.000	
42	GR	550.000	1000.000	537.200	1013.000	524.900	1027.000	520.500	1032.000		1494.000	
43	GR	519.500	1421.000	519.000	1432.000	519.200	1456.000	519.800	1466.000	519.800 499.800	1582.000	2
- u	GR	518.600	1509.000	510.700	1529.000	506.100	1548.000	500.800	1576.000 1701.000	501.000	1748.000	3 3
6	GR	498.600	1589.000	493.400	1636.000	498.600	1681.000	499.100	The same transfer and the same of the same		2014.000	1
45	GR	506.000	1774.000	506,800	1822.000	507.600	1902.000	506.700	1970.000	506.600 508.800	2168.000	
(A)	GR	507.200	2036.000	508.800	2079.000	511.000	2124.000	510.600	2147.000	550.400	2339.000	n a
	GR	504.100	2186.000	505.200	2194,000	515.400	2211.000	515.400	2306.000		0.0	
49 50	NC	0.090	0.055	0.036	0.100	0.300	0.0	0.0	0.0	0.0	•••	"•
51	X1	58.000	53.000	2032.000	2216.000	685.000	645.000	705.000	0.0	0.0	0.0	и
52	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15
#3 s3	GR	575.000	1000.000	566.700	1023.000	549.900	1067.000	537.400	1086.000	535.400	1090.000	•
54	GR	533.800	1094.000	533.800	1300.000	533.800	1548.000	533.800	1572.000	532.400	1585.000	36
35	6	525.700	1601.000	515.500	1616.000	506.100	1639.000	505.300	1653.000	501.300	1664.000	lu lu
€4154	GR	500.000	1668.000	500.000	1670.000	500.000	1675.000	501.300	1678.000	504.100	1684.000	"0
57	GR	506.000	1704.000	506.600	1753.000	508.400	1811.000	509.500	1882.000	509.300	1942.000	38
12	GŘ	507.400	1978.000	506.400	2015.000	506.100	2032.000	502.000	2045.000	500.800	2052.000	31
● ₹54	GR	496.500	2075.000	496.500	2113.000	496.500	2113.000	500.800	2170.000	501.300	2177.000	`
100	GR .	501.900	2197.000	507.900	• 2216.000	508,300	2237.000	511.200	2266.000	510.600	2306.000	

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GR	510.900	2366.000	512.600	2417.000	512,600	2481.000	513.700	2552.000	515.400	2593.000	_ (19	
GR	511.600	2614.000	514.600	2625.000	520.700	2636.000	520.700	2800.000	525.100	2804.000		
GR	550.600	2837.000	562.300	2857.000	575.600	2878.000	0.0	0.0	0.0	0.0		
NC	0.100	0.055	0.036	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
ET	0.0	0.0	0.0	0.0	40.400	0.0	0.0	0.0	0.0	0.0		91
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X1	60-000	30.000	4190-000	4378-000	460-000	410-000	410.000	0.0	0.0	0.0		
						3371.000				3422.000		•
						3596.000		3654.000	510.900	3713.000		ju
						Control of the Contro			509.800			
						4064.000		4120,000	509.600	4141.000		
						4212.000		4225.000	495.900	4262.000		16.
							505.900	4378.000	528.000	4379.000		i,
	0.0	0.0	0.0	0.400	0.600	0.0	0.0	0.0	0.0	0.0		O m
NH	3.000	0.200	4141.000	0.039	4378.000	0.060	4721.000	0.0	0.0	0.0		IS N
FT	0.0	0.0	0.0	0.0	8.400	0.0	0.0	. 0.0	0.0	0.0		19 - 8
				2019.000						2984.690		. 0 9
X1	60.100	75.000	3944.000	4378.000	80.000	35.000	41.000	0.0	0.0			76
. X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	525.000	516.500			21
GR	574.800	1000.000	550.300	2496.000	550.300	2525,000	526.100	2534.000	520.600	2561.000		
GR	520.400	2600.000	518.200	2669.000	517.500	2749.000	517.000	2835.000	517.500			n
GR	519.600	2928.000	520.800	2949.000	520.300	2957.000	513.700					73
GR	504.900	2999.000	503.200	3006.000	503.200	3007.000						74
GR	509.000	3024.000	518.900	3058.000								
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36	1.200	1.500	2.900	0.0	407.000	14.000	0100.000	0.010	304.300	304.300		
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BT	5105.000	519.700	0.0	5209.000	518.200	0.0	5276.000	517.500	0.0	5336.000		
	GR G	GR 511.600 GR 550.600 NC 0.100 FT 0.0 X1 59.000 GR 575.400 GR 539.400 GR 539.400 GR 539.400 GR 503.900 GR 503.900 GR 508.500 GR 508.500 GR 508.000 GR 510.800 GR 574.800 GR 511.100 GR 506.500 GR 495.900 NC 0.0 NC 0.0 NC 0.0 GR 574.800 GR 511.100 GR 506.500 GR 495.900 NC 0.0 CR 574.800 GR 511.100 GR 506.500 GR 511.100 GR 506.500 GR 511.100 GR 509.000 GR 511.100 GR 509.000 GR 511.100 GR 513.000 GR 514.200 NH 3.000 RT 3259.000 RT 3259.000 RT 3259.000 RT 533.800 RT 10.000	GR 511.600 2614.000 GR 550.600 2837.000 NC 0.100 0.055 ET 0.0 0.00 X1 59.000 69.000 GR 575.400 1000.000 GR 535.400 2200.000 GR 539.400 2200.000 GR 539.400 2349.000 GR 508.500 3188.000 GR 508.500 3188.000 GR 510.800 3512.000 GR 510.800 3512.000 GR 510.800 3512.000 GR 574.800 1000.000 GR 574.800 1000.000 GR 574.800 1000.000 GR 574.800 1000.000 GR 509.000 3751.000 GR 511.100 3933.000 GR 509.000 3751.000 GR 511.100 3933.000 GR 506.500 4160.000 GR 574.800 1000.000 GR 574.800 1000.000 GR 574.800 1000.000 GR 574.800 1000.000 GR 509.000 3751.000 GR 509.000 3751.000 GR 509.000 3751.000 GR 509.000 3751.000 GR 511.100 3933.000 GR 509.000 3751.000 GR 511.100 3933.000 GR 509.000 3751.000 GR 511.100 3933.000 GR 512.700 3483.000 GR 512.700 3483.000 GR 513.000 3151.000 GR 514.200 4627.000 GR 514.200 535.900 GR 514.200 525.900 GR 514.200 525.9000 GR 514.200 525.9000 GR 514.200 525.9000 GR 5	GR 550.600 2837.000 562.300 NC 0.100 0.055 0.036 ET 0.0 0.0 0.0 X1 59.000 69.000 3263.000 GR 575.400 1000.000 543.400 GR 539.400 2200.000 542.700 GR 539.400 2280.000 542.700 GR 503.900 2369.000 501.500 GR 508.500 3188.000 507.300 GR 508.500 3188.000 507.300 GR 508.000 3414.000 501.500 GR 523.800 3950.000 515.200 GR 523.800 3950.000 515.200 GR 500.000 3414.000 501.500 GR 500.000 3512.000 511.500 GR 510.800 3512.000 515.200 GR 523.800 3950.000 550.300 NC 0.100 0.055 0.038 ET 0.0 0.0 0.0 0.0 X1 60.000 3.751.000 510.300 GR 511.100 3933.000 511.200 GR 506.500 4160.000 506.000 GR 506.500 4160.000 506.300 GR 509.000 3751.000 500.000 GR 506.500 4160.000 506.000 GR 511.100 3933.000 511.200 GR 506.500 4160.000 506.000 GR 506.500 4160.000 506.000 GR 511.100 3933.000 511.200 GR 511.100 3933.000 511.200 GR 511.100 3933.000 511.200 GR 511.100 3933.000 510.000 GR 512.700 3483.000 512.400 GR 511.100 4275.000 3944.000 TT 0.0 0.0 0.0 0.0 X1 60.100 75.000 3944.000 TT 0.0 0.0 507.200 TT 0.0 0.0 507.	SR	RP 551.600 2614.000 514.600 2625.000 520.700 RP 550.600 2837.000 562.300 2857.000 575.600 NC 0.100 0.055 0.036 0.100 0.300 X1 59.000 69.000 3263.000 3437.000 40.000 RP 575.400 1000.000 565.700 1042.000 552.500 RP 534.400 1600.000 542.700 2219.000 543.400 RP 539.400 2200.000 542.700 2219.000 543.400 RP 539.400 2300.000 5525.600 2297.000 514.300 RP 503.900 2369.000 505.700 2386.000 505.500 RP 503.900 2369.000 505.700 2386.000 505.500 RP 508.500 301.000 509.300 3081.000 508.200 RP 508.500 3363.000 504.600 3278.000 505.500 RP 508.500 3414.000 505.300 3204.000 505.500 RP 508.500 3363.000 504.600 3278.000 501.500 RP 508.500 3363.000 504.600 3278.000 501.500 RP 508.500 3369.000 505.300 3892.000 501.500 RP 508.000 3263.000 504.600 3278.000 501.500 RP 508.000 3263.000 504.600 3278.000 501.500 RP 508.000 3703.000 510.500 3418.000 508.300 RP 508.000 3500.000 510.500 3418.000 506.300 RP 508.000 3500.000 510.500 3418.000 506.300 RP 508.000 3703.000 515.200 3703.000 512.000 RP 508.000 3703.000 515.200 3703.000 512.200 RP 509.000 3751.000 515.200 3703.000 512.200 RP 509.000 3751.000 515.000 3703.000 512.200 RP 509.000 3751.000 510.300 2496.000 565.100 RP 509.000 3751.000 507.200 3774.000 505.800 RP 509.000 3751.000 507.200 3730.000 512.200 RP 509.000 3751.000 507.200 3730.000 512.000 RP 509.000 3751.000 507.200 3734.000 505.800 RP 509.000 3751.000 507.200 3734.000 505.800 RP 509.000 3751.000 509.000 4378.000 507.500 RP 509.000 3751.000 509.000 4378.000 509.000 517.500 RP 509.000 3751.000 509.000 509.000 517.500 RP 509.000 3751.000 509.000 509.000 517.500 RP 509.000 3751.000 509.000 509.000 517.500 RP 509.000 309.000 509.000 509.000 5	GR 511,600 2614,000 514,600 2625,000 520,700 2636,000 R 556,600 2837,000 562,300 2857,000 575,600 2636,000 NC 0.100 0.00 0.00 0.00 0.00 0.00 X1 59,000 69,000 3263,000 3437,000 40,400 0.00 R 53,400 1600,000 543,400 1800,000 543,400 2140,000 R 533,400 2200,000 542,700 2219,000 543,200 2230,000 R 533,400 2200,000 555,500 2297,000 514,300 2356,000 R 503,300 2369,000 505,700 2386,000 505,100 2356,000 R 508,500 201,000 506,300 2687,000 506,500 2770,000 R 508,500 318,000 507,300 3204,000 506,500 2770,000 R 508,500 318,200 507,300 3278,000 508,500	RR 511,600 2614,000 514,600 2625,000 520,700 2636,000 70.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	GR \$11,600 \$214,000 \$14,600 \$267,000 \$207,000 \$207,000 \$207,000 \$207,000 \$200,000 \$20	GR \$11,600 \$11,600 \$614,600 \$625,000 \$52,000 \$75,600 \$70,700 \$280,000 \$75,000 \$70,00 <th< th=""><th>RE \$51,400 2814,000 \$144,000 \$144,000 \$285,000 \$285,000 \$720,000 \$720,000 \$200,000 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.</th><th>RE \$11,400 Pal 4,000 Span Span Span Pal Pal Pal Pal Pal Pal Pal Pal Pal Pal</th></th<>	RE \$51,400 2814,000 \$144,000 \$144,000 \$285,000 \$285,000 \$720,000 \$720,000 \$200,000 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.	RE \$11,400 Pal 4,000 Span Span Span Pal

	RT	517.500	0.0	5376.000	525.700	0.0	0.0	0.0	0.0	0.0	0.0	20 6
	NC	0.100	0.050	0.039	0.400	0.600	0.0	0.0	0.0	0.0	0.0	
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3538.000	4375.000	
0	X1	62.000	44.000	3596.000	3809.000	306.000	495.000	417.000	0.0	0.0	0.0	
	GR	540.600	1000.000	529.700	3488.000	529.700	3488.000	529.700	3510.000	524.100	3518.000	
	GR	511.200	3538.000	509.300	3555.000	509.400	3583.000	509.700	3596.000	505.800	3604.000	6
0	GR	505.000	3611.000	504.500	3615.000	504.500	3681.000	504.500	3739.000	505.000	3746.000	
1	GR	505.500	3752.000	508.000	3781.000	507.900	3788.000	505.600	3792.000	505.600	3801.000	
	GR	508.600	3809.000	509.300	3826.000	507.700	3845.000	505.500	3861.000	507.400	3872.000	'5
6	GR	511.200	3887.000	511.400	3911.000	512.500	3949.000	512.200	4012.000	511.200	4089.000	
	GR	511.200	4172.000	511.300	4253.000	510.200	4285.000	506.300	4313.000	506.200	4332.000	
	GR	505.800	4344.000	506.200	4352.000	506.200	4396.000	511.600	4428.000	511.600	4442.000	6
	GR	513.500	4448.000	525.300	4463.000	549.300	4482.000	575.100	4512.000	0.0	0.0	Y
J.	NC .	0.100	0.060	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
Δ	ET	0.0	0.0	0.0	0.0	13.400	0.0	U • U		EXA 1869	311.040 83.0	'6
•	XI	63 000	E0 000	2202 000	3623.000	545.000	1180.000	544.000	0.0	0.0	0.0	
Ė	GR	63.000 535.400	58.000	3392.000 525.900	3161.000	512.100	3187.000	511.100	3217.000	511.800	3258.000	
61	GR	511.900	3317.000	513.800	3356.000	514.000	3392.000	508.200	3406.000	505.600	3411.000	'
	GR	505.000	3412.000	505.000	3419.000	505.600	3423.000	507.000	3435.000	508.000	3447.000	10
14	GR	507.000	3479.000	505.800	3493.000	505.000	3502.000	505.000	3540.000	505.000	3583.000	
6) 11	GR	505.800	3586.000	509.000	3596.000	512.300	3623.000	512.500	3678.000	511.000	3701.000	
16	GR	511.200	3739.000	511.000	3787.000	509.800	3803.000	508.000	3810.000	507.200	3813.000	12
19	GR	508.000	3827.000	509.000	3845.000	508.300	3867.000	508.300	3883.000	510.300	3898.000	25
(A 20	GR	513.600	3944.000	514.000	3975.000	513.200	4106.000	512.400	4287.000	511.900	4508.000	"
n n	GR	512.600	4646.000	512.400	4831.000	511.500	5003.000	511.300	5094.000	512.000	5162.000	14
72	GR	510.600	5208.000	507.300	5277.000	506.200	5295.000	507.900	5318.000	506.900	5352.000	15
● 2.13	GR	507.000	5363.000	509.200	5373.000	509.200	5395.000	509:900	5402.000	525.200	5421.000	
24	GR	550.900	5444.000	567.500	5453.000	575.700	5465.000	0.0	0.0	0.0	0.0	16
25	NC	0.100	0.060	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	11_
21 26	ET	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	(\bullet, \bullet)
27	765	5.75.75.		25.250		257,361	2000 200	2012	24.95 A 65			" J
22	X1	64.000	52.000	2562.000	2803.000	400.000	750.000	499.000	0.0	0.0	0.0	.19
1 2.75	GR	539.000	2205.000	539,000	2218.000	518.600	2244.000	514.800	2290.000	513.400	2424.000	
38	GR	511.700	2498.000	513.300	2520.000	512.000	2562.000	509.700	2588.000	508.100	2622.000	
31	GR	507.000	2634.000	505.300	2652.000	505.300	2700.000	505.300	2741.000	507.000	2754.000	n_
C-12	GP	508.800	2768.000	511.100	2803.000	510.300	2861.000	511.100	2902.000	512.400	2969.000	7
31	GR	511.000	3040.000	510.900	3110.000	510.200	3169.000	508.700	3209.000	506.700	3231.000	
	GP	511.100	3260.000	512.400	3310.000	515.100	3441.000	515.000	3563.000	515.400	3680.000	n n
	GR	510.400	3774.000	509.600	3800.000	508.900	3819.000	509.700	3847.000	511.200 509.600	3908.000 4340.000	
i.	GR	511.100	3997.000	510.900	4095.000	510.100	4202.000	509.800	4271.000	513.500	4420.000	
△ 25, 26	GR	509.400	4363.000	508.900	4376.000	509.600	4385.000	509.900 546.200	4515.000	546.200	4548.000	l'on
	GR	513.500	4440.000	515.000	4448.000	527.300	4468.000	0.0	0.0	0.0	0.0	14. 24
	GR	554.900	4573.000	575.500	4627.000	0.300	0.0	7 0.0	0.0	0.0	0.0	
41.41	NC	0.060	0.060	0.039	0.100	0.300	0.0	4		J. V		"•
	X1	65.000	83.000	2131.000	2313.000	392.000	325.000	380.000	0.0	0 . 0	0.0	•
41	GR	569.800	1000.000	567.200	1052.000	564.800	1116.000	558.100	1214.000	551.800	1307.000	40
1 444	GR	549.100	1381.000	545.900	1416.000	540.300	1435.000	543.200	1467.000	542.300	1508,000	
- 5	GR	544.100	1532.000	544.100	1554.000	537.800	1576.000	532.800	1607.000	525.300	1656.000	36
	GR	522.300	1675.000	523.900	1693.000	523.900	1711.000	520.200	1728.000	515.500	1766.000	2)
\$00	GR	513.900	1770.000	511.900	1778.000	511.000	1782.000	511.000	1788.000	511.000	1796.000	•
48	GR	511.900	1797.000	515.700	1802.000	517.400	1814.000	517.900	1840.000	516.800	1868.000	n
4	GR	516.200	1947.000	515.700	2051.000	515.400	2105.000	510.600	2131.000	509.100	2135.000	23
●50.50	GP	507.500	2142.000	500.200	2174.000	500.200	2187.000	500.200	2187.000	507.500	2241.000	
31	GR	508.900	2253.000	509.700	2279.000	511.000	2313.000	511.000	2368.000	511.700	2441.000	M
1/1	GR	513.200	2508.000	512.400	2573.000	511.100	2634.000	512.500	2663.000	512.300	2782.000	15
0 /51	GP	514.000	2869.000	514.800	2987.000	514.900	3075.000	510.900	3134.000	509.500	3154.000	•
54	GR	510.200	3215.000	509.800	3260.000	511.100	3292.000	511.400	3405.000	511.800	3503.000	
(5.	GR	511.800	3595.000	510.400	3692.000	509.900	3754.000	509.000	3783.000	507.900	3795.000	и
€16.36	GR	509.000	3810.000	509.500	3864.000	510.300	3900.000	514.300	3909.000	514.300	3931.000	(0)
37	GR	515.000	3937.000	526.000	3954.000	536.000	3981.000	527.300	4012.000	524.600	4022.000	***************************************
35	GR	527.500	4031.000	534.400	4046.000	550.200	4080.000	551.400	4095.000	556.400	4115.000	n
950	GR	557.300	4132.000	569.400	4159.000	575.200	4178.000	0.0	0.0	0.0	0.0	
	NC	0.060	0.070	0.042	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

													Real Property and the
6	XI	66.000	82.000	1832.000	1995.000	350.000	337.000	350.000	0.0	0.0	0.0	21	
	GR	575.200	1000.000	572.000	1059.000	567.100	1123.000	563.700	1187.000	559.900	1262.000	∠ 155	
	GR	555.000	1327.000	549.700	1355.000	549.700	1381.000	547.400	1412.000	545.700	1454.000		
0	GR	543.000	1482.000	535.100	1503.000	534.400	1540.000	530.000	1574.000	526.400	1585.000		91
	GR	525.700	1605.000	523,900	1620.000	523.500	1626.000	520.800	1633.000	514.200	1645.000		
1	GR	511.500	1650.000	510.500	1652.000	510.500	1659.000	510.500	1665.000	511,400	1666.000		3
0	GR	514.000	1671.000	519.400	1680.000	519.400	1707.000	518.100	1717.000	516.900	1751.000		0
	GR	516.600	1802.000	516,300	1832.000	512.300	1842.000	509.300	1850.000	508.000	1855.000		2 9
	GP	505.700	1863.000	505.700	1890.000	505.700	1890.000	508.000	1920.000	508.500	1929.000		
0	GR	509.000	1962.000	510.500	1995.000	511,200	2039.000	512.000	2111.000	512.800	2158.000	•	0
	GR	513.200	2182.000	512.500	2235.000	512.200	2277.000	510.700	2318.000	515.500	2358.000		4
7	GR	517.400	2390.000	516.900	2437.000	516.500	2499.000	515.400	2556.000	513.300	2636.000		
0	GR	511.900	2661.000	512.500	2739.000	512,500	2821.000	512.500	2912.000	512.400	3043.000		0
9	GR	512.100	3119.000	512.000	3241.000	511.600	3354.000	510.800	3410.000	510.100	3477.000		4
19	GR	509.800	3519.000	509.800	3541.000	509,600	3564.000	508.700	3571.000	509.200	3578.000		
0"	GR	512.200	3593.000	515.900	3606.000	515.900	3623.000	518.800	3631.000	526.100	3645.000		0
12	GR	535.700	3669.000	544.000	3697.000	546.300	3736.000	549.700	3769.000	559.200	3809.000		
12	GR ·	569.900	3859.000	574.100	3881.000	0.0	0.0	0.0	0.0	0.0	0.0		
⊕ 14	NC	0.070	0.070	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		9
15			1987 7 (1977)	316, 755	159,75		5.50				1.6652778		10.
16	X1	67.000	89.000	2461.000	2664.000	635.000	400.000	680.000	0.0	0.0	0.0		11
9 12 -	GR	610.200	1000.000	606.200	1100.000	601.600	1167.000	596.800	1234.000	590.600	1303.000		
18	GR	584.700	1364.000	574.100	1407.000	573.300	1474.000	570.500	1499.000	568.600	1510.000		12
19	GR	566.900	1517.000	566.100	1526.000	565.300	1533.000	558.100	1544.000	554.500	1562.000		11
20	GR	554.600	1594.000	554.800	1608.000	549.100	1655.000	546.600	1684.000	541.700	1709.000		
21	GR	537.500	1730.000	530.700	1738.000	530.700	1758.000	523.800	1773.000	524.000	1787.000		14
n	GR	515.800	1798.000	512.700	1805.000	512.000	1816.000	511.000	1822.000	512.000	1831.000		15
92	GR	513.000	1840.000	515.000	1864.000	516.600	1882.000	516.600	1905.000	518.600	1927.000		
34	GR	521.000	1964.000	515.700	1985.000	512.800	2008.000	512.700	2053.000	513.700	2085,000		16
, 22	GR	514.400	2123.000	514.800	2184.000	515.500	2214.000	515.500	2550.000	514.700	2240.000	•	11
916	GR	514.200	2272.000	513.200	2314.000	510.300	2371.000	512.400	2390.000	511.600	2413.000		D m
n	GR	512.600	2434.000	514.400	2461.000	512.900	2475.000	511.800	2496.000	510.100	2512.000		18 Z.R
n	GR	506.000	2550.000	506.000	2574.000	506.000	2597.000	510.100	2638.000	511.300	2651.000		19 ENI
25	GR	513.900	2664.000	514.300	2691.000	513.900	2740.000	513.500	2777.000	512.900	2822.000		
30	GR	512.200	2874.000	511.900	2968,000	512.000	3056.000	512.800	3153.000	513.000	3236.000		1
	GR	513.700	3290.000	514.600	3373.000	514.700	3450.000	514.300	3542.000	514.700	3617.000		21
911	GR	514.800	3672.000	515.200	3712.000	514.800	3737.000	514.700	3795.000	514.800	3861.000		
73	GR	515.300	3924.000	517.100	3948.000	517.100	3969.000	519.200	3978.000	525.800	3993.000		144
A	GR	540.500	4019.000	555.300	4045.000	567.300	4097.000	573.500	4121.000	0.0	0.0		23
3 5	NC	0.075	0.045	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
	FT_	0.0	0.0	0.0	0.0	12.400	0.0	0.0	0.0	0.0	0.0		"
•	X1	68.000	68.000	2127.000	. 2327.000	300.000	1150.000	725.000	0.0	0.0	0.0		25
30	GR	600.000	1000.000	597.500	1048.000	593,400	1085.000	585.700	1125.000	575.500	1169.000		26
-	GR	555.200	1205.000	555.200	1242.000	557.800	1262.000	555.400	1283.000	553.900	1299.000		
00	GR	550.400	1312.000	538.000	1324.000	526.700	1340.000	521.600	1347.000	521.500	1363.000		11
27	GR	523.200	1375.000	520.600	1391.000	515.300	1414.000	513.400	1420.000	512.600	1428.000		28
46	GR	512.000	1433.000	512.600	1438.000	514.000	1448.000	513.300	1454.000	512.700	1460.000		La serie
O 11	GR	513.900	1469.000	515.400	1491.000	516.200	1534.000	516.000	1604.000	515.900	1659.000		· •
45	GR	515.500	1700.000	515.600	1738.000	515.300	1785.000	515.300	1846.000	515.800	1888.000		30
46	GR	516.600	1956.000	516.200	2023.000	515.600	2071.000	514.800	2127.000	513.300	2162.000		
@ 17	GR	513.200	2199.000	513.000	2213.000	506.500	2250.000	513.000	2287.000	513.900	2295.000		
43	GR	515.500	2327.000	515.900	2390.000	516.200	2459.000	515.200	2547.000	515.700	2627.000		32 5
n F	GR	516.000	2677.000	516.200	2778.000	516.400	2856.000	516,600	2959.000	516.700	3056.000		
2 50	GR	517.300	3080.000	518.000	3118.000	521.000	3150.000	523.900	3160.000	523.900	3171.000		
91	GR	523.900	3179.000	524.800	3189.000	536.400	3209.000	549.100	3221.000	574.500	3266.000		34
8	GR	599.800	3307.000	616.400	3343.000	626.000	3386.000	0.0	0.0	0.0	0.0		
•	NC	0.100	0.055	0.042	0.100	0.300	0.0	0.0	0.0	. 0.0	0.0		0 8
Я	FT	0.0	0.0	0.0	0.0	9.400	0.0	0.0	0.0	0.0	0.0		34
35 [1,781 188	V. V.	•	, ,		4 18 18 18 18 18 18 18 18 18 18 18 18 18				7
	X]	69.000	74.000	1851.000	2191.000	220.000	378.000	425.000	0.0	0.0	0.0		" • 1
57	GR	599.700	1000.000	593.500	1047.000	585.100	1092.000	575.900	1121.000	565.400	1146.000		35 24
58	GR	560.800	1150.000	560.400	1175.000	556.600	1189.000	555.900	1202.000	551.700	1213.000		14
	GR	546.500	1224.000	524.800	1253.000	520.900	1293.000	520.900	1322.000	520.900	1341.000		
	GR	517.000	1363.000	515.200	1382.000	514.300	1393.000	513.600	1398.000	513.000	1404.000		
	Mark Comment		1335.000	2 4 6 6 V V	10000	11,300	1000	313.000	10000				

									\cap				
	GR	513,600	1409.000	514.200	1415.000	515.300	1429.000	515.600	1453.000	515.300	1468.000	22	
	GR	513.900	1480.000	513.400	1489.000	514.500	1496 000	515.400	1500.000	515.400	1524.000		
	GR	518.500	1548.000	520.400	1570.000	520.700	1591.000	519.500	1621.000	519.200	1643.000		
	GR	517.900	1704.000	517.200	1751.000	516.400	1772.000	516.500	1802.000	517.100	1825.000		
0	GR	516.900	1851.000	515.600	1862.000	514,500	187 .000	513.000	1896.000	513.000	2019.000		(3)
	GR	513.000	2153.000	514.500	2164.000	514.900	2167.000	517.000	2191.000	518.000	2252.000		
	GR	519.000	2305.000	519.000	2365.000	518.700	2444.000	518.400	2516.000	517.900	2612.000		
0	GR	518.300	2725.000	518.900	2767.000	519.400	2854.000	520.500	2941.000	522.500	2983.000		9 6
	GR	525.500	3029.000	530.700	3050.000	531.000	3062.000	532.200	3076.000	539.100	3094.000		2 %
	GR	551.100	3124.000	551.300	3183.000	560.200	3220.000	561.300	3261.000	572.100	3280.000		Jan 1
0	GP	574.400	3302.000	584.800	3333.000	597.000	3380.000	599.100	3406.000	0.0	0.0		9
	NC	0.100	0.055	0.042	1.100	0.300	0.0	0.0	0.0	0.0	0.0		4
1	FT	0.0	0.0	0.0	j.0	11.400	0.0	0.0	0.0	0.0	0.0		0
0													9
3	XI	70.000	79.000	1960.000	211000	640.000	920.000	641.000	0.0	0.0	0.0		.
16	GR	600.200	1000.000	593.600	102(.000	584.800	1,033.000	583.900	1056.000	557.800	1080.000		10
Quit.	GR	557.800	1095.000	556.400	1107.000	550.400	1120.000	537.400	1150.000	522.400	1177.000		~
12	GR	520.500	1190.000	516.100	119 .000	515.100	1202.000	514.200	1209.000	515.100	1214.000	reconstruction of the second	
0	GR	516.200	1226.000	517.200	1259.000	518.100	1300.000	520.400	1331.000	520.900 521.500	1381.000		Δ
614	GR	520.700	1430.000	520.000	1464.000	519.300	1497.000	521.500	1519.000	522.100	1530.000 1720.000		110
16	GR	515.300	1550.000	516.100	1573,000	517.000 519.500	1596.000	521.100 515.600	1897.000	517.100	1906.000		
A 212	GR GR	521.900	1786.000	521.500 520.600	1850,000 1932,000	521.100	1953.000	520.600	1960.000	516.800	1969.000		116
	GR	515.400	1918.000	510.000	2000.000	510.000	2032.000	510.000	2066.000	515,400	2089.000		11
	GR	517.400	2098.000	520.300	2114.000	516.200	2139.000	518.800	2171.000	516.800	2202.000		
6 2.20	GR	516.700	2234.000	516.000	2241.000	514.700	2255.000	515.900	2264.000	517.200	2274.000		6
71	GR	520.000	2299.000	520.800	2335.000	521.500	2411.000	521.800	2503.000	522.000	2611.000		44
n	GR	522.100	2732.000	522.000	2859.100	522.200	2971.000	522.500	3063.000	523.000	3157.000		
0 173	GR	522.700	3209.000	526.200	3239.700	526.200	3254.000	526.200	3262.000	529.700	3273.000		•
H	GR	540.900	3284.000	550.200	3303.600	557.200	3338.000	564.000	3371.000	575.500	3419.000		14
25	GR	577.000	3439.000	585.200	3464.000	591.600	3486.000	598.400	3503.000	0.0	0.0		
2.24	NC	0.060	0.050	0.042	0.170	0.600	0.0	0.0	0.0	0.0	0.0		
27	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1850.000	2900.000		18 6
73				168 2000		178,000	1185,655						19. 8
0 721	X1	71.000	47.000	2253.000	2467.000	480.000	440.000	501.000	0.0	0.0	0.0		•) 7
16 ac	GR	599.100	1000.000	592.700	1041.000	584.600	1058.000	584.600	1079.000	576.000	1087.000		25
41	GR	560.900	1106.000	560.900	1115.000	556.200	1127.000	545.600	1149.000	535.500	1181.000		21
● 1 32	GR	525.500	1207.000	525.500	1300.000	525.500	1500.000	525.500	1800.000	525.500	2198.000		
31	GR	525.500	2209.000	520.600	2218.000	516.500	2230.000	515.300	2233.000	516.500	2245.000		
	GR	517.300	2253.000	517.000	2263.000	516.500	2272.000	512.500	2341.000	512.500	2367.000		72
•135	GR	512.500	2435.000	516.500	2457.000	518.300	2467.000	520.800	2497.000	521.900	2530.000		
- 51	GP	522.400	2581.000	522.900	2641.000	523.000	2725.000	522.900	2799.000	523.100	2858.000		
2 3	GR	523.100	5955.000	523.400	3063.000	523.700	3166.000	523.900	3273.000	526.400	3287.000		25
9 136	GP	526.400	3307.000	528.600	3315.000	548.500	3346.000	563.200	3374.000	578.200	3398.000		76
39	GR	590.500	3443.000	600.200	3477.000	0.0	0.0	0.0	0.0	0.0	0.0		
40	NC	0.060	0.050	0.044	0.100	0.300	0.0	0.0	0.0	0.0	0.0		27
	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		18
00	٧,	72 000		2420 000	2710 000	610 000	724 000	700 000	0.0	0.0	0.0		
0	X1	72.000	64.000	2430.000	2718.000	410.000	734.000	790.000 578.800	0.0 1048.000	0.0 560.900	1064.000		6
24	GR GR	600.100	1000.000	588.400 555.300		577.900 544.500	1106.000	527.100	1123.000	527.100	1200.000		20
4	GP	560.900	1074.000	527.100	1086.000	527.100	2000.000	527.100	2278.000	526.300	2289.000		
● 147	GR	527.100	2312.000	521,300	2335.000	518.700	2352.000	516.000	2359.000	515.000	2362.000		
45	GR	515.000	2312.000	516.000	2396.000	517.400	2403.000	520.800	2419.000	522.000	2430.000		12
49.17	GR	520.400	2438.000	519.400	2445.000	519.000	2450.000	512.300	2484.000	519.000	2524.000		-
● 9750	GR	519.700	2531.000	519.700	2538.000	519.000	2546.000	518.400	2554.000	519.000	2577.000		
SI	GR	519.500	2596.000	519.500	2624.000	519.500	2649.000	519.000	2669.000	518.200	2703.000		38
52	GR	519.000	2710.000	519.900	2718.000	520.600	2748.000	520.600	2773.000	519.400	2801.000		55
● £.53	GR	519.000	2820.000	518.400	2847.000	519.000	2856.000	519.900	2869.000	523.700	2905.000		
54	GR	523.800	2952.000	523.900	3043.000	524.200	3143.000	524.600	3231.000	525.200	3307.000		34
55	GR	525.900	3350.000	528.100	3362.000	528.100	3379.000	529.700	3384.000	550.000	3402.000		31
● 156	GR	564.100	3420.000	580.500	3445.000	590.800	3476.000	599.400	3508.000	. 0.0	0.0		0
47	NC	0.050	0.060	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		- 18
S													29
0 m	X1	73.000	56.000	2690.000	2855.000	950.000	490.000	575.000	0.0	0.0	0.0		0
MODEL ACCOUNTS			DESCRIPTION OF PROPERTY OF PERSONS ASSESSMENT OF THE PERSON OF THE PERSO	569.500	1013.000	569.500	1023.000	564.400	1035.000	558.100	1047.000		

Color													
Record R			558.100	1056.000	549.100	1067.000	540.800	1088.000	536.600	1096.000	530.900	1106.000	23
Color			530.900	2446.000	525.300	2462.000	523.800	2474.000	519.700	2493.000	517.400	2500.000	-
Color		GR	516.400	2503.000	516.400	2525.000	517.400	2537.000	518.300	2547.000	521.200		
6		GR	521.700	2614.000	521.000	2657.000	520.900	2690.000	520.200	2705.000	517.000	2773.000	
0.00 0.00	0	GR	517.000	2773.000	517.000	2793.000	520.206	2834.000	521.800	2855.000	521.900		o n
RE \$18,500 \$26,400 \$24,200 \$24,200 \$21,200 \$25,200 \$25,400		GR	522.000	2966.000	523.100	3036.000							
Color		GR	518.500	3206.000	520.200								
RR 526,000 7747,000 574,200 3953,000 526,900 3951,000 3978,00	0	GR	519.400	3388.000									101
Re	1	GR	526.000	3747.000	526.200	3853.000							7 #
Color		GR		4015.000	530.700								
No. 0.550	0	GR	600.400	4098.000									o'
FT		NC	0.050										
Time	7	FT	0.0		0.0								
0	0							No.	5				'0
GR		X1	74.000	58.000	2556.000	2796.000	970.000	230.000	640.000	0.0	0.0	0.0	a superior de la companya de la comp
GR S57, A00 1200, 000 556, S00 1291, 000 556, 500 1491, 000 556, 500 1491, 000 556, 500 1491, 000 525, 300 1291, 000 525, 300 525, 300 1291, 000 525,	18	GR	574.500	1000.000		1040.000							
GP 555,400 1505,000 552,300 1660,000 549,000 1716,000 526,200 1750,000 526,200 233,000 2154,000 2254,000	011	GR		1209.000	556.500	1229.000							'0
GP \$76,400 2014,000 \$72,000 \$25,000 2079,000 \$75,600 2094,000 \$74,00	11.	GR	555.400	1595.000	552.300	1660.000							
CR \$726,600 \$726,000 \$733,000 \$732	11	GR	526,400										
68 571,900 238,800 573,800 573,800 572,700 256,000 571,000 2586,000 518,400 2576,000 68 575,101 2839,000 570,700 2883,000 571,000 2793,000 572,700 2793,000 575,600 2796,000 69 575,101 2839,000 570,700 2883,000 571,000 2909,000 572,700 291,000 575,600 2999,000 69 576,400 3789,000 571,000 3846,000 575,500 3786,000 575,600 2999,000 69 570,300 3789,000 571,000 3846,000 571,000 371,000 3784,000 578,800 3773,000 69 570,300 3789,000 571,000 3846,000 571,000 3871,000 0.0 0.0 0.0 60 60 60 60 60 60 60	911	GR											'•
GR 518,400 2664,000 518,400 2721,000 521,000 2738,000 523,100 2755,000 525,500 2766,000 GR 524,400 2999,000 520,700 3823,000 525,500 3063,000 525,700 3104,000 525,600 3669,000 GR 524,400 2999,000 529,900 3029,000 525,500 3063,000 525,700 3104,000 525,800 3173,000 GR 524,400 526,200 3622,000 526,500 3660,000 525,500 3063,000 525,700 3104,000 525,800 3368,000 GR 549,800 3463,000 574,400 3490,000 530,900 3917,000 511,900 3828,000 KT 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 KT 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 KT 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 KT 150,000 57,000 2663,000 790,000 320,000 640,000 0.0 0.0 0.0 0.0 KT 150,000 57,000 2663,000 790,000 320,000 640,000 0.0 0.0 0.0 0.0 KT 150,000 57,000 2663,000 790,000 320,000 640,000 0.0 0.0 0.0 0.0 KT 150,000 57,000 2663,000 790,000 320,000 640,000 0.0 0.0 0.0 0.0 KT 150,000 57,000 2663,000 790,000 320,000 640,000 0.0 0.0 0.0 0.0 KT 150,000 57,000 2663,000 790,000 320,000 640,000 0.0 0.0 0.0 0.0 KT 150,000 57,000 2663,000 5563,000 1591,000 550,000 1241,000 560,200 1260,000 GR 571,500 1124,000 562,200 1157,000 5653,000 1160,000 572,000 1241,000 560,200 1260,000 GR 572,000 1769,000 550,300 1771,000 550,700 1805,000 550,500 1711,000 550,700 1805,000 550,500 1711,000 560,000 GR 572,000 2764,000 570,300 1771,000 550,700 1805,000 550,500 1711,000 560,000 GR 572,000 2764,000 570,	15	GR											10
68 575,100 2899,000 520,700 2883,000 521,000 2909,000 524,000 525,000 3173,000 68 526,700 3262,000 526,500 3366,000 526,500 3363,000 577,000 3574,000 527,800 3573,000 3574,000 527,800 3573,000 578,800 373,000 578,800 373,000 578,800 373,000 578,800 373,000 578,800 374,000 578,800 3855,000 589,800 589,800 574,800 3890,000 581,000 381,000 3821,000 3821,000 3821,000 3835,000 589,800 3835,000 589,800 3874,000 578,800 3890,000 580,	16	GR			WILLIAM NEW CONTROL OF THE PROPERTY OF THE PRO								
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GR \$30,300 3749,000 531,000 3804,000 531,000 3917,000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	19	GR	526.200	3262.000	526.500						CHICAGOS - DOMONDANA ARTHUR DESCRIPTION OF THE PARTY OF T		
GR 549,80C 3844,000 574,400 3890,000 609,900 391,000 0.0	6 10	GR	530.300	3789.000	531.000								13
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FT	12	NC	0.050	0.055	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
R3	€ 23	FT	0.0	0.0	0.0	0.0	5.400	0.0	0.0	0.0			
R3	25	V.1	75 000										16
RR 600,900 1000,000 590,300 1043,000 583,900 1051,000 577,100 577,100 1044,000 577,100 1044,000 577,100 1044,000 577,100 1044,000 577,100 1044,000 557,200 1241,000 550,200 1240,000 160,000													W_
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Total Tota	35	NC											26
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GR 625.300 1000.000 610.500 1049.000 598.400 1086.000 586.200 1125.000 580.300 1135.000 68 580.300 1144.000 547.100 1199.000 550.300 1226.000 550.300 1247.000 548.800 1276.000 580.300 1247.000 548.800 1276.000 580.300 11313.000 553.100 1391.000 551.700 1491.000 549.700 1548.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1574.000 549.700 1575.00 549.700 1574.000 549.700 1575.00 157	40		10.000	0.0	0.0	0.0							A Company of the Comp
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GR 549.800 1610.000 546.500 1647.000 545.900 1706.000 543.500 1746.000 535.500 1783.000 GR 531.000 1904.000 528.600 1970.000 528.200 2094.000 528.500 2262.000 533.800 2290.000 GR 533.800 2309.000 530.800 2343.000 523.700 2363.000 522.000 2367.000 517.500 2380.000 GR 517.500 2450.000 517.500 2503.000 522.000 2530.000 523.600 254.000 524.600 2573.000 GR 525.400 2637.000 525.900 2754.000 526.100 2882.000 526.600 3099.000 526.900 3158.000 GR 527.200 3252.000 526.600 3099.000 526.900 3158.000 GR 527.200 3252.000 584.200 3378.000 549.700 3332.000 562.900 3349.000 GR 574.700 3364.000 584.200 3378.000 600.100 3391.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	45		553.200	1313.000	553.100	1391.000		1491.000					
GR 531.000 1904.000 528.600 1970.000 528.200 2094.000 528.500 2262.000 533.800 2290.000 GR 533.800 2309.000 530.800 2343.000 523.700 2363.000 522.000 2367.000 517.500 2380.000 GR 517.500 2450.000 517.500 2503.000 522.000 2530.000 523.600 2540.000 524.600 2573.000 GR 527.200 3252.000 528.900 376.000 526.100 2882.000 526.600 3099.000 526.900 3158.000 GR 574.700 3264.000 584.200 3378.000 600.100 3391.000 0.0 0.0 0.0 0.0 GR 574.700 3364.000 584.200 3378.000 600.100 3391.000 0.0 0.0 0.0 0.0 SR 0.900 1.500 3.000 0.0 160.000 6.000 3320.000 2.000 517.500 X1 77.020 0.0 0.0 0.0 535.100 530.700 0.0 0.0 0.0 0.0 0.0 X3 10.000 0.0 0.0 0.0 535.100 530.700 0.0 0.0 532.000 539.700 0.0 X3 10.000 0.0 0.0 0.0 0.0 50.000 542.000 0.0 1746.000 539.700 0.0	•			1610.000	546.500	1647.000	545.900	1706.000			535.500		
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GR 525.400 2637.000 525.900 2754.000 526.100 2882.000 526.600 3099.000 526.900 3158.000 GR 527.200 3252.000 528.900 3276.000 542.200 3309.000 549.700 3332.000 562.900 3349.000 GR 574.700 3364.000 584.200 3378.000 600.100 3391.000 0.0 0.0 0.0 0.0 SR 0.900 1.500 3.000 0.0 160.000 50.000 2.000 517.500 X1 77.020 0.0 6.0 0.0 50.000 50.000 50.000 0.0 0.0 0.0 X2 0.0 0.0 1.000 535.100 530.700 0.0 0.0 0.0 0.0 X3 10.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 SR 1 23.000 1614.000 545.500 0.0 1686.000 542.000 0.0 1746.000 539.700 0.0	930					2503.000	522.000	2530.000	523.600	2540.000			
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SR 0.900 1.500 3.000 0.0 160.000 6.000 3320.000 2.000 517.500 517.500 X1 77.020 0.0 6.0 0.0 50.000 50.000 0.0 0.0 0.0 0.0 0.0									549.700	3332.000	562.900	3349.000	14
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S 8T 23.000 1614.000 545.500 0.0 1686.000 542.000 0.0 1746.000 539.700 0.0	58					STATE OF THE RESIDENCE OF THE PARTY OF THE P							36
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		BT	1796.000	537.400	0.0	1870.000	535.600	0.0	1950.000	534.600	0.0	2025.000	

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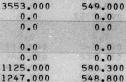
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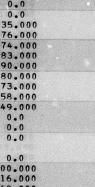
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GR	531.000	1904.000	528.600	1970.000	528.200	2094.000	528.500	2262.000	533.800	22
GR	533.800	2309.000	530.800	2343.000	523.700	2363.000	522,000	2367.000	517,500	23
GR	517.500	2450.000	517.500	2503.000	522.000	2530.000	523,600	2540.000	524.600	25
GR	525.400	2637.000	525.900	2754.000	526.100	2882.000	526,600	3099.000	526,900	31
GR	527.200	3252.000	528.900	3276.000	542.200	3309.000	549.700	3332.000	562.900	33
GR	574.700	3364.000	584.200	3378.000	600.100	3391.000	0.0	0.0	0.0	
NC	0.040	0.040	0.039	0.100	0.300	0.0	0.0	0.0	0.0	
FT	0.0	0.0	0.0	0.0	15.400	0.0	0.0	0.0	0.0	
xı	78.000	45.000	1739.000	1955.000	740.000	710.000	735.000	0.0	0.0	
GR	600.000	1000.000	575.000	1033.000	549.900	1071.000	537.500	1096,000	537,500	11
GR	537.500	1150.000	537.500	1158.000	536.800	1166.000	534.900	1183.000	534.900	12
GR	532.700	1220.000	528.300	1232.000	526.800	1262.000	527.300	1320,000	527.300	13
GR	527.900	1412.000	527.000	1457.000	527.400	1509.000	529.200	1564.000	530.100	16
GR	530.000	1721.000	527.900	1739.000	525,000	1754.000	521.600	1768.000	522.900	17
GR	521.200	1787.000	519.300	1795.000	519.300	1872.000	519.300	1940.000	521.200	19
GR	524.300	1955.000	526.200	1984.000	525.800	2056.000	526.000	2126,000	525.100	22
GR	525.100	2269.000	526.600	2327.000	529.000	2396.000	529.000	2464.000	529.300	25
CD	520 000	2540 000	E30 000	25/2 000	FE0 700	2502 200	F-F 100			

0.0

2607.000

0.0

3527.000

545.900

533.600

and the second	2074.000	260.200	6606.000	233.800	2290.000	
523.700	2363.000	522,000	2367.000	517.500	2380.000	
522.000	2530.000	523.600	2540.000	524.600	2573.000	
526.100	2882.000	526.600	3099.000	526.900	3158.000	
542.200	3309.000	549.700	3332.000	562.900	3349.000	
600.100	3391.000	0.0	0.0	0.0	0.0	
0.300	0.0	0.0	0.0	0.0	0.0	
15.400	0.0	0.0	0.0	0.0	0.0	1
740.000	710.000	735.000	0.0	0.0	0.0	
549.900	1071.000	537.500	1096,000	537.500	1100.000	
536.800	1166.000	534.900	1183.000	534.900	1216.000	
526.800	1262.000	527.300	1320.000	527.300	1368.000	
527.400	1509.000	529.200	1564.000	530.100	1658.000	
525.000	1754.000	521.600	1768.000	522.900	1780.000	
519.300	1872.000	519.300	1940.000	521.200	19+5.000	
525.800	2056,000	526.000	2126.000	525.100	2214.000	
529.000	2396.000	529.000	2464.000	529.300	2507.000	
550.700	2593.000	575.100	2625.000	600.000	2655.000	
16.400	0.0	0.0	0.0	0.0	0.0	
		760,000			N. B	
755.000	620.000	710.000	0.0	0.0	0.0	
550.600	1132.000	536.100	1168.000	536.100	1184.000	
533.400	1248.000	533.000	1271.000	530.100	1342.000	
531.000	1531.000	531.000	1597.000	530.000	1602.000	

									C 70 000	J L 7 0 0 0 0	201000	
12	GR	525.400	2637.000	525.900	2754.000	526.100	2882.000	526.600	3099.000	526.900	3158.000	
10	GR	527.200	3252.000	528.900	3276.000	542.200	3309.000	549.700	3332.000	562,900	3349.000	
14	GR	574.700	3364.000	584.200	3378.000	600.100	3391.000	0.0	0.0	0.0	0.0	
23	NC	0.040	0.040	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
15	FT	0.0	0.0	0.0	0.0	15.400	0.0	0.0	0.0	0.0	0.0	
17						50.0 3.00				•••	0.0	
15	XI	78.000	45.000	1739.000	1955.000	740.000	710.000	735.000	0.0	0.0	0.0	
19	GR	600.000	1000.000	575.000	1033.000	549.900	1071.000	537.500	1096.000	537.500	1100.000	
20	GR	537.500	1150.000	537.500	1158.000	536,800	1166,000	534.900	1183.000	534.900	1216.000	
2)	GR	532.700	1220.000	528.300	1232.000	526.800	1262.000	527.300	1320.000	527.300	1368.000	
22	GR	527.900	1412.000	527.000	1457.000	527.400	1509.000	529.200	1564.000	530.100	1658.000	
22	GR	530.000	1721.000	527.900	1739.000	525.000	1754.000	521.600	1768.000			
24	GR	521.200	1787.000	519.300	1795.000	519.300	1872.000			522.900	1780.000	
25	GR	524.300	1955.000	526.200	1984.000	525.800		519.300	1940.000	521.200	19+5.000	
	GR	525.100	2269.000	526.600			2056.000	526.000	2126.000	525.100	2214.000	
	GR	529.900	2548.000		2327.000	529.000	2396.000	529.000	2464.000	529.300	2507.000	
MA CONTRACTOR	FT			530.000	3563.000	550.700	2593.000	575.100	2625.000	600.000	2655.000	
74	- '	0.0	0.0	0.0	0.0	16.400	0.0	0.0	0.0	0.0	0.0	
25	X1	79.000	40.000	1602.000	1823.000	755.000	(20.000	710 000				
ı K	GR	600.000	1000.000	575.000	1070.000		620.000	710.000	0.0	0.0	0.0	
,	GR	536,100	1203.000	536.000	1227.000	550.600	1132.000	536.100	1168.000	536.100	1184.000	
22	GR	529.200	1411.000			533.400	1248.000	533.000	1271.000	530.100	1342.000	
	GR	525.000		529.200	1464.000	531.000	1531.000	531.000	1597.000	530.000	1602.000	
	GR		1610.000	522.000	1626.000	520.200	1636.000	520.200	1684.000	520.200	1711.000	
	GR	522.000	1753.000	522.500	1764.000	523.500	1792.000	526.200	1823.000	523.700	1844.000	
	GR	523.900	1854.000	529.500	1885.000	530.700	1907.000	529.400	1950.000	529.500	2015.000	
		530.000	2063.000	529.800	2109.000	529.100	2152.000	528.000	2197.000	528.700	2257.000	
	GR	529.600	2294.000	530.100	2308.000	550.300	2343.000	575.300	2380.000	600.100	2428.000	
	NC	0.040	0.040	0.043	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
	FT	0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	0.0	0.0	
	X1	80.000	32.000	1449.000	1767.000	460.000	412.000	430.000	0.0	0.0	0.0	
3	GR	600.000	1000.000	575.000	1064.000	550.000	1125.000	539.000	1142.000	539.000	1152.000	
	GP :	539.000	1178.000	535.000	1198.000	533.400	1261.000	532.000	1329.000	531.000	1366.000	
	GR	531.400	1420.000	531.400	1449.000	525.000	1463.000	522.700	1476.000	518.800	1499.000	
	GR	518.800	1527.000	518.800	1688.000	522.700	1718.000	523.900	1728.000	525.200	1737.000	
	-GR	527.400	1767.000	529.400	1792.000	531.700	1802.000	531.900	1846.000	529.400	1898.000	
	GR	527.900	1918.000	527.100	1936.000	529.800	1953.000	530.500	1963.000	564.400	1997.000	
	'GR	588.700	2025.000	600.000	2045.000	0.0	0.0	0.0	0.0	0.0	0.0	
	NC	0.040	0.090	0.043	0.100	0.300	0.0	0.0	0.0	0.0		
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0		0.0	
				0.0	0.0	7.100	0.0	0.0	0.0	1424.000	1815.000	
	X1	81.000	36.000	1424.000	1815.000	365.000	340.000	350.000	0.0	0.0	0.0	
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	GR	600.000	1000.000	575.100	1086.000	572.600		554.400			0.0	
180	GR	539.800	1180.000	539.800	1210.000	537.900	1108.000		1133.000	554.500	1155.000	
	GR	531.700	1304.000	530.500	1356.000	531.600	1222.000	535.900	1235.000	534.800	1273.000	
	GR	524.800	1451.000	523.500			1405.000	534.400	1424.000	530.500	1431.000	
		364.000	1451.000	263.200	1455.000	523.500	1466.000	524.800	1483.000	525.400	1491.000	

1483.000 525.400 1491.000 GR 527.100 1511.000 528.800 1533.000 524.800 1549.000 523.500 1554.000 523.500 1625,000 523.500 1690.000 524.800 1768.000 525.000 1780,000 527.600 1797.000 529.300 1815.000

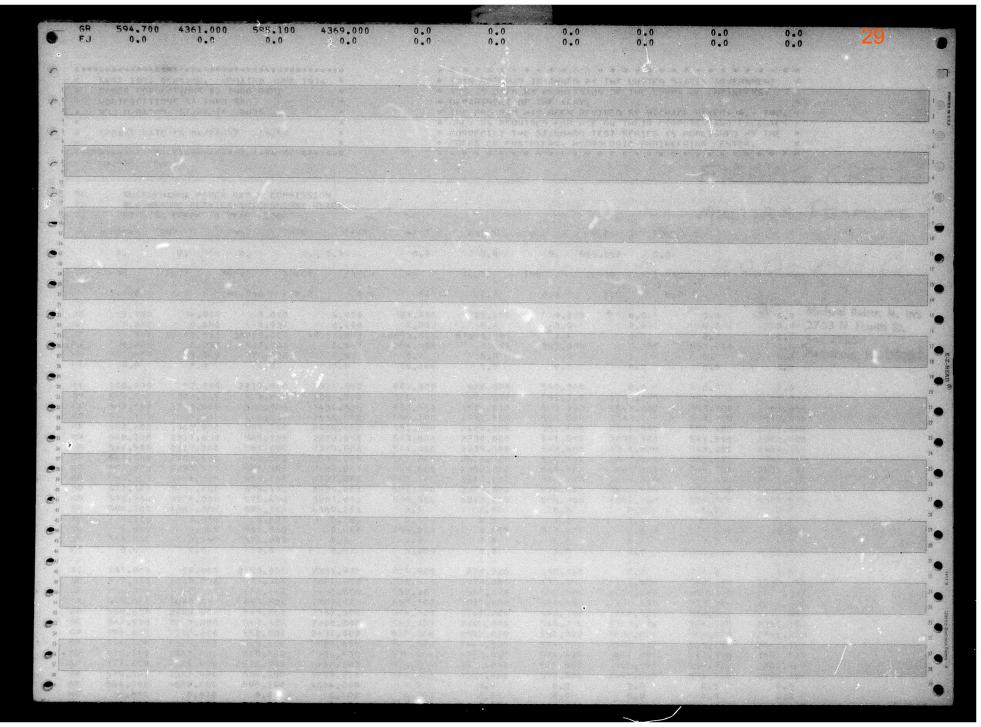
CONTRACTOR STREET	MATERIAL MANAGEMENT	And the second second second second	in the second second second second		State and a Depter of Constant to the Manual Constant		《图》是是图》					25
	GR	532.200	1845.000	534.000	1867.000	534.500	1880.000	550.000	1915.000	575.000	1951.000	40
	GR	600.000	1997.000	7.0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	NC	0.000	0.090	0.043	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
0	NH	5.000	0.075	1432.000	0.045	1507.000	5.090	1582.000	0.041	1738.000	0.100	
V	NH	1842.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	31
.FV	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1265.000	1738.000	
0										FA1.4990		
(A)	X1	82.000	33.000	1582.000	1738.000	690.000	660.000	685.000	0.0	0.0	0.0	(0)
100	GR	600.100	1000.000	586.800	1038.000	574.500	1068.000	558.000	1114.000	543.800	1141.000	2 🗒
	GR	544.100	1168.000	535.800	1198.000	535.800	1220.000	535.800	1268.000	535.700	1310.000	
9:	GR	535.700	1355.000	529.700	1376.000	527.700	1411.000	529.100	1422.000	527.900	1432.000	'0
6	GR	526.200	1446.000	523.100	1471.000	526.200	1497.000	527.300	1507.000	527.900	1520.000	4
	GR	526.800	1548.000	529.700	1582.000	527.200	1607.000	526.200	1624.000	522.800	1673.000	, _ R
0	GR	522.800	1673.000	522.800	1727.000	526.200	1733.000	528.500	1738.000	537.800	1764.000	,0
1/2	GR	550.100	1780.000	575.400	1807.000	600.600	1842.000	0.0	0.0	0.0	0.0	
^	. NC	0.055	0.100	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	,_
Q1	NH	5.000	0.055	1124.000	0.045	1212.000	0.100	1865.000	0.039	1990.000	0.100	'0
	NH	2058.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
4	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1135.000	1990.000	
	V.1	93 000	44 000	1045 000	1000 000	035 000	0.5.2			F		•
12	XI	83.000	44.000	1865.000	1990.000	935.000	957.000	950.000	0.0	0.0	0.0	10
A	GR	600.300	1000.000	598.000	1015.000	569.700	1039.000	552.600	1070.000	552.600	1092.000	n _
98	GR GR	537.600	1115.000	537.600	1124.000	528.000	1140.000	528.000	1149.000	528.000	1168.000	
		528.000	1185.000	528,900	1188.000	534.500	1212.000	535.400	1250.000	535.300	1284.000	12
	GR GR	535.400	1312.000	536.400	1327.000	534.600	1349.000	527.000	1352.000	524.500	1366.000	11 _
- W	GR GR	527.000	1381.000	528.900	1392.000	532.300	1432.000	532.000	1465.000	527.800	1489.000	
	GR	527.800	1505.000	532.800	1529.000	531.800	1566.000	532.300	1592.000	532.700	1636.000	C C
	GR	533.200	1659.000	533.300	1713.000	532.900	1770.000	531.500	1833.000	532.800	1865.000	8.
	GR	527.000 528.900		523.000	1888.000	523.000	1923.000	523.000	1954.000	527.000	1966.000	
10	NH	5.000	1971.000	534.200	1990.000	550.400	2030.000	575.300	2058.000	0.0	0.0	16
€ 26	NH	2268.000	0.085	1260.000	0.045	1338.000	0.100	1992.000	0.041	2191.000	0.100	17.
	FT	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•
		V • U	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1175.000	2191.000	18 2
A 10	X1	84.000	E2 000	1002 000	2101 000	400 000	720 000	700 000				19
	GR	600.800	53.000	1992.000 574.400	2191.000	490.000 550.100	730.000	700.000	0.0	0.0	. 0.0	9
	GR	538.100					1084.000	544.100	1099.000	544.100	1130.000	(9
(an	GR	530.000	1158.000	536.700	1170.000	534.600	1195.000	532.800	1232.000	533.100	1260.000	. In _ I
	GR	531.700	1274.000	529.100	1290.000	528.400	1302.000	529.100	1309.000	530.500	1325.000	
y v	GR	535.500	1338.000	533.800	1361.000	532.100	1369.000	534.400	1387.000	533.600	1408.000	The state of the s
O 16	GR	534.400	1427.000	535.700	1458.000	535,400	1481.000	530.700	1488.000	531.700	1499.000	H ₁
- 4	GR	534.400	1522.000	534.300	1564.000	533.200	1608.000	532.200	1620.000	534.000	1642.000	
27	GR	533.300	1692.000	532.900	1729.000	530.500	1748.000	533.200	1771.000	533.900	1790.000	
	GR	535.800	1979.000	532.000	1842.000	534.500	1869.000	536.300	1891.000	536.400	1930.000	18
	GR	525.000		534.300	1992.000	529.700	2003.000	528.000	2010.000	525.000	2022.000	
40	GR	550.100	2118.000	525.000	2173.000	528.000	2178.000	529.900	2181.000	532.800	2191.000	and the second s
	NC	0.090	2228.000	575.400	2246.000	599.600	2268.000	0.0	0.0	0.0	0.0	n a
	FT	0.090	0.100	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
41		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1260.000	2255.000	
0	X1	85.000	58.000	2026.000	2255 000	210 000	350 000	345 000	0.0			n
15	GR	599.600			2255.000	210.000	250.000	245.000	0.0	0.0	0.0	
40	GR.	542.000	1000.000	574.400	1042.000	548.600	1096.000	548.200	1106.000	544.300	1141.000	The state of the s
	GR	530.400	1147.000	542.000	1158.000	542.000	1191.000	535.200	1200.000	534.500	1219.000	n
	GR		1230.000	538.700	1243.000	537.000	1268.000	534.300	1291.000	534.700	1343.000	
		535.400	1425.000	534.900	1465.000	533.700	1496.000	535.100	1518.000	536.200	1529.000	, T
	GR	533.000	1544.000	532.000	1567.000	531.200	1576.000	530.400	1585.000	531.200	1593.000	n_
51	GR	532.900	1611.000	534.000	1658.000	534.500	1719.000	531.900	1752.000	531.300	1781.300	
	GR	530.700	1806.000	531.300	1810.000	532.600	1818.000	534.700	1848.000	535.900	1888.000	. 34
•	GR	534.500	1914.000	533.500	1928.000	535.600	1948.000	536.100	1977.000	534.700	1997.000	35 _ 9
	GR	536.000	2020.000	534.800	2026.000	530.700	2035.000	529.100	2046.000	526.500	2063.000	
, ,	GR	526.500	2099.000	526.500	2125.000	529.100	2148.000	530.100	2156.000	532.500	2174.000	36
	GR	532.200	2189.000	530.000	2208.000	529.300	2224.000	530.100	2236.000	534.000	2255.000	37 _ 3
9	GR	551.600	2294.000	574.200	2329.000	600.100	2336.000	0.0	0.0	0.0	0.0	
	NC	0.070	0.110	0.038	0.100	0.300	0.0	0.0	0.0	0.0	0.0	38
	NV	6.000	0.038	534.000	0.038	541.000	0.042	543.000	0.042	543.800	0.040	39
9	NV	543.900	0.040	560.000	0.0	0.0	0.0	0.0	0.0	0.0	0.000	
	FT	0.0	0.9	0.0	0.0	9.100	0.0	0.0	0.0	1265.000	1915.000	

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		"一个大大大大大大大大大大大大大大大大大大大大大大大大大大大大大大大大大大大大										20
	XI	86.000	31.000	1777.000	1915.000	1038.000	895.000	905.000	0.0	0.0	0.0	
	GR	600.100	1000.000	575.500	1046.000	568.100	1064.000	554.600	1082.000	554.600	1107.000	
	GR	536.100	1149.000	535.900	1161.000	535.100	1167.000	536.100	1174.000	536.000	1257.000	
6	GR	536.200	1318.000	539.100	1333.000	536.000	1343.000	536.000	1437.000	535.500	1527.000	0
	GR	534.700	1581.000	534.100	1612.000	535.700	1646.000	537.100	1711.000	537.100	1757.000	
	GR	533.500	1777.000	532.100	1812.000	531.000	1833.000	526.500	1871.000	531.000	1908.000	
@ :	GP	533.200	1915.000	551.100	1955.000	562.900	1986.000	564.200	2001.000	575.300	2025.000	0)
2	GR	600.500	2083.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1, 3
	NC	0.060	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
6	NV	6.000	0.038	536.000	0.038	542.000	0.042	542.500	0.042	544.400	0.040	0
	NV	544.500	0.040	560.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
. 7	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1276.000	1919.000	STATE OF THE STATE
6 1			1676			497 546		1000	10000	1210.000	2014 000	'0
1	X1	87.000	27:000	1623.000	1919.000	250,000	260.000	270.000	0.0	0.0	0.0	
10	GR	600.400	1000.000	574.400	1035.000	558.800	1065.000	558.800	1090.000	536.800	1132.000	
@ 11	GR	536.000	1144.000	535.600	1152.000	536.000	1160.000	535.500	1252.000	535.900	1328.000	'0
12	GR	540.700	1350.000	540.700	1358.000	535.500	1371.000	535.900	1501.000	536.400	1574.000	
13	GR	536.900	1623.000	532.700	1656.000	531.600	1678.000	530.800	1694.000	530.800	1785.000	
(n	GR	530.800	1904.000	531.600	1907.000	532.800	1910.000	537.000	1919.000	550.400	1946.000	16
15	GR	575.000	1973.000	600.100	2000.000	0.0	0.0	0.0	0.0	0.0	0.0	
16	NC	0.060	0.087	0.038	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
O 17	NV	6.000	0.038	536.000	0.038	543.000	0.045	545.000	0.045	545.700		110
18	NV .	545.800	0.043	560.000	0.0	0.0	0.045	0.0	0.045		0.043	
19	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	0.0	0.0	" The second of
C 20							0.0	U • U	0.0	1178.000	1855.000	io la
21	X1	88.000	34.000	1410.000	1604.000	925.000	860.000	920.000	0.0	0.0)	
21	GR	600.100	1000.000	574.700	1047.000	551.100	1087.000	551.100	1111.000		0.0	· · · · · · · · · · · · · · · · · · ·
0 2	GR	536.100	1147.000	536.700	1154.000	537.700	1234.000			536.600	1140.000	13
N	GR	540.400	1384.000	538.400	1410.000	535.700	1424.000	539.000	1308.000	540.600	1353.000	
15	GR	530.700	1438.000	530.700	1496.000	530.700		534.000	1428.000	532.200	1434.000	18
0	GR	537.300	1604.000	537.700			1552.000	532.200	1560.000	534.300	1570.000	17_
77	GR	534.000	1742.000		1658.000	537.900	1711.000	535.800	1726.000	534.500	1737.000	
71	GR	541.500		534.000	1763.000	534.000	1779.000	534,500	1781.000	536.500	1791.000	18 72
6 ×	NC		1841.000	550.200	1877.000	575.100	1914.000	599.900	1946.000	0.0	0.0	19_ EA
	NV	0.060	0.080	0.038	0.0	0.0	0.0	0.0	0.0	0.0	0.0	. •
ar [NV	6.000	0.038	538.000	0.038	544.000	0.045	546.500	0,045	547.400	0.043	10
	FT	547.500	0.043	565.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	n_{\perp}
77		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1241.000	1845.000	
34	×1	89.000	22 000	1407 000	1600 000	766 000	75.					72
@ .35	GR		32.000	1487.000	1699.000	766.000	754.000	760.000	0.0	0.0	0.0	n
	GR	603.500 554.300	1000.000	574.700	1065.000	555.800	1127.000	554.300	1146.000	554.300	1159.000	
	GR		1168.000	538.500	1201.000	538.000	1208,000	538.800	1215.000	539.500	1322.000	74
	GR	539.100	1438.000	539.500	1487.000	536,800	1500.000	534.600	1542.000	534.000	1562.000	25
	GR	532.600	1609.000	532.600	1615.000	532,600	1648.000	534.000	1667.000	534.900	1678.000	
		538.500	1699.000	538.500	1751.000	534.900	1780.000	534.500	1790.000	534.300	1795.000	176
	GR	534.300	1802.000	534.300	1808.000	534.500	1811.000	535.200	1820.000	550.100	1860.000	
	GR	575.600	1894.000	599.800	1932.000	0.0	0.0	0.0	0.0	0.0	0.0	
	NC	0.060	0.116	0.038	0.100	0.300	0.0	0.0	0.0	0.0	0.0	10
	NV	6.000	0.038	538.000	0.038	544.500	0.045	547.000	0.045	547.700	0.043	29
	NV	547.800	0.043	565.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
"L	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1221.000	1795.000	10
•	٧.	00.000			200 - 10 29 12							n _
	X1	90.000	24.000	1471.000	1726.000	150.000	150.000	150.000	0.0	0.0	0.0	
	GP	601.600	1000.000	585.100	1057.000	554.700	1122.000	554.700	1140.000	539.900	1174.000	. 11
	GR	539.200	1185.000	539.700	1194.000	539.500	1254.000	538.700	1365.000	539.700	1441.000	13
- N	GR	539.700	1471.000	535.800	1504.000	534.500	1513.000	533.800	1518.000	533.800	1600.000	
	GR	533.800	1658.000	534.500	1678.000	534.900	1689.000	539.000	1726.000	537.100	1762.000	in 3
	GR	536.500	1781.000	549.200	1819.000	575.500	1850.000	599.200	1912.000	0.0	0.0	Jane
(G-31	NC	0.060	0.110	0.038	0.100	0.300	0.0	0.0	0.0	0.0	0.0	***
51	NV	6.000	0.038	539.000	0.038	546.000	0.045	548.500	0.045	549.300	0.043	33
55	NV	549.400	0.043	565.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1. 3
₩354	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1273.000	1704.000	' ● I
37								A Part of Clark		• 0	2.0.000	
51	X1	91.000	22.000	1520.000	1704.000	910.000	908.000	905.000	0.0	0.0	0.0	
0	GR	590.300	1000,000	575.500	1039.000	549.300	1091.000	549.300	1112.000	548.500	1130.000	
	GR	546.600	1176,000	544.800	1218.000	543.200	1333.000	542.700	1451.000	543.200	1501.000	
							10001000	- 1 U U	1751,000	3730200	1501.000	

6		Control of the County of Property States and Control											
MINERAL MINISTRALIA	GR	544.100	1520.000	538,000	1537.000	536,000	1544.000	532.700	1554.000	532.700	1617.000	9 9 7 6	
	GR	532.700	1680.000	537.000	1696.000	539.100	1704,000	542.000	1728.000	549.900	1757.000	<u> </u>	0
	GH ·	575.800	1808.000	600.200	1854.000	0.0	0.0	0.0	0.0	0.0	0.0		
	NV	6.000	0.038	541.500	0.038	548.000	0.045	551.000	0.045	551.700	0.043		
0	NV	551.800	0.043	565.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		വ
•	FT	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		
1													7 1
0	Xì	92.000	30.000	1785.000	1975.000	935.000	900.000	905.000	0.0	0.0	0.0		l'of
1	GR	585.400	1000.000	577.700	1069.000	569.200	1140.000	560.400	1164.000	554.900	1199.000		2 4
	GR	555.300	1227.000	555.300	1248.000	555.300	1263.000	549.600	1291.000	548.900	1353.000		
P 5	GR	547.600	1438.000	545.100	1498.000	542.300	1567.000	543.100	1635.000	545.500	1696.000		, O
	GR	545.800	1737.000	544.900	1776.000	543.900	1785.000	540.000	1794.000	537.000	1804.000		4
	GR	532.400	1818.000	532.400	1877.000	532.400	1936.000	537.000	1951.000	538.700	1956.000		1.
0	GR	542.700	1975.000	545.700	1995.000	557.600	2020.000	575.600	2039.000	599.300	2087.000		0
	NC	0.070	0.110	0.038	0.100	0.300	0.0	0.0	0.0	0.0	0.0		6
() u	NV	6.000	0.038	542.000	0.038	549.000	0.045	552.000	0.045	552.900	0.043		1-
12	FT	553.000	0.043	570.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		'0
12		0.0	0.0	0.0	0.0	3.400	0.0	0.0	0.0	0.0	0.0		1
311	×1	93.000	34.000	1722.000	1858.000	765.000	903 000	705 000					190
151	GR	585.200	1000.000	575.700	1044.000	574.000	803.000 1068.000	795.000 563.200	0.0	0.0	0.0		
18	CB	560.600	1139.000	557.000	1151.000	554.600	1169.000	552.000	1108.000	560.900	1122.000		10
O 17	GR	551.800	1242.000	551.800	1314.000	552.000	1353.000	551.200	1370.000	552.000 548.000	1223.000		11.
18	GR	544.800	1441.000	544.500	1520.000	545.600	1569.000	549.900	1590.000	542.300	1402.000 1611.000		19
19	GR	541.100	1633.000	543.100	1649.000	547.600	1691.000	544.700	1722.000	539.800	1743.000		1
(20)	GR	538.000	1755.000	533.000	1790.000	533.000	1802.000	533.000	1841.000	538.000	1852.000		13
71	GR	540.900	1858.000	561.700	1876.000	575.000	1890.000	599.700	1923.000	0.0	0.0		14
23	NC	0.070	0.110	0.040	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
Q 22	NV	6.000	0.040	543.500	0.040	550,000	0.055	554.000	0.055	554.800	0.045		15
24	NV	554.900	0.045	570.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		16
25	FT	0.0	0.0	0.0	0.0	12.400	0.0	0.0	0.0	0.0	0.0		
24													
2	×1	94.000	30.000	1920.000	1930.000	435.000	448.000	445.000	0.0	0.0	0.0		18 19
	GR	595.100	1000.000	585.800	1096.000	578.300	1196.000	569.500	1227.000	564.300	1240.000		SEA
	GR GR	564.300	1254.000	559.300	1286.000	552.000	1304.000	553.500	1338.000	550.300	1368.000		
	GR	547.300	1430.000	547.900	1509.000	550.200	1540.000	550.500	1567.000	546.600	1598.000		70
	GR	545.400 539.500	1667.000	544.000	1706.000	545.100	1767.000	545.100	1792.000	540.300	1820.000		21
	GR	538.500	1828.000	538.500	1839.000	534.000	1884.000	534.000	1884.000	534.000	1910.000		
u	NC	0.070	0.110	540.500 0.042	1930.000	549.400	1942.000	574.500	1970.000	600.400	1993.000		177
€25	NV	6.000	0.042	545.500	0.0	0.0 552.000	0.0	0.0	0.0	0.0	0.0		13
26	NV	556.100	0.050	570.000	0.042		0.060	555.000	0.060	556.000	0.050		
11	FT	0.0	0.0	0.0	0.0	0.0 9.100	0.0	0.0	0.0	0.0	0.0	•	
3 10		946.062	a na a sha w		0.0	7.100	0.0	0.0	0.0	1489.000	2150.000		25
19	XI	95.000	41.000	1782.000	2147.000	115,000	520.000	380.000	0.0	0.0	0.0		26
40	GR	594.800	1000.000	585.800	1086.000	577.500	1166.000	574.400	1199.000	568.500	1208.000		
O 1	GR	568.500	1223.000	559.600	1265.000	552.000	1286.000	553.400	1323.000	550.200	1348.000		27
42	GR	548.700	1425.000	548.600	1478.000	551.800	1503.000	550.200	1518.000	546.400	1548.000		28
- 6	GR	546.400	1622.000	546.500	1691.000	547.400	1747.000	545.000	1782.000	540.900	1803.000		
9#	GR	538.700	1820.000	536.700	1835.000	538.700	1848.000	540.400	1858.000	540.700	1866.000		1º •
6	GR	538.800	1877.000	531.700	1904.000	538,800	1928.000	540.200	1933.000	544.800	1958.000		30
49	GR	541.700	1985.000	539.700	2013.000	539.200	2032.000	534.000	2073.000	539.200	2129.000		
90	GR	540.200	2137.000	542.900	2147.000	547.400	2164.000	563.600	2190,000	576.100	2208.000		
43	GR	600.000	2242.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		32 1
	NV	6.000	0.042	545.500	0.042	552.000	0.060	555.500	0.060	556.300	0.050		20
9 A	NV	556.400	0.050	570.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
	FT	0.2	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1405.000	2290.000		Э с
	v.1	04 000	42 44	1540	15.75 + 9.65		-156 [-198]						15 0
	XI	96.000	42.000	1562.000	1819.000	140.000	200.000	300.000	31 0.000	0.0	0.0		• 0
	GR	595.000	1000.000	585.100	1076.000	579.900	1134.000	578.100	1156.000	574.600	1181.000		26
	GR	563.100	1207.000	559.600	1226.000	552.100	1257.000	553.100	1289.000	550.700	1321.000		37: 3
	GR	548.900	1390.000	549.400	1405.000	551.900	1420.000	551.900	1430.000	547.900	1469.000		
	GR	546.900	1497.000	545.200	1562.000	540.600	1584.000	542.800	1630.000	541.400	1664.000		34
	GR	540.100	1679.000	537.900	1705.000	537.900	1735.000	537.900	1782.000	540.100	1796.000		39
	GR GR	541.500	1805.000	544.700	1819.000	545.900	1845.000	544.700	1910.000	544.300	1945.000		
	OR	544.900	2044.000	543.600	2131.000	544,500	2210.000	543.800	243.000	540.300	2261.000	Company of the Compan	Show and

	GR	539.700	2264.000	F/0 200	THE REAL PROPERTY AND ADDRESS OF THE PARTY AND							
	GR	575.000	2360.000	540.300	2275.000	540.800	2284.000	542.000	2303.000	550.200	2328.000	28
	NC	0.080	0.100	0.039	2401.000	0.0	0.0	0.0	0.0	0.0	0.0	20
	NV	6.000	0.039	546.000	0.039	0.300	0.0	0.0	0.0	0.0	0.0	
0	NV	556.800	0.047	570.000	0.039	552.500	0.055	556.000	0.055	556.700	0.047	
	FT	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0
The state of				0.0	0.0	9.100	0.0	0.0	0.0	1368.000	2360.000	
- 1	X1	97.000	45.000	1368.000	1/70 000	500 000						
	GR	624.900	1000.000		1478.000	530.000	250.000	540.000	0.0	0.0	0.0	101
	GR	592.100	1263.000	618.700	1079.000	617.400	1103.000	611.000	1143.000	599.600	1219.000	1,
	GR	550.400	1368.000	574.100	1299.000	553.600	1315.000	553.600	1344.000	551.300	1349.000	3
	GR	541.000		541.000	1384.000	538.200	1389.000	538.200	1423.000	538.200	1467.000	C.
	GR	547.400	1471.000	544.500	1478.000	546.800	1505.000	545.100	1543.000	545.400	1559.000	4
	GR	544.400	1614.000	546.500	1660.000	546.500	1697.000	546.600	1710.000	545.200	1738.000	
C.	GR	543.000	1777.000	542.300	1834.000	541.800	1893.000	541.500	1929.000	541.800	1937.000	5-7
10	GR	547.400	the second secon	545.100	2008.000	550.400	2044.000	551.300	2109.000	549.800	2177.000	
0	GR	545.500	2233.000	546.400	2307.000	544.800	2392.000	544.200	2403.000	545.000	2428.000	
	NV		2456.000	554.700	2484.000	575.500	2540.000	587.500	2593.000	595.700	2633.000	7
W.E	NV	6.000 557.100	0.039	546.000	0.039	553.000-	0.055	556.000	0.055	557.000	0.045	
@ 14	FT		0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	c 0 , 0 cc	
		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1113.000	2360.000	'
76	X1	98.000	47.000	1112 222	10/5							
(A)	GR ·		47.000	1113.000	1243.000	300.000	140.000	300.000	0.0	0.0	0.0	
11	GR	624.600 551.900	1000.000	600.400	1031.000	574.900	1054.000	555.800	1071.000	555.800	1101.000	"
	GR		1113.000	541.600	1122.000	538.000	1126.000	538.000	1161.000	538.000	1171.000	u u
20	GR	541.600	1197.000	543.100	1208.000	546.100	1243.000	547.800	1289.000	549.000	1319.000	THE RESERVE OF THE RE
	GR	547.600	1379.000	549.000	1437.000	549.000	1519.000	548.200	1628.000	547.800	1697.000	130
	GR	545.800	1720.000	545.800	1756.000	546.200	1798.000	544.100	1815.000	543.900	1828.000	H.
(3 n	GR	543.700	1838.000	543.900	1841.000	544.700	1851.000	545.700	1906.000	549.400	1929.000	
97	GR	549.700	1973.000	550.700	2009.000	550.700	2076.000	549.400	2159.000	548.000	2253.000	15
26	GR	546.500	2312.000	545.200	2361.000	546.100	2400.000	546.900	2426.000	546.500	2435.000	18
		545.500	2445.000	546.100	2452.000	551.300	2501.000	575.100	2569.000	588.500	2634.000	
970	GR NC	593.800	2672.000	599.900	2707.000	0.0	0.0	0.0	0.0	0.0	0.0	"•
	Annual management of the contract of the contr	0.090	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	18 7
-	NV	6.000	0.039	547.000	0.039	553.500	0.055	556.500	0.055	557.300	0.045	, , , , , , , , , , , , , , , , , , ,
- GF	NV FT	557.400	0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	19 6
31	Section 1	0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	0.0	0.0	n i
(A)	X1	00 000	50 000		A							
21	GR	99.000	52.000	1489.000	1681.000	420.000	180.000	340.000	0.0	0.0	0.0	
34	GR	555.600	1000.000	599.000	1026.000	575.600	1061.000	557.400	1073.000	557.400	1101.000	n
25	GR	550.100	1117.000	549.000	1148.000	547.400	1162.000	548.200	1170.000	548.500	1241.000	-
14	GR	542.100	1349.000	547.500	1389.000	547.200	1420.000	547.300	1489.000	545.000	1508.000	9
37	GR	544.200	1522.000	540.600	1529.000	540.600	1574.000	540.600	1616.000	542.100	1626.000	29
10 38	GR	548.000	1639.000	547.900	1681.000	547.100	1733.000	547.100	1799.000	546.500	1902.000	
39	GR	547.000	2240.000	546.000	2022.000	545.600	2074.000	545.600	2149.000	545.800	2210.000	"9
40	GR	546.500		546.900	2270.000	545.200	2276.000	543.300	2282.000	545.200	2289.000	18
A 41	GR	546.300	2294.000	548.400	2310.000	549.000	2372.000	549.100	2465.000	547.800	2565.000	17.
472	GR	554.200	2674.000	546.300	2793.000	547.800	2829.000	551.000	2871.000	554.900	2901.000	9
43	GR	587.400	2911.000	555.100	2917.000	561.000	2949.000	566.000	2976.000	575.900	3016.000	n,
94	NC	0.070	3081.000	599.600	3154.000	0.0	0.0	0.0	0.0	0.0	0.0	,
45	NV	6.000	0.080	0.037	0.100	0.300	0.0	0.0	0.0	0.0	0.0	9
45	NV	557.800		547.000	0.037	554.000	0.055	557.000	0.055	557.700	0.045	30
947	FT	0.0	0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	31
45		0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	9
49	X1	100.000	57.000	2217.000	2271 000	900 000	(20					10.
50	GR	599.900	1000.000	570.600	2371.000	800.000	620.000	550.000	0.0	0.0	0.0	n. T
51	GR	552.000	1350.000		1051.000	550.400	1091.000	551.300	1149.000	551.300	1257.000	
51	GR	550.700		552.000	1439.000	552.500	1524.000	553.300	1543.000	552.700	1567.000	34 6
g si	GR	550.400	1591.000	549.400	1635.000	550.100	1692.000	550.600	1743.000	550.700	1813.000	36 00
34	GR	548.100	1940.000	551.100	2058.000	551.100	2124.000	551.600	2171.000	550.400	2201.000	9.
45			2217.000	545.100	2223.000	543,000	2230.000	541.500	2235.000	541.500	2282.000	14 ·
	GR GR	541.500	2319.000	543.000	2329.000	544.600	2339.000	548.000	2371.000	548.100	2440.000	, i
		547.000	2481.000	547.000	2536.000	546.400	2610.000	550.700	2662.000	551.000	2740.000	"91
	GR	551.600	2823.000	550.300	2880.000	549,600	2982.000	548.800	2993.000	549.700	3000.000	n t
	GR	555.100	3046.000	557.000	3107,000	566.100 .	3141.000	566.100	3154.000	571.000	3173.000	
	GR	572.500	3201.000	575.400	3236.000	576.300	3325.000	576.400	3442.000	575.300	3636.000	*9
	GR	575.200	3785.000	575.400	3907.000	580,500	4013.000	590.200	4207.000	594.700	4337.000	



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79	X1	100.000	57.000	2217.000	2371.000	800.000	(20.000						19
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40	GR GR	572.500 575.200	3201.000 3785.000		3236.000	576.300	3325.000	576.40		2.000	575.300	3636.000	
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45	NV FT	558.000	0.045		0.0	0.0	0.0	0.0		0.0	0.0	0.0	36
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49	GR	599.800	1000.000		1028.000	550.500	1078.000	550.900		.000	552.100	1223.000	37
150	GR	552.300	1319.000		1431.000	552.000	1568.000	552.600		.000	555.300	1667.000	n a
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532 / TV E9262	GR	549.400	2813.000	549.000	2828.000	549.800	2844.000	554.200		.000	558.100	2942.000	18
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FT X1 X1 X1 X1 X1 X2 X1 X2 X3 X3 X4 X6 GR GR GR GR GR GR GR GR GR G	0.0 106.000 0.050 0.0 107.000 10.000 600.300 558.500 57.600 547.000 0.060 0.0	0.0 0.0 0.100 0.0 29.000 0.0 1000.000 1358.000 1634.000 1837.000 1978.000 2071.000 0.060	0.0 0.0 0.041 0.0 1837.000 0.0 589.700 557.000 557.700 555.500 547.300	0.0 0.100 0.0 0.0 2071.000 0.0 1122.000 1419.000	9.100 125.000 0.300 9.400 570.000 0.0	90.000 90.000 0.0 0.0	0.0 100.000 0.0 0.0	0.0 0.0 0.0	0.500 0.0	0.0 0.0	, on the second
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10 GR 15 GR 16 NC 17 ET 18 19 X1 20 GR 21 GR 22 GR 24 GR 25 GR 26 NC 27 ET 28 29 X1 30 X3 31 GR 32 GR	547.000 557.000 0.060 0.0	1978.000 2071.000 0.060	547.300	1858.000	556.800	1738.000	554.300	1769.000	554.900	1797.000	
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117 ET 18 19 X1 20 X3 6R 21 GR 22 GR 24 GR 25 GR 26 GR 27 ET 28 29 X1 20 X3 31 GR 32 GR	0.0		0.041	0.0	0.0	0.0	0.0	0.0	0.0	0.0	"
18 19 X1 X3 10 M20 M30 M6 M6 M6 M7 M6 M7		THE PERSON NAMED IN COLUMN	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	11
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77 GR 921 GR 24 GR 25 GR 25 GR 26 FT 27 ET 28 X1 29 X1 20 X3 31 GR 67 GR	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	13
22 GR 24 GR 25 GR 26 NC 27 ET 28 29 X1 30 GR 31 GR 32 GR	599.300	1000.000	589.100	1084.000	580,400	1148.000	574.200	1181.000	560.500	1239.000	
24 GR 25 GR NC 17 ET 28 X1 29 X1 20 X3 31 GR GR	558.100	1303,000	558.100	1388.000	557.400	1491.000	554.700	1556.000	553.500	1622.000	<u> </u>
35 GR NC 17 ET 38 X1 30 X3 31 GR GR	553.100	1663.000	561.100	1703.000	550.800	1738.000	549.800	1767.000	549.500	1775.000	15
17 NC ET 78 X1 33 X3 GR GR	546.500	1836.000	549.500	1891.000	550.600	1905.000	555.100	1919.000	560.700	2009.000	16
77 X1 20 X3 31 GR GR	562.100	2048.000	562.100	2070.000	575.700	2081.000	600.700	2117.000	0.0	0.0	
78 -29 X1 30 X3 31 GR -32 GR	0.055	0.080	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0	"•
97 X1 30 X3 31 GR 937 GR	0.0	0.0	0.0	0.0	9.400	0.0	0.0	0.0	0.0	0.0	18 %
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sı GR ●xı GR	10.000	0.0	0.0	1709.000	250.000	410.000	365.000	0.0	0.0	0.0	" ● 5
●31 GR	600.500	1000.000	575.000	11.21.000	560.200	0.0	0.0	0.0	0.0	0.0	20
	559.000	1371.000	556.900	1387.000	553.900	1418.000	559.700 554.200	1229.000	558.600	1304.000	n
37 GR	550.400	1487.000	559.000	1492.000	550.000	1496.000	550.000	1582.000	562.500	1458.000	
34 GR	550.500	1703.000	552.100	1709.000	552.400	1761.000	559.700	1783.000	560.300	1701.000 1849.000	
. •35 GR	560.900	1950.000	555.600	1969.000	565,600	2008.000	565.600	2019.000	565.600	2028.000	n_
as GR	574.500	2049.000	600.400	2101.000	0.0	0.0	0.0	0.0	0.0	0.0	
37 NC	0.080	0.090	0.041	0.100	0.300	0.0	0:0	0.0	0.0	0.0	The state of the s
●31 ET	0.0	0.0	0.0	0.0	6.400	0.0	0.0	0.0	0.0	0.0	25
39	0			1.00							11
40 XI	110.000	33.000	1095.000	1378.000	500.000	570.000	580.000	0.0	0.0	0.0	
●# GR	605.300	1000.000	604.000	1009.000	585.200	1038.000	575.200	1054.000	565.300	1073.000	27
4 GR	555.800	1095.000	553.700	1101.000	552.500	1108.000	549.800	1124.000	549.800	1147.000	28
⊕ GR	549.800	1175.000	552.500	1201.000	554.100	1217.000	552.800	1366.000	552.200	1303.000	
6 GR	551.500	1328,000	551.000	1346.000	551.500	1357.000	552.000	1369.000	554.000	1378.000	29
« GR	552.900	1391.000	555.500	1421.000	556.000	1464.000	556.000	1506.000	555.100	1529.000	10
●# GR	570.500	1589.000	560.400	1654.000	560.700	1734.000	555.600	1754.000	570.500	1789.000	
a NC	0.100	0.100	575.000 0.041	1820.000	599.400	1854.000	0.0	0.0	0.0	0.0	•
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51 X1	111.000	33.000	1327.000	1507.000	570.000	410.000	350.000	0.0	0.0	0.0	
57 GR	625.000	1000.000	600.000	1033.000	575.000	1065.000	557.500	1099.000	554.900		34 g
●® GR		1119.000	554.600	1119.000	554.600	1119.000	554.900	1145.000	555.400	1112.000	35 _ 👸
s GR		1229.000	559.900	1245.000	555.100	1270.000	557.500	1284.000	555.200	1186.000	
S GR	554.600 558.000	1327.000	554.500	1342.000	551,700	1392.000	554.500	1456.000	555.100	1466.000	38 8
→ GR	554.600	1507.000	556.400	1570.000	557.600	1625.000	556.500	1709.000	557.200	1787.000	11 - 9
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NH	554.600 558.000 554.900 556.700 560.700	0.100	1433.000	0.041	1625.000	0.100	1666.000	0.050	1713.000	0.100	

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GR	• 23	NH	2118.000	0.0	0.0	0.0							15
GR	24	X1	114 000	30 000	1279 000	1424 000	460 000	1660 000	EE0 000	0 0		0.00	16
## GR	26												II
GR 551,700 1360,000 551,700 1390,000 557,700 1400,000 558,300 1413,000 560,000 1244,000 565,500 1318,000 563,100 1604,000 565,300 1660,000 565,300 1660,000 565,300 1741,000 564,100 1810,000 562,400 1875,000 598,400 1992,000 588,400 1892,000 588,400 1992,000 588	17			1189.000	561.400								B E
GR 555,000 1454,000 565,500 1486,000 555,000 1518,000 563,100 1604,000 565,300 1600,000 665,300 1930,000 6756,600 1952,000 556,000 1952,000 556,000 1952,000 556,000 1952,000 556,000 1952,000 556,000 1952,000 576,000 100 1100 0.00 0.00 0.00 0.00 0.00 0	28												REA
GP 556,300 1741,000 556,100 1810,000 552,400 1875,000 1952,000 556,000 1977,000 558,400 1982,000 570,500 203,000 6756,000 1952,000 556,000 1977,000 558,400 1982,000 570,500 203,000 67 7,700 2022,000 574,800 2040,000 598,900 2070,000 624,100 2118,000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	279												" ● ₆
GR 556.000 1952.000 576.000 1952.000 556.000 1977.000 558.400 1982.000 570.500 2003.000 1	31		Committee of the Committee of Charges and										10
NC	1 2						556.000						21
FT 0.0 0.0 0.0 0.0 0.0 9.100 0.0 0.0 0.0 1189.000 2230.000 0.100 189.000 0.041 1342.000 0.100 2150.000 0.055 2220.000 0.100 0.0 0.0 0.0 0.0 0.0 0.0 0.0	13												n
NH 2386.000 0.0 0.100 1189.000 0.041 1342.000 0.100 2150.000 0.050 2220.000 0.100 NH 2386.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	34												n
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GR 625.300 1000.000 615.300 1079.000 611.800 1110.000 599.500 1132.000 574.500 1175.000	27	NH	2386.000	0.0	0.0	0.0	0.0	0.0	0.0		0.0		
GR 625.300 1000.000 615.300 1079.000 611.800 1110.000 599.500 1132.000 574.500 1175.000	● 33	X1	115-000	35.000	1189.000	1342 000	480 000	255 000	510 000	0.0	0.0	0.0	•
## GR 565.000 1189.000 560.100 1196.000 559.500 1208.000 555.500 1251.000 559.500 1300.000 1300.000 1300.000 1312.000 565.300 1342.000 565.300 1342.000 566.400 1455.000 565.800 1520.000 1360.000 1	40												16
GR 566.100 1590.000 566.500 1655.000 567.100 1734.000 566.300 1801.000 563.400 1850.000 GR 564.100 1875.000 563.700 1935.000 563.000 2020.000 561.500 2100.000 559.500 2150.000 GR 568.600 2157.000 555.000 2180.000 588.600 2209.000 560.000 2220.000 562.300 2232.000 GR 568.600 259.000 570.500 2280.000 570.500 2280.000 570.500 2280.000 570.500 2280.000 570.500 2280.000 570.500 2280.000 570.500 2280.000 570.500 2280.000 570.500 2280.000 570.500 2380.000 2290.000 6280.000 220.000 625.300 2380.000 2380.000 800.0	• II				560.100	1196.000							n
GR 564.100 1875.000 563.700 1935.000 563.000 2020.000 561.500 2100.000 559.500 2150.000 68 558.600 2157.000 555.000 2180.000 558.600 2200.000 560.000 2220.000 562.300 2232.000 68 558.600 2157.000 555.000 2280.000 574.800 2296.000 600.100 2320.000 625.300 2328.000 625.300 2386.000 600.0	V.												28
6 GR 558.600 2157.000 555.000 2180.000 558.600 2209.000 560.000 2220.000 562.300 2232.000 4 GR 570.506 2259.000 570.500 2280.000 574.800 2296.000 600.100 2320.000 625.300 2386.000 5 NC 0.080 0.080 0.041 0.100 0.300 0.0 0.0 0.0 0.0 0.0 0.0 6 T 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	43												79
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# FT 0.0 0.0 0.0 0.0 0.0 9.100 0.0 0.0 0.0 1283.000 2705.000	46												
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NH 2942.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	41												n 5
XI 116.000 56.000 1283.000 1375.000 250.000 280.000 265.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	9 /4												n
GR 624.800 1000.000 624.200 1012.000 623.500 1021.000 620.000 1038.000 615.100 1087.000 GR 605.200 1150.000 604.400 1165.000 604.100 1172.000 600.000 1196.000 575.400 1238.000 GR 562.400 1283.000 561.500 1290.000 560.600 1294.000 553.000 1331.000 GR 563.400 1346.000 560.600 1366.000 563.800 1375.000 567.000 1399.000 566.600 1423.000 GR 565.800 1459.000 567.700 1493.000 570.100 1541.000 570.500 1620.000 570.300 1674.000 GR 568.400 1747.000 567.800 1794.000 565.400 1850.000 564.000 1903.000 563.400 1950.000 GR 564.100 1988.000 564.400 2052.000 564.800 2112.000 565.200 2192.000 565.100 2308.000	51		117 222				25,759						и
GR 605.200 1150.000 604.400 1165.000 604.100 1172.000 600.000 1196.000 575.400 1238.000 1238.	57												15 00
GR 562.400 1283.000 561.500 1290.000 560.600 1294.000 553.000 1331.000 553.000 1331.000 560.600 1294.000 567.000 1399.000 566.600 1423.000 560.600 1423.000 570.500 1620.000 570.300 1674.000 570.500 1620.000 570.300 1674.000 568.400 1747.000 567.800 1747.000 565.400 1850.000 564.000 1903.000 563.400 1950.000 568.400 1988.000 564.400 2052.000 564.800 2112.000 565.200 2192.000 565.100 2308.000	, N												- Arman
GR 553.000 1346.000 560.600 1366.000 563.800 1375.000 567.000 1399.000 566.600 1423.000 570.500 1620.000 570.300 1674.000 8 GR 568.400 1747.000 567.800 1794.000 565.400 1850.000 564.000 1903.000 563.400 1950.000 565.100 2308.000	55	GR											
# GR 568.400 1747.000 567.800 1794.000 565.400 1850.000 564.000 1903.000 563.400 1950.000 GR 564.100 1988.000 564.400 2052.000 564.800 2112.000 565.200 2192.000 565.100 2308.000	0"								567.000	1399.000	566.600	1423.000	
GR 564.100 1988.000 564.400 2052.000 564.800 2112.000 565.200 2192.000 565.100 2308.000	57												n ,
													n
						2402.000	564.000	2444.000	563.100	2509.000	563.800	2542.000	

	GR	562,300	2569.000	560.800	2611.000	559,100	2639.000	559.600	25.317.000	556,000	2847.000	<u> </u>
6	GR	556.000	2662.000	556.000	2670.000	559.000	2684.000	560.300	2691.000	570.700	2730.000	34
	GR	570.700	2750.000	571.800	2783.000	575.300	2804.000	599.600	-2835.000	610.900	2880.000	
	GR	625.300	2942.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
6	NH	5.000	0.080	2303.000	0.041	2473.000	0.080	3802.000	0.050	3870.000	0.080	
)	NH	3992.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•
1	-1	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2303.000	3870.000	. •
• 2						65 (0.000)	- 100 at 100			6 6		
3	XI	117.000	67.000	2303.000	2473.000	650.000	175.000	525.000	0.0	0.0	0.0	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
	GR	624.600	1000.000	620.100	1071.000	600.400	1120.000	600.400	1150.000	600.200	1166.000	' '
• 5	GR	595.300	1207.000	592.400	1241.000	589.800	1281.000	589.800	1295.000	584.900	1402.000	1
	GR	588.300	1416.000	588.400	1450.000	586.000	1481.000	585.300	1562.000	575.400	1595.000	
7	GR	573.200	1644.000	572.600	1662.000	572.600	1820.000	571.500	1833.000	571.500	1922.000	
• 1	GR GR	571.500	1963.000	571.500	2048.000	571.500	2070.000	571.500	2080.000	570.500	2103.000	
, "	GR	570.100	2164.000	568.300	2203.000	568.300	5566.000	567.500	2303.000	565.300	2351.000	
, 10	GR	564.200	2356.000	562.000	2359.000	553.700	2370.000	553.700	2381.000	553.700	2381.000	The state of the s
• 11	GR	571.100	2402.000	564.300	2410.000	565.100	2420.000	570.000	2473.000	570.300	2522.000	'•
" I	GR	560.600	2580.000	570.300	2620.000	570.100	2700.000	569.400	2755.000	568.800	2830.000	
13	GR	566.000	2894.000 3150.000	566.400 567.500	2943.000 3201.000	565.800	2990.000	566.000	3040.000	567.500	3100.000	The second second
"	GR	565.000	3802.000	560.500	3814.000	566.500 559,200	3400.000	566.500	3600.000	565.800	3788.000	'o
14	GR	557.000	3856,000	559.200	3858.000	572.500	3822.000	557.000	3835.000	557.000	3842.000	10
6 12	GR	574.800	3931.000	625.300	3992.000	0.0	3870.000	572.500	3890.000	575.000	3904.000	
"	NC	0.100	0.100	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
19 [NH	5.000	0.080	2041.000	0.039	2242.000	0.080	3615.000	0.0	0.0	0.0	11
-70	NH	3835.000	0.0	0.0	0.0	0.0	0.0	0.0	0.050	3723.000	0.090	,,
21	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2041.000	3723.000	
72									0.0	2041.000	3123.000	ж
€ 23	X1	118.000	48.000	2041.000	2242.000	270.000	250.000	265.000	0.0	0.0	0.0	15
24.	GR	625.200	1000.000	616.300	1041.000	604.300	1102.000	604.100	1108.000	604.100	1142.000	
25	GR	601.300	1151.000	595.100	1205.000	592.800	1267.000	592.800	1277.000	591.100	1296.000	16
-26	GR	586.200	1391.000	586.200	1422.000	584.300	1439.000	582.500	1501.000	581.800	1551.000	n_
17	GR	574.800	1591.000	573.800	1600.000	574.900	1603.000	576.100	1621.000	574.200	1644.000	
28	GR	570.100	1682.000	574.100	1722.000	574.100	1743.000	572.800	1762.000	570.500	1800.000	" 2
6 129	GR	572.300	1891.000	572.100	1903.000	570.900	1958.000	572.100	2000.000	571.900	2041.000	19 Å
30	GR	570.100	2050.000	564.500	2068.000	562.500	2072.000	560.700	2077.000	560.700	2210.000	10 €
31	GR	570.000	2242.000	570.500	2455.000	570.000	2668.000	566.000	3348.000	568.000	3595.000	
●37	GR	568.000	3615.000	560.000	3644.000	558.000	3670.000	558.000	3705.000	568.000	3723.000	21
33	GR	575.000	3736.000	575.000	3760.000	625.000	3835.000	0.0	0.0	0.0	0.0	22
31	NC	0.080	0.080	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
•35	FT	0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	0.0	0.0	23
36	X1	119.000	() () ()	1000 000	0100 000	0.000,040						14
- "	x3	10.000	60.000	1892.000	2103.000	435.000	390.000	420.000	0.0	0.0	0.0	
30	GR	625.300	1000.000	0.0 611.100	0.0	0.0	0.0	0.0	573.100	560.000	0.0	° a
	SR	600.350	1275.000	594.800	1325.000	605.400	1166.000	603.500	1179.000	603.500	1195.000	26
-0	GR	580.300	1544.000	579.800	1551.000	592.500 579.800	1371.000	589.700	1412.000	586.200	1468.000	n
17	GR	577.200	1644.000	577.200	1681.000	577.000	1603.000	579.800 574.600	1607.000	579.800	1635.000	
0	GR	572,500	1763.000	570.500	1810.000	571.100	1881.000	573.100	1712.000	572.500	1751.000	28
-41	GR	563.400	1928.000	561.400	1940.000	561.400	1982.000	561.400	1892.000	565.400 563.400	1917.000	79
45	GR	564.200	2044.000	572.500	2103.000	571.300	2211.000	570.000	2350.000	567.900	2037.000	
46	GR	566.700	2944.000	567.600	3022.000	568.100	3167.000	567.900	3182.000	562.300	3209.000	736
6 47	GR	560.700	3214.000	559.200	3219.000	559.200	3230.000	559.200	3238.000	560.700	3247.000	31
41	GR	561.900	3254.000	567.500	3292.000	567.000	3396.000	566.800	3437.000	566.400	3593.000	
49	GR	564.700	3672.000	560.800	3727.000	559.700	3735,000	560.300	3743.000	574.500	3772.000	**
6 14	GR	574.500	3792.000	576.300	3802.000	582.600	3812.000	599.300	3828.000	626.100	3874.000	33
51	FT	0.0	0.0	0.0	0.0	16.400	0.0	0.0	0.0	0.0	0.0	.9
52												· · · · · · · · · · · · · · · · · · ·
	X1	120.000	53.000	1379.000	1569.000	795.000	660.000	765.000	70.0	0.0	0.0	15 8
	GR	625.600	1000.000	616.300	1029.000	614.100	1068.000	611.200	1087.000	611.000	1099.000	36
	GR	597.500	1140.000	597.300	1163.000	595.700	1166.000	594.700	1201.000	593.100	1252.000	-
	GR	576.500	1296.000	576.500	1308.000	576.500	1314.000	576.500	1340.000	575.200	1379.000	31
	GR	568.900	1401.000	565.800	1418.000	563.000	1433.000	563.000	1468.000	563.000	1500.000	
	GR	565.800	1520.000	566.900	1528.000	573.500	1569.000	572.900	1720.000	572.000	1912.000	
	GR	569.800	2206.000	566.000	2380.000	567.300	2417.000	564.600	2440.000	563.400	2444.000	31
	GR	560.800	2453.000	560.800	2460.000	560.800	2460.000	563.400	2473.000	564.200	2480.000	

	副設 こと こ 政策を	568.200	Solden W. St. a. South . St. of . South	-				The second				
	GR	566.300	2851.000	567.400	2609.000	568.100	2690.000	565.300	2804.000	564.400	2829.000	OF
	GR	560.800	3319.000	568.300	3022.000	566.100	3198.000	565.600	3262.000	562.700	3314.000	35
	GR	576.700		561.500	3323.000	562.700	3388.000	573.100	3431.000	573.300	3451.000	
	NC		3459.000	599.400	3483.000	626.100	3535.000	0.0	0.0	0.0	0.0	
•	ET	0.080	0.080	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
		0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	0.0	0.0	
4	٠.		- 4 部分 () () ()					TO THE STORY OF				
• 2	X1	121.000	45.000	1244.000	1379.000	850.000	780.000	840.000	0.0	0.0	0.0	
3	GR	625.400	1000.000	612.100	1052.000	601.900	1105.000	599.700	1127.000	599.200	1157.000	
4	GR	580.400	1187.000	580.400	1194.000	568.900	1244.000	564.500	1249.000	564.000	1250.000	1
. 5	GR	564.000	1311.000	564.000	1370.000	564.500	1371.000	570.000	1379.000	572.800		
6	GR	571.400	1563.000	570.500	1748.000	571.200	1897.000	572.800	1953.000	574.100	1404.000	
7	GR	572.800	2212.000	-570.800	2325.000	567.700	2364.000	564.800	2390.000		2109.000	
- 1	GR	562.100	2418.000	564.000	2437.000	564.800	2445.000	567.200	2477.000	564.000	2399.000	
9	GR	564.600	2616.000	566.900	2667.000	567,500	2802.000	568.000	2998.000	566.800	2550.000) `
10	GR	568.200	3398.000	570.600	3434.000	568.300	3442.000	566.800	3449.000	567.200	3145.000	
3 0	GR	577.900	3472.000	577.900	3488.000	580.100	3500.000	601.300	3522.000	567.300	3455.000	
17	NC	0.080	0.080	0.039	0.100	0.300	0.0			624.700	3561.000	
13	OT	5.000	20000.000	38000,000	48800.000	48800.000	87000.000	0.0	0.0	0.0	0.0	
14,	FT	0.0	0.0	0.0	0.0	10.400		0.0	0.0	0.0	0.0	
15		The second			y - X (5)	10.700	0.0	0.0	0.0	0.0	0.0	es. 'o
16	XI	155.000	51.000	1261.000	1352.000	720.000	650.000	715 000			*	10
17	GR	624.300	1000.000	605.300	1067.000	602.800	1074.000	715.000	0.0	0.0	0.0	
18	GR	582.600	1135.000	581.100	1150.000	572.800	1176.000	602.800	1094.000	582.700	1128.000	"
19	GR	573.400	1261.000	570.500	1267.000	565.000	1278.000	576.700	1231.000	574.800	1252.000	12
70	GR	570.500	1342.000	573,600	1352,000	575.200	1383.000	565.000	1303.000	565.000	1325.000	
21	GR	575.500	1575.000	576.100	1789.000	575.600		576.700	1432.000	573.800	1530.000	113
E.	GR	573.800	2301.000	571.900	2450.000	568.900	1982.000	574.800	2066.000	574.100	5500.000	14
23	GR	567.100	2603.000	565.500	2609.000	563.000	2533.000	563.200	2567.000	570.800	2590.000	
24	GR	565.500	2648.000	568.100	2658.000		2619.000	563.000	2628.000	563.000	2638.000	15
25	GR	567.200	3066.000	568.300	3188.000	572.300	2710.000	568.800	2750.000	569,200	2879.000	16
_ 26	GR	580.200	3464.000	580.300	3483.000	570.100	3358.000	578.200	3412.000	581.300	3448.000	
7,	GR	624.700	3597.000	0.0		598.100	3512.000	598.100	3530.000	599.800	3537.000	17
28	NC	0.080	0.080	0.039	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15
	OT	5.000	20000.000	38000.000	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
10	ET	0.0	0.0		48800.000	42400.000	87000.000	0.0	0.0	0.0	0.0	19
n H	table Militar		0.0	0.0	0.0	17.400	0.0	0.0	0.0	0.0	0.0	10
- 11	X1	123.000	43.000	1220 000	1500 000					1	5 5 W. L. C. C.	The state of the s
	GR	624.800	1000.000	1328.000	1502.000	550.000	600.000	545.000	0.0	0.0	0.0	21
	GR	594.600	1222.000	610.300	1039.000	608.200	1073.000	603.100	1105.000	594.600	1199.000	7
	GR	571.100	1335.000	594.800	1239.000	574,600	1278.000	573.900	1311.000	573.300	1328.000	
	GR	575.200		567.000	1350.000	567.000	1408.000	567.000	1470.000	571.100	1478.000	in the state of th
	GR	574.000	1487.000	578.300	1502.000	576.100	1575.000	574.100	1648.000	573.500	1950.000	,,
	GR	570.700	2200.000	573.500	2450.000	574.200	2738.000	573.500	2922.000	572.000	3100.000	
	GR	567.000	3132.000	567.000	3147.000	564.700	3156.000	564.700	3167.000	564.700	3178.000	8
1000	GR	573.100	3188.000	568.800	3195.000	573.100	3218.000	571.400	3300.000	571.500	3400.000	
	GR		3550.000	582.100	3580.000	582.100	3601.000	582.100	3629.000	583.500	3675.000	
	NC	584.100	3709.000	599.800	3738.000	624.800	3778.000	0.0	0.0	0.0	0.0	n_
	O.L	0.080	0.080	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
			17200.000	32900.000	42400.000	42400.000	77000.000	0.0	0.0	0.0	0.0	Total Control of the
•	FT	0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	0.0	0.0	29
	V 1	100 500							7+	100		
	X1	123.500	34.000	1328.000	1545.000	300.000	1500.000	300.000	0.0	0.0	0.0	
	K3 GR	16.000	0.0	0.0	0.0	0.0	0.0	0.0	573.300	579.000	0.0	11
		624.800	1000.000	610.300	1039.000	608,200	1073.000	603.100	1105.000	594.600	1199.000	
	GR	594.600	1222.000	594.800	1239.000	574.600	1278.000	573.900	1311.000	573.300	1328,000	
	GR	571.100	1335.000	567.000	1350.000	567.000	1498.000	567.000	1470.000	571.100	1478.000	33
21	GR	575.200	1487.000	581.000	1545.000	580.000	1580.000	575.000	1880.000	573.500	2580.000	
	GR	575.000	2700.000	573.500	2850.000	575.000	2930.000	572.000	3170.000	575.000	3500.000	, ч
	GR	580.000	3700.000	578.000	4100.000	580.000	4270.000	580.000	4470.000	590.000	4680.000	35
	3R	590.000	4710.000	595.000	5450.000	600.000	5580.000	625.000	5700.000			
	AC.	0.080	0.080	0.039	0.300	0.800	0.0	0.0		0.0	0.0	36
• F	ET	0.0	0.0	0.0	0.0	8.400	0.0	0.0	0.0	0.0	0.0	,,
57			American State				•••	0.0	0.0	0.0	0.0	
58	(1	124.000	39.000	1266.000	1556.000	320.000	350 000	730 000	8 0000000000000000000000000000000000000			n 3
	(3	10.000	0.0	0.0	0.0		350.000	320.000	0.0	0.0	0.0	
	R	629.300	1000.000	611.800	1056.000	0.0	0.0	0.0	592.800	579.500	9.0.0	
Sec. 198	The state of the s	NEW TOWNSHIP AND ADDRESS OF THE PARTY OF THE		211.000	1030.000	599.800	1075.000	583.000	1096.000	583.000	1109.000	

							Example to the first of the	10000000000000000000000000000000000000				36
	GR	575.300	1127.000	580.500	1160.000	577.100	1179.000	575.700	1187.000	580.300	1196.000	30
	GR	592.800 571.800	1266.000	590.700	1310.000	589.300	1326.000	580.700	1350.000	575.700	1371.000	
	GR		1387.000	568.000	1403.000	568.000	1443.000	568.000	1502.000	571.800	1513.000	
	GR	574.100 575.000	1520.000	585.500	1556.000	587.000	1856.000	582.500	2101.000	581.000	2400.000	
	GP	577.500		573.000	2830.000	575.000	2930.000	580.000	3300.000	580.000	3480.000	
.1	GR	590.000	4560.000	580.000	3730.000	581.000	4050.000	585.000	4480.000	590.000	4530.000	
	OR	390.000	4560.000	595.000	5200.000	600.000	5330.000	625.000	5520.000	0.0	0.0	
	X1	124.100	0.0	0.0	0.0	115.000	350.000	115.000	0.0	0.600	0.0	
1	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	593.400	580.100	0.0	1
	NC	0.080	0.080	0.041	0.300	0.800	0.0	0.0	0.0	0.0	0.0	;'
	FT	0.0	0.00	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	
1	- M. 21.00							CONTROL CONTROL CONTROL CONTROL				4
	X1	126.010	39.000	1269.000	1425.000	115.000	350.000	115.000	0.0	0.0	0.0	and the second second second
, ,	X3	10.000	0.0	0.0	0.00	0.0	0.0	0.0	591.000	581.500	0.0	
10	GR	630.400	1000.000	630.200	1009.000	624.400	1029.000	600.500	1100.000	594.200	1108.000	and the second s
• II	GR	580.700	1138.000	581.700	1238.000	581.700	1251.000	575.900	1269.000	575.900	1269.000	'•
12	GR	568.000	1334.000	568.000	1347.000	568.000	1393.000	576.600	1408.000	577.600	1425.000	
13	GR	577.600	1425.000	580.000	1440.000	580,000	3590.000	592.000	3618.000	592.000	3638.000	
14	GR	592.300	3655.000	593.900	3691.000	594.100	3814.000	594.500	3913.000	594.700	4001.000	*
15	GR	594.800	4071.000	594.900	4144.000	594.800	4231.000	594.500	4333.000	594.600	4430.000	10
16	GR	594.900	4481.000	597.600	4558.000	598.900	4653.000	598,900	4744.000	599.800	4782.000	
O 17	GR	603.800	4843.000	609.600	4901.000	620.500	4960.000	630.200	5032.000	0.0	0.0	"
18	SB	0.900	1.500	3.000	0.0	106.000	6.000	2470.000	1.280	568.000	568.000	n
15	X1	126.020	0.0	0.0	0.0	80.000	90 000	00 000				,,
	χż	0.0	0.0	1.000	584.700	585.500	80.000	80.000	0.0	0.0	0.0	
27	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0 593.100	0.0	0.0	14
73	BT	42.000	1157.000	595.300	0.0	1184.000	590.500	0.0	1216.000	585.500 594.200	0.0	15
74	BT	1239.000	594.200	0.0	1335.000	593.700	0.0	1508.000	592.500	0.0	1594.000	
25	RT	592.100	0.0	1667.000	591.900	0.0	1716.000	591.700	0.0	1813.000	591.500	16
26	BT	0.0	1883.000	591.200	0.0	1932.000	590.700	0.0	2043.000	589.500	0.0	17_
บ	RT	2184.000	589.200	0.0	2312.000	588.500	0.0	2418.000	587.900	0.0	2567.000	
28	BT	587.100	0.0	2727.000	586.700	0.0	2814.000	586.400	0.0	2912.000	586.100	
● 29	RT	0.0	3051.000	585.900	0.0	3161.000	585.500	0.0	3374.000	585.500	0.0	11_6
30	BT	3497.000	585.500	0.0	3612.000	585.500	0.0	3745.000	585.500	0.0	3869.000	70
31	BT	586.100	0.0	3967.000	586.600	0.0	4057,000	588.000	0.0	4210.000	592.000	
9 2	RT	0.0	4227.000	592.300	0.0	4263.000	593.900	0.0	4386.000	594.100	0.0	i o
33	BT	4485.000	594.500	0.0	4573.000	594.700	0.0	4643.000	594.800	0.0	4716.000	n
34	RT	594,900	0.0	4803.000	594.800	0.0	4905.000	594.500	0.0	5002.000	594.600	73
• »	NC	0.0	5053.000	594.900	0.0	5130.000	597.600	0.0	0.0	0.0	0.0	
	ET	0.100	0.060	0.039	0.300	0.800	0.0	0.0	0.0	0.0	0.0	и
-		0.0		30.00	0.0	8.400	0.0	0.0	0.0	0.0	0.0	25 _
34	X1	127.000	42.000	1103.000	1254.000	900.000	100,000	835.000	0.0	0.0	0.0	
40	GR	630.400	1000.000	607.500	1047.000	582.800	1087.000	582.800	1103.000	575./00	1117.000	26
	GR	574.500	1127.000	570.500	1160.000	570.500	1176.000	570.500	1179.000	574.500	1228.000	n
42	GR	575.400	1239.000	578.900	1254.000	581.000	1295.000	580.900	1392.000	581.900	1524.000	.9,
4)	GR	580.500	1632.000	581.300	1674.000	580.100	1730.000	579.600	1805.000	584.500	1895.000	
9 4	GR	584.500	3065.000	592.000	3093.000	592.000	3113.000	592.300	3702.000	593.900	3738.000	29
45	GR	594.100	3861.000	594.500	3960.000	594.700	4048.000	594.800	4118.000	594.900	4191.000	30
46	GR	594.800	4278.000	594.500	4380.000	594.600	4477.000	594.900	4528.000	597.600	4605.000	
1 7	GR	598.900	4700.000	598.900	4791.000	599.800	4829.000	603.800	4890.000	609.600	4948.000	31
41	GR	620.500	5007.000	630.200	5079.000	0.0	0.0	0.0	0.0	0.0	0.0	2 7
45	NC	0.100	0.080	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
●6	FT	. 0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0	· · · · · · · · · · · · · · · · · · ·
31	XI	128.000	50 000	1111 000	1350 000	750 000	750					и
57	GR		50.000	1111.000	1250.000	750.000	350.000	750.000	0.0	0.0	0.0	34 B
9,	GR	650.300 576.200	1300.000	625.600 572.000	1027.000	600.200	1066.000	583.400	1092.000	583.400	1111.000	
55	GR	577.600	1250.000	581.200	1139.000	572.000	1189.000	572.000	1226.000	576.200	1244.000	36
-	GR	583.500	1509.000	580.100	1522.000	582.300 580.100	1323.000	583.100	1394.000	583.300	1454.000	37 _ 9
57	GR	582.200	1801.000	583.100	1877.000	583.800	1892.000	580.300 583.000	1642.000	580.600	1721.000	
58	GR	580.700	2025.000	582.800	2066.000	585.500	2116.000	585.500	2551.000	580.100 592.000	1960.000	
-	GR	592.000	2599.000	592.300	3188.000	593.900	3224.000	594.100	3347.000	594.500	3446.000	79
	GR	594.700	3534.000	594.800	3604.000	594.900	3677.000	594.800	3764.000	594.500	3866.000	
September 1								234.000	3104.000	324.300	3300.000	

	GR	594.600	3963.000	594.900	4014.000	597.600	4091.000	598.900	4186,000	598,900	4277.000	37
•	GR	599.800	4315.000	603.800	4376.000	609.600	4434.000	620.500	4493.000	630.200	4565.000	
	NC	0.100	0.090	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
	ET	0.0	0.0	0.0	0.0	6.400	0.0	0.0	0.0	0.0	0.0	
•				11 12 19 19 19	10.23.000		1000.040	198,003			1.00.000	
E	XI	129.000	44.000	1144.000	1265.000	390.000	475.000	415.000	0.0	0.0	0.0	
	GR	650.300	1000.000	625.600	1039.000	599.000 573.500	1083.000	585.300	1103.000	585.300	1122.000	CANADA CONTRACTOR
0'	GR GR	578.500 576.500	1144.000	576.600 577.900	1158.000	579.800	1180.000	573.500	1200.000	573.500	1220.000	
, ,	GR	578.400	1377.000	581.000	1424.000	581.500	1298.000	581.600 582.400	1332.000	579.100 580.100	1357.000	2
	GR	581.100	1578.000	582.700	1649.000	581.900	1707.000	582.300	1815.000	582.500	2002.000	1_
	GR	583.900	2092.000	584.300	2225.000	582.700	2302.000	592.200	2346.000	592.200	2368.000	
,[GR	594.100	2383.000	594.400	2511.000	594.700	2689.000	594.800	2835.000	594.900	2933.000	, '
	GR	594.800	3081.000	594.900	3151.000	598.000	3242.000	598.100	3344.000	598.400	3415.000	5
	GR	602.500	3479.000	609.900	3551.000	621,500	3632.000	630.600	3736.000	0.0	0.0	
10	NC	0.100	0.090	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
1 11	ET	0.0	0.00	0.0	0.0	8.400	0.0	0.0	0.0	0.0	3370.040	7
12		SEA, SEE			4.74 (4.50)			\$50,500			3664,950	
13	XI	130.000	57.000	1066.000	1180.000	620.000	880.000	632.000	0.0	0.0	0.0	
1 4	GR	650.500	1000.000	625.600	1015.000	600.200	1024.000	589.400	1042.000	589.100	1057.000	'e
15	GR	584.200	1066.000	578.000	1073.000	572.000	1104.000	578.000	1141.000	579.200	1154.000	10
16	GR	583.000	1180.000	578.700	1200.000	583.200	1237.000	584.700	1281.000	584.700	1355.000	n
- O17	GR GR	584.500 585.800	1416.000	584.900 585.400	1487.000 1781.000	584.600 586.100	1564.000 1827.000	584.900	1612.000	584.900	1669.000	
10	GR	587.000	2001.000	587.400	2058.000	587.700	2118.000	587.500 584.800	1887.000 2193.000	586.400 584.400	1946.000	12
-	GR	584.100	2372.000	585.300	2468.000	585.800	2561.000	586.100	2660.000	586.300	2270.000 2765.000	u_
71	GR	586.100	2803.000	595.300	2827.000	595.300	2850.000	595.300	2885.000	595.300	2975.000	
n	GR	603.800	3000.000	605.200	3052.000	606.400	3133.000	604.900	3207.000	604.900	3255.000	"
O 22	GR .	606.000	3276.000	607.800	3382.000	608.100	3450.000	609.700	3514.000	610.800	3589.000	15_
14	GR	614.000	3633.000	614.800	3660.000	616.400	3686.000	622.200	3747.000	627.700	3772.000	16
25	GR	636.400	3800.000	649.800	3853.000	0.0	0.0	0.0	0.0	0.0	0.0	
O 76	NC.	0.050	0.090	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0	"•
n	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	18 8
78		121 000		10/2 000	2075 000	F00 000	26385888	100	1651 200			19
•	K1 GR	131.000	1000.000	1943.000	2075.000	500.000	550.000	800.000	0.0	0.0	0.0	
31	GR	579.700	1137.000	577.000	1024.000	607.000 579.700	1073.000	589,400	1113.000	589.400	1122.000	. 20
31	GR	596.600	1296.000	586.900	1141.000	586.900	1150.000 1546.000	582.900 588.000	1161.000	586.600 588.200	1755.000	21
В	GR	539.500	1841.000	589.000	1923.000	584.700	1943.000	581.600	1955.000	577.000	1974.000	
34	GR	577.000	2002.000	577.000	2019.000	581.600	2063.000	582.800	2075.000	584.900	2103.000	
6 15	GR	584.900	2161.000	584.900	2218.000	583.700	2244.000	584.600	2282.000	582,000	2304.000	n
34	GR	584.700	2325.000	586.700	2348.000	585.500	2377.000	585.100	2396.000	586.600	2416.000	25
is	GR	588.000	2435.000	585.600	2455.000	587.000	2487.000	587.000	2535.000	586.400	2581.000	eren beren er er er er er
3 3	GR	586.400	2640.000	587.400	2701.000	587.800	2774.000	588.600	2822.000	587.700	2937.000	
39	GR	587.900	3006.000	587.900	3076.000	590.200	3138.000	587.800	3189.000	588.200	3227.000	28
40	GR	596.600	3251.000	596.600	3256.000	600.700	3273.000	600.200	3302.000	600.800	3330.000	n n
	GR .	604.400	3350.000	605.600	3412.000	606.900	3526.000	608.000	3618.000	612.500	3751.000	
47	GR GR	612.900	3824,000	613.500	3882.000	613.300	3897.000	613.900	3923.000	614.900	3967.000	18
-	NC	0.050	0.090	625.200	4030.000	636,500	4072.000	650.600	4135.000	0.0	0.0	29
-45	FT	0.050	0.090	0.041	0.100	0.300 7.400	0.0	0.0	0.0	0.0	0.0	
46								· · ·		0.0		
•	X1	132.000	69.000	2301.000	2492.000	340.000	250.000	550.000	0.0	0.0	0.0	11
48	GR	637.400	1000.000	614.800	1033.000	589.700	1090.000	589.700	1102.000	582.400	1117.000	n i
49	GR	580.500	1121.000	582.400	1131.000	585.400	1148.000	586.800	1200.000	587.300	1269.000	
	GR	588.200	1344.000	588.100	1451.000	588.500	1585.000	589.700	1688.000	589.600	1768.000	12
	GR	587.400	1847.000	586.900	1878.000	589.600	1930.000	588.400	2005.000	587.400	2086.000	и
52	GR	586.600	2132.000	587.400	2146.000	589.400	2198.000	589.800	2284.000	589.400	2301.000	₂₅
	GR	586.600	2315.000	584.500	2322.000	580.000	2339.000	584.500	2360.000	586.000	2371.000	• • • • • • • • • • • • • • • • • • • •
54	GR	586.300	2372.000	584.500	2379.000	580.000	2395.000	580.000	2417.000	580.000	2430.000	34
	GR	584.500	2470.000	586.000	2483.000	586.800	2492.000	587.400	2565.000	588.300	2597.000	n g
	GR	587.200	2684.000	585.600	2715.000	588.000	2755.000	587.500	2819.000	589.200	2872.000	• 3
	GR	590.200	2941.000	590.800	3001.000	590.600	3089.000	590.400	3130.000	587.100	3173.000	и ">
	GR	587.600	3194.000	606.000	3254.000	606.600	3332.000	607.600	3373.000	606.000	3386.000	39
	GR	606.000	3413.000	605.600	3422.000	603.300	3455.000	608.700	3538.000	609.900	3595.000	
	GR	612.200	3670.000	614.800	3803.000	616,700	3905.000	617.200	4005.000	618.200	4036.000	

2837,000 3045,000 3215,000 3447,000 3665,000 0.050 0.0 52,000 1000,000 1706,000 1861,000 2028,000 2367,000 2572,000 2898,000 3069,000 3304,000 3588,000 0.050	595.200 586.000 605.000 614.600 619.700 0.039 0.0 2476.000 624.800 594.600 594.800 594.800 594.800 594.800 594.800 601.300 612.200 649.700 0.039	2930.000 3075.000 3270.000 3509.000 3677.000 0.100 0.0 2678.000 1307.000 1725.000 1878.000 2040.000 2431.000 2637.000 2930.000 3389.000 3389.000	595.100 586.000 605.200 614.600 622.000 0.300 8.400 310.000 600.300 594.700 593.700 593.700 595.500 594.800 595.300	2970.000 3076.000 3290.000 3547.000 3700.000 0.0 580.000 1100.000 1413.000 1791.000 1891.000 2150.000	593.800 592.000 608.000 615.500 637.000 0.0 0.0 600.000 596.200 594.800 593.100	2989.000 3150.000 3297.000 3568.000 0.0 0.0 0.0 1117.000 1519.000	592.000 593.500 611.100 616.800 649.300 599.376 0.0 596.200 596.200	3002.000 3168.000 3346.000 3621.000 3795.000 0.0 0.0	38
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	GR	592.100	1129.000	594.300	1160.000	594.900	1169.000	596.400	1203.000	597.400	1221.000	•
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	GR	598.300	2845.000	599.900	2878.000	598.000	2885.000	604.100	2917.000	604.100	2939.000	
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11	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1220.000	2335.000	√ ′•
13	XI	142.000	50.000	1277.000	1446.000	365.000	350.000	365.000	0.0	0.0	0.0	
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	GR	598.500	1566.000	598.700	1597.000	598.700	1655.000	598.100	1718.000	598.200	1787.000	n
	GR	598.700	1847.000	599.100	1928.000	600.100	1999.000	598.700	2065.000	600.200	2103.000	
	GR GR	600.700	2197.000	601.300	2298.000	601.700 599.600	2453.000	602.000	2563.000 2949.000	601.900	2662.000	•
	GR	599.800	2974.000	603.700	3000.000	604.700	3024.000	604.700	3039.000	604.700	2965.000 3190.000	ļu .
	GR	614.800	3209.000	614.800	3222.000	625.400	3239.000	637.300	3277.000	649.900	3314.000	в
CONTRACTOR STATE	NC	0.0	0.0	0.0	0.100	0.600	0.0	0.0	0.0	0.0	0.0	16
25	ET	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0	II _
	X1	143.010	50.000	1222.000	1385.000	260.000	267.000	267.000	0.0	-0.700	0.0	n N
	GR	650.000	1000.000	637.800	1058.000	626.700	1115.000	625.700	1179.000	604.800	1204.000	
	GR GR	592.000	1214.000	598.500 595.800	1222.000	595.800 596.900	1228.000	592.000 600.000	1236.000	592.000	1272.000	"●;
	GR	602.600	1460.000	601.800	1477.000	601.800	1509.000	602.200	1385.000	601.400	1444.000	20
	GR	602.700	1755.000	602.200	1807.000	602,600	1835.000	601.600	1864.000	602.100	1921.000	21
	GR	602.200	2003.000	602.600	2102.000	602.800	2223.000	602.400	2319.000	602.000	2433.000	n
	GR GR	602.800	2523.000	610.300	2656.000 2925.000	604.900 610.300	2739.000 2935.000	604.900	2815.000	606.300	2882.000 2959.000	n
	GR	612.400	2980.000	612.400	3008.000	613.500	3066.000	613.700	3115.000	614.200	3156.000	14
TOTAL STATE OF THE	GR	614.700	3238.000	615.200	3325.000	616.300	3367.000	627.300	3403.000	650.100	3463.000	
STATE OF THE PARTY	NC	0.0	0.0	0.0	0.100	0.300	0.0	0.0	0.0	0.0	0.0	B •
40	ET	.0.0	0.0	0.0		6.400	. 0.0	0.0	0.0	0.0	0.0	14
	X1	143.000	0.0	0.0	0.0	260.000	268.000	268.000	0.0	0.700	0.0	n
	NC	0.0	0.060	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	п
0	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	25
45	X1	144.000	66.000	1606.000	1796.000	570.000	330.000	600.000	0.0	0.0	0.0	
	GR	650.100	1000.000	636.400	1067.000	629.200	1126.000	625.800	1163.000	604.200	5.000	Exercise the season of the sea
	GR GR	604,800	1208.000	599.400	1229.000	598.400	1245.000	597.900	1254.000	598.500	0.000	
	GR	599.600	1271.000	598.900	1328.000	601.600 599.200	1379.000	599.300 602.300	1419.000	602.900	1- 3.000	11
Charles Service	GR	598.900	1638.000	598.000	1646.000	597.000	1656.000	597.000	1700.000	597.000	1754.000	B
	GR	598.000	1759.000	599.600	1767.000	603.500	1796.000	603.500	1831.000	604.400	1888.000	34
	GP	604.000	1939.000	604.600	2008.000	603.000	2068.000	602.100	2106.000	596.300	2143.000	14 8
	GR GR	596.700 603.500	2169.000	604.900	2186.000	603.200	2246.000	502.100	2309.000	603.000	2397.000	
	GR	607.900	2840.000	603.400	2545.000	603.500	2625.000	605.600	2678.000 3006.000	606.600	2756.000 3014.000	36
THE RESERVED TO SERVED TO	GR	611.000	3034.000	614.400	3049.000	614.400	3070.000	616.000	3091.000	616.900	3149.000	37 0
	GR	617.300	3229.000	617.100	3301.000	615.600	3313.000	616.300	3349.000	616.800	3422.000	, ~
	GR	617-600	3489.000	618.300	3571.000	620.100	3621.000	622.900	3644.000	633.100	3683.000	•
	GR NC	650.100	3732.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
		0.0	0.050	0.0	0.0	0.0	0.0	0.0	0.0	0.0.	0.0	

### 25 10 10 10 10 10 10 10 1		K1 SR SR SR SR SR SR SR SR SR SR SR SR SR	145.000 650.100 608.200 599.300 600.400 604.100 597.800 609.400 613.000 616.700 618.700 649.900	56.000 1000.000 1211.000 1273.000 1450.000 1669.000 1810.000 2340.000 2340.000 2340.000 3106.000 3313.000 3723.000	1669.000 639.700 608.200 601.300 599.300 600.500 599.000 608.400 613.300 616.700 621.200 0.0	375.000 637.100 599.300 604.500 599.000 600.200 608.400 611.400 613.500 614.900 624.600 0.0	0.0 620.000 1080.000 1247.000 1354.000 1502.000 1699.000 2099.000 2477.000 2825.000 3167.000 3600.000 0.0	0.0 560.000 630.700 597.800 604.100 604.700 597.800 604.400 608.800 610.600 614.400 629.200 0.0	0.0 0.0 1135.000 1251.000 1414.000 1572.000 1707.000 1860.000 2128.000 2552.000 2923.000 3181.000 3577.000 0.0	0.0 622.400 597.800 604.800 604.400 597.800 604.400 607.700 611.000 616.100 617.900 634.500 0.0	0.0 1186.000 1285.000 1255.000 1431.000 1618.000 1771.000 1912.000 2230.000 2637.000 3010.000 3241.000 3629.000 0.0	40
# 1	### ### #### #########################					**************************************			Andrews Andrews		(
The state of the s	######################################		\$1201 E	48	10.00	14 25 E 17 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		386 28	THE STATE OF THE S	4/A 4/A 4/A 1/A 1/A 1/A 1/A 1/A 1/A 1/A 1/A 1/A 1	1	
## 14	## 15		**************************************	25, 18. 25, 18.					1990.00 2062.75 2062.85			
			4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	25.17 40 25.15 40 56.48	32 4 39		101 3 0 5 1 1 1 6 5 7 1 6 6 5 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 6 7 1 6 6 7 1 6 6 7 1 6 6 7 1 6 6 7 1 6	4/7				

	HANNEL MIN E			MIN EL DISCHARGE GROUND %CFS<	CWSEL TQ	EG	TOPWID	STENCL	STENCR	WSELK	
36.30	130.00	513.00	532.00	475.00 24300.00	491.37 5194.89	492.31	312.44	0.0	0.0	0.0	
36.30	130.00	513.00	532.00	475.00 45700.00	494.83 8153.49	496.64	365.82	0.0	0.0	0.0	
36.30	130.00	513.00	532.00	475.00 58500.00	496.80 10007.84	499.01	381.85	0.0	0.0	0.0	
36.30	130.00	513.00	532.00	475.00102000.00	502.40 16074.20	505.77	427.53	0.0	0.0	0.0	
36.40	10.00	0.0	0.0	475.00 24300.00	491.40 5213.40	492.33	312.51	0.0	6.0	0.0	
36.40	10.00	0.0	0.0	475.00 45700.00	494.87 8184.41	496.67	366.10	0.0	0.0	0.0	
36.40	10.00	0.0	0.0	475.00 58500.00	496.85 10044.53	499.05	382.16	0.0	0.0	. 0.0	
36.40	10.00	0.0	0.0	475.00102000.00	502.46 16126.57	505.81	427.89	0.0	0.0	0.0	
38.00	100.00	0.0	0.0	476.50 24300.00	492.14 9932.24	492.58	346.49	0.0	0.0	0.0	
/ 38.00	100.00	0.0	0.0	476.50 45700.00	496.21 14895.58	497.10	380.71	0.0	0.0	0.0	1
= 38.00	100.00	0.0	0.0	476.50 58500.00	498.40 18317.72	499.54	391.05	0.0	0.0	0.0	
38.00	100.00	0.0	0.0	476.50102000.00	504.51 29442.75	506.44	420.17	0.0	0.0	0.0	
39.00	315.00	0.0	0.0	477.60 24300.00	492.57 9473.18	492.81	821.36	0.0	0.0	0.0	
39.00	315.00	0.0	0.0	477.60 45700.00	497.10 17774.74	497.47	841.49	0.0	0.0	0.0	
39.00	315.00	0.0	0.0	477.60 58500.00	499.54 23146.87	499.97	852.26	0.0	0.0	0.0	
39.00	315.00	0.0	0.0	477.60102000.00	506.45 41619.26	507.06	881.66	0.0	0.0	0.0	
40.00	410.00	0.0	0.0	478.60 24300.00	492.89 16807.83	492.96	1786.08	0.0	0.0	0.0	
40.00	410.00	0.0	0.0	478.60 45700.00	497.53 37058.72	497.61	1804.09	0.0	0.0	0.0	
7 40.00	410.00	0.0	0.0	478.60 58500.00	500.01 50628.57	500.10	1813.74	0.0	0.0	0.0	
40.00	410.00	0.0	0.0	478.60102000.00	507.08 98514.19	507.19	1839.82	0.0	0.0	0.0	
41.00	460.00	0.0	0.0	478.00 24300.00	492.99 18660.50	493.04	2471.42	0.0	0.0	0.0	
41.00	460.00	0.0	0.0	478.00 45700.00	497.61 44677.93	497.67	2699.92	0.0	0.0	0.0	
41.00	460.00	0.0	0.0	478.00 58500.00	500.10 63092.50	500.15	2711.76	0.0	0.0	0.0	
41.00	460.00	0.0	0.0	478.00102000.00	507.17130072.00	507.23	2740.82	0.0	0.0	0.0	
42.01	250.00	0.0	0.0	477.00 24300.00	493.01 8779.41	493.24	1888.58	0.0	0.0	0.0	
42.01	250.00	0.0	0.0	477.00 45700.00	497.63 26593.81	497.74	2862.30	0.0	0.0	0.0	
42.01	250.00	0.0	0.0	477.00 58500.00	500.11 41802.78	500.20	2896.01	0.0	0.0	0.0	
42.01	250.00	0.0	0.0	477.00102000.00	507.18102388.44	507.26	2924.02	0.0	0.0	0.0	
42.02	25.00	0.0	0.0	477.00 24300.00	493.03 8885.16	493.26	1890.22	0.0	0.0	0.0	
42.02	25.00	0.0	0.0	477.00 45700.00	497.64 26730.49	497.75	2862.37	0.0	0.0	0.0	
42.02	25.00	0.0	0.0	477.00 58500.00	500.12 41937.76	500.21	2896.02	0.0	0.0	0.0	
42.02	25.00	0.0	0.0	477.00102000.00	507.18102521.31	507.26	2924.03	0.0	0.0	0.0	
42.10	25.00	492.00	493.00	477.00 24300.00	493.08 6756.94	493.30	1897.50	0.0	0.0	0.0	
42.10	25.00	492.00	493.00	477.00 45700.00	497.65 20949.54	497.76	2862.33	0.0	0.0	0.0	
42.10	25.00	492.00	493.00	477.00 58500.00	500.12 34587.50	500.22	2896.00	0.0	0.0	0.0	
42.10	25.00	492.00	493.00	477.00102000.00	507.54106134.69	507.62	2926.07	0.0	0.0	0.0	
42.20	50.00	0.0	0.0	477.00 24300.00	493.13 9048.16	493.34	1904.68	0.0	0.0	0.0	
42.20	50.00	0.0	0.0	477.00 45700.00	497.68 25753.40	497.79	2862.72	0.0	0.0	0.0	
42.20	50.00	0.0	0.0	477.00 58500.00	500.14 41924.42	500.23	2896.07	0.0	0.0	0.0	
42.20	50.00	0.0	0.0	477.00102000.00	507.55106071.94	507.62	2926.09	0.0	0.0	0.0	
	en and the second							0.0	0.0		

SECT	ER I	CHANNEL	ROADWAY	LOW	CHORD	GROUND	DISCHARGE %CFS<	CWSEL	то	EG	TOPWID	STENCL	STENCR	WSELK	
	43.00	230.		0.0	0.0		24300.00		19580.02	THE PARTY OF A STATE OF THE PARTY OF THE PAR	2708.79	0.0	0.0	0.0	
	43.00	230.		0.0	0.0	THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	45700.00		47251.38	497.83	3320.94	0.0	0.0	0.0	
	43.00	230.		0.0	0.0		58500.00		67731.44	500.26		0.0	0.0	0.0	
V '	43.00	230.	0.0	0.0	0.0	481.00	102000.00	507.60	148684.81	507.64	3430.94	0.0	0.0	0.0	
	44.00	415.		0.0	0.0		20000.00		4755.85	494.17	599.29	0.0	0.0	0.0	
	44.00	415.		0.0	0.0		38000.00		11566.20	498.35	1565.57	0.0	0.0	0.0	
	44.00	415.		0.0	0.0		48800.00		18298.09	500.63	1621.36	0.0	0.0	0.0	
	44.00	415.	00	0.0	0.0	480.60	87000.00	507.60	49163.30	507.85	1797.10	0.0	0.0	0.0	
Market Street,	45.00	420.	0.0	0.0	0.0	481.50	20000.00	494.02	3531.23	495.31	274.49	0.0	0.0	0.0	
,1	45.00	420.	00	0.0	0.0	481.50	38000.00	497.95	7280.82	499.25	1226.39	0.0	0.0	0.0	
11	45.00	420.	0.0	0.0	0.0	481.50	48800.00	500.34	11911.60	501.19	1238.01	0.0	0.0	0.0	
	45.00	420.	0.0	0.0	0.0	481.50	87009.00	507.62	34045.30	508.09	1646.20	0.0	0.0	0.0	•
	46.00	565.	00	0.0	0.0	482.20	20000.00	495.87	4691.17	496.69	695.42	0.0	0.0	0.0	
	46.00	565.	00	0.0	0.0	482.20	38000.00	499.68	11196.98	500.26	1224.90	0.0	0.0	0.0	
	46.00	. 565.		0.0	0.0		48800.00		15602.67	501.92	1239.34	0.0	0.0	0.0	
	46.00	565.		0.0	0.0		87000.00		40554.98	508.40	1525.57	0.0	0.0	0.0	
	47.00	630.	00	0.0	0.0	484.00	20000.00	497.13	5987.73	497.52	1021.70	0.0	0.0	0.0	
	47.00	630.		0.0	0.0		38000.00		10842.91	500.86	1157.83	0.0	0.0	0.0	
/ IVI	47.00	630.		0.0	0.0		48800.00		13850.42	502.46	1165.89	0.0	0.0	0.0	
	47.00	630.		0.0	0.0		87000.00		30704.48	508.70	1408.68	0.0	0.0	0.0	
1	48.00	610.	00	0.0	0.0	486-00	20000.00	497.80	5331.98	498.30	624.38	0.0	0.0	0.0	
IN	48.00	610.		0.0	0.0		38000.00	CONTRACTOR OF STREET, AND ADDRESS OF STREET, S	9549.41	501.75	929.21	0.0	0.0	0.0	
1 10	48.00	610.		0.0	0.0		48800.00		12099.34	503.36	938.65	0.0	0.0	0.0	
	48.00	610.		0.0	0.0		87000.00		25991.78	509.32	1171.42	0.0	0.0	0.0	4.
1	49.00	555.	00	0.0	0.0	486-30	20000.00	498.62	6123.05	498.98	660.47	0.0	0.0	0.0	
	49.00	555.		0.0	0.0		38000.00		10698.42	502.54	710.94	0.0	0.0	0.0	
	49.00	555.		0.0	0.0		48800.00		13178.26	504.19	723.82	0.0	0.0	0.0	
	49.00	555.		0.0	0.0		87000.00		25334.20	509.99	995.87	0.0	0.0	0.0	
	50.00	465.	0.0	0.0	0.0	486.20	20000.00	499.02	5851.13	499.53	519.18	0.0	0.0	0.0	
	50.00	465.		0.0	0.0		38000.00		9503.86	503.28	543.67	0.0	0.0	0.0	
	50.00	465.		0.0	0.0		48800.00		11412.67	505.05	553.87	0.0	0.0	0.0	
	50.00	465.		0.0	0.0	CONTRACTOR OF THE PARTY OF THE	87000.00		20198.79	510.89	988.51	0.0	0.0	0.0	
SE	CTION	DIS	CHARGE	CWSFL		CWSEL DIF	F CWSFL D	IFF CWS	FI -WSFI K	TOPWID	T.W. DIF	F LEN	GTH.		
	MBER		CFS			EACH Q	EACH SE	CTION	-L HOLLK	.010	1.W. DIF	LLN			
	1.0		00.000		.302	0.0	0.0		0.0	306.922	0.0		0.0		
	1.0		00.000		.697	3.395			0.0	351.926	-45.004		0.0		
	1.0		00.000		.239	1.542			0.0	371.863	-64.941		0.0		
	1.0	10 1020	00.000	467	.641	5.402	0.0		0.0	864.156	-557.234	1	0.0		
	1.0		00.000	461	.105	0.0	3.8	03	0.0	356.227	0.0	450	0.000		
	1.0		00.000		.016	3.911			0.0	498.984	-142.758	451	0.000		
	1.0		00.000		.984	1.968			0.0	750.832	-394.605		0.000		
	1.02	50 1050	00.000	472	.805	5.821	5.1	64	0.0	3811.156	-3454.930	450	0.000		
	1.00	00 243	00.000	462	.443	0.0	1.3	39	0.0	374.895	0.0	686	0.000		
	1.00	00 457	00.000	466	.626	4.182	1.6	10	0.0	681.844	-306.949		0.000		
	1.00	00 585	00.000	468	.694	2.069	1.7		0.0	1052.117	-677.223		0.000		
	1.00	00 1020	00.000	474	.245	5.552	1.4	41	0.0	4771.719	-4396.824		0.000		
	1.10	00 243	00.000	463	.430	0.0	0.9	87	0.0	211.359	0.0	700	0.000		
	1.10		00.000		.666	4.236			0.0	1019.195	-807.836		0.000		
	1.10		00.000		.087	2.421	1.3		0.0	2361.301	-2149.941		0.000		

	HANNEL MIN		K EL OF	MIN EL DISCHARGE GROUND %CFS<	CWSEL TO	Ee	TOPWID	STENCL	STENCR	WSELK	
50.00	805.00	U.0	0.0	461.40 24300.00	477.97 6973.33	478.91	254.86	0.0	0.0	0.0	
20.00	805.00	0.0	0.0	461.40 45700.00	479.60 8533.63	481.91	1147.95	0.0	0.0	0.0	
(20.00	805.00	0.0	0.0	461.40 58500.00	480.81 10256.30	483.48	2014.26	0.0	0.0	0.0	
20.00	805.00	0.0	0.0	461.40102000.00	483.60 16973.63	486.76	2066.44	0.0	0.0	0.0	
20.00	003.00		•••	401.40102000.00	403100 10710103	400010	2000011				
21.00	525.00	0.0	0.0	462.80 24300.00	478.89 7882.23	479.50	504.95	0.0	0.0	0.0	
21.00	525.00	0.0	0.0	462.80 45700.00	481.86 12255.23	483.04	898.54	0.0	0.0	0.0	
₩ 21.00	525.00	0.0	0.0	462.80 58500.00	483.31, 15009.24	484.74	1281.43	0.0	0.0	0.0	
1 21.00	525.00	0.0	0.0	462.80102000.00	485.83 21013.59	488.37	1412.21	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30 24300.00	479.15 9636.12	479.93	195.70	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30 45700.00	482.13 12866.25	483.95	343.94	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30 58500.00	483.46 14422.87	486.00	669.83	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30102000.00	485.45 17163.32	491.33	833.48	0.0	0.0	0.0	
23.01	445.00	v.• v		420420102000400	103,13 11103,32	171.33	000.10				
23.02	30.00	482.50	485.00	458.30 24300.00	479.18 9662.04	479.96	195.77	0.0	0.0	0.0	
23.02	30.00	482.50	485.00	458.30 45700.00	482.92 13768.22	484.57	544.78	0.0	0.0	0.0	
23.02	30.00	482.50	485.00	458.30 58500.00	484.64 16099.46	486.81	832.15	0.0	0.0	0.0	
23.02	30.00	482.50	485.00	458.30102000.00	485.94 18101.68	491.43	847.13	0.0	0.0	0.0	
22.00	EF 00	0.0		458.30 24300.00	479.42 9415.52	480.04	275.86	0.0	0.0	0.0	
23.00	55.00	0.0	0.0	458.30 45700.00	483.42 14284.44	484.73	670.08	0.0	0.0	0.0	
23.00	55.00	0.0	0.0	458.30 58500.00	485.42 17415.54	484.73	841.12	0.0	0.0	0.0	
23.00	55.00 55.00	0.0	0.0	458.30102000.00	489.70 25880.07	492.38	898.11	0.0	0.0	0.0	
7 23.00	25,00	0.0	0.0	430.30102000.00	103.10 25000.01	472.36	070.11	0.0			
24.00	370.00	0.0	0.0	462.80 24300.00	479.48 7312.45	480.46	281.83	0.0	0.0	0.0	
24.00	370.00	0.0	0.0	462.80 45700.00	483.43 11208.77	485.40	409.45	0.0	0.0	0.0	
/R 24.00	370.00	0.0	0.0	462.80 58500.00	485.37 13574.36	487.81	946.12	0.0	0.0	0.0	
24.00	370.00	0.0	0.0	462.80102000.00	489.89 21320.65	493.26	1035.02	0.0	0.0	0.0	
25.00	750.00	0.0	0.0	465.20 24300.00	480.54 6366.38	481.43	761.89	0.0	0.0	0.0	
	750.00	0.0	0.0	465.20 45700.00	486.05 15047.50	486.84	1326.33	0.0	0.0	0.0	
S25.00	750.00	0.0	0.0	465.20 58500.00	488.70 21180.36	489.44	1384.59	0.0	0.0	0.0	
25.00	750.00	0.0	0.0	465.20102000.00	494.43 38335.12	495.27	1427.94	0.0	0.0	0.0	
						•		1			
26.00	450.00	0.0	0.0	465.50 24300.00	481-16 5861.21	482.37	537.07	0.0	0.0	0.0	
F-26.00	450.00	0.0	0.0	465.50 45700.00	486.39 12148.86	487.75	891.35	0.0	0.0	0.0	
26.00	450.00	0.0	0.0	465.50 58500.00	488.95 16448.24	490.31	942.09	0.0	0.0	0.0	
26.00	450.00	0.0	0.0	465.50102000.00	494.60 28636.33	496.27	1023.77	0.0	0.0	0.0	
27.00	540.00	0.0	0.0	467.80 24300.00	482.39 8177.28	483.05	553.55	0.0	0.0	0.0	
27.00	540.00	0.0	0.0	467.80 45700.00	487.41 15303.75	488.37	631.89	0.0	0.0	0.0	
1 27.00	540.00	0.0	0.0	467.80 58500.00	489.77 19453.89	490.88	733.77	0.0	0.0	0.0	
27.00	540.00	0.0	0.0	467.80102000.00	495.17 30914.83	496.88	798.17	0.0	0.0	0.0	
28.00	940.00	0.0	0.0	468.50 24300.00	483.24 6423.10	484.17	378.89	0.0	0.0	0.0	
, 28.00	940.00	0.0	0.0	468.50 45700.00	488.12 11791.41	489.58	436.38	0.0	0.0	0.0	
/ V 28.00	940.00	0.0	0.0	468.50 58500.00	490.40 14875.47	492.17	592.05	0.0	0.0	0.0	
28.00	940.00	0.0	0.0	468.50102000.00	495.72 23818.45	498.50	687.84	0.0	0.0	0.0	

	HANNEL MIN E		C EL OF	MIN EL DISCHARGE GROUND %CFS<	CWSEL	TQ	EG	TOPWID	STENCL	STENCR	WSELK	
20.00	805.00	v.0	0.0	461.40 24300.00	477.97	6973.33	478.91	254.86	0.0	0.0	0.0	
20.00	805.00	0.0	0.0	461.40 45700.00	479.60	8533.63	481.91	1147.95	0.0	0.0	0.0	
(20.00	805.00	0.0	0.0	461.40 58500.00	480.81		483.48	2014.26	0.0	0.0	0.0	
20.00	805.00	0.0	0.0	461.40102000.00		16973.63	486.76	2066.44	0.0	0.0	0.0	
	005.00		•									
21.00	525.00	0.0	0.0	462.80 24300.00		7882.23	479.50	504.95	0.0	0.0	0.0	
~ 21.00	525.00	0.0	0.0	462.80 45700.00	481.86	12255.23	483.04	898.54	0.0	0.0	0.0	
(L) 21.00	525.00	0.0	0.0	462.80 58500.00	483.31	15009.24	484.74	1281.43	0.0	0.0	0.0	
/ 21.00	525.00	0.0	0.0	462.80102000.00	485.83	21013.59	488.37	1412.21	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30 24300.00	479-15	9636.12	479.93	195.70	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30 45700.00		12866.25	483.95	343.94	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30 58500.00		14422.87	486.00	669.83	0.0	0.0	0.0	
23.01	445.00	0.0	0.0	458.30102000.00		17163.32	491.33	833.48	0.0	0.0	0.0	
23.01	443.00	V • U	0.0	730130102000100	4,,3,43	1,103.32	171.033	000.10	V.V		y• y	
23.02	30.00	482.50	485.00	458.30 24300.00	479.18	9662.04	479.96	195.77	0.0	0.0	0.0	
23.02	30.00	482.50	485.00	458.30 45700.00		13768.22	484.57	544.78	0.0	0.0	0.0	
23.02	30.00	482.50	485.00	458.30 58500.00		16099.46	486.81	832.15	0.0	0.0	0.0	
23.02	30.00	482.50	485.00	458.30102000.00		18101.68	491.43	847.13	0.0	0.0	0.0	
22.52				450 20 24202 00	470 42	0435 50	400 04	275.86	0.0	0.0	0.0	
23.00	55.00	0.0	0.0	458.30 24300.00		9415.52	480.04	670.08	0.0	0.0	0.0	
23.00	55.00	0.0	0.0	458.30 45700.00		14284.44	484.73	841.12	0.0	0.0	0.0	
€ 23.00	55.00	0.0	0.0	458.30 58500.00			492.38	898.11	The second secon	at his horizontal at the black of the state	0.0	
7 23.00	55.00	0.0	0.0	458.30102000.00	469.70	25880.07	472.38	090.11	0.0	0.0	0.0	
24.00	370.00	0.0	0.0	462.80 24300.00	479.48	7312.45	480.46	281.83	0.0	0.0	0.0	
24.00	370.00	0.0	0.0	462.80 45700.00	483.43	11208.77	485.40	409.45	0.0	0.0	0.0	
R 24.00	370.00	0.0	0.0	462.80 58500.00	485.37	13574.36	487.81	946.12	0.0	0.0	0.0	
V\ 24.00	370.00	0.0	0.0	462.80102000.00		21320.65	493.26	1035.02	0.0	0.0	0.0	
25.00	750.00	0.0	0.0	465.20 24300.00	480 54	6366.38	481.43	761.89	0.0	0.0	0.0	
/<25.00	750.00	0.0	0.0	465.20 45700.00		15047.50	486.84	1326.33	0.0	0.0	0.0	
25.00	750.00		0.0	465.20 58500.00		21180.36	489.44	1384.59	0.0	0.0	0.0	
		0.0		465.20102000.00		38335.12	495.27	1427.94	0.0	0.0	0.0	
25.00	750.00	0.0	0.0	403.20102000.00	494.43	36333.12	+93.21	1421.74	0.0	•••	0.0	
26.00	450.00	0.0	0.0	465.50 24300.00	481 - 16	5861.21	482.37	537.07	0.0	0.0	0.0	
26.00	450.00	0.0	0.0	465.50 45700.00	486.39	12148.86	487.75	891.35	0.0	0.0	0.0	
26.00	450.00	0.0	0.0	465.50 58500.00	488.95	16448.24	490.31	942.09	0.0	0.0	0.0	
26.00	450.00	0.0	0.0	465.50102000.00	494.60	28636.33	496.27	1023.77	0.0	0.0	0.0	
27.00	540.00	0.0	0.0	467.80 24300.00	482.39	8177.28	483.05	553.55	0.0	0.0	0.0	
27.00	540.00	0.0	0.0	467.80 45700.00		15303.75	488.37	631.89	0.0	0.0	0.0	
(1) 27.00	540.00		0.0	467.80 58500.00		19453.89	490.88	733.77	0.0	0.0	0.0	
27.00	540.00	0.0	0.0	467.80102000.00	Principal Company of the Company of	30914.83	496.88	798.17	0.0	0.0	0.0	
21.00	340.00	0.0	0.0	401.00102000.00	472011	30914.03	470.00	70.1	,	•••		
28.00	940.00	0.0	0.0	468.50 24300.00	483.24	6423.10	484.17	378.89	0.0	0.0	0.0	
, 28.00	940.00	0.0	0.0	468.50 45700.00		11791.41	489.58	436.38	0.0	0.0	0.0	
V 28.00	940.00	0.0	0.0	468.50 58500.00		14875.47	492.17	592.05	0.0	0.0	0.0	
28.00	940.00	0.0	0.0	468.50102000.00	495.77		498.50	687.84	0.0	0.0	0.0	

						<u>_</u>						45
NUMBER L	CHANNEL MIN LENGTH ROAD	WAY LO	W CHORD	MIN EL DISCHARGE GROUND %CFS<	CWSEL	TQ	EG	TOPWID	STENCL	STENCR	WSELK	
29.00	790.00	0.0	0.0	470.10 24300.00		7132.73	485.19	838.93	0.0	0.0	0.0	
29.00	790.00	0.0	0.0	470.10 45700.00		15560.60	490.53	1014.20	0.0	0.0	0.0	
/W 29.00	790.00	0.0	0.0	470.10 58500.00		20790.27	493.10	1037.87	0.0	0.0	0.0	
29.00	790.00	0.0	0.0	470.10102000.00	498.71	36545.99	499.56	1096.26	0.0	0.0	0.0	
30.00	410.00	0.0	0.0	471.00 24300.00		7962.98	485.63	928.21	0.0	0.0	0.0	
/ X 30.00	410.00	0.0	0.0	471.00 45700.00		18310.19	490.83	992.64	0.0	0.0	0.0	
30.00	410.00	0.0	0.0	471.00 58500.00		24675.47	493.38	1018.34	0.0	0.0	0.0	
30.00	410.00	0.0	0.0	471.00102000.00	499.14	44271.82	499.82	1119.38	0.0	0.0	0.0	
31.00	575.00	0.0	0.0	472.90 24300.00	The Contract	7104.00	486.25	1082.99	0.0	0.0	0.0	
1/17 31.00	575.00	0.0	0.0	472.90 45700.00		16636.99	491.21	1218.06	0.0	0.0	0.0	
V 31.00	575.00	0.0	0.0	472.90 58500.00		22809.90	493.70	1251.78	0.0	0.0	0.0	
31.00	575.00	0.0	. 0.0	472-90102000.00	499.49	42351.91	500.12	1303.01	0.0	0.0	0.0	
32.00	630.00	0.0	0.0	470.80 24300.00		5277.31	487.61	824.15	0.0	0.0	0.0	
1- 32.00	630.00	0.0	0.0	470.80 45700.00	490.90	11567.86	492.16	894.07	0.0	0.0	0.0	
1 432.00	630.00	0.0	0.0	470.80 58500.00		15834.91	494.53	913.49	0.0	0.0	0.0	
32.00	630.00	0.0	0.0	470.80102000.00	499.59	29746.50	500.87	991.37	0.0	0.0	0.0	
33.00	380.00	0.0	0.0	469.00 24300.00	487.49	8880.27	488.10	1086.11	0.0	0.0	0.0	
,A 33.00	380.00	0.0	0.0	469.00 45700.00	491.85	16975.86	492.53	1149.47	0.0	. 0.0	0.0	
JF 33.00	380.00	0.0	0.0	469.00 58500.00	494.17	22434.83	494.86	1160.05	0.0	0.0	0.0	
33.00	380.00	0.0	0.0	469.00102000.00	500.36	40615.66	501.15	1228.49	0.0	0.0	0.0	
34.00	480.00	0.0	0.0	475.40 24300.00	487.78	5509.39	488.72	957.67	0.0	0.0	0.0	
	480.00	0.0	0.0	475.40 45700.00	492.16	12406.11	493.02	1018.80	0.0	0.0	0.0	
β 34.00	480.00	0.0	0.0	475.40 58500.00	494.45	17182.77	495.30	1055.67	0.0	0.0	0.0	
34.00	480.00	0.0	0.0	475.40102000.00	500.60	33437.45	501.54	1123.46	0.0	0.0	0.0	
35.00	720.00	0.0	0.0	477.60 24300.00	489.15	4887.21	490.27	1223.95	0.0	0.0	0.0	
35.00	720.00	0.0	0.0	477.60 45700.00		11412.07	494.01	1454.67	0.0	0.0	0.0	
35.00	720.00	0.0	0.0	477.60 58500.00		16453.04	496.12	1548.90	0.0	0.0	0.0	
35.00	720.00	0.0	0.0	477.60102000.00		35357.77	502.16	1633.50	0.0	0.0	0.0	
36.00	740.00	0.0	0.0	474.20 24300.00	490.99	6931.46	491.69	351.93	. 0.0	0.0	0.0	
36.00	740.00	0.0	0.0	474.20 45700.00		10675.12	495.64	374.24	0.0	0.0	0.0	
36.00	740.00	0.0	0.0	474.20 58500.00		13175.85	497.87	385.17	0.0	0.0	0.0	
36.00	740.00	0.0	0.0	474.20102000.00		21565.77	504.34	412.02	0.0	0.0	0.0	
_36.10	60.00	0.0	0.0	475.00 24300.00	490.93	4855.63	491.95	310.65	0.0	0.0	0.0	
36.10	60.00	0.0	0.0	475.00 45700.00	494.03	7448.52	496.08	319.62	0.0	0.0	0.0	
36.10	60.00	0.0	0.0	475.00 58500.00	495.85	9094.88	498.39	374.12	0.0	0.0	0.0	
36.10	60.00	0.0	0.0	475.00102000.00		14527.16	504.98	416.64	0.0	0.0	0.0	
36.20	10.00	513.00	532.00	475.00 24300.00	490.96	4872.24	491.98	310.93	0.0	0.0	0.0	
36.20	10.00	513.00	532.00	475.00 45700.00	494.10	7503.98	496.13	319.85	0.0	0.0	0.0	
36.20	10.00	513.00	532.00	475.00 58500.00		9168.10	498.44	374.75	0.0	0.0	0.0	
36.20	10.00	513.00	532.00	475.00102000.00		14658.96	505.05	417.59	0.0	0.0	0.0	
1												
1												

SECT	ION CH	ANNEL MIN EL	OF MAX	EL OF	MIN FL	DISCHARGE	CWSEL	TQ	EG	TOPWID	STENCL	STENCE	WEST IN	46
NUMB	IER LE	NGTH ROADWAY	Y LOW	CHORD	GROUND	%CFS<								
	43.00	230.00	0.0	0.0		24300.00		19580.02		2708.79	0.0	0.0		
	43.00	230.00	0.0	0.0		45700.00		47251.38		3320.94	0.0	0.0	2.5	
	43.00	230.00	0.0	0.0		58500.00		67731.44		3338.24	0.0	0.0		
V .	43.00	230.00	0.0	0.0	481.00	102000.00	507.60	148684.81	507.64	3430.94	0.0	0_0		
	44.00	415.00	0.0	0.0		20000.00		4755.85	494.17	599.29	0.0	0_0		
1	44.00	415.00	0.0	0.0	480.60	38000.00	497.79	11566.20	498.35	1565.57	0.0	0.0		
/ N	44.00	415.00	0.0	0.0	480.60	48800.00	500.23	18298.09	500.63	1621.36	0.0	0_0	9.00	
	44.00	415.00	0.0	0.0	480.60	87000.00	507.60	49163.30	507.85	1797.10	0.0	0_0		
	45.00	420.00	0.0	0.0	481.50	20000.00	494.02	3531.23	495.31	274.49	0.0	0_0	04.00	
.1,	45.00	420.00	0.0	0.0	481.50	38000.00	497.95	7280.82	499.25	1226.39	0.0	0.40	9.00	
15	45.00	420.00	0.0	0.0	481.50	48800.00	500.34	11911.60	501.19	1238.01	0.0	0_0		
	45.00	420.00	0.0	0.0	481.50	87009.00	507.62	34045.30	508.09	1646.20	0.0	0_0	TLE .	
	46.00	565.00	0.0	0.0	482.20	20000.00	495.87	4691.17	496.69	695.42	0.0	0_0	-	
	46.00	565.00	0.0	0.0		38000.00		11196.98		1224.90	0.0	0.0	0.00	
12	46.00	565.00	0.0	0.0		48800.00		15602.67		1239.34	0.0	0_0	TA	
	46.00	565.00	0.0	0.0		87000.00		40554.98		1525.57	0.0	0.0	OIL DE	
	47.00	630.00	0.0	0.0	494 00	20000.00	497 13	5987.73	497.52	1021.70	0.0	0	9.0	
1	47.00	630.00	0.0	0.0		38000.00		10842.91	500.86	1157.83	0.0	0.0	TLE CONTRACTOR	
/ M	47.00	630.00	0.0	0.0		48800.00		13850.42		1165.89	0.0	0_0		
-	47.00	630.00	0.0	0.0		87000.00	The second secon	30704.48		1408.68	0.0	0_0	OF ATT	
		630.00	0.0	0.0	484.00	87000.00	508.20	30104.40	508.70	1408.08	0.0	-	Washing .	
1	48.50	610.00	0.0	0.0	486.00	20000.00	497.80	5331.98	498.30	624.38	0.0	0_0	01_00	
/ N	48.00	610.00	0.0	0.0	486.00	38000.00	501.04	9549.41	501.75	929.21	0.0	0_0	6 _1	
V	48.00	610.00	0.0	0.0	486.00	48800.00	502.57	12099.34	503.36	938.65	0.0	0.0	T.00	
	48.00	610.00	0.0	0.0	486.00	87000.00	508.58	25991.78	509.32	1171.42	0.0	T_0	0.3	
1	49.00	555.00	0.0	0.0	486.30	20000.00	498.62	6123.05	498.98	660.47	0.0	0_0		
10	49.00	555.00	0.0	0.0		38000.00		10698.42	502.54	710.94	0.0	0_0		
VU	49.00	555.00	0.0	0.0		48800.00		13178.26	504.19	723.82	0.0	0_0	TANK TO SERVICE STATE OF THE S	
	49.00	595.00	0.0	0.0		87000.00	The state of the s	25334.20	509.99	995.87	0.0	0.0	91_30	
	50.00	465.00	0.0	0.0	486.20	20000.00	400.02	5851.13	499.53	519.18	0.0	0_0	W.M	
10	50.00	465.00	0.0	0.0		38000.00		9503.86	503.28	543.67	0.0	0.0	(FLD)	
/1	50.00	465.00	0.0	0.0		48800.00		11412.67	505.05	553.87	0.0	0_0	7.3	
	50.00	465.00	0.0	0.0		87000.00		20198.79	510.89	988.51	0.0	0_0	G.00	
c r	CTION	DISCHARGE	CWSEL		CHCEL DIE	e cueri n	TEE ONE	רו שכבו א	TODUTO					
	MBER	CFS	CWSEL		EACH Q	F CWSEL D EACH SE		EL-WSELK	TOPWID	T.W. DI	FF LEN	5 18		
	1.010		457	.302	0.0	0.0		0.0	306.922	0.0		0_0		
	1.010			.697	3.395			0.0	351.926	-45.00		0.0		
	1.010			.239	1.542			0.0	371.863	-64.94		0.0		
	1.010			.641	5.402			0.0	864.156	-557.23		0.0		
	1.020	24300.000	461	.105	0.0	3.8	03	0.0	356.227	0.0	45	a_gaa		
	1.020			.016	3,911			0.0	498.984	-142.75		0.000		
	1.020			.984	1.968	4.7		0.0	750.832	-394.60		0.000		
	1.020			.805	5.821	5.1		0.0	3811.156	-3454.93		0.000		
	1.000	24300.000	462	.443	0.0	1.3	30	0.0	374.895	0.0		0.000		
	1.000			.626	4.182			0.0	The second section of the second section is the second section of the second section is a second section of the second section of the second section is a second section of the section of the second section of the secti	A STATE OF THE PARTY OF THE PAR				
	1.000			.694	2.069	1.7		0.0	681.844	-306.94		0.000		
	1.000			246	5.552	1.4		0.0	4771.719	-677,22 -4396,82		0.000		
	, ,,,,	24200 000												
	1.100			.430	0.0	0.9		0.0	211.359	0.0		0.000		
	1.100	45700.000		666	4,236			0.0	1019.195	-807.83		0.000		
	1.100	58500.000 102000.000	470. 475.		5.544	1.3		0.0	2561.301	-2149.94		0_000		
					in the late	1.3	X'S	0.0	4935.129	-4723.77	70	0.100		

	CHANNEL MIN LENGTH ROAD		EL OF CHORD	MIN EL I	%CFS<	CWSEL	TO	Eè	TOPWID	STENCL	STENCR	WSELK
10.00	860.00	0.0	0.0	456.70	24300.00	469.21	8209.09	469.48	3214.88	0.0	0.0	0.0
1 10.00	860.00	0.0	0.0	456.70	45700.00		34647.36	474.23	4419.25	0.0	0.0	0.0
H 10.00	860.00	0.0	0.0		58500.00		51415.77	476.24	4658.92	0.0	0.0	0.0
10.00	860.00	0.0	0.0		105000.00		75543.38	478.66	4945.16	0.0	0.0	0.0
11.00	675.00	0.0	0.0	459.40	24300.00	469.65	7571.29	469.96	2822.57	0.0	0.0	0.0
11.00	675.00	0.0	0.0	459.40	45700.00	474.23	29686.05	474.32	4137.62	0.0	0.0	0.0
11.00	675.00	0.0	0.0	459.40	58500.00	476.23	44880.45	476.30	4321.93	0.0	0.0	0.0
11.00	675.00	0.0	0.0	459.40	105000.00	478.64	67234.38	478.74	4626.09	0.0	0.0	0.0
11.10	75.00	0.0	0.0	459.40	24300.00	469.83	8019.23	470.10	2902.64	0.0	0.0	0.0
11.10	75.00	0.0	0.0	459.40	45700.00	474.27	29692.20	474.36	4098.54	0.0	0.0	0.0
11.10	75.00	0.0	0.0	459.40	58500.00	476.26	44730.84	476.33	4248.57	0.0	0.0	0.0
M 11.10	75.00	0.0	0.0	459.40	105000.00	478.68	67012.31	478.78	4431.33	0.0	0.0	0.0
12.01	5.00	480.00	476.90		24300.00	469.78		470.17	1583.37	0.0	0.0	0.0
12.01	5.00	480.00	476.90	452.90	45700.00	474.24	23517.72	474.39	3640.96	0.0	0.0	0.0
12.01	5.00	480.00	476.90	452.90	58500.00	476.25	32609.55	476.34	4036.19	0.0	0.0	0.0
12.01	5.00	480.00	476.90	452.90	105000.00	478.67	48848.30	478,79	4484.27	0.0	0.0	0.0
12.10	110.00	480.00	476.90	452.90	24300.00	469.90	8268.83	470.27	1656.89	0.0	0.0	0.0
12.10	110.00	480.00	476.90	452.90	45700.00	474.28	23715.88	474.43	3648.17	0.0	0.0	0.0
12.10	110.00	480.00	476.90	452.90	58500.00	475.29	32774.10	476.37	4041.75	0.0	0.0	0.0
12.10	110.00	480.00	476.90	452.90	102000.00	478.72	49181.27	478.84	4489.82	0.0	0.0	0.0
13.10	5.00	0.0	0.0	460.00	24300.00	469.88	6419.80	470.31	1497.76	0.0	0.0	0.0
13.10	5.00	0.0	0.0	460.00	45700.00	474.31	22842.24	474.44	4013.98	0.0	0.0	0.0
13.10	5.00	0.0	0.0	460.00	58500.00	476.28	35740.82	476.38	4304.26	0.0	0.0	0.0
13.10	5.00	0.0	0.0	460.00	105000.00	478.71	56102.19	478.85	4537.01	0.0	0 6 0	0.0
13.20	115.00	0.0	0.0	460.00	24300.00	470.08	6806.98	470.47	2031.35	0.0	0.0	0.0
13.20	115.00	0.0	0.0	460.00	45700.00	474.35	23140.77	474.48	4024.42	0.0	0.0	0.0
13.20	115.00	0.0	0.0	460.00	58500.00	476.31	35992.40	476.41	4307.58	0.0	0.0	0.0
∨ 13.20	115.00	0.0	0.0	460.00	102000.00	478.74	56377.83	478.89	4539.81	0.0	0.0	0.0
14.00	635.00	0.0	0.0		24300.00	470.53	10671.93	470.76	2348.04	0.0	0.0	0.0
14.00	635.00	0.0	0.0		45700.00		27160.61	474.56	3882.43	0.0	0.0	0.0
1.000	635.00	0.0	0.0		58500.00		39976.17	476.45	4236.61	0.0	0.0	0.0
14.00	635.00	0.0	0.0	456.00	102000.00	478.79	60476.95	478.94	4472.95	0.0	0.0	0.0
16.01	684.00	0.0	0.0	458.00	24300.00	470.01	5101.14	471.75	191.00	0.0	0.0	0.0
16.01	684.00	0.0	0.0		45700.00		19099.80	474.74	2997.67	0.0	0.0	0.0
16.01	684.00	0.0	0.0		58500.00		27905.69	476.58	3794.65	0.0	0.0	0.0
16.01	684.00	0.0	0.0	458.00	105000.00	478.74	42490.75	479.08	4030.29	0.0	0.0	0.0
16.02	10.00	485.70	494.60	458.00	24300.00	469.99	4308.39	471.79	188.00	0.0	0.0	0.0
16.02	10.00	485.70	494.60	458.00	45700.00	474.50	17391.58	474.75	2981.61	0.0	0.0	0.0
16.02	10.00	485.70	494.60	458.00	58500.00	476.39	25448.70	476.59	3277.09	0.0	0.0	0.0
16.02	10.00	485.70	494.60	458.00	02000.00	478.83	38458.67	479.10	3479.08	0.0	0.0	0.0

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SECT		ANNEL MIN			MIN EL DISCHARGE GROUND %CFS<	CWSEL	TQ	EG	TOPWID	STENCL	STENCR	WSELK	
	16.03	76.00	485.70	494.60	458.00 24300.00	470.33 4	496.94	472.03	188.00	0.0	0.0	0.0	
	16 03	76.00	485.70	494.60	458.00 45700.00	474.55 17	572.71	474.81	2986.45	0.0	0.0	0.0	
V	16.03	76.00	. 485.70	494.60	458.00 58500.00	476.44 25	623.45	476.63	3280.08	0.0	0.0	0.0	
	16.03	76.00	485.70	494.60	458.00102000.00	478.88 38	747.91	479.15	3483.15	0.0	0.0	0.0	
	16.04	10.00	0.0	0.0	458.00 24300.00	470.44 5	406.33	472.07	191.00	0.0	0.0	0.0	
	16.04	10.00	0.0	0.0	458.00 45700.00	474.51 19	524.54	474.83	3008.09	0.0	0.0	0.0	
*	16.04	10.00	0.0	0.0	458.00 58500.00	476.40 28	320.40	476.65	3802.30	0.0	0.0	0.0	
1	16.04	10.00	0.0	0.0	458.00102000.00	478.84 43	1186.66	479.18	4040.24	0.0	0.0	0.0	
	16.00	60.00	0.0	0.0	459.00 24300.00	471.37 6	396.10	472.24	484.27	0.0	0.0	0.0	
	16.00	60.00	0.0	0.0	459.00 45700.00	474.70 22	673.95	474.87	3907.63	0.0	0.0	0.0	
	16.00	60.00	0.0	0.0	459.00 58500.00	476.54 33	3240.89	476.68	4282.23	0.0	0.0	0.0	
	16.00	60.00	0.0	0.0	459.00102000.00	479.02 51	088.25	479.22	4606.56	0.0	0.0	0.0	IN A SHARE OF THE SHARE
	18.01	738.00	6.0	0.0	459.00 24300.00	471.97 4	684.69	474.01	170.00	0.0	0.0	0.0	
	18.01	738.00	0.0	0.0	459.00 45700.00	474.96 16		475.35	3517.08	0.0	0.0	0.0	
	18.01	738.00	0.0	0.0	459.00 58500.00	476.75 24	Alexander of the second	477.03	3696.41	0.0	0.0	0.0	
	18.01	738.00	0.0	0.0	459.00102000.00	479.30 39	747.53	479.63	3960.64	0.0	0.0	0.0	
	18.02	10.00	473.10	478.50	459.00 24300.00	471.81 4	223.67	474.12	207.55	0.0	0.0	0.0	
Ko	18.02	10.00	473.10	478.50	459.00 45700.00	475.15 14	042.07	475.37	3536.27	0.0	0.0	0.0	
200	18.02	10.00	473.10	478.50	459.00 58500.00	476.91 20	408.50	477.05	3711.95	0.0	0.0	0.0	
	18.02	10.00	473.10	478.50	459.00102000.00	479.49 32	798.59	479.66	3976.00	0.0	0.0	0.0	
	18.03	27.00	473.10	478.50	459.00 24300.00	471.96 4	305.51	474.21	208.29	0.0	0.0	0.0	
	18.03	27.00	473.10	478.50	459.00 45700.00	475.18 14		475.40	3538.75	0.0	0.0	0.0	
	18.03	27.00	473.10	478.50	459.00 58500.00	476.93 20		477.07	3713.83	0.0	0.0	0.0	
1000	18.03	27.00	473.10	478.50	459.00102000.00	479.52 32	2698.94	479.68	3977.82	0.0	0.0	0.0	
	18.04	10.00	0.0	0.0	459.00 24300.00	472.36 4	930.77	474.27	170.00	0.0	0.0	0.0	
	18.04	10.00	0.0	0.0	459.00 45700.00	475.09 16	5852.07	475.45	3530.19	0.0	0.0	0.	
	18.04	10.00	0.0	0.0	459.00 58500.00	476.85 25	5144.52	477.11	3706.09	0.0	0.0	0.0	
	18.04	10.00	0.0	0.0	459.00102000.00	479.42 40	520.93	479.74	3970.20	0.0	0.0	0.0	
1 .	18.00	55.00	0.0	0.0	459.00 24300.00	472.96 5	329.98	474.44	250.85	0.0	0.0	0.0	
ML	18.00	55.00	0.0	0.0	459.00 45700.00	475.21 16		475.50	3542.27	0.0	0.0	0.0	
14.	18.00	55.00	0.0	0.0	459.00 58500.00	476.94 25		477.15	3714.62	0.0	0.0	0.0	
	18.00	55.00	0.0	0.0	459.00102000.00	479.51 40	743.24	479.78	3978.16	0.0	0.0	0.0	
40	19.00	1283.00	0.0	0.0	460.70 24300.00	475.81 9	9824.07	476.27	506.47	0.0	0.0	0.0	
1,	19.00	1283.00	0.0	0.0	460.70 45700.00	476.40 13	3584.41	477.11	3060.95	0.0	0.0	0.0	
	19.00	1283.00	0.0	0.0	460.70 58500.00	477.89 18		478.50	3342.07	0.0	0.0	0.0	
	19.00	1283.00	0.0	0.0	460.70102000.00	480.63 31	1599.27	481.30	3761.78	0.0	0.0	0.0	
	19.10	805.00	0.0	0.0	461.90 24300.00	476.36 5	5780.23	477.59	304.98	0.0	0.0	0.0	
	19.10	805.00	0.0	. 0.0	461.90 45700.00	477.45 8	3446.05	479.23	1966.14	0.0	0.0	0.0	
	19.10	805.00	0.0	0.0	461.90 58500.00	478.79 11	1320.66	480.41	2136.32	0.0	0.0	0.0	
	19.10	805.00	0.0	0.0	461.90102000.00	481.57 19	9474.87	483.27	2436.67	0.0	0.0	0.0	

SUMMARY PRINTOUT FOR MULTIPLE PROFILES Fishing Greek

FISHING CREEK 500 YEAR F

	HANNEL MIN E ENGTH ROADW		X EL OF W. CHORD	MIN EL DISCHARGE GROUND %CFS<	CWSEL TO	e EG	TOPWID	STENCL	STENCR	WSELK	
1.01	0.0	0.0	0.0	448.20 24300.00	457.30 2566.2	460.35	306.92	0.0	0.0	456.10	7
1.01	0.0	0.0	0.0	448.20 45700.00	460.70 5143.94		351.93	0.0	0.0	459.20	
1.01	0.0	0.0	0.0	448.20 58500.00	462.24 6680.32	467.10	371.86	0.0	0.0	460.70	
1.01	0.0	0.0	0.0	448.20102000.00	467.64 14085.07	473.02	864.16	0.0	0.0	464.90	1
1.02	450.00	0.0	0.0	448.20 24300.00	461.10 5514.29		356.23	0.0	0.0	0.0	1
1.02	450.00	0.0	0.0	448.20 45700.00	465.02 10048.25		498.98	0.0	0.0	0.0	4
1.02	450.00	0.0	0.0	448.20 58500.00	466.98 12966.91		750.83	0.0	0.0	0.0	
1.02	450.00	0.0	0.0	448.20102000.00	472.80 27515.61	474.47	3811.16	. 0.0	0.0	0.0	,
1.00	680.00	0.0	0.0	448.20 24300.00	462.44 6909.70	463.25	374.89	0.0	0.0	0.0	10
A 1.00	680.00	0.0	0.0	448.20 45700.00	466.63 12393.20	467.93	681.84	0.0	0.0	0.0	
7. 1.00	680.00	0.0	0.0	448.20 58500.00	468.69 16061.32		1052.12	0.0	0.0	0.0	
1.00	680.00	0.0	0.0	448.20102000.00	474.25 34813.19	475.26	4771.72	0.0	0.0	0.0	. 12
B 1.10	700.00	0.0	0.0	449.40 24300.00	463.43 4321.27	464.69	211.36	0.0	0.0	0.0	u
10 1.10	700.00	0.0	0.0	449.40 45700.00	467.67 6777.68		1019.20	0.0	0.0	0.0	14
1.10	700.00	0.0	0.0	449.40 58500.00	470.09 10181.03		2361.30	0.0	0.0	0.0	
1.10	700.00	0.0	0.0	449.40102000.00	475.63 35958.11	475.89	4935.13	0.0	0.0	0.0	
102.00	230.00	0.0	0.0	446.00 24300.00	464.15 7890.28	465.09	298.09	0.0	0.0	0.0	
2.00	230.00	0.0	0.0	446.00 45700.00	469.16 15207.13		2767.23	0.0	0.0	0.0	The state of the
2.00	230.00	0.0	0.0	446.00 58500.00	471.15 22346.64		3443.27	0.0	0.0	0.0	18
5.00	230.00	0.0	0.0	446.00102000.00	475.73 52697.01		5055.29	0.0	0.0	0.0	19
3.01	125.00	0.0	0.0	449.50 24300.00	453.94 5567.88	465.62	162.00	0.0	0.0	0.0	
3.01	125.00	0.0	0.0	449.50 45700.00	469.30 14404.26		3062.35	0.0	0.0	0.0	
3.01	125.00	0.0	0.0	449.50 58500.00	471.42 22891.14		4087.02	0.0	0.0	0.0	14
3.01	125.00	0.0	0.0	449.50102000.00	475.86 55237.27		5121.92	0.0	0.0	0.0	
3.02	210.00	467.60	476.10	449.50 24300.00	463.97 5903.88	465.64	274.92	0.0	0 0		
3.02	10.00	467.60	476.10	449.50 45700.00	468.97 11942.30		2881.20	0.0	0.0	0.0	
3.02	10.00	467.60	476.10	449.50 58500.00	471.30 20190.35		4083.86	0.0	0.0	0.0	
3.02	/10.00	467.60	476.10	449.50102000.00	476.01 45652.81		5242.07	0.0	0.0	0.0	b
3.10	21.00	467.60	476.10	449.50 24300.00	464.02 5944.90	465.68	275.45	0.0	0.0	0.0	
3.10	21.00	467.60	476.10	449.50 45700.00	469.61 13720.84		3252.44	0.0	0.0	0.0	it.
3.10	21.00	467.60	476.10	449.50 58500.00	471.33 20288.28		4094.98	0.0	0.0	0.0	78
3.10	21.00	467.60	476.10	449.50102000.00	476.02 45725.74		5242.60	0.0	0.0	0.0	n en en en
3.20	10.00	0.0	0.0	449.50 24300.00	464.04 5624.71	465.70	162.00	0.0	0.9	0.0	30
3.20	10.00	0.0	0.0	449.50 45700.00	470.52 18733.04		3599.83	0.0	0.0	0.0	
3.20	10.00	0.0	0.0	449.50 58500.00	471.77 24756.82		4389.82	0.0	0.0	0.0	41
3.20	10.00	0.0	0.0	449.50102000.00	475.97 56349.91	476.23	5160.92	0.0	0.0	0.0	n
4.01	ZZ31,00	0.0	0.0	449 30 34300 00	46E 06 10073 07		1200 00				13
4.01	30.00	0.0	0.0	448.30 24300.00 448.30 45700.00	465.96 13867.36		1292.23	0.0	0.0	0.0	
4.01	30.00	0.0	0.0	448.30 45700.00	471.16 31917.61	471.31	5279.79	0.0	0.0	0.0	
4.01	30.00	0.0	0.0	448.30102000.00	472.31 39567.16 476.22 77106.00		5438.82	0.0	0.0	0.0	35

	500 M					34.14.97					2,5		
FISHING C	REFK 500 YEAR	F							20.00				
	CHANNEL MIN E ENGTH ROADW		X EL OF	MIN EL GROUND	DISCHARGE %CFS<	CWSEL	ТО	EG	TOPWID	STENCL	STENCR	WSELK	
50.00	465.00	0.0	0.0	486.20	20000.00	499.02	5850.17	499.53	519.18	0.0	0.0	499.02	
50.00	465.00	0.0	0.0	486.20	38000.00	502.33	9502.17	503.28	548.66	0.0	0.0	502.33	
50.00	465.00	0.0	0.0	486.20	48800.00		11411.62	505.05	553.87	0.0	0.0	503.83	
50.00	465.00	0.0	0.0	486.21	87000.00	509.22	20195.80	510.89	988.50	0.0	0.0	509,22	
51.00	225.00	0.0	0.0	486.1	00000.00	499.23	5628.93	499.82	448.99	0.0	0.0	0.0	
~ 51.00	225.00	0.0	0.0		38000.00	502.59	9255.66	503.68	475.12	0.0	0.0	0.0	
() 51.00	225.00	0.0	0.0	486.1	0 48800.00	504.11	11155.47	505.51	481.02	0.0	0.0	0.0	
51.00	225.00	0.0	0.0	486.1	87000.00	509.61	20230.42	511.30	1123.39	0.0	0.0	0.0	
52.00	225.00	0.0	0.0	489.3	00.00000	499.42	4462.52	500.34	351.21	0.0	0.0	e 0.0	
52.00	225.00	0.0	0.0	and the state of t	0 38000.00		7711.87	504.41	385.36	0.0	0.0	0.0	10/
R 52.00	225.00	0.0	0.0		0 48800.00		9428.89	506.37	391.76	0.0	0.0	0.0	
52.00	225.00	0.0	0.0		87000.00		17778.59	512.21	1277.45	0.0	0.0	0.0	
				100 6	00.0000	400 07	3708.13	501.48	252.39	0.0	0.0	0.0	
52.10	275.00	0.0	0.0		0 38000.00	ALC: YES THE RESIDENCE OF THE PARTY OF THE P	6175.45	506.18	287.16	0.0	0.0	0.0	
5 52.10	275.00 275.00	0.0	0.0	and the second state of the second se	0 48800.00		7462.70	508.51	302.55	0.0	0.0	0.0	
52.10		0.0	0.0		0 87000.00		14044.09	514.86	1228.34	0.0	0.0	0.0	
								500.46	205.39	0.0	0.0	0.0	
53.00		0.0	0.0		0 20000.00	500.66	3510.68 5937.87	502.46	278.95	0.0	0.0	0.0	
53.00	275.00	0.0	0.0		0 38000.00 0 48800.00		7289.76	509.92	294.84	0.0	0.0	0.0	
53.00		0.0	0.0	Charles and the second second	0 87000.00		15685.10	515.89	1375.92	0.0	0.0	0.0	
									202.00			0.0	
54.00		0.0	0.0		0 20000.00		3933.17	504.82	203.08	0.0	0.0	0.0	
11 54.00		0.0	0.0	FIRST PROPERTY OF THE PARTY OF	0 38000.00		7009.94	510.33	282.40	0.0	0.0	0.0	
JU 54.00		0.0	0.0		0 48800.00 0 87000.00		- 8835.27 14241.43	519.29	1400.39	0.0	0.0	0.0	
54.00	805,00	0.0	0.0	491.5	0.87000.00	314.31	14241.43		.,0000				
55.00	655.00	0.0	0.0	491.8	0 20000.00	504.95	4681.07	506.25	232.57	0.0	0.0	0.0	
55.00		0.0	0.0		0 38000.00		8743.36	511.91	326.67	0.0	0.0	0.0	
√ 55.00	655.00	0.0	0.0		0 48800.00		11203.93	514.60	339.30	0.0	0.0	0.0	
55.00	655.00	0.0	0.0	491.8	0 87000.00	518.42	20890.88	521.10	1141.40	0.0	0.0	0.0	
56.00	380.00	0.0	0.0	491-7	0 20000.00	505,36	3368.20	507.42	201.34	0.0	0.0	0.0	
56.00		0.0	0.0		0 38000.00		7385.30	512.83	447.53	0.0	0.0	0.0	
56.00		0.0	0.0		0 48800.00		10193.99	515.40	479.61	0.0	0.0	0.0	necessaria (Crespon)
56.00		0.0	0.0		0 87000.00	519.20	19518.49	521.81	1150.16	0.0	0.0	0.0	
	500.00		0.0	403.4	0 20000.00	507 51	3515.91	509.15	511.62	0.0	0.0	0.0	
57.00		0.0	The second secon	And the control of th	0 38000.00		9164.80	513.99	682.68	0.0	0.0	0.0	
X 57.00		0.0	0.0		0 48800.00		13059.20	516.39	693.07	0.0	0.0	0.0	
57.00		0.0	0.0		0 87000.00		26311.0-4	522.67	1280.68	0.0	0.0	0.0	
									(22.21		0.0	0.0	
58.00		0.0	0.0		0 20000.00		4078.10	511.14	623.31	0.0	0.0	0.0	
JY 58.00		0.0	0.0		0 38000.00	A comprehensive and the second of the second of the second	8429.84	515.33	959.27	0.0	0.0	0.0	
~ 58.00	705.00	0.0	0.0	496.5	0 48800.00		12022.93	523.45	1195.48	0.0	0.0	0.0	

													U2
	HANNEL MIN E		W CHORD	MIN EL GROUND	DISCHARGE %CFS<	CWSEL	ТО	EG	TOPWID	STENCL	STENCR	WSELK	
68.00	725.00	0.0	0.0		20000.00	518.48	3339.49	518.90	1723.01	0.0	0.0	0.0	
68.00	725.00	0.0	. 0.0		38000.00	520.95		521.30	1760.56	0.0	0.0	0.0	
XH68.00	725.00	0.0	0.0	SECTION SECTIO	48800.00	SAN DESCRIPTION OF THE PROPERTY OF THE	12535.21	522.82	1799.83	0.0	0.0	0.0	
V 1,98.00	725.00	0.0	0.0	506.50	87000.00	527.77	32097.71	528.08	1855.65	0.0	0.0	0.0	
69.00	425.00	0.0	0.0	513.00	20000.00	519.69	3265.41	520.34	1474.25	0.0	0.0	0.0	
17 69.00	425.00	0.0	0.0	513.00	38000.00	521.62	6262.80	522.42	1678.96	0.0	0.0	0.0	
1 69.00	425.00	0.0	0.0		48800.00	522.95		523.68	1717.83	0.0	0.0	0.0	
69.00	425.00	0.0	0.0	513.00	87000.00	527.95	23427.34	528.50	1790.13	0.0	0.0	0.0	
70.00	641.00	0.0	0.0		20000.00	521.98	3476.67	522.78	1371.68	0.0	0.0	0.0	
1 70.00	641.00	0.0	0.0		38000.00	524.09	6618.85	524.91	2047.01	0.0	0.0	0.0	
77 70.00	641.00	0.0	0.0		48800.00	525.11	8759.41	525.90	2057.61	0.0	0.0	0.0	
70.00	641.00	0.0	0.0	510.00	87000.00	529.13	20295.18	529.72	2106.31	0.0	0.0	0.0	
71.00	501.00	0.0	0.0	512.50	20000.00	523.44	3571.67	524.55	863.49	0.0	0.0	0.0	
1 71.00	501.00	0.0	0.0	512.50	38000.00	525.54	6025.97	527.10	2075.27	0.0	0.0	0.0	
1 71.00	501.00	0.0	0.0		48800.00		7741.78	528.04	2102.83	0.0	0.0	0.0	
71.00	501.00	0.0	0.0	512.50	87000.00	529.94	17604.98	530.97	2121.64	0.0	0.0	0.0	
72.00	790.00	0.0	0.0	512.30	20000.00	525.90	5098.60	526.20	1058.77	0.0	0.0	0.0	
XL 72.00	790.00	0.0	0.0	512.30	38000.00	528.50	10016.85	528.85	2258.60	0.0	0.0	0.0	
72.00	790.00	0.0	0.0	And the second s	48800.00		12549.10	529.81	2262.33	0.0	0.0	0.0	
72.00	790.00	0.0	0.0	512.30	7000.00	531.83	21014.11	532.39	2267.52	0.0	0.0	0.0	
73.00	575.00	0.0	0.0	516.40	20000.00	526.79	6163.20	527.00	1478.33	0.0	0.0	0.0	
AM 73.00	575.00	0.0	0.0		38000.00		11501.62	529.63	1542.14	0.0	0.0	0.0	
M 73.00	575.00	0.0	0.0		48800.00		13958.73	530.66	1568.74	0.0	0.0	0.0	
73.00	575.00	0.0	0.0	516.40	87000.00	532.95	23231.28	533.39	2920.98	0.0	0.0	0.0	
74.00	640.00	0.0	0.0	518.40	20000.00	527.46	4145.34	527.97	1866.18	0.0	0.0	0.0	
1 74.00	640.00	0.0	0.0		38000.00		9750,55	530.39	2033.68	0.0	0.0	0.0	
74.00	640.00	0.0	0.0		48800.00		12744.30	531.43	2078.28	0.0	0.0	0.0	
74.00	640.00	0.0	0.0	518.40	87000.00	533.70	22481.63	534.24	2091.01	0.0	0.0	0.0	
1 0 75.00	640.00	0.0	0.0		20000.00	528.46	4476.62	529.40	925.18	0.0	0.0	0.0	
75.00	640.00	0.0	0.0		38000.00	530.52		531.80	1388.28	0.0	0.0	0.0	
75.00	640.00	0.0	0.0		48800.00	531.47	ACTION OF THE PERSON OF THE PE	532.85	1440.67	0.0	0.0	0.0	
75.00	640.00	0.0	0.0	516.00	87000.00	534.10	15781.79	535.73	1597.89	0.0	0.0	0.0	
77.01	130.00	0.0	0.0		20000.00	528.48		530.10	223.48	0.0	0.0	0.0	
77.01	130.00	0.0	0.0		38000.00		10835.11	532.27	1348.04	0.0	0.0	0.0	
77.01	130.00	0.0	0.0		48800.00		13651.52	533.35	1394.59	0.0	0.0	0.0	
77.01	130.00	0.0	0.0	517.50	87000.00	535.46	22659.11	536.26	1508.08	0.0	0.0	0.0	
77.02	50.00	530.70	535.10		20000.00	528,65	3241.79	530.21	223.95	0.0	0.0	0.0	
77.02	50.00	530.70	535.10		38000.00		17728.61	534.31	1468.00	0.0	0.0	0.0	
77.02	50.00	530.70	535.10		48800.00		22272.90	535.61	1505.11	0.0	0.0	0.0	
77.02	50.00	530.70	535.10	517.50	87000.00	538.66	36599.73	539.06	1531.82	0.0	0.0	0.0	

													· 53
SECTION NUMBER	CHANNEL MI		K EL OF K CHORD	MIN EL GROUND	DISCHARGE %CFS<	CWSEL	то	EG:	TOPWID	STENCL	STENCR	WSELK	
77.00	60.00	0.0	0.6	517.50	00.00005	530.40	7159.10	530.68	935.55	0.0	0.0	0.0	
77.0	60.00	0.0	0.0	517.50	38000.00	534.12	17817.79	534.34	1468.77	0.0	0.0	0.0	
VK 77.01	60.00	0.0	0.0	517.50	48800.00	535.38	22378.24	535.64	1505.92	0.0	0.0	0.0	
∧` 77.01	60.00	0.0	0.0	517.50	87000.00	538.69	36758.78	539.09	1532.06	0.0	0.0	0.0	
78.00		0.0	0.0	519.30	20000.00	530.98	7783.10	531.21	1339.76	0.0	0.0	0.0	
10 78.01		0.0	0.0		38000.00		17392.54	534.68	1352.63	0.0	0.0	0.0	
VX 78.0	735.00	0.0	0.0	519.30	48800.00	535.73	21869.45	536.00	1395.74	0.0	0.0	0.0	
78.0	735.00	0.0	0.0	519.30	87000.00	539.09	35953.09	539.51	1483.42	0.0	0.0_	0.0	
79.0	CHICART COST CONTROL C	0.0	0.0	520.20	20000.00	531.40	4646.56	532.05	1000.01	0.0	0.0	0.0	
K 79.01		0.0	0.0	520.20	38000.00	534.71	10769.27	535.28	1078.61	0.0	0.0	0.0	
1 79.0		0.0	0.0		48800.00	535.99	13902.55	536.61	1091.13	0.0	0.0	0.0	
79.0	710.00	0.0	0.0	520.20	87000.00	539.36	24140.11	540.22	1164.12	0.0	0.0	0.0	
80.0	430.00	0.0	0.0	518.80	20000.00	532.21	6755.07	532.60	645.80	0.0	/ O.O	0.0	
80.0	430.00	0.0	0.0	518.80	38000.00	535.16	11081.36	535.83	770.47	0.0	0.0	0.0	
18 80.01	430.00	0.0	0.0	518.80	48800.00	536.40	13372.29	537.22	777.91	0.0	0.0	0.0	
D 80:01	430.00	0.0	0.0	518.80	87000.00	539.65	20567.15	541.03	831.19	0.0	0.0	0.0	
81.0	350.00	0.0	0.0	523.50	20000.00	532.47	3889.77	533.19	420.92	0.0	0.0	0.0	
JI 81.0	350.00	0.0	0.0	523.50	38000.00	535.48	7359.31	536.54	632.85	0.0	0.0	0.0	
XI 81.00	350.00	0.0	0.0	523.50	48800.00	536.73	9134.52	538.02	655.43	0.0	0.0	0.0	
81.00	350.00	0.0	0.0	523.50	87000.00	539.97	14662.88	542.12	712.63	0.0	0.0	0.0	
82.0	585.00	0.0	0.0	522.80	20000.00	534.22	3829.19	535.08	393.81	0.0	0.0	0.0	
V 1 82.00	685.00	0.0	0.0	522.80	38000.00	537.27	6409.77	538.76	569.85	0.0	0.0	0.0	
1 V 82.0	685.00	0.0	0.0	522.80	48800.00	538.63	7825.70	540.46	577.30	0.0	0.0	0.0	
82.0	685.00	0.0	0.0	522.80	87000.00	542.21	12269.86	545.25	594.91	0.0	0.0	0.0	<u> </u>
83.0	950.00	0.0	0.0	523.00	20000.00	536.52	4564.94	537.23	869.95	0.0	0.0	0.0	
83.0	950.00	0.0	0,0	523.00	38000.00	540.32	8930.98	541.14	894.30	0.0	0.0	0.0	
83.0	950.00	0.0	0.0	523.00	48800.00	542.07	11415.58	542.97	901.29	0.0	0.0	0.0	
83.0	950.00	0.0	0.0	523.00	87000.00	546.98	19837.42	548.20	920.92	0.0	0.0	0.0	
84.0	700.00	0.0	0.0	525.00	20000.00	537.71	6233.23	538.12	1040.12	0.0	0.0	0.0	
84.00	700.00	0.0	0.0	525.00	38000.00	541.46	11725.80	541.98	1067.20	0.0	0.0	0.0	
84.0	700.00	0.0	0.0	525.00	48800.00	543.23	14902.75	543.82	1079.28	0.0	0.0	0.0	
84.00	700.00	0.0	0.0	525.00	87000.00	548.28	25863.48	549.08	1135.59	0.0	0.0	0.0	
85.00		0.0	0.0	526.50	20000.00	537.95	4368.08	538.50	1055.1	0.0	0.0	0.0	
85.00	245.00	0.0	0.0	526.50	38000.00	541.72	9544.31	542.30	1080.72	0.0	0.0	0.0	
85.00		0.0	0.0		48800.00		12620.32	544.12	1132.95	0.0	0.0	0.0	
85.00	245.00	0.0	0.0	526.50	87000.00	548.56	23423.44	549.37	1190.31	0.0	0.0	0.0	
86.00	905.00	0.0	0.0	526.50	20000.00	540.00	3777.87	540.89	790.08	0.0	0.0	0.0	
86.00	905.00	0.0	0.0	526.50	38000.00	543.45	7473.92	544.31	805.59	0.0	0.0	0.0	
86.00		0.0	0.0	526.50	48800.00	. 545.05	9935.07	546.05	812.80	0.0	0.0	0.0	
86.00	905.00	0.0	0.0	526.50	87000.00	549.92	18397.72	551.21	834.72	0.0	0.0	0.0	

	ANNEL MIN EL		EL OF CHORD	MIN EL GROUND	DISCHARGE %CFS<	CWSEL	TO	EG	TOPWID	STENCL	STENCR	WSELK	
87.00	270.00	0.0	0.0		20000.00	541.00	6631.46	541.33	803.06	0.0	0.0	0.0	
87.00	270.00	0.0	0.0		38000.00		11377,15	544.77	816.02	0.0	0.0	0.0	
87.00	270.00	0.0	0.0		48800.00		14869.37	546.50	822.38	0.0	0.0	0.0	
87.00	276.00	0.0	0.0		0 87000.00	CONTROL OF THE PROPERTY OF THE PARTY OF THE	26078.31	551.65	841.12	0.0	0.0	0.0	
0,00	2.00		• •	550.00	0 01000.00	330.70	20010-31	331.03	041.12	0.0	0.0	0.0	
88.00	920.00	0.0	0.0	530 7	20000.00	541.92	4415.89	542.66	713.38	0.0	0.0	0.0	
88.00	920.00	0.0	0.0		0 38000.00		7894.71	546.30	735.30	0.0	0.0	0.0	
88.00	920.00	0.0	0.0		0 48800.00		10252.64	548.00	744.71	TO SERVICE SERVICE AND SERVICE			
88.00	920.00		0.0		0 87000.00		18415.45			0.0	0.0	0.0	
50.00	920.00	0.0	0.0	530 • 1	0 87000.00	55/.65	18415.45	553.19	793.71	0.0	0.0	0.0	
89.00	760.00	0.0	0.0	532.6	00.00005	543.53	4713.52	544.13	651.88	0.0	0.0	0.0	
89.00	760.00	0.0	0.0	532.6	0 38000.00	547.24	8495.34	547.94	669.60	0.0	0.0	0.0	
89.00	760.00	0.0	0.0	532.6	0 48800.00	548.75	10881.20	549.63	676.81	0.0	0.0	0.0	
89.00	760.00	0.0	0.0	532.6	87000.00	553.53	19029.58	554.84	694.96	0.0	0.0	0.0	
90.00	150.00	0.0	0.0		00.00005	543.80	4896.19	544.39	637.79	0.0	0.0	0.0	
90.00	150.00	0.0	0.0	533.8	0 38000.00	547.52	8667.79	548.24	657.48	0.0	0.0	0.0	
90.00	150.00	0.0	0.0	533.8	0 48800.00	549.03	11121.40	549.94	665.45	0.0	0.0	0.0	
90.00	150.00	0.0	0.0	533.8	0 87000.00	553.79	19355.23	555.17	682.32	0.0	0.0	0.0	
91.00	905.00	0.0	0.0	532 7	0 20000.00	545.11	4093.27	546.39	528.64	0.0	0.0	0.0	
91.00	905.00	0.0	0.0		38000.00	549.14	7129.58	550.54	638.75	0.0	0.0	0.0	
91.00	905.00	0.0	0.0		0 48800.00	550.60		552.26	669.95	0.0	0.0	0.0	
91.00	905.00	0.0	0.0		87000.00	and the second second section in the second section is	16527.96	557.51	689.05	0.0	0.0	0.0	
92.00	905.00	0 0	0 0	E22 4	20000 00	E 4 7 10	EE04 03	E47 00	EE0 00	0.0			
		0.0	0.0		00.00005	547.18	5586.03	547.98	550.09	0.0	0.0	0.0	
92.00	905.00	0.0	0.0		38000.00		9635.30	552.47	726.19	0.0	0.0	0.0	
92.00	905.00	0.0	0.0		0 48800.00		12283.77	554.22	737.20	0.0	0.0	0.0	
92.00	905.00	0.0	0.0	532.4	87000.00	558.14	21425.23	,559.51	842.20	0.0	0.0	0.0	
93.00	795.00	0.0	0.0	533.0	00.00005	548.09	3794.82	549.65	449.47	0.0	0.0	0.0	
93.00	795.00	0.0	0.0		38000.00	552.78	6992.73	554.31	693.70	0.0	0.0	0.0	
93.00	795.00	0.0	0.0		48800.00	554.29	CONTRACTOR OF THE PARTY OF THE	556.11	699.67	0.0	0.0	0.0	
93.00	795.00	0.0	0.0		87000.00		15923.11	561.46	730.39	0.0	0.0	0.0	
04 00	44E 00	0 0	0 0	524.0	20000 00	540.00	2520 00	EE1 01	E05 00		8 8		
94.00	445.00	0.0	0.0		20000.00	549.33	3539.00	551.01	505.83	0.0	0.0	0.0	
94.00	445.00	0.0	0.0		38000.00	554.66	6974.16	555.67	650.44	0.0	0.0	0.0	
94.00	445.00	0.0	0.0		0 48800.00		9244.63	557.42	654.93	0.0	0.0	0.0	
94.00	445.00	0.0	0.0	534.0	87000.00	560.84	16095.78	562.79	678.70	. 0.0	0.0	0.0	
95.00	380.00	0.0	0.0	531.7	00.00005	551.25	9337.79	551.48	821.03	0.0	0.0	0.0	
95.00	380.00	0.0	0.0		38000.00		13375.89	556.14	902.30	0.0	0.0	0.0	
95.00	380.00	0.0	0.0		48800.00		18644.06	557.89	909.52	0.0	0.0	0.0	
95.00	380.00	0.0	0.0		87000.00		30767.39	563.30	938.38	0.0	0.0	0.0	
v v				/									
96.00	300.00	0.0	0.0		00.00000		7225.17	551.66	999.76	0.0	0.0	0.0	
96.00	300.00	0.0	0.0		38000.00		12326.14	556.37	1095.39	0.0	0.0	0.0	
96.00	300.00	0.0	0.0		48800.00		16632.36	558.09	1104.17	0.0	0.0	0.0	
96.00	300.00	0.0	0.0	537 9	87000.00	563 03	28402.56	563.52	1137.20	0.0	0.0	0.0	

	CHANNEL MIN EL I		EL OF	MIN EL G	%CFS<	CWSEL	. то	E G	TOPWID .	STENCL	STENCR	WSELK	55	
97.00	540.00	0.0	0.0		20000.00	551.72	5527.68	552.11	1126.86	0.0	0.0	0.0		
97.00	540.00	0.0	0.0	538.20	38000.00	556.55	10950.47	556.78	1176.26	0.0	0.0	0.0		
97.00	540.00	0.0	0.0	538.20	48800.00	558.15	14174.32	558.49	1181.84	0.0	0.0	0.0		
97.00	540.00	0.0	0.0	538.20	87000.00	563.46	24740.03	563.94	1200.30	0.0	0.0	0.0		
98.00	300.00	0.0	0.0		20000.00		4655.14	552.49	1390.14	0.0	0.0	0.0		
98.00	300.00	0.0	0.0		38000.00		10641.71	557.02	1446.61	0.0	0.0	0.0		
98.00	300.00	0.0	0.0		48800.00		14386.18	558.72	1452.58	0.0	0.0	0.0		
98.00	300.00	0.0	0.0	536.70	87000.00	563.75	26673.84	564.16	1472.62	0.0	0.0	0.0		
99.00	340.00	0.0	0.0	540.60	20000.00	552.65	7050.38	552.84	1752.86	0.0	0.0	0.0		
99.00	340.00	0.0	0.0	540.60	38000.00	557.14	14849.52	557.25	1824.75	0.0	0.0	0.0		
99.00	340.00	0.0	0.0	540.60	48800.00	558.77	19991.29	558.93	1864.74	0.0	0.0	0.0		
99.00	340.00	0.0	0.0	540.60	87000.00	564.14	36800.40	564.36	1897.42	0.0	0.0	0.0		
100.00	550.00	0.0	0.0	541.50	20000.00		4985.94	553.61	1930.39	0.0	0.0	0.0		
100.00	550.00	0.0	0.0		38000.00		13391.61	557.73	2032.45	0.0	0.0	0.0		
100.00	550.00	0.0	0.0		48800.00		18853.70	559.35	2041.46	0.0	0.0	0.0		
100.00	550.00	0.0	0.0	541.50	87000.00	564.52	38856.79	564.71	2072.06	0.0	0.0	0.0		
SECTION	DISCHARGE	CWSEL		CWSEL DIF			SEL-WSELK	TOPWID	T.W. D	IFF LEN	IGTH			
NUMBER	CFS			EACH Q	EACH SE	PITON	0.0	519.177	0.0	4.4	55.000			
50.0			0.023	0.0	0.0		0.0	548.665	-29.4		5.000			
50.0			2.333	3.310	0.0		0.0	553.869	-34.6		55.000			
50.0			8.831	1.498 5.386	0.0	4	0.0	988.503	-469.3		55.000			
50.0	00 87000.000	209	217	5.366	· · ·		0.0	766.203	-0/.5		,3,000			
51.0			.226	0.0	0.2		0.0	448.995	0.0		25.000			
51.0			2.591	3.365	0.2		0.0	475.120	-26.17		25.000			
51.0			.115	1.524	0.2		0.0	481.018	-32.0		25.000			
51.0	00 87000.000	509	.607	5.492	0.3	40	0.0	1123.391	-674.3	70 . 20	25.000			
52.0	00 20000.000	499	.415	0.0	0.1	89	0.0	351.213	0.0	22	25.000			
52.0		502	.761	3.346	0.1	70	0.0	385.358	-34.1	46 22	25.000			
52.0	00 48800.000	504	.267	1.506	0.1	52	0.0	391.756	-40.5		25.000			
52.0	00 87000.000	509	.627	5.361	0.0	21	0.0	1277.448	-926.2	35 22	25.000			
52.1	000.0000	499	9.873	0.0	0.4	58	0.0	252.395	0.0	27	75.000			
52.1			3.188	3.315	0.4		0.0	287.161	-34.7	66 27	75.000			
52.1			.667	1.479	0.4		0.0	302.549	-50.1	54 27	75.000			
52.1			.136	5.468	0.5	08	0.0	1228.341	-975.9	47 27	75.000			
53.0	00 20000.000	500	.656	0.0	0.7	83	0.0	205.386	0.0		75.000			
53.0			.176	3.519	0.9	88	0.0	278.953	-73.5		75.000			
53.0			5.782	1.606	1.1		0.0	294.840	-89.4		75.000			
53.0	00 87000.000	512	2.069	6.287	1.9	33	0.0	1375.919	-1170.5	33 27	75.000			
54.0	00 20000.000		3.318	0.0	2.6		0.0	203.076	0.0		05.000			
54.0			7.749	4.431	3.5		0.0	282.398	-79.3		05.000			
54.0			.860	2.111	4.0		0.0	299.196	-96.1		05.000			
54.0	00 87000.000	514	.505	4.645	2.4	37	0.0	1400.390	-1197.3	14 80	05.000			
55.0	000.0000	504	.948	0.0	1.6		0.0	232.571	0.0		55.000			
55.0		509	.893	4.945	2.1		0.0	326.667	-94.0		55.000			
55.0			2.257	2.364	2.3	97	0.0	339.302	-106.7		55.000			
55.0			3.420	6.163	3.9	15	0.0	1141.396	-908.8	26 65	55.000			
56.0	000.0000	505	3.358	0.0	0.4	10	0.0	201.345	0.0	38	30.000			
56.0			.540	5.182			0.0	447.528	-246.1		30.000			
56.0			3.095	2.554	0.8		0.0	479.611	-278.2	67 38	80.000			
	00 87000.000		.198	6.103	0.7		0.0	1150.158	-948.8	13 38	80.000			

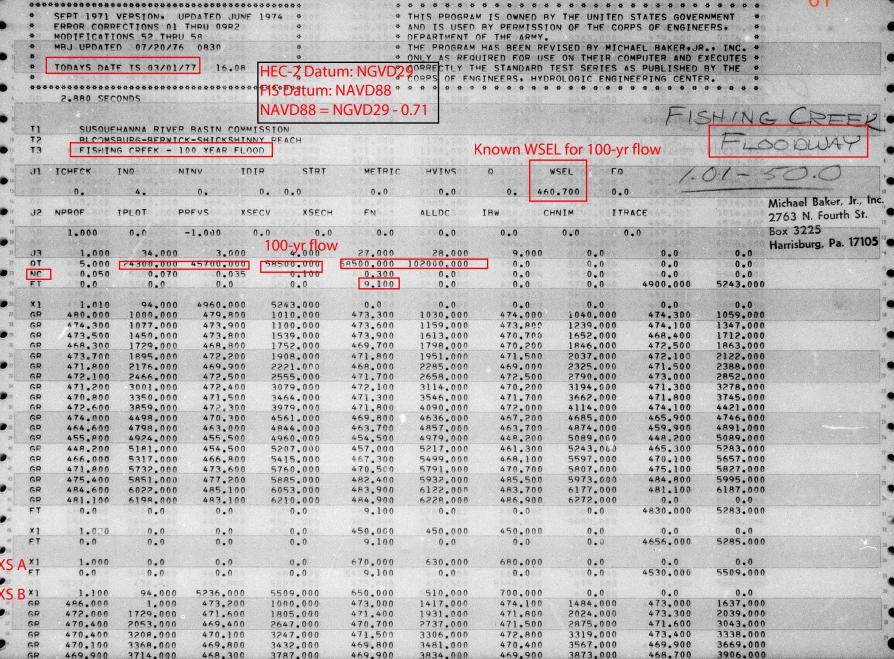
					DO	ANGE,	PA						
SUMMARY PRI	NTOUT FOR M	ULTIPLE P	KULLES	ereret suggest	11 A C 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1	1 4 18 1					STRWIN.	1458.4F	
FISHING CRE	FK 500 YEAR	F		601	14650 E				ATALESTY		1.5		
SECTION CH		L OF MAX	EL OF M	IN EL	*CFS	CWSEL	то	EG	TOPWID	STENCL	STENCE	WSELK	
NUMBER LE	NGTH ROADW	IAY LOW	CHORD G	SROUND	ACT 3.	100					0.0	553.09	
100.00	550.00	0.0	0.0		20000.00	553.09	4977.08	553.61	1929.98	0.0	0.0	557.59	
100.00	550.00	0.0	0.0		38000.00		13391.27	557.73 559.35	2041.46	0.0	0.0	559.17	
100.00	550.00	0.0	0.0		48800.00		18851.92	564.71	2072.06	0.0	0.0	564.52	
100.00	550.00	0.0	0.0	541.50	87000.00	564.52	38857.89	304.11	我想在一个	8.30			
						FE2 15	3551.99	554.27	1620.82	0.0	0.0	0.0	
101.00	180.00	0.0	0.0		20000.00		10641.75	557.97	1874.07	0.0	0.0	0.0	
101.00	180.00	0.0	0.0		38000.00	550 25	15580.47	559.56	1885.41	0.0	0.0	0.0	
101.00	180.00	0.0	0.0		48800.00		33880.44	564.86	1913.50	0.0	0.0	0.0	
101.00	180.00	0.0	0.0	542.60	87000.00	201.33			Design Control				
	-75 -6	0.0	0.0	542.30	20000.00	555.13	5244.39	555.82	1363.92	0.0	0.0	0.0	
105.00	740.00	0.0	0.0		38000.00	558.71		559.12	1641.69	0.0	0.0	0.0	
102.00	740.00	0.0	0.0	STATISTICS HOLDER TO ARREST TO	48800.00		12496.16	560.48	1649.06	0.0	0.0	0.0	
102.00	740.00	0.0	0.0		87000.00		26570.58	565.51	1674.81	0.0	0.0	0.0	
102.00	740.00	0.0	0.0	5.5			4						
	285.00	0.0	0.0	545-00	20000.00	555.46	4491.00	556.37	1227.78	0.0	0.0	0.0	
103.00	CONTRACTOR AND AND STREET, STR	0.0	0.0		38000.00		8120.93	559.72	1644.35	0.0	0.0	0.0	
103.00	285.00		0.0		48800.00		11293.14	561.00	1668.56	0.0	0.0	0.0	
103.00	285.00	0.0	0.0		87000.00		24852.39	565.85	1879.11	0.0	0.0	0.0	
103.00	285.00	0.0	0.0	-77-00		10 May 10			3.13.2 . Nov				
	380.00	0.0	0.0	543.00	20000.00	556.17	4123.73	557.41	425.82	0.0	0.0	0.0	
104.00		0.0	0.0		38000.00	560.05		561.52	1118.48	0.0	0.0	0.0	
104.00	380.00	0.0	0.0		48800.00	560.93	7695.59	562.94	1141.62	0.0	0.0	0.0	
104.00	380.00	0.0	0.0		87000.00		15416.47	567.48	1210.91	0.0	0.0	0.0	
104.00	380.00	0.0		T. C. S.	CONTRACTOR OF							0.0	
100 01	145.00	0.0	0.0	541.00	20000.00	556.44	4622.26	557.87	397.29	0.0	0.0	0.0	
106.01	145.00	0.0	0.0		38000.00	560.57		562.46	666.88	0.0	0.0	0.0	
106.01	145.00	0.0	0.0		48800.00	561.36		564.17	689.58	0.0	0.0	0.0	
	145.00	0.0	0.0		87000.00	565.81	12767.59	569.41	732.51	0.0	0.0	U•U	
106.01	1-7.0	0.8	1.5				400	多数的。新型			0.0	0.0	
106.02	30.00	557.10	557.90	541.00	20000.00	557.87		558.89	434.96	0.0	0.0	0.0	
106.02	30.00	557.10	557.90	541.00	38000.00	562.04		563.51	709.28	0.0	0.0	0.0	
106.02	30.00	557.10	557.90	541.00	48800.00	562.76		564.83	718.69	0.0	0.0	0.0	
106.02	30.00	557.10	557.90		87000.00	565.83	12792.79	569.41	732.60	0.0	0.0	0.0	
100.02									421 00	0.0	0.0	0.0	
106.00	100.00	0.0	0.0	541.50	20000.00	558.13		559.07	431.08	0.0	0.0	0.0	
106.00	100.00	0.0	0.0		38000.00		10004.92	563.85	717.17	0.0	0.0	0.0	
106.00	100.00	0.0	0.0		48800.00	564.22	12000.70	565.35	723.02	0.0	0.0	0.0	
106.00	100.00	0.0	0.0	541.50	87000.00	568.93	3 21112.14	570.35	744.32	0.0			
								E60 70	229.10	0.0	0.0	0.0	
107.00	755.00	0.0	0.0		00.00000		3623.28	560.70	739.93	0.0	0.0	0.0	
15 107.00	755.00	0.0	0.0		38000.00	564.18	10688.35	564.82	746.55	0.0	0.0	0.0	
107.00	755.00	0.0	0.0		48800.00		13315.87	566.40	764.57	0.0	0.0	0.0	
107.00	755.00	0.0	0.0	547.00	87000.00	570.32	2 23440.31	571.40	164.51	0.0	•••		
								561 67	301.91	0.0	0.0	0.0	
108.00	350.00	0.0	0.0		00.00000	560.56	4024.37	561.67	850.43	0.0	0.0	0.0	
A 108.00	350.00	0.0	0.0		0 38000.00		10971.55	565.19	858.02	0.0	0.0	0.0	
			0.0	546.5	0 48800.00	566.L	1 13687.47	566.80					
108.00	350.00	0.0	0.0		0 87000.00	Tonas de la constante de la co	4 24001.68	571.80	881.87	0.0	0.0	0.0	

	CHANNEL MIN EL		X EL OF	MIN EL I	%CFS<	CWSEL	TQ	EG	TOPWID	STENCL	STENCE	WSELK	
109.00	365-00	0.0	0.0		20000.00	561.79	5545.20	562.37	533.42	0.0	0.0	0.0	
109.00	365.00	0.0	0.0	550.00	38000.00	564.98	10704.90	565.63	838.51	0.0	0.0	0.0	
109.00	365.00	0.0	0.0	550.00	48800.00	566.49	13316.17	567.27	870.00	0.0	0.0	0.0	, i
109.00	365.00	0.0	0.00	550.00	87000.00	571.21	23235.77	572.29	902.86	0.0	0.0	0.0	
110.00	580.00	0.0	0.0	549.80	20000.00	562.63	6365.51	563.04	691.35	0.0	0.0	0.0	
1 110.00	580.00	0.0	0.0	549.30	38000.00	565.66	10214.59	566.41	705.29	0.0	0.0	0.0	
110.00		0.0	0.0	549.110	48800.00	567.19	12511.01	568.13	711.89	0.0	0.0	0.0	
110.00		0.0	0.0	9.80	87000.00	571.82	20553.51	573.32	751.73	0.0	0.0	0.0	
111.00	550.00	0.0	0.0	551.70	20000.00	563.29	4652.00	563.75	804.92	0.0	0.0	0.0	
J 111.00		0.0	0.0	551.70	38000.00	566.56	8363.54	567.29	824.69	0.0	0.0	0.0	
111.00		0.0	0.0	551.70	48800.00	568.20	10558.88	569.06	834.59	0.0	0.0	0.0	
111.00		0.0	0.0	551.70	87000.00	573.08	18373.93	574.36	873.89	0.0	0.0	0.0	
0/112.00	405.00	0.0	0.0	553.10	20000.00	563.95	4893.94	564.43	898.41	0.0	0.0	0.0	
1/112.00		0.0	0.0	553.10	38000.00	567.34	9074.78	568.02	915.77	0.0	0.0	0.0	
112.00		0.0	0.0	553.10	48800.00	569.03	11583.23	569.81	924.43	0.0	0.0	0.0	
1112.00		0.0	0.0	553.10	87000.00	574.05	20599.93	575.14	9/8.13	0.0	0.0	0.0	5.31
113.00	100.00	0.0	0.0	551.50	20000.00	564.05	3441.67	564.95	761.83	0.0	0.0	0.0	,
113.00	100.00	0.0	0.0	551.50	38000.00	567.44	6696.40	568.57	774.29	0.0	0.0	0.0	
113.00		0.0	0.0	551.50	48800.00	569.12	8662.97	570.38	780.47	0.0	0.0	0.0	
113.00		0.0	0.0	551.50	87000.00	574.10	15771.31	575.75	828.28	0.0	0.0	0.0	
114.00	550.00	0.0	0.0	551.70	20000.00	565.69	3>39.64	566.64	792.84	0.0	0.0	0.0	
		0.0	0.0	551.70	38000.00	569.07	7264.72	570.29	870.84	0.0	0.0	0.0	
114.00		0.0	0.0	551.70	48800.00	570.75	9348.90	572.08	882.01	0.0	0.0	0.0	
114.00		0.0	0.0	551.70	87000.00	575.73	16999.74	577.38	925.23	0.0	0.0	0.0	
1115.00	0 510.00	0.0	0.0	555.00	20000.00	567.17	3473.31	567.88	1062.30	0.0	0.0	0.0	
115-00	510.00	0.0	0.0	555.00	38000.00	570.64	7306.04	571.42	1100.02	0.0	0.0	0.0	
115.00		0.0	0.0	555.00	48800.00	572.33	9725.49	573.15	1108.86	0.0	0.0	0.0	
115.00		0.0	0.0	555.00	87000.00	577.35	18751.20	578.33	1128.64	0.0	0.0	0.0	
116.00	265.00	0.0	0.0	553.00	20000.00	568.03	3920.73	568.69	1180.50	0.0	0.0	0.0	
A 116.00		0.0	0.0	553.00	38000.00	571.48	8118.11	572.10	1521.73	0.0	0.0	0.0	
116.00		0.0	0.0	553.00	48800.00	573.19	10925.59	573.79	1545.66	0.0	0.0	0.0	•
116.00		0.0	0.0	553.00	87000.00	578.28	21781.24	578.88	1574.72	0.0	0.0	0.0	
- 117.00	525.00	0.0	0.0	553.70	20000.00	569.11	3214.70	569.72	1354.57	0.0	0.0	0.0	
P117.00	525.00	0.0	0.0	553.70	38000.00	572.38	8078.34	572.78	2047.35	0.0	0.0	0.0	
117.00		0.0	0.0	553.70	48800.00	574.02	11774.34	574.36	2272.73	0.0	0.0	0.0	
117.00		0.0	0.0	553.70	87000.00	578.99	27784.17	579.27	2353.04	0.0	0.0	0.0	
(118.00	0 265.00	0.0	0.0	558.00	20000.00	569.95	4384.34		1242.37	0.0	0.0	0.0	
118.00	265.00	0.0	0.0	558.00	38000.00	572.82	9078.27	573.31	2022.69	0.0	0.0	0.0	
118.00		0.0	0.0	558.00	49800.00	574.35	12622.48	574.80	2099.04	0.0	0.0	0.0	
118.00		0.0	0.0	558.00	87000.00	579.16	27956.08	579.55	2200.19	0.0	0.0	0.0	

UMR		HANNEL MIN EI ENGTH ROADW		X EL OF	MIN EL GROUND	SCFS<	CWSEL	TQ	EG	TOPWID	STENCL	STENCR	WSELK	
	19.00	420.00	0.0	0.0		50000.00	570.98	4888.68	571.22	1713.0R	0.0	0.0	0.0	
THE PERSON NAMED IN COLUMN 1	19.00	420.00	0.0	0.0		38000.00	573.71	10074.74	573.96	2041.78	0.0	0.0	0.0	
	19.00	420.00	0.0	0.0	THE RESERVE THE PROPERTY OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TO	48800.00	575.10	13608.56	575.37	2087.97	0.0	0.0	0.0	
1	19.00	420.00	0.0	0.0	559.20	87000.00	579.64	28433.60	579.94	2171.77	0.0	0.0	0.0	
1	20.00	765.00	0.0	0.0	560.80	20000.00	572.09	5643.13	572.23	1704.16	0.0	0.0	0.0	
6 1	20.00	765.00	0.0	0.0	560.80	38000.00	574.70	10804.24	574.88	2073.55	0.0	0.0	0.0	
L 1	20.00	765.00	0.0	0.0	560.80	48800.00	576.02	14201.91	576.23	2103.10	0.0	0.0	0.0	
1	20.00	765.00	0.0	0.0	560.80	87000.00	580.33	28373.93	580.59	2177.03	.0.0	0.0	0.0	
1	21.00	840.00	0.0	0.0	562.10	20000.00	572.99	6152.30	573.15	2016.73	0.0	0.0	0.0	
1,1	21.00	840.00	0.0	0.0	562.10	38000.00	575.59	11807.78	575.78	2253.36	0.0	0.0	0.0	
1	21.00	840.00	0.0	0.0	562.10	48800.00	576.88	15358.18	577.10	2261.07	0.0	0.0	0.0	
' 1	21.00	840.00	0.0	0.0	562.10	87000.00		29648.05	581.31	2315.03	0.0	0.0	0.0	
1	22.00	715.00	0.0	0.0	563.00	20000.00	573.98	3840.40	574.25	1275.00	0.0	0.0	0.0	
/1	22.00	715.00	0.0	0.0	563.00	38000.00	576.51	7526.62	576.85	2218.73	0.0	0.0	0.0	
61	22.00	715.00	0.0	0.0	563.00	48800.00	577.76	10122.26	578.11	2248.59	0.0	0.0	0.0	
1	22.00	715.00	0.0	0.0	563.00	87000.00		21370.39	582.11	2341.89	0.0	0.0	0.0	
1	23.00	545.00	0.0	0.0	564.70	20000.00	575.48	3594.05	576.01	2172.58	0.0	0.0	0.0	
1 1	23.00	545.00	0.0	0.0		38000.00		7943.32	578.28	2278.23	0.0	0.0	0.0	
	23.00	545.00	0.0	0.0		48800.00		10671.24	579.42	2300.24	0.0	0.0	0.0	
1 1	23.00	545.00	0.0	0.0		87000.00		21890.57	583.08	2384.99	0.0	0.0	0.0	
1	23.50	300.00	0.0	0.0	567.00	17200.00	576.84	2265.67	578.90	229.89	0.0	0.0	0.0	
1	23.50	300.00	0.0	0.0	567.00	32900.00	579.79	9750.49	580.01	2875.64	0.0	0.0	0.0	
	23.50	300.00	0.0	0.0	567.00	42400.00	580.90	12851.13	581.11	3218.24	0.0	0.0	0.0	
1	23.50	300.00	0.0	0.0	567.00	77000.00	584.27	25985.20	584.49	3300.21	0.0	0.0	0.0	
, 1	24.00	320.00	0.0	0.0	568.00	17200.00	578.67	2264.57	580.82	175.92	0.0	0.0	0.0	
	24.00	320.00	0.0	0.0	568.00	32900.00	580.24	4528.66	581.77	1557.18	0.0	0.0	0.0	
	24.00	320.00	0.0	0.0	568.00	42400.00	581.33	5994.19	582.78	1945.82	0.0	0.0	0.0	
1	24.00	320.00	0.0	0.0	568.00	77000.00	584.64	13094.85	585.63	2670.95	0.0	0.0	0.0	
, 1:	24.10	115.00	0.0	0.0	568.60	17200.00	579.42	2325.87	581.49	177.07	0.0	0.0	0.0	
11:	24.10	115.00	0.0	0.0	568.60	32900.00	581.90	5943.82	582.78	1935.69	0.0	0.0	0.0	
	24.10	115.00	0.0	0.0	568.60	42400.00	582.94	7730.90	583.80	2259.84	0.0	0.0	0.0	
13	24.10	115.00	0.0	0.0	568.60	77000.00	585.65	14270.98	586.49	2735.53	0.0	0.0	0.0	
17	26.01	115.00	0.0	0.0	568.00	17200.00	580.05	2138.46	582.38	156.00	0.0	0.0	0.0	
	26.01	115.00	0.0	0.0		32900.00	582.56	5125.66	583.84	2326.96	0.0	0.0	0.0	
17	26.01	115.00	0.0	0.0	568.00	42400.00	583.65	7182.86	584.68	2329.50	0.0	0.0	0.0	15
17	26.01	115.00	0.0	0.0	568.00	77000.00	586.42	14039.98	587.30	2335.98	0.0	0.0	0.0	
12	26.02	80.00	585.50	584.70	568.00	17200.00	580.51	2320.69	582.62	156.00	0.0	0.0	0.0	
-12	26.02	80.00	585.50	584.70	568.00	32900.00	586.88	15399.75	587.02	2337.06	0.0	0.0	0.0	
	26.02	80.00	585.50	584.70	568.00	42400.00		17223.13	587.67	2338.46	0.0	0.0	0.0	
100000000000000000000000000000000000000	26.02	80.00	585.50	584.70	568-00	77000.00	590-05	26054.29	590.34	2344.45	0.0	0.0	0.0	

SECTION	CHANNEL MIN EL		EL OF	MIN EL DISCHAR		ТО	EG	TOPWID	STENCL	STENCR	WSELK	
127.0		0.0	0.0	570.50 17200.		4235.55	585.06	809.41	0.0	0.0	0.0	
V _ 127.0		0.0	0.0	570.50 32900.		9018.06	587.60	1994.71	0.0	0.0	0.0	
1 127.0	0 835.00	0.0	0.0	570.50 42400.	00 587.76	10617.04	588.35	1998.18	0.0	0.0	0.0	
127.0	0 835.00	0.0	0.0	570.50 77000.	00 590.36	18410.50	591.07	2012.11	0.0	0.0	0.0	
128.0		0.0	0.0	572.00 17200.		4739.81	585.99	1026.32	0.0	0.0	0.0	
2, 128.0		0.0	0.0	572.00 32900.			588.51	1475.56	0.0	0.0	0.0	
L 128.0		0.0	0.0	572.00 42400.		9239.14	589.44	1479.91	0.0	0.0	0.0	
128.0	750.00	0.0	0.0	572.00 77000.	00 591.01	14237.68	592.39	1494.51	0.0	0.0	0.0	
129.0		0.0	0.0	573.50 17200.		4407.63	586.61		0.0	0.0	0.0	
A 129.0		0.0	0.0	573.50 32900.		7667.13	589.30	1231.32	0.0	0.0	0.0	
A 158.0		0.0	0.0	573.50 42400.		9119.10	590.40		0.0	0.0	0.0	
129.0	0 415,00	0.0	0.0	573.50 77000.	00 592.43	14157.87	593.73	1277.19	0.0	0.0	0.0	
,130.0	00 632.00	0.0	0.0	572.00 17200.	00 587.38	3006.64	588.31	1664.74	0.0	0.0	0.0	
N130.0		0.0	0.0	572.00 32900.				1773.15	0.0	0.0	0.0	
1 130.0		0.0	0.0	572.00 42400.		9079.75		1778.53	0.0	0.0	0.0	
130.0	632.00	0.0	0.0	. 572.00 77000.	00 595.05	17012.97	595.73	1793.79	0.0	0.0	0.0	
131.0	00.00	0.0	0.0	577.00 17200.		4637.05	589.76	2018.39	0.0	0.0	0.0	
70 131.0	00.00	0.0	0.0	577.00 32900.	00 591.66	9154.80	591.99	2129.03	0.0	0.0	0.0	
131.0	00.00	0.0	0.0	577.00 42400.	00 592.80	12110.71	593.14		0.0	0.0	0.0	
131.0	00.00	0.0	0.0	577.00 77000.	00 596.26	23380.60	596.63	2152.61	0.0	0.0	0.0	
132.0	0 550.00	00	0.0	580.00 17200.	00 590.16	3542.92	590.53	1918.11	0.0	0.0	0.0	
7 132.0	550.00	0.0	0.0	580.00 32900.	00 592.25	7825.96	592.59	2124.96	0.0	0.0	0.0	
132.0	550.00	0.0	0.0	580.00 42400.	00 593.33	10720.20	593.67	2130.94	0.0	0.0	0.0	
132.0	550.00	0.0	0.0	580.00 77000.	00 596.68	22193.71	597.05	2149.46	0.0	0.0	0.0	
133.0	0 560.00	0.0	0.0	580.80 17200.	00 591.25	3737.28	591.52	2452.26	0.0	0.0	0.0	
133.0		0.0	0.0	580.80 32900.		7716.44	593.32	2582.09	0.0	0.0	0.0	
入 133.0		0.0	0.0	580.80 42400.		10545.95	594.30	2618.27	0.0	0.0	0.0	
133.0	560.00	0.0	0.0	580.80 77000.	00 597.23	22570.49	597.51	2736.70	0.0	0.0	0.0	
134.0	0 865.00	0.0	0.0	581.00 17200.	00 592.49	2846.93	592.90	2161.12	0.0	0.0	0.0	
134.0	0 865.00	0.0	0.0	581.00 32900.	00 593.99	5199.51	594.49	2243.04	0.0	0.0	0.0	
L 134.0	0 865.00	0.0	0.0	581.00 42400.	00 594.82	6816.21	595.34	2274.60	0.0	0.0	0.0	
134.0	0 865.00	0.0	0.0	581.00 77000.	00 597.70	14017.38	598.23	2318.45	0.0	0.0	0.0	
135.0	0 625.00	0.0	0.0	585.00 17200.	00 594.68	2931.17	595.06	1736.95	0.0	0.0	0.0	
135.0		0.0	0.0	585.00 32900.	00 596.35	5431.23	596.82	2283.48	0.0	0.0	0.0	
7 135.0		0.0	0.0	585.00 42400.		6934.07	597.65	2287.90	0.0	0.0	0.0	
135.0	0 625.00	0.0	0.0	585.00 77000.	00 599.61	12969.76	600.23	2302.02	0.0	0.0	0.0	
136.0	0 575.00	0.0	0.0	586.00 17200.	00 595.91	4226.84	596.13	2092.76	0.0	0.0	0.0	
1 136.0		0.0	0.0	586.00 32900.			597.98	2114.10	0.0	0.0	0.0	
136.0		0.0	0.0	586.00 42400.		9298.87	598.85	2124.04	0.0	0.0	0.0	
136.0	0 575.00	0.0	0.0	586.00 77000.	00 600.93	15781.73	601.47	2146.58	0.0	0.0	0.0	
	The state of the s		2 6 5 Y					4				
					44.0				•			
		Contract of the										

•		CHANNEL MIN EL LENGTH ROADWA		X EL OF	MIN EL GROUND	DISCHARGE %CES<	CWSEL	то	FG	TOPWID	STENCL	STENCR	WSELK	/
ı	137.00		0.0	0.0		17200.00	596.76	3132.46	597.15	1898.25	0.0	0.0	0.0	***************************************
● 2	137.00		0.0	0.0		32900.00	598.54			1933.71	0.0	0.0	0.0	10
1	l 137,00		0-0	0.0		42400.00	599.38			1950.40	0.0	0.0	0.0	
t	137.00		9.9	0.0		77000.00		16117.42			0.0	0.0	0.0	**************************************
• 5	138.00	615.00	0.0	0.0	588.50	17200.00	598.07	4235.67	598.28	1698.22	0.0	0.0	0.0	•
1	, 138.00		0.0	0.0		32900.00	599.72			1828.56	0.0	0.0	0.0	*
	V 138.00		0.0	0.0		42400.00	600.55			2029.66	0.0	0.0	0.0	s and s
0	138.00		0.0	0.0		77000.00		16979.70		2118.75	0.0	0.0	0.0	
16	139.00	590.00	0.0	0.0	589.00	17200.00	599.04	2969.52	599.69	995.24	0.0	0.0	0.0	,
12	. 139.00		0.0	0.0		32900.00	600.80			1778.55	0.0	0.0	0.0	
المدا	W 139.00		0.0	. 0.0		42400.00	601.65			1826.18	0.0	0.0	0.0	•
-4	139.00		0.0	0.0		77000.00		12879.05		1834.63	0.0	0.0	0.0	'e
15	140.00	385.00	0.0	0.0	580 50	17200.00	600,15	3967.95	600.60	1215.62	0.0	0.0	0.0	18
-	140.00		0.0	0.0		32900.00	602.15			1768.28	0.0	0.0	0.0	nady here.
	£ 140.00		0.0	0.0		42400.00	602.99			1771.99	0.0	0.0	0.0	53 M. Bassafe Maring
T.	140.00		0.0	0.0		77000.00		16170.23		1814.38	0.0	0.0	0.0	17
20				•••	307.30	71000.00	003.34	10110.23	600.13	1014.36	••	0.0		Parker Parker Po
21	141.00		0.0	0.0	590.50	17200.00	601.68		602.25	1282.33	0.0	0.0	0.0	14
22	141.00		0.0	0.0		32900.00	603.71		604.38	1798.12	0.0	0.0	0.0	
on/	7 141.00		0.0	0.0		42400.00		8544.65		1870.47	0.0	0.00.0	0.0	
24	141.00	890.00	0.0	0.0	590.50	77000.00	607.08	15044.27	607.95	1890.80	0.0	0.0	0.0	16
25	142.00	365.00	0.0	0.0	592.00	17200.00	602.59	4724.35	602.88	1806.39	0.0	0.0	0.0	n_
27	7 142.00	365.00	0.0	0.0	592.00	32900.00	604.70	9479.43	605.00	2013.10	0.0	0.0	0.0	18
28 /	7/142.00	365.00	0.0	0.0	592.00	42400.00	605.61	12101.39	605.94	2016.60	0.0	0.0	0.0	
• 11	142.00	365.00	0.0	0.0	592.00	77000.00	608.18	21225.65	608.63	2026.47	0.0	0.0	+710.000	"•
30 31	143,01	267.00	0.0	0.0	591.30	17200.00	602.76	2737.78	604.04	1406.49	0.0	0.0	0.0	20
→ 32	143.01	267.00	0.0	0.0		32900.00	604.93			1647.23	0.0	0.0	0.0	21 🚗
33	143.01	267.00	0.0	0.0		42400.00	605.86			1689.75	0.0	0.0	0.0	22
34	143.01	267.00	0.0	0.0		77000.00		15286.77	609.40	1721.22	0.0	0.0	0.0	77
25	n 143.00	268.00	0.0	0.0	592.00	17200.00	604.16	3581.33	604.89	1472.52	0.0	0.0	0.0	•
v.	143.00	268.00	0.0	0.0		32900.00	605.77			1653.66	0.0	0.0	0.0	
-uX	143.00		0.0	0.0		42400.00	606.62			1691.41	0.0	0.0	0.0	- 15
37	143.00		0.0	0.0		77000.00		15216.01	610.09	1721.09	0.0	0.0	0.0	14
40	- 144 00	600.00		94.430	504 30	17200 00	40F 44	4102-61	(AF 06	1400 14	0.0			π _
	144.00	600.00	0.0	0.0		17200.00	607.37	4103.61	605.96	1489.16	0.0	0.0	0.0	
a K	144.00	600.00	0.0	0.0		42400.00	608.16			1671.90	0.0	0.0	0.0	18
-1	144.00	600.00	0.0	0.0		77000.00		14156.03		1814.17	0.0	0.0	0.0	n •
45		1.177 (198.1			19333435			755,758						30
-4	145.00	560.00	0.0	0.0		17200.00	606.53			724.26	0.0	0.0	0.0	31
1	145.00	560.00	0.0	0.0		32900.00	608.28	4247.29		1013.04	0.0	0.0	0.0	
46	145.00	560.00 560.00	0.0	0.0		77000.00	609.10			1203.16	0.0	0.0	0.0	37
10%														n •
51	SECTION	DISCHARGE	CWSE		CWSEL DIF		TFF CWS	EL-WSFLK	TOPWID	T.W. DIF	LEN	STH		у
52	NUMBER 100.0	CFS 00 20000.000	ee.	3.092	EACH Q 0.0	EACH SE	CITON	0.0	1929.977	0.0	FE	0.000		33
51	100.0			7.591	4.499	0.0		0.0	2032.448	-102.470		0.000		
· ·	100.0			9.167	1.576	0.0		0.0	2041.458	-111.481		0.000		36
-4	100.0			4.521	5.354	0.0		0.0	2072.065	-142.087		0.000		n
57					7867,60							2009		38
58	101.0			3.146	0.0	0.0		0.0	1620.818	0.0		0.000		39
2	101.04			7.726	4.580	0.1		0.0	1874.074	-253.256		0.000		
	101.00	00 48800.000	559	9.254	1.528	0.0	88	0.0	1885.409	-264.591	18	0.000		



ecoliticani dell'alla della constitu													
	GR	466.300	3975.000	465.200	4037.000	465.600	4143.000	466.000	4228.000	468.600	4541.000	62	
	GR	465.900	4833.000	467.300	4871.000	467.800	4919.000	473.500	4938.000	474.100	4947.000		
	GR	474.100	4957.000	474.000	4968.000	472.100	4997.000	470.500	5050.000	470.200	5118.000		
	GR	469.700	5189.000	466.800	5236.000	460.700	5263.000	449.400	5265.000	449.400	5282.000		
•	GR	479.400	5282.000	479.400	5290.000	449.400	5290.000	449.400	5325.000	479.400	5325.000		. 0
	GR	479.400	5333.000	449.400	5333.000	449.400	5368.000	479.400	5368.000	479.400	5376.000		
1	GR	449.400	5376.000	449.400	5411.000	479.400	5411.000	479.400	5419.000	449.400	5419.000		
● 1	GR	449.400	5454.000	479.400	5454.000	479.400	5462.000	449.400	5462.000	449.400	5488.000		
	GR	454.800	5493.000	462.900	5501.000	466.300	5509.000	469.900	5549.000	468.600	5605.000		2
	GR	475.100	5757.000	477.800	5896.000	482.500	5973.000	483.900	6022.000	484.300	6036.000		
•	GR	482.700	6046.000	482.900	6062.000	483.900	6105.000	486.300	6153.000	485.500	6157.000		
	GR	485.800	6181.000	487.200	6204.000	488.600	6235.000	490.800	6254.000	490.800	6275.000		4
7	GR	493.700	6297.000	496.400	6403.000	496.400	6443.000	495.800	6448.000	0.0	0.0		
•	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4160.000	5545.000		
9			,										. 6
XS C	X1	2.000	95.000	5349.000	5545.000	350,000	170.000	230.000	0.0	0.0	0.0		
• H	GR	485.000	1.000	468.500	1000.000	471.100	1126.000	470.800	1178.000	470.200	1216.000		•
	GR.	470.700	1265.000	473.000	1339.000	473.500	1405.000	473.900	1470.000	474.800	1548.000		4
13	GR	475.400	1624.000	476.000	1663.000	477.400	1714.000	476.200	1764.000	474.900	1810.000		
● 14	GR	473.600	1835.000	473.400	1863.000	472.800	1984.000	471.100	2159.000	471.400	2295.000		
15	GR	471.900	2382.000	471.800	2491.000	471.400	2572.000	470.400	2664.000	469.400	2754.000		10
16	GR	468.100	2873.000	468.700	2978.000	468.200	3088.000	468.200	3204.000	467.800	3316.000		H
• 17 ·	GR	467.800	3434.000	469.400	3553.000	468.500	3660.000	468.200	3791.000	469.300	3914.000		•
H	GR	468.100	4059.000	467.300	4189.000	466,800	4338.000	465.900	4478.000	466.800	4596.000		12
19	GR	466.400	4721.000	466.900	4769.000	. 467.000	4799.000	467.200	4826.000	467.100	4834.000		
● 20	GR	465.000	4857.000	455.400	4886.000	461.700	4906.000	465.400	4941.000	469.200	4958.000		•
21	GR	469.200	4972.000	467.000	4988.000	466.300	5049.000	466.300	5127.000	466.400	5207.000		14.
73	GR	466.400	5259.000	465.900	5308.000	460.600	5349.000	456.800	5361.000	454.800	5368.000		
6 13	GR	446.000	5397.000	446.000	5451.000	446.000	5516.000	454.800	5533.000	460.900	5545.000		•
74	GR	470.600	5560.000	473.700	5610.000	474.800	5661.000	475.400	5703.000	475.400	5726.000		16
75	GR	475.400	5741.000	476.600	5785.000	480.000	5840.000	481.300	5888.000	481.700	5926.000		1,,
● 26	GR	482.400	5959.000	484.900	5972.000	485.100	5987.000	485.100	6012.000	484.900	6020.000		
27	GR	485.700	6038.000	489.600	6072.000	490.400	6110.000	491.100	6129.000	491.900	6155.000		15
28	GR	492.600	6203.000	498.500	6239.000	499.000	6271.000	499.700	6308.000	499.700	6323.000		. \$
● 71	GR	496.800	6343.000	496.800	6356.000	496.800	6362.000	504.900	6376.000	510.200	6388.000		
30	NC	0.0	0.0	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0		70
31	FI	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4140.000	5689.000		21
● 17													
22	X1	3.010	68.000	5527.000	5689.000	50.000	125.000	125.000	0.0	0.0	0.0		27
34	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	464.500	476.100	0.0		71
● 15	GR ·	485.000	1.000	467.100	1032.000	465.600	1048.000	467.200	1062.000	468.400	1128.000		•
1.0	GR	469.600	1200.000	468.300	1256.000	470.100	1276.000	471.800	1335.000	472.700	1362.000		и
27	GR	473.700	1407.000	472.700	1461.000	472.800	1521.000	473.800	1562.600	475.300	1623,000		
● ≈	GR	475.700	1663.000	476.000	1726.000	475.200	1778.000	474.800	1861.000	468.700	1880.000		
39	GR	468.800	1898.000	469.200	1941.000	470.100	2019.000	471.500	2111.000	470.900	2199.000		26
40	GR	470.800	2307.000	471.700	2432.000	471.700	2533.000	471.600	2629.000	470.200	2740.000		17
3 -41	GR	469.800	2835.000	469.900	2959.000	467.600	3084.000	469.000	3183.000	469.400	3303.000		•
- 47	GR	468.400	3399.000	468.600	3482.000	468.700	3588.000	468.700	3754.000	468.900	3909.000		. 28
43	GR	466.400	4042.000	464.500	4136.000	464.900	4204.000	465.800	4296.000	466.200	4427.000		
10 -11	GR	466.700	4547.000	467.300	4681.000	467.300	4776.000	465.800	4807.000	466.600	4839.000		•
45	GR	466.500	4863.000	466.500	4882.000	466.500	4925.000	466.600	4983.000	466.900	5065.000		10
46	GR	466.300	5140.000	466.600	5223.000	466,400	5289.000	467.600	5387.000	466.000	5439.000		
	GR	458.000	5486.000	449.500	5527.000	449.500	5527.000	449.500	5689.000	449.500	5689.000		
42	GR	455.000	5700.000	476.100	5761.000	485.400	6002.000	0.0	0.0	0.0	0.0		n
un [3]	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	4140.000	5689.000		
Ø-30 .			1 200 000			3.100	44.63 C	0.0	3.0	+1+0.000	6.00.1.00		
51	X1	3.020	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0		34 .
52	BT	9.000	5387.000	467.600	467.600	5439.000	469.600	466.000	5486.000	474.500	458.000		
	BT	5527.000	478.600	449.500		478.500	473.500	5689.000	479.000	473.500	5689.000		35
51	BT	479.000			5527.000						0.0		35
40	FT		449.500	5700.000	479.000	455.000	5761.000	476.100	476.100	0.0			- 73
446	EI	0.0	0.0	0.0	0.0	.100	0.0	0.0	0.0	4140.000	5689.000		110
COLUMN TO SERVICE STATE OF THE				•		21 222	21 225	21 222		/	0.0		
€ 54	V 1			0.0	0.0	21.000	21.000	21.000	0.0	0.0	0.0		STATE OF THE PARTY.
57	X1	3.100	0.0						0 0				
58 58	X1 X2 FT	3.100 0.0 0.0	0.0	0.0	0.0	0.0 9.100	0.0	1.000	0.0	0.0	0.0 5689.000		29

	XI	3.200	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0	63
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	464.500	476.100	0.0	03
	ET	0.0	3 0.0	0.0	0.0	9.100	0.0	0.0	0.0	3850.000	6100.000	
•	XI	4.010	39.000	5880.000	6100.000	400.000	10.000	30.000	0.0	0.0	0.0	•
	GR	480.000	1.000	466.000	1000.000	470.000	1530.000	471.000	3025.000	470.000	3525.000	
	GR	470.000	4330.000	474.000	4500.000	470.000	4590.000	465.000	4820.000	465.000	4920.000	
	GR	464.000	5000.000	460.000	5150.000	460.500	5160.000	460.000	5165.000	459.000	5180.000	'•
1	GR	460.000	5195.000	460.000	5300.000	457.000	5380.000	460.000	5700.000	466.100	5765.000	,
	GR	466.100	5785.000	465.000	5805.000	460.000	5880.000	448.300	5920.000	448.300	6075.000	
	GR	455.000	6082.000	475.000	6100.000	483.000	6200.000	485.000	6305.000	486.500	6330.000	•
	GR	490.000	6415.000	495.000	6460.000	500.000	6520.000	501.000	6580.000	500.000	6638.000	
	GR	504.900	6650.000	505.000	6690.000	510.000	6800.000	515.000	6875.000	0.0	0.0	
•	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3850.000	6100.000	' •
10	X1	4.020	0.0	0.0	0.0	15.000	15.000	15.000	0.0	0.0	0.0	•
• 11.	х3	10.000	0.0	480.000	0.0	490.000	0.0	0.0	470.000	475.000	0.0	' •
12_	FT	0.0	0.0	0.0	0.0	99,100	0.0	0.0	0.0	3850.000	6100.000	
13	SB	1.250	1.500	3.000	0.0	133.000	16.000	4100.000	1.900	451.000	451.000	
	X1	4.100	0.0	0.0	0.0	17,000	17.000	17 000	0.0	0.0		
16	XS	0.0	0.0	1.000	476.000	474.100	0.0	17.000	0.0	0.0	0.0	110
A 17	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	n
18	RT	29.000	1.000	480.000	0.0	1000.000	475.500	0.0	474.200 1785.000	475.000 474.700	0.0	
19	BT	1960.000	474-100	0.0	2141.000	474.600	0.0	2473.000	474.200	0.0	0.0 4029.000	
20	BT	475.300	0.0	4554.000	478.100	0.0	4758.000	478.500	0.0	4813.000	479.300	n.
21	BT	0.0	4887.000	479.800	0.0	4941.000	480.200	0.0	5018.000	480.500	0.0	
12	RT	5053.000	480.700	0.0	5140.000	480.900	0.0	5243.000	481.000	0.0	5333.000	
10 11	RT	481.200	0.0	5415.000	481.500	0.0	5525.000	482.100	0.0	5551.000	482.600	150
71	BT	0.0	.5581.000	482.500	0.0	5676.000	482.900	0.0	5878.000	482.900	0.0	
25	BT	5885.000	483.000	0.0	6028.000	483.000	0.0	6064.000	483.300	0.0	6099.000	
26	RT	483.900	0.0	6118.000	484.100	0.0	6134.000	485.200	0.0	0.0	0.0	"•
27	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3850.000	6100.000	in T
78				454.000		488 (66)						
2 77	X1	4.200	0.0	0.0	0.0	66.000	66.000	66.000	410.0	0.0	0.0	100
39	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	471.000	475.000	0.0	
	ET	6/0.0 m	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3540.000	5918.000	in .
		F 010	70 000	5400 000	5010 000							
	X1	5.010	70.000	5603.000	5918.000	5,000	5.000	5.000	0.0	0.0	0.0	and the second s
	BT	12.000	5603.000	482.200	482.200	5603.000	482.200	479.400	5625.000	482.300	479.500	23
	RT	5625.000	482.300	482.300	5718.000	483.200	483.200	5718.000	483.200	478.200	5815.000	
77	BT	483.800	478.800	5815.000	483.800	483.800	5821.000	483.800	483.800	5821.000	483.800	
	6R	478.800	5918.000	484.300	479.300	5918.000	484.300	484.300	0.0	0.0	0.0	25
. 39	GR	472.900	1.000	471.000 474.000	1000.000	471.000 475.100	3536.000	471.100	3683.000	471.200	3987.000	
40	GR	476.500	5055.000	477.000	5095.000		4779.000	475.700	4979.000	476.400	5054.000	
4 1	GR	479.900	5358.000	480.300	5401.000	477.500 481.400	5157.000	478.600	5240.000	479.300	5295.000	<i>n</i>
- 0	GR	482.200	5603.000	467.000	5603.000	467.000	5467.000 5603.000	481.900 467.000	5511.000 5625.000	482.000	5572.000	
43	GR	482.300	5625.000	483.200	5718.000	456.100	5718.000	456.100	5718.000	467.000 453.100	5625.000 5750.000	The state of the s
9 11	GR	448.400	5783.000	443.400	5815.000	443.400	5815.000	483.800	5815.000	483.800	5821.000	29
45	GR	442.800	5821.000	442.800	5821.000	448.600	5853.000	450.200	5886.000	466.100	5918.000	
46	GR	466.100	5918.000	484.300	5918.000	483.400	6009.000	479.200	6028.000	481.200	6068.000	
90	GR	481.600	6093.000	485.500	6119.000	487.200	6148.000	490.100	6180.000	494.700	6209.000	11
44	GR	496.600	6241.000	496.600	6260.000	501.500	6287.000	501.500	6341.000	502.300	6388.000	11
49	GR	500.300	6406.000	498.600	6423.000	498.600	6441.000	505.000	6460.000	506.300	6473.000	
90	GR	506.300	6495.000	507.100	6525.000	509.500	6587.000	511.200	6633.000	514.400	6652.000	n a
51,100	GR	515.400	6668.000	516.300	6719.000	521.300	6794.000	525.200	6844.000	531.000	6889.000	u
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	3540.000	5918.000	25 _ 2
6 13	v 1	S 100		0.0	(30),000	10.000	10.000	10.000				•
45	X1	5.100	0.0	0.0	0.0	18.000	18.000	18.000	0.0	0.0	0.0	
	X2	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0	37
SI	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2980.000	5821.000	, ,
A	X1	6.010	94.000	5593.000	5821.000	5.000	5.000	5.000	0.0	0.0	0.0	
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	467.200	475.000	0.0	37
	GR	480.000	1.000	471.500	1000.000	471.400	1152.000	471.800	1242.000	471.800	1327.000	

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CONTRACTOR DE	Section 1		SARTIPONIA O CONTRACTO CONTRACTO									
•	GR GR	470.400	1483.000	469.000	1604.000	467.500	1724.000	467.900	1842.000	469.300	1944.000	64
	GR	469.600	2079.000	468.600	2256.000	469,200	2444.000	469.300	2587.000	468.500	2684.000	94 0
		467.500	2745.000	466.500	2758.000	465.800	2764.000	460.600	2808.000	465.800	2834.000	
	GR	467.700	2843.000	472.000	2866.000	471.400	2923.000	470.700	3042.000	464.100	3074.000	
	GR	464.200	3084.000	467.300	3101.000	468.300	3141.000	469.700	3191.000	468.800	3265.000	
	GR	467.400	3316.000	466.200	3336.000	466.200	3392.000	466.200	3465.000	469.000	3516.000	
	GR	469.500	3594.000	468.700	3675.000	468.800	3845.000	469.100	3977.000	469.000	4107.000	
● 2	GR	468.300	4221.000	468.000	4370.000	467.900	4483.000	467.800	4567.000	467.600	4625.000	
	GR	466.300	4674.000	465.900	4721.000	465.200	4756.000	462.200	4772.000	464.800	4787.000	eren i de la companya
	GR	465.700	4800.000	466.400	4832,000	466.600	4880.000	467.000	4939.000	467.400	5013.000	
•	GR	467.400	5090.000	467.100	5179.000	467.500	5250.000	467.700	5292.000	468.000	5378.000	
	GR	468.100	5443.000	468.400	5486.000	467.900	5496.000	467.900	5519.000	468.300	5537.000	
7.	GR	467.100	5574.000	465.800	5593.000	459.400	5602.000	455.800	5608.000	454.800		*
•	GR	451.500	5632.000	451.500	5685.000	451.500	5685.000	454.800	5751.000	455.100	5614.000	
	GR	455.100	5770.000	454.800	5778.000	452.600					5758.000	
	GR						5791.000	454.800	5804.000	456.100	5811.000	· .
	GR	472.700	5821.000	478.800	5835.000	478.800	5851.000	478.200	5863.000	479.500	5870.000	1
		482.500	5905.000	488.300	5953.000	492.800	5993.000	495.200	6023.000	497.100	6057.000	
11	GR	499.300	6071.000	499.300	6083.000	496.800	6088.000	502.000	6108.000	0.0	/ O.O	,
· _ "	NC	0.050	0.070	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
● H	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2980.000	5821.000	' •
CVC	D		2000,000									10
S XS		6.000	0.0	0.0	0.0	110.000	290.000	205.000	0.0	0.0	0.0	
● 17	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2840.000	5394.000	"•
18		5.67.000	3859 695	287.398	1010.019	467,666			1027,000	4631.595	4199.36%	. 12
CYC	EX1	7.000	95.000	5136.000	5394.000	80.000	780.000	680.000	0.0	0.0	0.0	
مرم	GR	480.000	1.000	471.500	1000.000	471.000	1211.000	471.400	1323.000	470.400	1455.000	130
21	GR	469.900	1556.000	469.300	1640.000	469.200	1654.000	467.200	1672.000	466.700	1728.000	lu lu
n	GR	466.300	1861.000	469.100	1977.000	469.800	2101.000	468.700	2200.000	468.900	2308.000	
23	GR	469.100	2429.000	467.600	2538.000	468.200	2660.000	466.900	2720.000	466.200	2745.000	15
и.	GR	465.800	2763.000	467.500	2785.000	472.300	2816.000					
25	GR	470.300	2978.000	469.500	3024.000	463,300		472.100	2856.000	470.600	2929.000	,
20	GR	467.700	3145.000				3045.000	465.300	3058.000	467.000	3093.000	v _o
17	GR			468.100	3195.000	468.800	3274.000	467.200	3304.000	466.200	3315.000	
40		459.100	3393.000	466.200	3511.000	467.200	3527.000	467.200	3570.000	467.300	3597.000	18
20	GR	466.600	3605.000	464.000	3637.000	466.600	3661.000	467.200	3666.000	467.800	3730.000	19
17	GR	468.000	3836.000	468.500	3936.000	469.400	4021.000	469.900	4108.000	467.800	4225.000	
30	GR	467.900	4330.000	468.200	4409.000	468.100	4486.000	468.000	4597.000	466.900	4663.000	16
31	GR	465.100	4706.000	460.500	4725.000	465.300	4740.000	466.500	4793.000	467.700	4825.000	
21	GR	467.100	4861.000	465.400	4886.000	465.300	4924.000	467.800	4945.000	467.500	5026.000	1.0
33	GR	468.300	5074.000	468.700	5112.000	468.800	5136.000	460.600	5151.000	456.300	5157.000	. 11
34	GR	454.900	5166.000	454.300	5170.000	454.300	5246.000	454.300	5314.000	454.900	5319.000	
9 11	GR	455.700	5325.000	457.100	5343.000	460.500	5360.000	468.400	5394.000	467.500	5439.000	" •
36	GR	465.900	5457.000	464.500	5475.000	465.300	5495.000	465.800	5531.000	470.200	5554.000	и
#	GR	473.700	5592.000	481.600	5613.000	482.900	5636.000	483.300	5686.000	484.800	5703.000	
€ 28	GR	487.600	5724.000	492.600	5756-000	497.400						" 。
37	ET	0.0					5777.000	503.600	5802.000	503.600	5823.000	
46		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2480.000	5042.000	
CNC	-v1	0 000	((000	(717 000	5040 000	270 005	740 000	705 000	4 加思等。在设计			n.
S XS	Ex 1	8.000	66.000	4717.000	5042.000	270.000	740.000	725.000	0.0	0.0	0.0	
	GR	480.000	1.000	471.500	1000.000	471.400	1220.000	471.000	1339.000	470.300	1423.000	78
- 43	GR	469.600	1566.000	469.200	1623.000	468.400	1667.000	468.400	1772.000	467.800	1925.000	29 1
9 4	GR	467.700	2068.000	468.300	2533.000	467.600	2370.000	468.000	2480.000	470.100	2552.000	
45	GR	470.700	2651.000	471.000	2719.000	471.200	2819.000	464.500	2871.000	465.100	2884.000	26
41.	GR	465.500	2949.000	465.800	3019.000	465.900	3127.000	465.900	3252.000	465.200	3372.000	
00	GR	464.800	3449.000	465.300	3500.000	466.200	3603.000	466.900	3715.000	466.800	3873.000	
46	GR	466.300	4018.000	466.200	4129.000	466.300	4205.000	466.400	4240.000	466.500	4285.000	
4	GR	466.500	4335.000	468.000	4381.000	468,500	4435.000	469.500	4498.000	470.500	4571.000	
	GP	470.700	4653.000	470.500	4678.000	470.300						
51	GR	457.700	4719.000	456.900			4691.000	464.500	4708.000	464.500	4717.000	7
14	and the second second second				4729.000	456.000	4740.000	456.000	4850.000	456.000	4979.000	
	GR	456.900	4983.000	459.000	4992.000	464.300	5009.000	.467.600	5042.000	467.800	5103.000	X .
	GR /	466.100	5160.000	464.900	5201.000	461.400	5233.000	460.300	5246.000	458.700	5264.000	
24 J=	GR	460.300	5265,000	470.300	5270.000	475.900	5282.000	483.000	5299.000	484.400	5309.000	24
25	GR	484.700	5331.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11
2 50	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2465.000	5042.000	" •
57					24 58 25 16	443 8.78		365,718				38
VC C	- X1	9.000	66.000	4680.000	4999.000	20.000	30.000	30.000	0.0	0.0	0.0	
(GR GR	480.000	1.000	471.500	1000.000	471.300	1222.000	471.000	1339.000	470.400	1422.000	
	GR	469.600	1570.000	469.200	1622.000	468.500	1668.000	468.300	1772.000	467.700	1924.000	

								THE RESERVE OF THE PARTY OF THE		THE REAL PROPERTY OF THE PARTY			
	GR	467.600	2052.000	468.000	2216.000	467.500	2376.000	468.100	2486.000	470.100	2552.000	65	
	GR	470.900	2649.000	471.300	2715.000	471.200	2815.000	464.700	2855.000	465.400	2888.000	00	
	GR	465.700	2955.000	466.000	3018.000	466.100	3123.000	465.800	3250.000	465.100	3374.000		
	GR	464.800	3450.000	465.400	3508.000	466.200	3605.000	466.700	3719.000	467.000	3875.000		
	GR	466.300	4028.000	466.100	4128.000	466.200	4206.000	466.400	4244.000	466.500	4287.000		
	GR	466.600	4326.000	468.400	4387.000	468.800	4449.000	469.900	4507.000	471.000	4567.000		
	GR	470.700	4612.000	470.700	4647.000	470.500	4656.000	470.500	4680.000	468.800	4685.000		1.4
	GR	461.700	4700.000	461.800	4700.000	460.700	4704.000	460.000	4707.000	456.000	4718.000		0 7
- L	GR	456.000	4940.000	460.700	4957.000	461.400	4974.000	466.000	4999.000	467.200	5021.000		2 4
	GR	467.500	5067.000	466.900	5143.000	466.200	5187.000	466.200	5223.000	464.100	5229.000		
	GR	465.500	5242.000	470.400	5266.000	474.600	5276.000	479.700	5286.000	485.400	5301.000		
	GR	485.100	5323.000	0.0	0.0	0.0	0.0	0.0	0.0	/0.0	0.0		4
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1830.000	4761.000		150
Ц	×1	10.000	73.000	4497.000	4761.000	845.000	795.000	860.000	0.0	0.0	0.0		
10	GP	480.000	1.000	471.500	1000.000	471.200	1135.000	471.100	1222.000	470.600	1316.000		
• n	GR	469.600	1448.000	469.200	1562.000	467.900	1661.000	466.700	1792.000	466.000	1867.000		•
- 17	GR	465.200	2008.000	465.000	2171.000	464.600	2182.000	464.600	2251.000	464.800	2269.000	•	
D D	GR	464.800	2310.000	463.600	2328.000	464.500	2346.000	464.400	2387.000	464.400	2446.000		
● 14	GR	464.400	2497.000	464.700	2522.000	465.400	2566.000	467.100	2607.000	467.400	2655.000		
15	GR	468.300	2740.000	470.400	2828.000	471.000	2876.000	470.200	2948.000	468.900	3054.000		10
12	GR	467.700	3131.000	466.500	3207.000	467.000	3258.000	467.200	3340.000	467.500	3460.000		
● 17	GR	467.700	3573.000	468.000	3548.000	467.500	3710.000	467.40C	3776.000	467.200	3826.000		
18	GR -	467.200	3858.000	467.200	3910.000	467.600	3980.000	467.800	4050.000	468.000	4120.000		13
19	GR	468.000	4189.000	468.800	4272.000	468.400	4371.000	468.400	4429.000	467.800	4470.000		
70	GR	467.500	4497.000	465.800	4501.000	461.400	4511.000	460.900	4519.000	456.700	4583.000		
71	GR	456.700	4609.000	456.700	4670.000	460.900	4694.000	462.800	4705.000	464.900	4726.000		14
17	GR	469.700	4761.000	469.900	4789.000	468,600	4869.000	468,400	4964.000	468.200	5031.000		
(1 11 ·	GR	468.100	5072.000	465.600	5087.000	469.400	5099.000	475.600	5108.000	485.100	5131.000		•
и	GR	494.500	5152.000	494.600	5172.000	494.500	5193.000	0.0	0.0	0.0	0.0		
25	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1720.000	4911.000		
VCI					1000	174,930							• .
X2 I	X1	11.000	77.000	4716.000	4911.000	300.000	600.000	675.000	0.0	0.0	0.0		115 12
78	GR	485.000	1.000	471.100	1052.000	471.300	1132.000	471.000	1223.000	470.200	1312.000		10
25	GR	469.100	1392.000	468.800	1458.000	467.900	1468.000	465.500	1477.000	462.200	1489.000		• 6
N	GR	465.500	1522.000	466.400	1531.000	466.800	1558.000	466.800	1594.000	465.900	1662.000		10
	GR	465.800	1737.000	465.300	1870.000	465.300	1954.000	464.900	2032.000	464.500	2050.000	. 14	21
, CP	GR	464.500	2138.000	464.800	2196.000	464.900	2218.000	464.100	2230.000	464.600	2237.000		•
11	GR	464.600	2279.000	464.600	2367.000	465.100	2381.000	468.100	2418.000	469.900	2459.000		22
	GR	469.800	2519.000	470.700	2612.000	470.600	2676.000	470.700	2761.000	471.600	2891.000		23
25	GR	471.700	2917.000	470.500	2961.000	470.200	3014.000	470.200	3111.000	469.300	3199.000		
36	GR	467.900	3351.000	467.900	3435.000	467.000	3461.000	468.500	3491.000	468.400	3549.000		74
77	GR	468.500	3660.000	469.200	3804.000	469.400	3923.000	469.800	4009.000	469.200	4091.000		25
(F) 13	GR	468.500	4231.000	467.900	4311.000	467.100	4412.000	466.000	4418.000	468.200	4430.000		•
39	GR	469.000	4508.000	468.800	4582.000	468.800	4636.000	467.700	4688.000	465.600	4716.000		76
40	GR	461.900	4722.000	460.200	4728.000	459.400	4731.000	459.400	4809.000	459.400	4887.000		и
(4)	GR	460.200	4889.000	462.300	4896.000	467.600	4911.000	464.800	4931.000	473.500	4943.000		•
49	GR	475.800	4971.000	477.500	5027.000	478.500	5104.000	480.900	5166.000	485.600	5232.000		28
- 1	GR	487.600	5268.000	489.300	5303.000	0.0	0.0	0.0	0.0	0.0	0.0		21
44	NC	0.0	0.0	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0		
45	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1720.000	4911.000		39
⊕ 10	X 1	11.100	0.0	0.0	0.0	195.000	15.000	75.000	0.0	0.0	0.0		31
48	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	469.600	484.000	0.0		12 - 1
49	ET	0.0	0.0	0.0	0.0	9.100		0.0	0.0	1670.000	5092.000		1
⊕ 50			0.0	0.0	0.0	9.100	0.0	0.0	0.0	10.0.000	3092.000		n o
51	X1	12.010	80.000	4900.000	5092.000	5.000	5.000	5.000	0.0	0.0	0.0		31
12	х3	10.000	0.0	0.0	0.0	0.0	0.0	.0.0	469.600	484.000	0.0	/	
● 52	BT	6.000	4900.000	480.000	473.900	4992.000	482.100	475.400	4992.000	482.100	461.700	(
54	BT	4998.000	482.100	461.700	4998.000	482.100	475.400	5092.000	484.200	476.900	0.0		34 9
55	GR	485.000	1.000	471.400	1177,000	470.500	1269.000	469.300	1364.000	466.700	1417.000		
9 55	GR	468.200	1438.000	468.000	1469.000	465.500	1481.000	465.500	1541.000	466.200	1553.000		
H	GR	465.800	1605.000	465.600	1656.000	465.600	1734.000	466.100	1763.000	466.100	1842.000		38
50	GR	466.000	1935.000	465.000	1990.000	464.500	2003.000	464.500	2083.000	464.800	2110.000		\
	GR	464.900	2141.000	464.600	2161.000	464.600	2200.000	464.600	2279.000	465.000	2313.000		(0)
	GR	467.200	2262.000	468.900	2422.000	470.500	2474.000	470.500	2544.000	470.500	2681.000		

							new new						Addison to the same
	GR	470.700	2827.000	471.000	2942.000	471.000	3022.000	470.800	3079.000	470.300	3153.000	66	
	GR	470.500	3182.000	470.800	3200.000	470.100	3213.000	469.000	3292.000	469.200	3385.000	00	
	GR	469.700	3473.000	469.900	3553.000	470.700	3631.000	474.000	3648.000	474.000	3692.000		
•	GR	471.700	3715.000	472.100	3736.000	475.100	3766.000	476.700	3827.000	478.000	3866.000		
	GR	477.200	3907.000	475.000	3986.000	473.300	4061.000	473.300	4154.000	472.900	4238.000		
	GR	472.200	4317.000	471.800	4404.000	471.800	4470.000	471.600	4516.000	472.100	4530.000		
	GR	472.100	4547.000	480.000	4900.000	460.000	4900.000	452.900	4940.000	454.900	4992.000		
	GR	461.700	4992.000	461.700	4998.000	461.700	4998.000	456.900	5040.000	463.300	5092.000		
	GR	484.200	5092.000	485.400	5425.000	485.500	5448.000	485.700	5507.000	488.400	5577.000		1 5
	GR	490.900	5629.000	497.700	5654.000	502.400	5677.000	507.400	5709.000	507.400	5731.000		
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1670.000	5092.000		•
								488 888		472-99	27/1/2/10/2		4
	XI	12.100	0.0	0.0	0.0	110.000	110.000	110.000	0.0	0.0	0.0		1500
	X2	10.000	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0		
	FŤ	0.0	0.0	0.0	0.0	0.0	0.0	0.0	469.000	0.0	0.0		^ *
•		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1650.000	5148.000		"
17	×1	13.100	95.000	.4937.000	5148.000	5.000	5.000	5.000	0.0	0.0	0.0		
14	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	469.000	0.0	0.0		
• H	GR	485.000	1.000	471.300	1084.000	470.800	1185.000	470.200	1277.000	468.900	1359.000		'-
	GR	467.300	1402.000	465.700	1423.000	466.800	1448.000	467.000	1469.000	465.500			
14	GR	464.300	1505.000	465.500	1537.000	466.000	1551.000	466.200	1576.000	465.900	1489.000 1618.000		
9 17	GR	465.700	1690.000	465.700	1758.000	466.000	1841.000	465.800	1869.000	466.000	1909.000		11_
19.	GR	465.700	1948.000	464.700	1974.000	464.600	2028.000						
10 E	GR	464.500	2069.000	464.400				464.800	2037.000	464.300	2055.000		
	GR	469.000	2288.000	469.900	2131.000	464.900 470.700	2151.000	465.000 470.700	2215.000 2419.000	465.100	2247.000 2470.000		112
	GR	470.000	2626.000	470.000									
	GR			and the property of the property of the party of the part	2748.000 3071.000	470.300	2858.000	470.800	2934.000	471.000	3003.000		
	GR	471.100	3038.000	470.700 469.600		470.700	3137.000	470.800	3176.000	470.700	3216.000		15
	GR	470.300	3263.000		3326.000	469.300	3347.000	469.800	3382.000	470.100	3488.000		
		471.500	3551.000	474.200	3563.000	474.200	3586.000	473.700	3590.000	474.800	3606.000		10
	GR	473.000	3620.000	474.600	3645.000	486.600	3683.000	486.600	3710.000	485.000	3726.000		17
	GR	480.700	3756.000	476.900	3798.000	474.900	3826.000	472.800	3885.000	472.700	3965.000		9 6
"12	GR	472.900	4063.000	474.000	4125.000	475.400	4146.000	476.000	4163.000	474.800	4186.000		7
20	GR	473.400	4237.000	472.800	4301.000	472.800	4345.000	473.600	4370.000	473.200	4417.000		19 EAS
	GR	472.800	4472.000	472.000	4503.000	471.800	4554.000	470.200	4640.000	469.700	4768.000		9 6
	GR	470.100	4852.000	469.500	4902.000	468.300	4937.000	465.400	4952.000	460.500	4961.000		10
- "	GR	460.000	4962.000	460.000	5046.000	460.000	5128.000	460.500	5129.000	463.100	5133.000		21
	GR	474.600	5148.000	495.300	5182.000	499.200	5208.000	500.600	5378.000	512,500	5551.000		
11	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1630.000	5148.000		12
		12 200		0.0		100 000	105 000	115 000	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	17 12			21
IS XS	J_{x3}^{x1}	13.200	0.0	0.0	0.0	100.000	195.000	115.000	0.0	0.0	0.0		
		10.000	0.0	0.0	0.0	0.0	0.0	0.0	469.000	0.0	0.0		
	NIC.	0.050	0.080	0.037	0.100	0.300	0.0	0.0	0.0	0.0	0.0		18
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1620.000	4976.000		
10	, X1	14.000	OF 000	4717 000	4047 000	30 000	720 000	(35 000	0 0	0.0			
SXSE	⟨ x̂ 3	10.000	95.000	4717.000	4967.000	20.000	720.000	635.000	0.0	0.0	0 0		7
	GR	485.000	0.0		0.0	0.0	0.0	0.0	469.000	0.0	0.0		, -
0	GR	465.500	1.000	471.200	1094.000	470.800	1227.000	469.300	1325.000	466.900	1405.000		
(B-14)	GR		1423.000	466.600	1445.000	466.900	1466.000	465.700	1482.000	465.500	1512.000		29
45	GR	466.100	1558.000	466.100	1617.000	466.200	1678.000	466.000	1741.000	466.200	1796.000		10
46	GR	465.400	1876.000	465.200	1935.000	464.900	1960.000	464.700	1996.000	464.100	2010.000		
94	GR	464.300	2026.000	464.300	2087.000	464.600	2149.000	464.800	2197.000	465.700	2221.000		11.
	GR	468.300	2269.000	470.400	2315.000	470.500	2387.000	470.200	2428.000	469.900	2522.000		1
n -		469.800	2629.000	469.900	2748.000	470.100	2826.000	470.600	2919.000	470.700	2993.000		
	'GR	470.700	3028.000	471.000	3108.000	470.600	3174.000	470.300	3274.000	469.500	3385.000		33
-	GR	471.500	3450.000	472.000	3530.000	474.600	3545.000	474.600	3570.000	473.800	3577.000		124
12	GR	474.600	3585.000	473.100	3599.000	474.500	3612.000	476.400	3633.000	487.600	3658.000		
	GR	485.800	3709.000	479.200	3737.000	474.400	3800.000	472.200	3865.000	471.100	3939.000		35 8
	GR	471.000	4019.000	472.600	4103.000	474.100	4139.000	475.800	4169.000	473.400	4199.000		
4 [GR	473.100	4238.000	474.400	4284.000	474.700	4317.000	474.400	4370.000	474.200	4424.000		
	GR	472.900	4496.000	471.800	4541.000	468.800	4642.000	466.700	4691.000	465.500	4717.000		11_
€ 26	GR	464.900	4722.000	460.700	4730.000	456.000	4739.000	456.000	4824.000	456.000	4893.000		9
» L	GR	450.800	4913.000	463.400	4923.000	465.700	4967.000	466.500	5035.000	475.200	5062.000		4
35	GR	490.400	5097.000	488.200	5113.000	491.200	5140.000	489.200	5154.000	488.000	5172.000		39
	GR	500.800	5194.000	508.900	5234.000	510.000	5273.000	511.500	5284.000	511.500	5310.000		9
	GR	512.500	5364.000	512,900	5492,000	512,900	5562,000	509.700	5599.000	513.300	5668.000		

	NC	0.060	0.090	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		AND THE RESERVE
•	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1545.000	4621.000	67	
	VI	16 010		477,376			37.00,000						
6	X1	16.010	90.000	4430.000	4621.000	44.000	714.000	684.000	0.0	0.0	0.0		
	GR	485.000	1.000	471.300	1070.000	0.0 470.900	1175.000	0.0	474.000	480.700	0.0		. 01
	GR	466.200	1396.000	468.700	1411.000	466.600	1427.000	469.100 465.300	1287.000	466.200	1367.000		
6 2	GR	467.100	1475.000	467.400	1506.000	466.900	1533.000	466.900	1438.000	467.000 466.200	1454.000		1 aver
3	GR	465.700	1801.000	465.900	1870.000	466.100	1901.000	465.400	1921.000	464.700	1939.000		
1	GR	464.700	1974.000	466.400	1995.000	469.300	2034.000	469.900	2110.000	469.700	2150.000		
•	GR	468.700	2196.000	469.500	2223.000	470.200	2257.000	470.500	2323.000	470.200	2360.000		30
	GR	470.100	2440.000	469.600	2538.000	469.600	2634.000	469.800	2765.000	470.000	2842.000		
	GR	470.900	2914.000	471.400	2955.000	471.700	3098.000	472.400	3244.000	471.500	3306.000		
	GR GR	471.000	3370.000	471.500	3425.000	471.000	3454.000	471,500	3473.000	472.600	3492.000		
16	GR	475.300 476.100	3521.000 4143.000	475.300	3547.000	475.300	3700.000	475.200	4053.000	476.100	4073.000		
6 H	GR	471.000	4344.000	479.600 469.300	4198.000	485.200 465.000	4243.000	485.500	4261.000	475.200	4299.000		
12	GR	458.000	4538.000	458.000	4621.000	461.200	4425.000 4636.000	461.200	4428.000	458.000	4430.000		
G G	GR	466.000	4741.000	466.500	4800.000	471.800	4883.000	463.200 473.300	4643.000	465.400 475.500	4661.000		777
1 4	GR	477.200	5119.000	477.200	5138.000	480.500	5197.000	482.700	5262.000	482.200	5038.000 5286.000		
15	GR	479.700	5308.000	482.100	5350.000	484.800	5472.000	489.600	5509.000	501.000	5543.000		19
76	GR	506.400	5565.000	506.600	5667.000	505.400	5694.000	505.700	5707.000	510.700	5730.000		
•	GR	512.000	5784.000	512.600	5847.000	514.000	5887.000	515.500	5954.000	517.700	6033.000		•
18	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1645.000	4721.000		12
6 2	×1	16.020	92.000	4530.000	4721.000	10 000	10 000		24,014	442.50			13
n	Х3	10.000	0.0	0.0	0.0	10.000	10.000	10.000	0.0 474.000	0.0	0.0		
73	BT	12.000	4115.000	494.600	494.600	4115.000	494.600	0.0 491.500	The state of the s	0.0	0.0		"
. 12	BT	4210.000	493.100	493.100	4530.000	488.500	488.500	4530.000	4210.000 488.500	493.100 484.600	490.000		•
h.	BT	487.100	483.300	4624.000	487.100	487.100	4627.000	487.000	487.000	4627.000	487.000		
251	BT	483.200	4721.000	485.706	481.800	4721.000	485.700	485.700	0.0	0.0	0.0		
● 76	GR	485.000	1.000	471.300	1070.000	470.900	1175.000	469.100	1287.000	466.200	1367.000		17.
27	GR	466.200	1396.000	468.700	1411.000	466.600	1427.000	465.300	1438.000	467.000	1454.000		18 10
	GR	467.100	1475.000	467.400	1506.000	466.900	1533.000	466.900	1589.000	466.200	1664.000		REA
•	GR GR	465.700	1801.000	465.900	1870.000	466.100	1901.000	465.400	1921.000	464.700	1939.000		. 6
316	GR	464.700	1974.000	466.400	1995.000	469.300	2034.000	469.900	2110.000	469.700	2150.000		20
2 11	GR	470.100	2440.000	469.500	2223.000 2538.000	470.200 469.600	2257.000	470.500	2323.000	470.200	2360.000		n
13	GR	470.900	2914.000	471.400	2955.000	471.700	2634.000 3098.000	469.800 472.400	2765.000 3244.000	470.000 471.500	2842.000 3306.000		
34	GR	471.000	3370.000	471.500	3425.000	471.000	3454.000	471.500	3473.000	472.600	3492.000		
35	GR	475.800	3521.000	475.300	3547.000	472.300	3578.000	472.300	3653.000	477.100	3669.000		13 •
34	GR	481.000	3691.000	493.700	3769.000	494.900	3795.000	495.400	3872.000	496.100	3993.000		74
Я	GR	495.200	4096.000	494.600	4115.000	475.400	4115.000	475.400	4210.000	493.100	4210.000		
	GR	488.500	4530.000	458.000	4530.000	458.000	4624.000	487.100	4624.000	487.000	4627.000		6.9
"10	GR GR	458.000	4627.000	458.000	4721.000	485.700	4721.000	484.600	4849.000	484.300	5134.000		28
Q 41	GR	484.100	5192.000 5463.000	480.900 501.300	5241.000	481.200	5272.000	482.900	5353.000	484.700	5440.000		77
41	GR	504.000	5639.000	510.400	5520.000 5658.000	504.100 513.800	5560.000 5793.000	505.700	5599.000	504.000	5619.000		
41	GR	516.000	5965.000	516.000	5982.000	516.500	6021.000	514.000 517.500	5879.000 6114.000	515.200 518.600	5940.000		
9 11	GR	520.500	6232.000	525.100	6325.000	0.0	0.0	0.0	0.0	0.0	6156.000		27 🛖
- 6	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1645.000	4721.000		
46													
9	X1	16.030	0.0	0.0	0.0	76.000	76.000	76.000	0.0	0.0	0.0		•
	X2	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0		2 7
	X3 FT	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.000	0.0	0.0		n_
51		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1545.000	4621.000		
Si .	X1 -	16.040	0.000	4430.000	4621.000	10.000	10.000	10.000	0.0	0.0	0 0		
(6)	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0 474.200	0.0 480.900	0.0		35
- 54	GR	485.000	1.000	471.300	1070.000	470.900	1175.000	469.100	1287.000	466.200	1367.000		16
55	GR	466.200	1396.000	468.700	1411.000	466.600	1427.000	465.300	1438.000	467.000	1454.000		
	GR	467.100	1475.000	467.400	1506.000	466.900	1533.000	466.900	1589.000	466.200	1664.000		
91	GR	465.700	1801.000	465.900	1870.000	466.100	1901.000	465.400	1921.000	464.700	1939.000		28
7 m	GR	464.700	1974.000	466.400	1995.000	469.300	2034.000	469.900	2110.000	469.700	2150.000		
	GR	468.700	2196.000	469.500	2223.000	470.200	2257.000	470.500	2323.000	470.200	2360.000		9
	GR	470.100	2440.000	469.600	2538.000	469.600	2634.000	469.800	2765.000	470.000	2842,000		

	GR	470.900	2914.000	471.400	2955.000	471.700	3098.000	472.400	3264.000	471.500	3306.000	68	
	GR	471.000	3370.000	471.500	3425.000	471.000	3454.000	471,500	3473.000	472.600	3492.000	00	
	GR	475.300	3521.000	475.300	3547.000	475.300	3700.000	475.200	4053.000	476.100	4073.000		
	GR	476.100	4143.000	479.600	4198.000	485.200	4243.000	485.500	4261.000	475.200	4299.000		
	GR.	471.000	4344.000	469.300	4392.000	465.000	4425.000	461.200	4428.000	458.000	4430.000		
	GR	458.000	4538.000	458.000	4621.000	461.200	4636.000	463.200	4643.000	465.400	4661.000		
- 1	GR	466.000	4741.000	466.500	4800.000	471.800	4883.000	473.300	4957.000	475.500	5038.000		
	GR	477.200	5119.000	477.200	5138.000	480.500	5197.000	482.700	5262.000	482.200	5286.000		
1	GR	479.700	5308.000	482.100	5350.000	484,800	5472.000	489.600	5509.000	501.000	5543.000		2
	GR	506.400	5565.000	506.600	5667.000	505.400	5694.000	505.700	5707.000	510.700	5730.000		
•	GR	512.000	5784.000	512.600	5847.000	514.000	5887.000	515.500	5954.000	517.700	6033.000		
4	NC	0.060	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		4
	ΕT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1595.000	4661.000		3
CVC		17 000	05 000						11.64.76.6				
SXS	XI	16.000	95.000	4392.000	4661.000	60.000	60.000	60.000	0.0	0.0	0.0		
	х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.200	0.0	0.0		7
	GR GR	485.000	1.000	471.300	1070.000	470.900	1175.000	469.100	1287.000	466.200	1367.000		
	GR	466.200	1396.000	468.700	1411.000	466.600	1427.000	465.300	1438.000	467.000	1454.000		
	GR	465.700	1475.000	467.400	1506.000	466.900	1533.000	466.900	1589.000	466.200	1664.000		'9
10	GR	464.700	1974.000	465.900 466.400	1870.000	466.100	1901.000	465.400	1921.000	464.700	1939.000		
"[GR	468.700	2196.000	469.500	1995.000	469.300	2034.000	469.900	2110.000	469.700	2150.000		
	GR	470.100	2440.000	469.600	2223.000 2538.000	469.600	2257.000 2634.000	470.500 469.800	2323.000 2765.000	470.200	2360.000		B.
1	GR	470.900	2914.000	471.400	2955.000	471.700	3098.000	472.400	3244.000	470.000 471.500	2842.000 3306.000		11
ı, F	GR	471.000	3370.000	471.500	3425.000	471.000	3454.000	471.500	3473.000	472.600	3492.000		
	GR	475.300	3521.000	475.300	3547.000	472.300	3578.000	472.300	3653.000	471.600	3743.000		120
	GR	470.500	3832.000	469.800	3914.000	469.700	3993.000	475.200	4053.000	476.100	4073.000		
77	GR	476.100	4143.000	479.600	4198.000	485.200	4243.000	485.500	4261.000	475.200	4299.000		
● 112	GR	471.000	4344.000	469.300	4392.000	465.000	4425.000	461.200	4436.000	459.000	4442.000		15
14	GR	459.000	4538.000	459.000	4628.000	461.200	4636.000	463.200	4642.000	465.400	4661.000		- 18
46	GR	466.000	4741.000	466.500	4800.000	471.800	4883.000	473.300	4957.000	475.500	5038.000		
@ /h	68	477.200	5119.000	477.200	5138.000	480.500	5197.000	482.700	5262.000	482.200	5286.000		"e .
2	GR	479.700	5308.000	482.100	5350.000	484.800	5472.000	489.600	5509.000	501.000	5543.000		н
18	GR	506.400	5565.000	506.600	5667.000	505,400	5694.000	505.700	5707.000	510.700	5730.000		
● 29	GR	512.000	5784.000	512.600	5847.000	514.000	5887.000	515.500	5954.000	517.700	6033.000		
30	FT	0.0	0.0	0.0	0.0	9.100	7 0.0	0.0	0.0	1490.000	4154.000		79
31		439,000							and the state of				
● 32	X1	18.010	67.000	3984.000	4154.000	758.000	678.000	738.000	0.0	0.0	0.0		•
11	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.600	472.200	0.0		27
24	GR	485.000	1.000	471.300	1039.000	470.700	1095.000	470.200	1179.000	469.900	1234.000		77.2
9 35	GR	468.300	1317.000	468.400	1424.000	467.100	1467.000	467.500	1517.000	470.800	1551.000		•
36	GR	473.300	1572.000	474.700	1629.000	473.700	1688.000	472.800	1758.000	469.900	1811.000		*
37	GR		1872.000	468.700	1949.000	468.500	5033.000	468.800	5165.000	468.700	2264.000		25
● 199	GR	468.800	2343.000	469.700	2393.000	470.600	2480.000	471.100	2582.000	471.200	2724.000		•
39	GR	471.500	2851.000	471.900	2953.000	472.000	3003.000	472.100	3043.000	472.100	3083.000		128
4	GR	472.100	3100.000	472.200	3111.000	471.000	3243.000	470.700	3362.000	470.400	3504.000		n_
441	GR	470.300	3632.000	471.100	3700.000	472.600	3780.000	474.700	3849.000	478.500	3894.000		•
-47	GR	478.500	3917.000	465.900	3984.000	465.900	3984.000	459.000	4001.000	459.000	4038.000		n
	GR	459.000	4038.000	459.000	4042.000	459.000	4042.000	459.000	4096.000	459.000	4096.000		29
€144	GR	459.000	4100.000	459.000	4100.000	459.000	4145.000	464.300	4154.000	464.300	4154.000		20
*	GR	473.500	4200.000	473.500	4221.000	473.100	4257.000	473.300	4299.000	474.500	4359.000		
	GR	479.700	4396.000	484.100	4432.000	486.700	4446.000	491.600	4485.000	499.600	4508.000		n.
	GR	512.900	4530.000	525.000	4556.000	0.0	0.0	0.0	0.0	0.0	0.0		75
.,	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000		
	V.	10 000		0 0	0.0	10 000	10 000	10 000					33
9150	X1	18.020	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0		26
27	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.600	0.0	0.0		
40	RT BT	18.000	3917.000	478.500	478.500	3984.000	478.800	465.900	3984.000	478.800	474.000		35
14		4001.000	478.900	474.000	4038.000	479.000	474.000	4038.000	479.000	459.000	4042.000		- 2
	RT	479.000	459.000	4042.000	479.000	475.500	4096.000	479.300	475.500	4096.000	479.300		
	RT	459.000	4100.000	479.300	459.000	4100.000	479.300	474.000	4145.000	479.500	474.000		37
17	BT	4154.000	479.500	474.000	4154.000	479.500	464.300	4200.000	475.000	473.500	4221.000		73
4	BT	474.300	473.500	4257.000	473.100	473.100	0.0	0.0	0.0	0.0	0.0		
	ET	0.0	. 0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000		"
	X1	18.030	0.0	0.0	0.0	27.000	27.000	27.000	0.0	0.0	0.0		

	XS	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0	
	X 3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.700	0.0	0.0	69
	NC	0.060	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000	
	×ı	18.040	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0	
1	XR	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.700	473.100	0.0	
● 2	NC	0.060	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
3	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000	, ,
c vc	M×1	18.000	67.000	3917.000	4154.000	55.000	55.000	55.000	0.0	0.0	. 0.0	' .
S XS	IVI X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.800	0.0	0.0	
1	GR	485.000	1.000	471.300	1039.000	470.700	1095.000	470.200	1179.000	469.900	1234.000	
•	GR	468.300	1317.000	468.400	1424.000	467.100	1467.000	467.500	1517.000	470.800	1551.000	
91	GR	473.300	1572.000	474.700	1629.000	473.700	1688.000	472.800	1758.000	469.900	1811.000	
10	GR	468.900	1872.000	468.700	1949.000	468.500	2033.000	468.800	2162.000	468.700	2264.000	,_
	GR GR	468.800	2343.000	469.700	2393.000	470.600	2480.000	471.100	2582.000	471.200	2724.000	· · · · · · · · · · · · · · · · · · ·
	GR	471.500 472.100	2851,000	471.900	2953.000	472.000	3003.000	472.100	3043.000	472.100	3083.000	, * 78
12	GR	470.300	3100.000	472.200 471.100	3111.000 3700.000	471.000 472.600	3243.000	470.700 474.700	3362.000	470.400 478.500	3504.000	9
15.	GR	478.500	3917.000	465.900	3984.000	465.900	3984.000	459.000	3849.000 4001.000	459.000	3894.000 4038.000	
18	GR	459.000	4038.000	459.000	4042.000	459.000	4042.000	459.000	4096.000	459.000	4096.000	
04	GR	459.000	4100.000	459.000	4100.000	459.000	4145.000	464.300	4154.000	464.300	4154.000	· · · · · · · · · · · · · · · · · · ·
14	GR	473.500	4200.000	473.500	4221.000	473.100	4257.000	473.300	4299.000	474.500	4359.000	11
19	GR	479.700	4396.000	484.100	4432.000	486.700	4446.000	491.600	4485.000	499.600	4508.000	
28	GR	512.900	4530.000	525.000	4556.000	0.0	0.0	0.0	0.0	0.0	0.0	"•
n	NC	0.070	0.080	0.035	0.500	0.700	0.0	0.0	0.0	0.0	0.0	11
22	ΕT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2650.000	4535.000	. 15
S XS	NXI	19.000	80.000	4140.000	4525.000	1750.000	1500.000	1283.000	0.0	0.0	0.0	N. T.
ک ۸	×3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	476.300	0.0	0.0	PERSONAL DESIGNATION OF THE PERSON OF THE PE
● 26	GR	483.800	1000.000	481.300	1049.000	479.300	1136.000	478.600	1211.000	477.800	1252.000	"• <u>_</u>
22	GR	476.600	1291.000	474.900	1327.000	474.400	1383.000	473.800	1544.000	474.600	1611.000	is N
26,	GR	474.700	1650.000	475.300	1723.000	478.600	1741.000	475.300	1790.000	474.200	1805.000	REW.
977	GR	474.200	1870.000	474.200	1991.000	474.400	2084.000	474.800	2248.000	474.800	2447.000	• 8
N .	GR	473.200	2622.000	471.600	2660.000	472.600	2758.000	473.400	2821.000	471.600	2850.000	15
	GR GR	471.900	2919.000	472.100	3003.000	472.000	3118.000	472.100	3224.000	472.200	3274.000	n = 0
57	GR	472.400 476.500	3349.000 3867.000	474.100	3566.000	474.600	3610.000	474.800	3689.000	475.700	3772.000	
32	GR	470.700	4174.000	478.000 465.600	3975.000 4187.000	479.000 462.500	4096.000	479.000 462.100	4140.000	474.900	4162.000 4252.000	
9 15	GR	462.100	4309.000	462.500	4310.000	465.000	4317.000	465.900	4327.000	462.100 465.500	4349.000	n •
36	GR.	462.500	4360.000	462.100	4361.000	462.100	4370.000	462.100	4370.000	462.500	4383.000	
22	GR	462.800	4392.000	462.500	4401.000	460.700	4447.000	460.700	4447.000	460.700	4476.000	
9 38	GR	462.500	4484.000	465.000	4495.000	473.700	4525.000	473.800	4588.000	474.700	4607.000	l* ●
379	GR	475.900	4641.000	476.900	4687.000	478.800	4735.000	478.800	4752.000	474.900	4762.000	
40	GR	475.400	4779.000	477.200	4804.000	477.700	4823.000	485.200	4866.000	491.200	4889.000	11 - 2
9 41	GR	491.200	4906.000	500.200	4916.000	510.000	4932.000	517.200	4949.000	526.200	4972.000	•
. 0	FT	0.0	0.0	0.0	0.0	9,100	0.0	0.0	0.0	2070.000	3291.000	18
94	X1	19.100	0.0	0.0	0.0	750.000	800.000	805.000	0.650	1.200	0.0	"
45	хз	10.000	0.0	0.0	0.0	6.0	0.0	0.0	477.000	0.0	0.0	b
6	FT	0.0	0.0	0.0	0.0	5.400	0.0	0.0	0.0	0.0	0.0	7
S XS	Ox1	20.000	58.000	2998.000	3282.000	750.000	800.000	805.000	0.0	0.0	0.0	•
2 72	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	478.300	0.0	0.0	
# 50	GR.	508.100	1000.000	507.300	1046.000	504.500	1093.000	501.300	1171.000	494.400	1248.000	л. — п. —
54	GR	490.700	1306.000	487.000	1348.000	486.600	1371.000	485.200	1383.000	483.700	1410.000	u
52	GR	479.700	1450.000	477.800	1570.000	477.400	1622.000	478.600	1663.000	480.500	1730.000	
•	GR	480.100	1784.000	479.500	1851.000	478.600	1910.000	478.800	1968.000	479.100	2001.000	2 0 0
54	GR:	479.100	2029.000	479.700	2094.000	480.400	2181.000	480.200	2240.000	480.200	2269.000	
8	GR	480.300	2360.000	480.500	2458.000	480.500	2521.000	480.500	2578.000	480.800	2649.000	lu_ i
94	GR	480.100	2719.000	479.300	2793.000	477.800	2858.000	477.100	2935.000	477.700	2976.000	•
24	GR	480.500	2998.000	475.700	3049.000	465.200	3067.000	463.200	3076.000	461.400	3084.000	118
•	GR	461.400	3142.000	461.400	3197.000	463.200	3211.000	464.600	3222.000	469.800	3257.000	37
	GR	478.800	3282.000	477.800	3330.000	477.100	3390.000	477.100	3411.000	477.800	3425.000	
	GR	482.500	3469.000	485.900	3495.000	489.700	3527.000	497.300	3564.000	498.500	3587.000	

	CONTRACTOR OF THE PARTY OF	CONTRACTOR OF THE PROPERTY OF								400		STANDARD AND THE PROPERTY OF T
-	X5	0.0	0.0	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0	70
	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.700	0.0	0.0	
	NC	0.060	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000	
		2000	84,000			407 756						
	X1	18.040	0.0	0.0	0.0	10.000	10.000	10.000	0.0	0.0	0.0	
	ХЗ	10.000	0.0	0.0	0.0	0.0	0.0	0.0	474.700	473.100	0.0	
•	NC	0.060	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	/
	FT	0.8	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	4154.000	
		从来是了东京				48.00			986,800			
	X1	18.000	67.000		4154,000	55.000	55.000	55.000	0.0	C 0.0	. 0.0	
	X3	10.000	0.0	LJUD	licated	Rag	e "san	ne,as	Page	69	0.8	
_ //	GR	485.000	1,000				1099.000		1179 000	469.900	1234.000	
•	GR	468.300	1317.000	468.400	1424.000	467.100	1467.000	467.500	1517.000	470.800	1551.000	
9	GR	473.300	1572.000	474.700	1629.000	473.700	1688.000	472.800	1758.000	469.900	1811.000	
- 10	GR	468.900	1872.000	468.700	1949.000	468.500	2033.000	468.800	2162.000	468.700	2264.000	,
9 11	GR	468.800	2343.000	469.700	2393.000	470.600	2480.000	471.100	2582.000	471.200	2724.000	
12	GP	471.500	2851.000	471.900	2953.000	472,000	3003.000	472.100	3043.000	472.100	3083.000	Y
	GR	472.100	3100.000	472.280	3111.000	471.000	3243.000	470.700	3362.000	470.400	3504.000	
91	GR	470.300	3632.000	471.100	3700.000	472.600	7 3780.000	474.700	3849.000	478.500	3894.000	•
15	GR	478.500	3917.000	465.900	3984.000	465.900	3984.000	459.000	4001.000	459.000	4038.000	. 10
14	GR	459.000	4038.000	459.000	4842.000	459.000	4042.000	459.000	4096.080	459.000	4096.000	11-
	GR	459.000	4100.000	459.000	4100,000	459.000	4145.000	464.300	4154.000	464.300	4154.000	
lg F	GR	473.500	4200.000	473.500	4221.000	473.100	4257.000	473.300	4249.000	474.500	4359.000	12
"	GR	479.700	4396.000	484.100	4432.000	486.700	4446.000	491.600	4485.000	499.600	4508.000	in
● 20	GR	512.900	4530.000	525.000	4556.000	0.0	0.0	0.0	0.0	0.0	0.0	
"[NC	0.070	0.080	0.035	0.500	0.700	0.0	0.0	0.0	0.0	0.0	11
	ET	0.0	0.0	0.0	0.0	2.100	0.0	0.0	0.0	2650.000	4535.000	. 16_
9 #		本种和 。本位的	1124,395				9 F F T T T T T T T T T T T T T T T T T	1000			4000 900	
w [X1	19.000	80.000	4140.000	4525.000	1750.000	1500.000	1283.000	0.0	0.0	0.0	14
	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	476.300	0.0	0.0	17 L
	GR GR	483.800	1000.000	481.300	1049.000	479.300	1136.000	478.600	1211.000	477.800	1252.000	77
"_		476.600	1291.000	474.900	1327.000	474.400	1383,000	473.800	1544.000	474.600	1611.000	78 Z.R
•	GR GR	474.700	1650.000	475.300	1723.000	478.600	1741.000	475.300	1790.000	474.200	1805.000	11 _ }
	GR	474.200	1870.000	474.200	1991.000	474.400	2084.000	474.800	2248.000	474.800	2447.000	6
4.17	GR	473.200	2622.000	471.600	2660.000	472.600	2758.000	473.400	2821.000	471.600	2850.000	19
	GR	471.900	2919.000	472.100	3003.000	472.000	3118.000	472.100	3224.000	472.200	3274.000	2)
	GR	472.400 476.500	3349.000	474.100	3566.000	474.600	3610.000	474.800	3689.000	475.700	3772.000	,, "
,	GR	470.700	3867.000	478.000	3975.000	479.000	4096.000	479.000	4140.000	474.900	4162.000	
•	GR	462.100	4174.000	465.600	4187.000	462.500	4198.000	462.100	4199.000	462.100	4252.000	13
20	GR.	462.500	4360.000	462.100	4310.000	465.000	4317.000	465.900	4327.000	465.500	4349.000	
20	GR.	462.800	4392.000	462.500	4361.000	462.100	4370.000	462.100	4370.000	462.500	4383.000	
9 38	GR	462.500	4484.000	465.000	4495.000	473.700	4447.000	460.700	4588 000	460.700 474.700	4476.000 4607.000	25
37	GR	475.900	4641.000	476.900	4587.000	478.800	4735.000	478.800	4752.000	474.900	4762.000	
4	GR	475.400	4779.000	477.200	4804.000	477.700	4823.000	485.200	4866.000	491.200	4889.000	
241	GR	491.200	4906.000	500.200	4916.000	510.000	4932.000	517.200	4949.000	526.200	4972.000	n a
- 10	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2070.000	3291.000	13
0		Secretary of the second	51.0		V • V		2,980 - 8 8		0.0	20000	5271.000	
944	X1	19.100	0.0	0.0	0.0	750.000	800.000	805.000	0.650	1.800	0.0	"
45.	х3	10.000	0.0	0.0	0.0	6:0	0.0	0.0	477.000	0.0	0.0	30
66	FT	0.0	0.0	0.0	0.0	5.400	0.0	0.0	0.0	0.0	0.0	
90					· · ·	J. 100	0.0	y•.	0.0	0.0	0.0	
45.	X 1	20.000	58.000	2998.000	3282.000	750.000	800.000	805.000	0.0	0.0	0.0	9 5
6	х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	478.300	0.0	0.0	
# 50	GR-	508.100	1000.000	507.300	1046.000	504.500	1093.000	501.300	1171.000	494.400	1248.000	**
51	GR	490.700	1306.000	487.000	1348.000	486.600	1371.000	485.200	1383.000	483.700	1410.000	u u
52	GR	479.700	1450.000	477.800	1570.000	477.400	1622.000	478.600	1663.000	480.500	1730.000	Office
9 11	GR	488.100	1784.000	479.500	1851.000	478.600	1910.000	478.800	1968.000	479.100	2001.000	35 0 0
ы	GR	479.100	2029.000	479.700	2094.000	480.400	2181.000	480.200	2240.000	480.200	2269.000	3
55	GR /	480.300	2360.000	480.500	2458.000	480.500	2521.000	480.500	2578.000	480.800	2649.000	
	GP	480.100	2719.000	479.300	2793.000	477.800	2858.000	477.100	2935.000	477.700	2976.000	10
57	GR	480.500	2998.000	475./00	3049.000	465.200	3067.000	463.200	3076.000	461.400	3084.000	n ×
	GR	461.400	3142.000	461.400	3197.000	463.200	3211.000					
	GR	478.800						464.600	3222.000	469.800	3257.000	19
			3282.000	477.800	3330.000	477.100	3390.000	477.100	3411.000	477.800	3425.000	
	GR	482.500	3469.000	485.900	3495.000	489.700	3527.000	497.300	3564,000	498,500	3587.000	

S. S	SHARES ADDRESS CAMES					and the second second							
	GR NC	500.		96.000	514.500	3619.000	525.600	3641.000	0.0	0.0	0.0	0.0	71 👗
	ET	0.	070	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
			U	560 0 K	0.0	0.7	10.400	0.0	0.0	0.0	0.0	1.0.0	
S XS	D X1	21.	000	54.000	2225.000	2592.000	600.000	600.000	525.000	0.0	0.0	0.0	
) NO	X3	10.		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	GR	523.		000.000	524.000	1050.000	523.700	1124.000	523.400	1182.000	520.100	1223.000	
0 1	GR	517.		244.000	510.600	1277.000	500.700	1302.000	498.600	1315.000	494.800	1342.000	
	GR	490.		354.000	489.700	1398.000	488.800	1439.000	485.200	1462.000	483.500	1543.000	. 1
	GR GR	482.		550.000	482.900	1713.000	482.700	1744.000	482.200	1846.000	481.800	1953.000	3.
	GR	480.		25.000	480.100 475.500	2077.000	479.600 465.400	2111.000	479.000 463.800	2174.000	480.100 462.800	2202.000	
1	GR	462.		314.000	462.800	2360.000	463.800	2376.000	464.800	2391.000	464.900	2414.000	
	GR			43.000	472.300	2481.000	474.000	2527.000	477.700	2592.000	477.700	2673.000	
	GR	478.		000.517	478.900	2734.000	479.410	2778.000	481.100	2819.000	482.800	2855.000	5
10	GR	489.	600 28	89.000	493.800	2931.000	499.400	2966.000	499.400	3006.000	500.200	3046.000	
9 11	GR			106.000	505.500	3138.000	515.200	3177.000	525.300	3203.000	0.0	1320.000	
12	NC			0.0	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0	4
- 12	FT	0.	0.	0.0	0.0	6.0	9.100	0.0	0.0	0.0	1299.000	1575.000	
15	×1	23.	010	39.000	1299.000	1497.000	600.000	455.000	445.000	0.0	0.0	0.0	~
15	×1	10.		0.0	0.0	0.0	0.0	0.0	0.0	488.000	481.500	-0.0	100
9 17	GR	542.		000.000	542.100	1020.000	540.000	1060.000	536.900	1119.000	526.400	1139.000	n _e
18	GR	520.		69.000	512.700	1198.000	510.400	1225.000	500.600	1267.000	490.800	1283.000	· u
19	GR	480.	200 12	299.000	471.500	1318.000	466.200	1324.000	464.200	1331.000	458.300	1353.000	
9 - 20	6 GR			16.000	458.300	1442.000	464,200	1488.000	465.300	1497.000	473.500	1516.000	
B	GR	Bullion in Comment of the Comment of the		569.000	480.100	1593.000	482.300	1647.000	482.700	1720.000	482.800	1764.000	The state of the s
n	GR	482.		788.000	483.000	1876.000	483.200	1943.000	483.800	2001.000	484.200	2075.000	15
	GR GR	484. 505.		24.000	488.600	2164.000	491.000	2205.000	498.000	2235.000	499.800	2250.000	
25	SB		900	1.500	2.600	2330.000	524.200 131.000	2390.000	525.000 4200.000	24.37.000	0.0 459.000	0.0 459.000	
₩126	हा			0.0	0.0	0.0	9.100	0.0	0.0	0.0	1299.000	1575.000	"6
27	,	9	esh les			7.00			4.00	1 0 0 0 0	1237.000	15/5.000	
28	×1	23.	020	0.0	0.0	0.0	30.000	30.000	30.000	0.0	0.0	0.0	
129	X2			0.0	1.000	485.000	482.500	0.0	0.0	0.0	0.0	0.0	
30	Х3	CHARLEST THE RESIDENCE		0.0	0.0	0.0	0.0	0.0	0.0	489.000	482.500	0.0	75
31	PT			285.000	489.000	0.0	1590.000	488.000	0.0	1720.000	482.500	0.0	21
32	RI			83.000	0.0	2120.000	484.500	0.0	2200.000	491.000	0.0	0.0	
34	NC FT	0.	070	0.080	0.035	0.300	0.500 9.100	0.0	0.0	0.0	0.0 1299.000	0.0 1575.000	" "
● 135			O.	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1299.000	1575.000	"
CYC	QXI	23.	000	39.000	1299.000	1569.000	55.000	55.000	55.000	0.0	0.0	0.0	24
2 /\J	GR	542.		000.000	542.100	1020.000	540.000	1060.000	536.900	1119.000	526.400	1139.000	14
- 138	GR	520.	500 11	69.000	512.700	1198.000	510.400	1225.000	500.600	1267.000	490.800	1283.000	•
39	GR	480.		99.000	471.500	1318.000	466.200 -	1324.000	464.200	1331.000	458.300	1353.000	26
	GR	458.		16.000	458.300	1442.000	464.200	1488.000	465.300	1497.000	473.500	1516.000	u
4.8	GR	479.		69.000	480.100	1593.000	482.300	1647.000	482.700	1720.000	482.800	1764.000	•
0	GR	482.		88.000	483.000	1876.000	483.200	1943.000	483,800	2001.000	484.200	2075.000	
9:41	GR GR	484. 505.		24.000	488.600 514.900	2164.000	491.000 524.200	2205.000	498.000 525.000	2235.000	499.800	2250.000	29
45	NC		070	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0	25 W
45	FT	o.		0.0	0.0	0.0	9.100	0.0	0.0	0.0	1239.000	1472.000	11 //-
94.87				ra boe	14.00 (1.00	1.37.556	W#4.200	1375,850		1192,000	多多数。2000	1450,000	"•
SXS	R X1	24.	000	46.000	1239.000	1472.000	380.000	280.000	370.000	0.0	0.0	0.0	at .
49	GR	549.		000.000	549.600	1016.000	556.500	1046.000	564.400	1097.000	569.200	1128.000	33
9 5 50	Daniel Shows	573.		48.000	570.700	1166.000	559.900	1185.000	550.700	1205.000	525.200	1216.000	•
21	GR	499.		27.000	487.000	1239.000	486.300	1248.000	473.700	1259.000	470.000	1267.000	
Ø 553	GR	465.		79.000	462.800	1285.000	462.800	1346.000	462.800	1405.000	465.200	1416.000	35
9	GP GP	467. 483.		26.000	470.000	1446.000 1639.000	474.900 483.900	1472.000	475.900 484.200	1500.000	479.800 484.000	1539.000	935
23	GR	484.		08.000	483.100	1845.000	484.200	1689.000	484.400	1906.000	484.400	1970.000	
1 055	GR	484.		32.000	484.600	2121.000	484.900	2167.000	485.800	2220.000	485.800	2240.000	
51	GR	489.		60.000	492.300	2326.000	497.100	2358.000	509.000	2394.000	515.300	2415.000	30
55	GR	525.		45.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
9 65	NC		080	0.080	0.035	0.500	0.700	0.0	0.0	0.0	0.0	0.0	
	ET	0.	0	0.0	0.0	0.0	9,100	0.0	0.0	0.0	1365.000	1890.000	

					THE RESERVE			775 795				72	
S XS S	X1	25.000	44.000	1394.000	1624.000	920.000	250.000	750.000	0.0	0.0	0.0	12	
	GR	574.600	1000.000	550.300	1035.000	525.000	1066.000	499.800	1094.000	488.300	1116.000		
	GR .	488.300	1132.000	486.300	1144.000	479.700	1164.000	477.500	1180.000	477.600	1256.000		
	GR GR	479.300	1278.000	476.500	1316.000	475.700	1377.000	474.700	1394.000	469.200	1401.000		
E SE	GR	467.000	1413.000	465.200	1423.000	465.200	1470.000	465.200	1515.000	467.000	1521.000		
0	GR	478.000	1817.000	473.200 474.000	1557.000 1830.000	475.200 474.000	1610.000 1895.000	477.800 480.700	1624.000 1924.000	478.000 480.700	1803.000 1936.000		1 3
	GR	482.400	1979.000	483.100	2085.000	484.100	2160.000	484.200	2273.000	484.400	2372.000		9
	GR	484.400	2410.000	484.800	2460.000	486.600	2476.000	486.600	2492.000	491.700	2511.000		
0	GR	493.000	2528.000	500.100	2549.000	511.500	2573.000	524.900	2599.000	0.0	0.0		
4	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1445.000	1940.000		
VC T 1						477,473			1976,609		Amata dan		
XS T 💿	X1	26.000	44.000	1462.000	1634.000	440.000	450.000	450.000	0.0	0.0	0.0		
1	GR	525.000	1000.000	514.300	1038.000	514.000	1058.000	507.300	1077.000	507.300	1099.000		
10	GR	504.700	1113.000	502.200	1125.000	502.200	1140.000	495.300	1164.000	491.600	1185.000		1.2
	GR	490.500	1206.000	484.800	1216.000	484.200	1245.000	481.800	1286.000	483.000	1324.000		•
	GR	485.500	1339.000	486.700	1398.000	487.000	1408.000	484.200	1420.000	480.900	1438.000	and the same of	
	GR	475.800	1462.000	472.100	1469.000	468.000	1479.000	465.500	1485.000	465.500	1530.000		9
14	GR GR	465.500	1561.000	468.000	1584.000	469.400	1596.000	474.100	1613.000	477.200	1634.000		,
15	GR	477.600	1817.000	475.300	1833.000	474.000	1850.000	474.000	1910.000	475.300	1919.000		
1	GR	490.000	2003.000	484.400 500.000	2046.000	484.600 509.900	2120.000	489.400 524.300	2154.000 2253.000	489.400	2173.000		11
19	NC	0.0	0.0	0.0).100	0.300	0.0	0.0	0.0	0.0	0.0		12
19	FT	0.0	0.0	0.0	5.0	9.100	0.0	0.0	0.0	1490.000	1830.000		
● 20		3357 786		4-1	3-3-27-13-27	483.2430	145.9.899	5945.450	1866.566	4.65.666	THE STATE OF THE S		120
XS U	X1	27.000	34.000	1602.000	1830.000	600.000	325.000	540.000	0.0	0.0	0.0		14
22	GR	521.000	1000.000	521.000	1016.000	517.300	1033.000	505.100	1071.000	499.100	1099.000		
● 23	GR	498.700	1135.000	492.600	1173.000	487.400	1235.000	487.500	1267.000	487.500	1306.000		
24	GR	485.900	1320.000	476.600	1337,000	476.600	1474.000	476.000	1514.000	475.700	1561.000		.14
25	GR	475.300	1602.000	473.700	1621.000	469.800	1633.000	468.900	1641.000	467.800	1652.000		111
● 28	GR	467.800	1719.000	467.800	1791.000	468.900	1798.000	470.500	1808.000	474.900	1830.000		9 to
7.	GR	480.400	1858.000	482.300	1879.000	484.200	1900.000	485.700	1913.000	485.700	1932.000		18 2
21	GR	489.600	1940.000	499.500	1967.000	513.100	1989.000	525.100	2012.000	0.0	0.0		19 EAL
100	NC -	0.080	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		9 0
31	FI	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1780.000	2100.000		
XS V	X1	28.000	38.000	1877.000	2095.000	915.000	950.000	940.000	0.0	0.0	0.0		21
11	GR	525.100	1000.000	516.600	1051.000	506.500	1080.000	499.900	1107.000	496.200	1147.000		22
34	GR	493.000	1199.000	490.400	1226.000	490.400	1245.000	490.400	1258.000	490.100	1323.000		
15	GR	488.700	1365.000	485.700	1397.000	499.400	1416.000	502.300	1444.000	505.800	1484.000		
H H	GR	510.700	1542.000	515.700	1586.000	515.000	1604.000	500.500	1661.000	500.000	1678.000		24
27	GR	481.000	1716.000	477.700	1747.000	474.900	1804.000	472.500	1835.000	475.500	1877.000		15
30	GR	472.700	1921.000	471.200	1943.000	470.500	1951.000	468.500	1974.000	468.500	2004.000		
39	GR	468.500	2044.000	470.500	2056.000	471.900	2065.000	475.500	2076.000	485.700	2095.000		14
47	GR	485.700	2106.000	500.500	2124.000	524.900	2140.000	0.0	70.000	0.0	0.0		77
3. 21	NC	0.080	0.080	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
4)	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		
S XS W	X1	29.000	46.000	2154.000	2293.000	730.000	800.000	790.000	0.0	0.0	0.0		29
S VS VV	GR	529.700	1000.000	525.700	1032.000	521.900	1062,000	520.100	1100.000	517.100	1157.000		30
46	GR	514.800	1212.000	496.000	1246.000	496.000	1258.000	500.800	1282.000	490.800	1311.000		
100	GR	490.800	1324.000	484.600	1337.000	484.200	1375.000	485,300	1420.000	485.000	1460.000		31
45	GR	485.500	1478.000	484.900	1493.000	485.500	1512.000	482.200	1538.000	478.700	1599.000		11 E
45	GR	478.600	1658.000	481.200	1707.000	481.500	1758.000	480.600	1787.000	478.200	1839.000		
950	GR	477.000	1908.000	476.600	2020.000	476,600	2073.000	474.400	2092.000	475.100	2119.000		" 9
31	GR	474.800	2154.000	473.100	2171.000	472.000	2185.000	470.100	2208.000	470.100	2232.000		34
37	GR	470.100	2281.000	472.000	2288.000	473.100	2293.000	480.400	2306.000	488.300	2323.000		35 0
53	GR	488.500	2338.000	499.400	2355.000	512.700	2369.000	524.400	2382.000	535.400	2400.000		. 9
S4	GR '	549.700	2418.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7-2	16 and
55 77	FT	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		31 _ 9
9 56													9 3
S XS X	X1	30.000	36.000	1923.000	2321.000	350.000	420.000	410.000	0.0	0.0	0.0		38
58	GR	524.800	1000.000	521.400	1090.000	512.600	1188.000	499.000	1228.000	497.700	1257.000		39
00	GR	494.600	1290.000	490.600	1310.000	490.200	1329.000	485.800	1370.000	482.000	1431.000		
	GR	478.000	1518.000	482.700	1633.000	480.100	1694.000	477.900	1751.000	481.300	1799.000		

A

MINISTER SE													
10	GR GR	481.900	1859.000		1923.000	480.500		476.800	2013.000	475.600	2057.000	73	
	GR	474.000			2119.000	475.200		475.500	2181.000	474.400	2201.000		
	GR	496.300	2210.000		2246.000	474.000	2281.000	475.000	2296.000	496.300	2321.000		
	GR	550.700	2339.000		2345.000	500.200		524.400	2370.000	541.200	2389.000		
	NC		2407.000		0.0	0.0	0.0	0.0	0.0	0.0	0.0		•
1	140	0.0	0.0	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0		
XS Y	×1	31.000	49.000	1765.000	2007.000	310.000	620.000	575.000					
1	GR	524.500	1000.000	520.500	1080.000	513.100	1145.000		0.0	0.0	0.0		
	GR	497.300	1254.000	491.700	1284.000	490.800		501.200	1188.000	500.000	1227.000		7
	GR	478.800	1447,000	480.200	1485.000	482.200	1306.000 1537.000	485.600	1353.000	481.800	1385.000		,_ ;
	GR	480.200	1765.000	474.900	1789.000	474.900	1805.000	481.600	1635.000	481.400	1716.000		
	GR	475.800	1852.000	475.100	1865.000	472.900	1906.000	475.400	1816.000	476.600	1828.000		
	GR	475.100	1972.000	476.100	1985.000	480.900	2007.000	472.900 480.900	1918.000	472.900	1943.000		
• •	GR	478.700	2135.000	480,500	2160.000	481.600	2203.000	484.300	2046.000	480.500	2095.000		
35	GR	487.000	2334.000	485.400	2354.000	483.200	2384.000	478.700	2423.000	486.100	2309.000		6
# 11	GR	477.400	2443.000	480.200	2466.000	486.100	2488.000	487.900	2499.000	476.100	2433.000		
- 17	GR	489.800	2524.000	500.300	2536.000	524.500	2566.000	550.000	2604.000	487.900	2518.000		
11	NC .	0.0	0.070	0.0	0.300	0.500	0.0	0.0	0.0	0.0	0.0		
VC 7	XI	33 000	F2 444	1.20 (A.10) (A.10)	3132.499				10490600	A 55 (20 A)	V.0		'.
XS Z	GR	32.000 524.900	53.000	1313.000	1427.000	770.000	350.000	630.000	0.0	0.0	0.0		118
	GR	499.900	1000.000	518.300	1055.000	514.200	1111.000	505.100	1157.000	501.000	1198.000		
12	GR	492.300	1207.000	499.000	1222.000	499.400	1240.000	502.200	1250.000	492.300	1273.000		0
16	GR		1280.000	486.200	1299.000	478.300	1313.000	474.50C	1323.000	470.800	1333.000		12
A 20	GR	470.800	1367.000	470.800	1407.000	474.500	1418.000	477.600	1427.000	480.800	1459.000		
43	GR	483.500	1506.000	481.900	1526.000	481.100	1552.000	480.800	1563.000	482.900	1580.000		13
22	GR		1608.000	483.900	1640.000	485.400	1694.000	485.800	1721.000	485.400	1746.000		
	GR	483.900	1769.000	481.900	1788.000	481.600	1799.000	485.600	1814.000	488.500	1846.000		
	GR	482.400	1860.000	485.300	1910.000	483.900	1969.000	480.400	1987.000	482.400	2006.000		•
25.7	GR	482.100	2023.000	480.300	2042.000	480.100	2070.000	479.200	2099.000	480.500	2121.000		
	GR	529.600	2158.000	494.600	2187,000	495.200	2210.000	499.700	2219.000	515.000	2242.000		
77	NC	0.0	2263.000	539.000	2289.000	550.700	2318.000	0.0	0.0	0.0	0.0		•
78	FT	0.0	0.0	0.0	0.100	0.300	0.0	0.0	0.0	0.0	0.0		16 69
023		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1280.000	2246.000	A Section	REA
XS A	Δ×1	33.000	57.000	1403.000	1581.000	475.000	175.000	380.000	0.0	505.500	4000000000		9 5
NJ F	6R	526.200	1000.000	516.800	1063.000	511.800	1111.000	503.200		0.0	0.0		. 20
€ 32	GR	491.700	1208.000	491.700	1227.000	485.700	1248.000	480.700	1151.000 1258.000	499.100	1193.000		21
33	GR	483.500	1298.000	483.500	1337.000	482.500	1353.000	482.200	1387.000	483.100	1269.000		9.
34	GR	476.800	1408.000	475.200	1416.000	469.000	1446.000	469.000		480.200	1403.000		172
69 33	GR	475.200	1553.000	476.600	1565.000	480.400	1581.000	482.400	1480.000	469.000	1500.000		23
36	GR	481.900	1649.000	485.400	1683.000	485.800	1718.000	486.000	1813.000	482.300	1630.000		
2	GR	484.200	1856.000	482.900	1873.000	483.000	1891.000	485.800	1904.000	485.800	1831.000		A S
Ø 31	GR	485.900	1955.000	484.900	1969.000	484.700	1985.000	483.100	1999.000	488.400	1931.000		25
. 39	GR	481.700	2059.000	480.800	2082.000	480.300	2114.000	480.000	2131.000	480.900 482.300	2028.000		7
40	GR	480.700	2175.000	484.900	2198.000	484.900	2222.000	485.500	2277.000	485.700	2157.000		
91	GR	485.900	2342.000	496.900	2370.000	497.000	2396.000	499.200	2407.000		2320.000		27
44	GR	535.100	2466.000	550.700	2509.000	0.0	0.0	0.0	0.0	524.100	2440.000		73
	NC	0.0	0.060	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
94	FT	0.0.	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		79
VC A	DX 1	34.000	50,000	17// 225						0.0	. 0		20
XS A	Bx 1	530.400		1764.000	1977.000	250.000	525.000	480.000	0.0	0.0	0.0		2)
- 45	GR	497.200	1000.000	526.400	1071.000	522.900	1129.000	514.500	1170.000	500.600	1189.000		. 9
45	GR	480.700	1218.000	499.900	1229.000	492.300	1250.000	492.300	1274.000	484.100	1290.000		31 - 5
@ 50	GR	483.900	1301.000	482.600	1320.000	483.600	1389.000	483.700	1468.000	483.500	1540.000		. *
9	GR	483.900	1566.000	480.800	1586.000	480.600	1604.000	484.200	1616.000	483.600	1649.000		"
51	GR	477.000	1689.000	484.200	1720.000	484.200	1747.000	483,900	1764.000	480.700	1782.000		34
652	GR	479.100	1793.000	475.400	1797.000	475.400	1864.000	475.400	1932.000	477.000	1938.000		Uan
a a	GR	484.800	1945.000	486.100	1962.000	488.500	1977.000	486.800	1985.000	486.600	2010.000		" 9 9
n Fill	GR		2021.000	485.100	2047.000	485.500	2078.000	486.300	2130,000	486.600	2211.000		36 00
64	GR	487,100	2243.000	490.500	2270.000	490.500	2288.000	494.100	2299.000	504.700	2321.000		- 2
CONTRACT AND LINES		505.300	2341.000	509.000	2356.000	525.100	2379.000	535.500	2397.000	550.000	2428.000		") 1
. 15			24300.000	45700.000	58500.000	58500.000	102000.000						SECURIOR SECTION AND ADDRESS.
53	OT					20,200.000	102000.000	0.0	0.0	0.0	0.0		38 2
57	NC ET	0.080	0.060	0.035	0.100	0.300	0.0	0.0	0.0	0.0	0.0		3 7

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	ALC: NO. OF THE PARTY OF		A STATE OF THE STA	THE RESERVE OF THE PARTY OF THE						A 10 May		THE RESIDENCE AND A SECOND CONTRACTOR OF THE PROPERTY OF THE P
S XS A	GR.	35.000 530.100	56.000	2118.000	2287.000	575.000	775.000	720.000	0.0	0.0	0.0	74
	GR	489.000	1140.000	500.400	1028.000	495.300	1050.000	494.900	1101.000	489.000	1119.000	
	GR	484.800	1216.000	492.100	1149.000	492.100	1167.000	485.700	1181.000	483.700	1200.000	
	GR	485.800	1357.000	482.800	1235.000	483.700	1255.000	483.800	1284.000	485.600	1317.000	
	GR	485.700	1737.000	486.300 485.300	1443.000	486.400	1525.000	486.300	1616.000	486.300	1695.000	
1	GR	487.700	1875.000	487.700	1793.000	484.900	1812.000	484.400	1831.000	486.400	1856.000	
· 2	GR	487.200	2033.000	486.900	1907.000	486.900	1936.000	484.100	1960.000	485.900	1999.000	
ak.	GR	477.600	2134.000	477.600	2198.000	485.400	2095.000	484.600	2118.000	478.000	2133.000	` •
	GR	488.700	2287.000	489.200	2319.000	477.600	2260.000	478.000	2262.000	479.900	2268.000	1 6
	GR	491.300	2489.000	491.600	2528.000	488.900	2358.000	489.300	2397.000	491.100	2439.000	
	GR	503.600	2694.000	504.800	2705.000	493.900	2577.000	497.300	2627.000	503.600	2677.000	
7	GR	549.700	2810.000	0.0	0.0	519.800	2733.000	536.100	2772.000	544.200	2797.000	
	NC	0.090	0.060	0.038	0.300	0.0	0.0	0.0	0.0	0.0	0.0	1. 1
9	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	0.0	0.0	
\G			San			2.100	0.0	0.0	0.0	2870.000	3220.000	
SXSA	D ^{X1}	36.000	28.000	2870.000	3198.000	900.000	720.000	740 000				
7 V2 Y	V x3	10.000	0.0	0.0	0.0	0.0	0.0	740.000	0.0	0.0	0.0	
AS	GR :	535.000	1000.000	500.000	1070.000	495.000	1088.000	0.0 493.600	510.000	0.0	0.0	
1 14	GR	497.500	1120.000	495.000	1130.000	490.000	1130.000	489.000	1200.000	495.000	1102.000	
15	GR	495.000	1248.000	490.000	1255.000	497.000	1440.000	495.000	1530.000	495.000	1220.000	
16	GR	486.000	2870.000	485.000	2990.000	480.000	3015.000	474.200	3045.000	495.000	1565.000	10
17	GR	480.000	3175.000	485.000	3198.000	490.000	3215.000	495.000	3250.000	474.200 500.000	3150.000	W.
34	GR	520.000	3380.000	525.000	3410.000	535.000	3425.000	0.0	0.0	0.0	3275.000	
19	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2629.000	0.0 3130.000	**
20		4350				•		10001100	10000 3000	2023.000	3130.000	13
2)	×1	36.100	39.000	2629.000	3130.000	€0.000	60.000	60.000	0.0	0.0	0.0	
22	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	494.100	517.400	0.0	\
	GR	510.000	1000.000	513.000	1282.000	508.300	1292.000	494.100	1325.000	508.700	1325.000	15
	GR	508.700	1328.000	494.100	1328.000	494.100	1368.000	509.000	1368.000	509.000	1371.000	
	GR	494.100	1371.000	509.400	1405.000	514.200	1415.000	526.800	2610.000	517.400	2629.000	No.
69	GR GR	486.000	2682.000	485.000	2718.000	518.200	2718.000	518.200	2723.000	485.000	2723.000	12 9 pt
		484.000	2756.000	476.000	2858.000.	519.900	2858.000	519.900	2863.000	476.000	2863.000	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
20	GR GR	475.000	2875.000	475 000	2900.000	478.000	2937.000	490.000	2985.000	491.000	2995.000	H H
	GR	494.000	2998.000	521.200	2998.000	521.200	3003.000	494.000	3003.000	505.000	3024.000	" . B
10	ET	503.000	3070.000	522.500	3110.000	532.000	3130.000	535.000	3420.000	0.0	0.0	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
49 37		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2629.000	3130.000	/ F3 / T - 5
13	×1	36.200	0.0	0.0	0.0	10.000	9.570					
34	RT	8.000	1282.000	513.000	0.0	10.000	10.000	10.000	0.0	0.0	0.0	\
€ 35	BT	1415.000	514.200	514.200	513.000	1292.000	513.100	508.300	1405.000	514.200	509.400	
34	BT	531.800	522.500	3130.000	2610.000 532.000	526,800	526.800	2629.000	527.000	517.400	3110.000	
y y	ET	0.0	0.0	0.0	0.0	532.000	0.0	0.0	0.0	0.0	0.0	N
9 33		1,00		•••	0.0	9.100	0.0	0.0	0.0	2629.000	3130.000	25 _
39	X1	36.300	0.0	0.0	0.0	130.000	130 000	120 000				7.9
40	XS	0.0	0.0	0.0	0.0	0.0	130.000	130.000	0.0	0.0	0.0	20
9	ET	0.0	0.0	0.0	0.0	9.100	0.0	1.000	0.0	0.0	0.0	37
42		373 555	500 W H T 80 W H		0.0	7.100	0.0	0.0	0.0	2629.000	3130.000	
43	X1	36.400	0.0	0.0	0.0	10.000	10.000	10.000	0 0			
9 11	Х3	10.000	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	29
45	NC	0.045	0.080	0.039	0.300	0.500	0.0	0.0	494.100	532.000	0.0	
46	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	0.0	0.0	
9 0			1836.356	647.1450			V U	0.80	0.0	2265.000	2630.000	F .
- 4	X1	38.000	22.000	2265.000	2624.000	65.000	75.000	100.000	0.0	0.0	0.0	
	GR	520.000	2200.000	495.500	2265.000	495.500	2265.000	490.600	2300.000		0.0	
9 30	GR	479.400	2328.000	477.500	2337.000	476.500	2342.000	476.500	2473.000	481.600 476.500	2322.000	n .
31	GR	477.500	2585.000	479.000	2589.000	480.100	2593.000	482.900	2605.000	486.600		4
4	GR	499.200	2650.000	512.400	2678.000	509.200	2702.000	514.800	2713.000	524.800	2624.000	
90	GR	534.200	2752.000	549.400	2775.000	0.0	0.0	0.0	0.0	0.0	0.0	25
SA	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2151.000	2850.000	
27 18						two		9.00	V. V	2171.000	2030-000	
9	X1	39.000	39.000	2151.000	2391.000	200.000	150.000	315.000	0.0	0.0	0.0	31 🐧
. 9	GR	520.000	1960.000	490.000	2035.000	486.500	2090.000	486.900	2122.000	489.200	2151.000	[· · · · · · · · · · · · · · · · · · ·
51	GR	487.100	2169.000	483.700	2191.000	479.500	2203.000	479.000	2211.000	478.500	2219.000	······································
9	GR	478.500	2271.000	478.500	2335.000	479.000	2337.000	480.400	2343.000	484.900	2366.000	37
	GR	485.500	2391.000	484.800	2432.000	484.300	2455.000	483.500	2518.000	484.100	2556.000	

	CONTRACTOR OF THE PARTY OF THE	The second secon	The state of the s	American and an owner was an owner				was a stand war.			The state of the s		
	GR	484.400	2618.000	483.800	2677.000	483,200	2717.000	481.100	2739.000	478.400	2747.000	75	
	GR	477.600	2749.000	477.600	2776.000	477.600	2800.000	478.400	2803.000	479.600	2809.000		
	GR	485.900	2837.000	499.300	2863.000	514.700	2890.000	513.000	2913.000	516.100	2917.000		
	GR .	520.500	2931.000	530.400	2952.000	539.600	2974.000	549.400	2991.000	0.0	0.0		
	QT	5.000	24300.000	45700.000	58500.000	48800.000	102000.000	0.0	0.0	0.0	0.0		6
	NC	0.0	0.045	0.0	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
1	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1780.000	2465.000		
● 7										1,00,000	2403.000		1
XS A	F X1	40.000	49.000	1905.000	2072.000	415.000	380.000	410.000	0.0	0.0	0.0		
NO A	GR	520.000	1405.000	490.000	1485.000	487.900	1725.000	488.100	1732.000				13
	GR	487.700	1786.000	486.900	1851.000	485.800	1905.000	484.300	1916.000	488.100	1732.000		3
4.	GR	479.300	1937.000	478.600	1942.000	478.600	1986.000	478.600	2035.000	480.200	1930.000		
2	GR	480.200	2051.000	485.400	2072.000	487.300	2114.000	486.900		479.300	2042.000		4
	GR	487.400	2346.000	488.100	2415.000	487.700	2506.000		2181.000 2583.000	487.100	2249.000		5
	GR	485.400	2829.000	485.300	2882.000	486.300	2933.000	486.500 485.200		486.000	2710.000		
10	GR	485.800	3096.000	486.800	3128.000	485.400	3152.000		2991.000	484.500	3032.000		16
(9 11	GR	478.900	3176.000	478.900	3208.000	478.900	3240.000	481.100	3165.000	479.500	3173.000		
12	GR	489.300	3259.000	500.800	3273.000			479.500	3244.000	480.300	3248.000		
11	GR	523.000	3328.000	531.200	3341.000	519.800	3292.000	521.000	3301.000	521.000	3319.000		4.0
(D) 14	QT	5.000	24300.000	45700.000		540.100	3359.000	549.600	3371.000	0.0	0.0		100
161	NC	0.045	0.045	0.039	58500.000	48800.000	102000.000	0.0	0.0	0.0	0.0		
JA.	FT	0.0	0.0	0.034	0.100	0.300	0.0	0.0	0.0	0.0	0.0		Jab
1 17		0.0	D. Buch	0.0	0.0	9.100	0.0	0.0	0.0	1525.000	2730.000		n,
VCHA	⊏×1	41.000	57.000	1904.000	2096.000	470 000	300 000	460 000					9
S XS A	GR	510.000	1250.000	495.000	1295.000	470.000	390.000	460.000	0.0	0.0	0.0		12
	GR	489.500	1817.000	488.200		493.000	1500.000	492.800	1654.000	492.400	1740.000		13
7	GR	480.900	1928.000		1856.000	485.800	1875.000	485.100	1904.000	483.700	1921.000		
71	GR	479.400	2063.000	479.400	1932.000	478.800	1934.000	478.800	1998.000	478.800	2058.000		14
Ø · 73	GR	487.500	2214.000	480.300 488.700	2071.000	490.000	2096.000	485.700	2114.000	487.000	2130.000		15
34	GR	488.000	2712.000	488.700	2298.000	488.100	2367.000	488.000	2423.000	485.800	2583.000		
25	GR	487.000	3185.000	485.300	2835.000	488.500	2925.000	488.100	3009.000	487.600	3108.000		16
	GR	486.300	3552.000	486.600	3220.000	486.400	3256.000	486.900	3343.000	486.600	3432.000		17
27	GR	487.500			3637.000	486.600	3705.000	487.200	3801.000	487.200	3839.000		
75	GR	478.000	3861.000	484.600	3876.000	482.000	3886.000	478.800	3897.000	478.000	3899.000		18
0 1	GR .	502.100		478.000	3942.000	478.800	3946.000	480.100	3953.000	490.200	3974.000		10
20	GR	537.600	4068.000	520.900	4011.000	520.900	4027.000	522.000	4036.000	527.300	4047.000		
2 31	NC			551.200	4087.000	0.0	0.0	0.0	0.0	0.0	0.0		10
Ø −77	FT	0.0	0.0	0.042	0.500	0.700	0.0	0.0	0.0	0.0	0.0		211
13		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	2760.000		
34	×1	42.010	27 000	10EE 000	2125 000	100 000	250.000	252 222					n n
0	GR	511.600	37.000	1955.000	2125.000	100.000	250.000	250.000	0.0	0.0	. 0.0		a l
, J.	GR	492.600	1000.000	511.800	1027.000	510.800	1042.000	509.800	1053.000	505.400	1073.000		9
n T	GR	494.000	1100.000	494.000	1113.000	494.000	1125.000	494.000	1145.000	494.000	1218.000		
	GR	495.400	1308.000	494.000 495.700	1413.000	494.000	1543.000	494.700	1582.000	495.200	1640.000		75
39	GR	484.200	1988.000	477.000	1771.000	495.800	1815.000	482.200	1955.000	482.200	1955.000		3
1 to	GR	492,000			2073.000	479.200	2106.000	479.200	2106.000	494.600	2125.000		
	GR	481.900	2400.000 3585.000	490.000	2905.000	492.500	3330.000	490.000	3570.000	485.000	3580.000		U
47	GR	500.000		481.900	3640.000	484.000	3690.000	485.000	3785.000	490.000	3860.000		
0	FT		3980.000	520.200	4005.000	0.0	0.0	0.0	0.0	0.0	0.0		-
0-11	Е !	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1490.000	2760.000		139
45	X1	42.020	37.000	1955.000	2106 000	35 000	25 000	25 222					
4	X3	10.000			2105.000	25.000	25.000	25.000	0.0	0.0	0.0		
9 a	GR	511.600	0.0	0.0	0.0	0.0	0.0	0.0	492.500	491.900	0.0		21
48	GR	492.600		511.800	1027.000	510.800	1042.000	509.800	1053.000	505.400	1073.000		
6	GR	494.000	1100.000	494.000	1113.000	494.000	1125.000	494.000	1145.000	494.000	1218.000		maria di
₽ 450	GR	495.400	1308.000		1413.000	494.000	1543.000	494.700	1582.000	495.200	1640.000		31
51.1	GR		1695.000	495.700	1771.000	495.800	1815.000	482.200	1955.000	482.200	1955.000		
. 57		484.200	1988.000	477.000	2073.000	479.200	2106.000	479.200	2106.000	494.600	2125.000		
	GR GR	492.000	2400.000	490.000	2905.000	492.500	3330.000	490-000	3570.000	485.000	3580.000		23
94		481.900	3585.000	481.900	3640.000	484.000	3690.000	485.000	3785.000	490.000	3860.000		7
9.17	GR	500.000	3980.000	520.200	4005.000	0.0	0.0	0.0	0.0	0.0	0.0		4
Ø49	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0.	0.0	1490.000	2760.000		n
	SB	0.0	1.500	2.500	0.0	151.000	0.0	1786.000	0.0	0.0	0.0		9
													3
	X1	42.100	0.0	0.0	0.0	25.000	25.000	25.000	0.0	0.0	0.0		39
	XS	0.0	0.0	1.000	493.000	492.000	0.0	0.0	0.0	0.0	0.0		9
Sharker should be in	X3	10,000	0.0	0.0	0.0	0.0	0.0	0.0	492.600	492.000	0.0	and the state of t	SHEET

	RT	34.000	1000.000	511,600	***0.0	1027 000				(#####################################	ALLEN OF PRINCIPAL		8
	RT	1053.000	509.800	0.0	1073.000	1027.000	511.800	0.0	1042.000	510.800	0.0	/6	
	BT	494.000	0.0	125.000	494.000	0.0	0.0	1100.000	492.600	0.0	1113.000		
	BT	0.0	1308.000	494.000	0.0	1413.000	1145.000	494.000	0.000	1218.000	494.000		
	BT	1582.000	494.700	0.0	1640.000	495.200	494.000	0.0	1543.000	494.000	0.0		
	BT	495.700	0.0	1815.000	495.800		0.0	1695.000	495.400	0.0	1771.000		.91
	BT	493.000	2106.000	494.900	491.900	0.0	1955.000	496.000	482,200	1955.000	496.000		
	RT	2400.000	492.000	0.0	2905.000	2106.000	494.900	479.200	2125.000	494.600	0.0		
	BT	490.000	0.0	3580.000	485.000	0.0	0.0	3330.000	492.500	0.0	3570.000		9
1	RT	0.0	3690.000	484.000	0.0	3785.000	3585.000	481.900	0.0	3640.000	481.900		2 8
	RT	3980.000	500.000	0.0	4005.000	520.200	485.000	0.0	3860.000	490.000	0.0		
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	0.0	0.0		
1				See See		2.100	0.0	0.0	0.0	1490.000	2760.000		- 1
	Xl	42.200	37.000	1955.000	2125.000	50.000	50.000	50.000	0.0				
1	GR	511.600	1000.000	511.800	1027.000	510.800	1042.000	509.800	0.0	0.0	0.0		(9)
15	GR	492.600	1100.000	494.000	1113.000	494.000	1125.000	494.000	1053.000	505.400	1073.000		
(III	GR	494.000	1308.000	494.000	1413.000	494.000	1543.000	494.700	1582.000	494.000	1218.000		7
12_	GR	495.400	1695.000	495.700	1771.000	495.800	1815.000	482.200	1955.000	495.200	1640.000		
13	GR	484.200	1988.000	477.000	2073.000	479.200	2106.000	479.200	2106.000	482.200	1955.000	•	
() II	GR	492.000	2400.000	490.000	2905.000	492.500	3330.000	490.000	3570.000	494.600 485.000	2125.000		1.
PE - PE	GR	481.900	3585.000	481.900	3640.000	484.000	3690.000	485.000	3785.000	490.000	3580.000		
18.	GR	500.000	3980.000	520.200	4005.000	0.0	0.0	0.0	0.0	0.0	3860.000)	10
	NC	0.050	0.045	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
15	OT	5.000	24300.000	45700.000	58500.000	48800.000	102000.000	0.0	0.0	0.0	0.0		
19	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1520.000	2980.000		- '
KS AC	_ 440	2.5					1475 2006				2960.000		13
V2 AC		43.000	59.000	2146.000	2442.000	230.000	236.000	230.000	0.0	0.0	0.0		"
	GR	509.500	1000.000	509.500	1010.000	508.500	1023.000	504.600	1043.000	506.700	1064:000		
0	GR	509.500	1073.000	509.500	1098.000	507.200	1108.000	500.400	1124,000	492.800	1159.000		•
	GR	492.900	1183.000	493.300	1263.000	493.700	1324.000	493.900	1384.000	493.700	1463.000		
	GR	493.700	1535.000	493.100	1607.000	493.500	1677.000	493.900	1744.000	494.100	1829.000		
0"	GR GR	493.400	1902.000	492.900	1937.000	493.600	1965.000	493.100	2011.000	437.000	2023.000		"•
	NAME OF TAXABLE PARTY.	487.000	2059.000	486.500	2085.000	484.800	2112.000	486.900	2138.000	486.900	2146.000		18 (9
	GR	484.500	2159.000	482.800	5505.000	481.600	2217.000	481.000	2224.000	481.000	2279.000		7 7
0	GR GR	481.000	2333.000	481.700	2335.000	484.300	2342.000	485.200	2373.000	486.300	2419.000		19 6
	GR	487.500	2442.000	487.400	2468.000	487.200	2475.000	490.000	3020.000	493.000	3040.000		
0	GR	493.000	3065,000	490.000	3085.000	488.000	3150.000	486.500	3550.000	485.000	4030.000		
	GR	482.500	4085.000	482.500	4115.000	485.000	4135.000	490.000	4400.000	495.000	4450.000		" •
4	OT	505.000	4475.000	507.000	4480.000	507.000	4495.000	510.000	4510.000	0.0	0.0		77
9:	NC	6.000	20000.000	38000.000	48800.000	48800.000	87000.000	0.0	0.0	0.0	0.0		
	FT	0.0	0.050	0.0	0.600	0.800	0.0	0.0	0.0	0.0	0.0		29
37		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1495.000	2540.000		78
VOA	1 1 1	44.000	61.000	2114 000	2255 000	275 010							1,
XS A	GR	507.800	1000.000	2114.000 507.800	2355.000	275.000	700.000	415.000	0.0	0.0	0.0		9
40	GR	507.800	1073.000	507.800	1013.000	506.700	1024.000	503.100	1050.000	506.200	1065.000		28
100	GR	495.200	1190.000	495.400	1098.000	507.000	1112.000	491.000	1149.000	492.000	1163.000		27
- 12	GR	496.200	1596.000	495.600	1277.000	495.700	1342.000	495.700	1407.000	495.800	1518.000		
n	GR	494.600	1933.000	495.300	1649.000	493,900	1711.000	493.300	1807.000	493.600	1875.000		78
94	GR	494.900	2088.000	488.900	2114.000	495.300 485.600	2008.000	495.500	2064.000	494.700	2088.000		29
45	GR	480.600	2186.000	480.600	2231.000		2141.000	483.400	2160.000	482.000	2173.000		
45	GR	482.000	2312.000	481.500	2319.000	480.600	2259.000	482.000	2288.000	482.700	2303.000		30
	GR	483.700	2337.000	490.300	2355.000	490.900	2321.000	481.500	2330.000	482.000	2332.000		31 🕳
48	GR	492.700	2611.000	494.200	2623.000	495.300	2403.000	491.200	2491.000	491.700	2570.000		
0	GR	498.300	2703.000	498.300	2731.000	501.300	2635,000	495.300	2661.000	495.700	2682.000		37 3
1000	GR	509.100	2860.000	522.000	2881.000	511.300		501.300	2803.000	506.500	2828.000		33
- 51	GR	525.200	3031.000	0.0			2921.000	512.200	2970.000	513.500	3010.000		
N.	NC	0.0	0.095	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		134 6
19:	FT	0.0	0.0	0.0	0.0	0.300 9.100	0.0	0.0	0.0	0.0	0.0		35 8
. 14	100		2108.884	0.6-0 medi	0.0	9.100	0.0	0.0	0.0	1780.000	2674.000		75
35	X1	45.000	40.000	2431.000	2674.000	305 000	435 000	/20 000					36 2
19.	GR	535.200	1000.000	520.700	1031.000	395.000 509.200	425.000	420.000	0.0	0.0	0.0		31 - 3
57	GR	506.500	1386.000	506.500	1411.000	505.600	1060.000	506.500	1065.000	506.500	1305.000		91
58	GR	495.400	1536.000	495.800	1608.000		1422.000	492.300	1461.000	493.300	1495.000	*	
0	GR	495.500	1931.000	494.600	1985.000	495.900 495.200	1701.000	496.100	1790.000	495.800	1874.000		77
	GR	496.100	2318.000	496.100			2040.000	495.500	2113.000	495.700	2201.000		9
	AMMADEL DESCRIPTION OF THE PARTY OF THE PART	70.100	2310.000	490.100	2379.000	495.800	2431.000	493.500	2444.000	487.800	2463.000		

	GR	485.200	2470.000	483,000	2478,000	481,500	2483,000	481.500	2545,000	481.500	2602.000	***********	
•	GR	483.000	2608.000	484.000	2612.000	486.300	2631.000	489.300	2652.000	499.400	2674.000	77	
	GR	505.400	2683.000	505.400	2704.000	516,200	2729.000	525.800	2773.000	531.500	2851.000	77	
	NC	0.040	0.100	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
•	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1645.000	2560.000		•
_ 1	Xì	46.000	35.000	2374.000	2560.000	530.000	570.000	565.000	0.0	0.0	0.0		79
	GR	535.200	1000.000	504.600	1085.000	504.500	1342.000	500.900	1358.000	495.600	1405.000		
31	GR	495.700	1470.000	496.100	1522.000	496.200	1626.000	496.400	1725.000	496.500	1805.000		,
	GR	496.800	1866.000	496.300	1935.000	495.600	1993.000	494.700	2102.000	493.800	2187.000		
•	GR	492.700	2255.000	491.700	2321.000	490.600	2374.000	488.700	2391.000	484.700	2399.000		
, k	GR	483.800	2411.000	482.200	2433.000	482.200	2467.000	482.200	2503.000	483.800	2530.000		
7	GR	484.100	2535.000	488.100		490.300	2560.000	497.800	2581.000	497.800	2592.000		
	GR	519.200	2611.000	519.200	2633.000	520,200	2638.000	529.900	2651.000	535.200	2660.000		
9	NC	0.060	0.100	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
10	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1570.000	2350.000		
(1)										1310.000	2330.000		
72	X1	47.000	48.000	2160.000	2327.000	325.000	660.000	630.000	0.0	0.0	0.0		
. 13	GR	535.200	1000.000	520.500	1031.000	510.000	1055.000	503.800	1072.000	503.800	1200.000		
10	GR	503.800	1282.000	501.800	1298.000	497.200	1317.000	497.200	1364.000	497.100	1434.000		'
15	GR	497.000	1519.000	496.700	1600.000	496.800	1680.000	496.100	1749.000	495.600	1835.000		110
- 16	GR	495.000	1913.000	494.100	1940.000	491.300	1997.000	485.800	2010.000	485.200	2018.000		
(9 -17	GR	484.900	2025.000	484.900	2024.000	484.900	2027.000	485.200	2031.000	486.900	2051.000		"
18	GR	488.600	2071.000	490,900	2095.000	489.200	2124.000	487.900	2160.000	485.500	2191.000		- 12
19	GR	485.300	2203.000	484.900	2212.000	484.000	2234.000	484.000	2250.000	484.000	2283.000	Company of the Company of	
(9 20	GR	484.900	2296.000	485.900	2310.000	492.300	2327.000	491.500	2344.000	488.000	2359.000		13
n	GR	484.600	2382.000	485.900	2400.000	492.400	2418.000	498.300	2440.000	498.300	2460.000		H
17	GR	521.300	2480.000	521.300	2509.000	535.500	2528.000	0.0	0.0	0.0	0.0		
(73 74	ET	0.0	0.0	0.0	0.0	9.100	7 0.0	0.0	0.0	1580.000	2175.000		15
25	X1	48.000	38.000	1994.000	2172.000	570.000	620.000	610.000	0.0	0.0	0.0		
(1) 76	GR	535.400	1000.000	526.200	1021.000	512.500	1049.000	503.500	1067.000	503.500	1279.000		17
27	GR	501.400	1289.000	497.800	1313.000	499.000	1354.000	498.300	1397.000	498.100	1479.000		18
28	GR	498.600	1563.000	496.700	1625.000	494.100	1704.000	492.300	1767.000	492.500	1843.000		
(2) 29	GR	491.900	1871.000	487.500	1893.000	488,000	1914.000	487.400	1928.000	489.400	1942.000		19
30	GR	491.600	1969.000	489,900	1994.000	487.900	2001,000	486.800	2009.000	486.000	2014.000		20
11	GR	486.000	2076.000	486.000	2133.000	486.800	2138.000	488.200	2148.000	489.100	2172.000		100
(2) 32	GR	496.600	2190.000	497.000	2211.000	499.500	. 2219.000	514.200	2234.000	530.900	2251.000		270
13	GR	530.900	2266.000	531.700	2276.000	534.700	2284.000	0.0	0.0	0.0	0.0		.,
31	FT	0.0	0.0	0.0	0.0	15.400	0.0	0.0	0.0				
9 B									0.0	0.0	0.0		23.
	X1	49.000	40.000	1781.000	1998.000	549.000	555.000	555.000	0.0	0.0	0.0		14
	GR	534.700	1000.000	520.300	1028.000	503.900	1069.000	503.900	1100.000	503.900	1200.000		1,5
-	GR	503.900	1294.000	503.900	1315.000	501.200	1333.000	497.600	1361.000	494.000	1378.000		
37	GR	492.400	1401.000	492.000	1455.000	491.160	1482.000	491.300	1510.000	495.300	1522.000		25
	GR	495.800	1532.000	495.200	1544.000	491.900	1557.000	489.800	1571.000	491.000	1593.000		27
100	GR	491.900	1635.000	492.900	1695.000	494.700	1739.000	493.000	1781.000	491.100	1810.000		
D	GR	488.500	1835.000	487.000	1846.000	486,300	1850.000	486.300	1913.000	486.300	1974.000		35
11	GR	487.000	1978.000	488.100	1985.000	492.600	1998.000	499.200	2015.000	499.200	2034.000		70
1	GR	514.300	2061.000	514.500	2081.000	516.100	2099.000	524.800	2122.000	535.300	2179.000		
45	NC	0.080	0.095	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		20
(B) 47	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		
45	X1	50.000	32.000	1987.000	2290.000	420.000	468.000	465.000	0.0	0.0	0 0		100
49	GR	525.000	1222.000	505.500	1262.000	505.500				0.0	0.0		
	GR	505.500	1675.000	505.000	1680.000		1300.000	505.500	1400.000	505.500	1500.000		
51	GR	487.000	1828.000	487.000		495.000	1703.000	494.000	1778.000	490.000	1813.000		
52	GR	492.800	1968.000		1848.000	490.000	1869.000	492.600	1910.000	492.100	1948.000		
4 13	GR	486.200		490.200	1987.000	488.900	2020.000	488.400	2043.000	487.500	2059.000		35_
. 14	GR	491.000	2081.000	486.200	2106.000	486.200	2150.000	487.500	2155.000	489.100	2163.000		
35	ISR	535.000	2190.000	500.800	2218.000	500.800	2233.000	522.100	2258.000	522.100	2276.000		49
3 10	FJ	0.0	2292.000	550.900	2310.000	0.0	0.)	0.0	0.0	0.0	0.0	V	37
51	6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	. h	я
51					<u> </u>		- J				V.V		T IV

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******* SEPT 1971 VERSION. UPDATED JUNE 1974 * * THIS PROGRAM IS OWNED BY THE UNITED STATES GOVERNMENT ERROR CORRECTIONS 01 THRU 09R2 * AND IS USED BY PERMISSION OF THE CORPS OF ENGINEERS. MODIFICATIONS 52 THRU 58 * DEPARTMENT OF THE ARMY. MBJ UPDATED 07/20/76 * THE PROGRAM HAS BEEN REVISED BY MICHAEL BAKER, JR., INC. * * ONLY AS REQUIRED FOR USE ON THEIR COMPUTER AND EXECUTES * TODAYS DATE IS 03/02/77 20.34 * CORRECTLY THE STANDARD TEST SERIES AS PUBLISHED BY THE * * CORPS OF ENGINEERS. HYDROLOGIC ENGINEERING CENTER. ************ 2.807 SECONDS TI SUSQUEHANNA RIVER BASTN COMMISSION TZ BLOOMSBURG-BERWICK-SHICKSHINNY REACH T3 FISHING CREEK - 100 YEAR FLOOD ICHECK TNO NINV IDIR STRT METRIC HVINS WSEL FO Michael Baker, Jr., Inc. 0. 0. 0.0 0.0 0.0 503.831 0.0 2763 N. Fourth St. NPROF .12 IPLOT PRFVS XSECV XSECH FN ALLDC IBW CHNIM ITRACE Box 3225 Harrisburg, Pa. 17105 1.000 0.0 -1.000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 J3 1.000 34.000 3.000 4.000 27.000 28.000 9.000 0.0 0.0 0.0 NC 0.080 0.095 0.039 0.100 0.300 0.0 0.0 0.0 0.0 0.0 OT 5.000 2000.000 38000.000 48800.000 48800.000 87000.000 0.0 0.0 0.0 0.0 FT 0.0 0.0 0.0 0.0 10,400 0.0 0.0 0.0 0.0 0.0 X1 50.000 32.000 1987.000 2190.000 420,000 468.000 465.000 0.0 0.0 0.0 GR 525.000 505.500 1222.000 262.000 505.500 1300.000 505.500 1400.000 505.500 1500.000 GR 505.500 1675.000 505.000 1680.000 495.000 1703.000 494.000 1778.000 490.000 1813.000 GR 487.000 1828.000 487.000 1348.000 490.000 1869.000 492.600 1910,000 492.100 1948.000 GP 492.800 1968.000 490.200 1987.000 488.900 2020.000 488.400 2043.000 487.500 2059.000 GR 486.200 2081.000 486.200 2106.000 486,200 2150.000 487.500 2155.000 489.100 2163.000 GR 491.000 2190.000 500.800 2218.000 500.800 2233.000 522.100 2258.000 522.100 2276.000 GR 535.000 2292.000 550.900 2310.000 0.0 0.0 0.0 0.0 0.0 0.0 NH 4.000 1657.000 0.085 0.055 1914.000 0.036 2052.000 0.095 2234.000 0.0 X 1 51.000 34.000 1914.000 2052.000 205.000 230.000 225.000 0.0 0.0 0.0 GR 535,000 1000.000 521.200 1024.000 506.000 1039.000 506.000 1300.000 506.000 1633.000 GR 506.000 1657.000 504.100 1670.000 495.300 1691.000 493.100 1711.000 492.700 1744.000 GR 490.300 1759.000 488.400 1766.000 490.200 1779.000 491.500 1801.000 490.200 1823.000 GR 490.200 1848.000 490.300 1876.000 490.100 1914.000 488.500 1935.000 488.000 1963.000 GR 486.100 2003.000 488.000 2042.000 490.000 2052.000 492.500 2078.000 492.500 2098.000 GR 491.100 2112.000 500.700 2134.000 500.700 2146.000 516.000 2168.000 516.000 2185.000 GR 518.900 2190.000 527.400 2200.000 535.100 2212.000 550.000 2234.000 0.0 0.0 NC 0.060 0.060 0.060 0.100 0.500 0.0 0.0 0.0 0.0 0.0 NH 4.000 0.085 1925.000 0.060 2051.000 0.036 2297.000 0.085 2421.000 0.0 FT 0.0 0.0 0.0 0.0 0.0 9.400 0.0 0.0 0.0 0.0 52.000 29.000 2051.000 2297.000 223.000 217.000 225.000 0.0 0.0 0.0 GR 535.400 1000.000 525.800 1042.000 510.000 1064.000 1073.000 506.500 506.500 1925.000 GR 505.800 1937.000 494.900 1963.000 493.300 1982.000 492.400 2017.000 491.200 2032.000 GR 492.800 2051.000 491.100 2068.000 490.100 2085.000 489.800 2091.000 489.300 2101.000 GR 489.300 2164.000 489.300 489.800 2232.000 2234.000 490.900 2238.000 492.300 2253.000 GR 492.900 2278.000 497.900 2297.000 501,900 2314.000 501.900 2328.000 512.100 2347.000 GR 512.100 2365.000 524.400 2379.000 535.400 2398.000 550.200 2421.000 0.0 0.0 NC 0.060 0.060 0.060 0.100 0.700 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 4.400 0.0 0.0 0.0 0.0 0.0 4.000 0.085 1897.000 0.050 1952.000 0.036 2147.000 0.080 2265.000 0.0 52.100 17.000 1952.000 2147.000 297.000 251.000 275.000 0.0 0.0 0.0 525.000 1000.000 507.500 1022.000 507.500 1897.000 505.000 1911.000

	GR	495.000	1050 000							nergen and a series of the series			and an entire
	GR	505.000	1952.000	489.600 509.000	1971.000	489.600	2136.000	495.000	2147.000	500.000	2177.000	/9	
	GR	520.000	2255.000	525.000	2227.000	509.000	2246.000	510.000	2247.000	515.000	2248.000		
	NH	4.000	0.085	2057.000	0.040	2107.000	0.036	0.0 2309.000	0.0	0.0	0.0		
49	FT	0.0	0.0	0.0	0.0	10.400	0.036	.0.0	0.070	2466.000	0.0		
								•		0.0	0.0		
	X1	53.000	27.000	2107.000	2309.000	298.000	252.000	275.000	0.0	0.0	. 0.0		
	GR	550.100	1000.000	524.900	1019.000	508.400	1030.000	508.400	1080.000	508.400	2000.000		- MED
	GR	508.400	2035.000	508.400	2057.000	507.500	2068.000	504.400	2084.000	501.200	2107.000		2 6
•	GR	492.500	2125.000	491.000	2131.000	489.900	2135.000	489.900	2206.000	489.900	2270.000		- 4
	GR GR	491.000	2276.000	492.200	2283.000	500.400	2309.000	501.600	2330.000	502.700	2351.000		•
	GR	502.700	2358.000	506.300	2374.000	506,300	2393.000	509.100	2400.000	525.300	2419.000		4
	NH	534.100	0.100	549.900 2088.000	2466.000	0.0	0.0	0.0	0.0	0.0	0.00		,_
9		904.500	0.100	2000.000	0.050	2148.000	0.038	2343.000	0.080	2520.000	0.0		
18	×1	54.000	26.000	2148.000	2343.000	813.000	797.000	805.000	0.0				- 6
(1)	GR	549.800	1000.000	526.300	1013.000	512.600	1028.000	512.300	1029.000	0.0 512.300	0.0		1_
17	GR	510.800	2097.000	507.700	2117.000	504,900	2148.000	495.600	2156.000	493.500	2163.000		
13	GR	491.500	2169.000	491.500	2239.000	491.500	2312.000	493.500	2317.000	495.800	2323.000		
(9 14	GR	502.300	2343.000	505.000	2368.000	505.700	2383.000	505.700	2396.000	514.400	2409.000		'
15	GR	514.400	2426.000	524.300	2454.000	527.000	2467.000	535.200	2483.000	544.600	2507.000		10
15	GR	550.100	2520.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
11	NC	0.650	0.055	0.030	0.100	0.300	0.0	0.0	0.0	0.0	0.0		9
14	NH	4.000	0.085	1802.000	. 0.040	1848.000	0.036	2043.000	0.070	2229.000	0.0		12
(D to	X1	55.000	29.000	1848.000	20/2 000	(50.000		1.1 电影线电影 传言					13
71	GR	550.000	1000.000	525.800	2043.000	659.000 513.800	662.000	655.000	0.0	0.0	0.0		"9
η	GR	513.800	1771.000	513.800	1802.000	512.500	1028.000	513.800	1100.000	513.800	1500.000		14
(3) 23	GR	497.600	1863.000	497.000	1868.000	495.300	1875.000	507.300 491.800	1831.000	504.100	1848.000		15
24	GR	491.800	2013.000	495.300	2022.000	496.900	2026.000	502.700	2043.000	491.800 504.700	1947.000 2068.000		
15	GR	505.500	2094.000	505.500	2126.000	508,600	2135.000	508.600	2146.000	515.100	2157.000		
(3) 76	GP	526.000	2180.000	526.000	2197.000	537.300	2209.000	549.900	2229.000	0.0	0.0		17
17	NC	0.055	0.095	0.030	0.100	0.300	0.0	0.0	0.0	0.0	0.0		18 N
n n	NH	4.000	0.085	1645.000	0.050	1668.000	0.036	1865.000	0.070	2218.000	0.0		RE
9 11													100 6
114	X J	56.000	32.000	1668.000	1865.000	374.000	368.000	380.000	0.0	0.0	0.0		20 00
0	GR GR	549.800	1000.000	525.100	1012.000	516.300	1019.000	516.300	1300.000	516.300	1617.000		. 21
-91	GR	516.300 496.000	1645.000	515.800	1651.000	510.200	1668.000	499.700	1702.000	498.700	1706.000		9
31	GR	491.700	1712.000	491.700	1738.000	496.000	1763.000	496.400	1770.000	496.000	1776.000		22
0	GR	505.800	1932.000	505.400	1836.000 1968.000	497.400 505.900	1852.000	502.400	1865.000	506.100	1890.000		73
	GR	510.700	2115.000	510.700	2131.000	515.600	2010.000	506.400 515.600	2054.000 2164.000	506.700	2102.000		
	GR	540.200	2196.000	550.500	2218.000	0.0	0.0	0.0	0.0	525.700	2172.000		
● 31	FT	0.0	0.0	0.0	0.0	8.400	0.0	0.0	0.0	0.0	0.0		25
37	NH	4.000	0.085	1406.000	0.060	1529.000	0.036	1774.000	0.060	2339.000	0.0		26
- 47													
0	X1	57.000	35.000	1529.000	1774.000	530.000	500.000	500.000	0.0	0.0	0.0		20
4	GR	550.000	1000.000	537.200	1013.000	524.900	1027.000	520.500	1032.000	520.500	1406,000		25
0	GR	519.500	1421.000	519.000	1432.000	519.200	1456.000	519.800	1466.000	519.800	1494.000		29
	GR GR	518.600	1509.000	510.700	1529.000	506.100	1548.000	500.800	1576.000	499.800	1582.000		9
	GR	498.600 506.000	1589.000	493.400	1636.000	498.600	1681.000	499.100	1701.000	501.000	1748.000		30
0	GR	506.000	2036.000	506.800	1822.000	507.600	1902.000	506.700	1970.000	506.600	2014.000		31
a	GR	504.100	2186.000	508,800 505,200	2079.000	511.000	2124.000	510.600	2147.000	508.800	2168.000		
. 6	NC	0.090	0.055	0.036	2194.000	515,400	2211.000	515.400	2306.000	550.400	2339.000		
⊘ 50		3 3 0 3 0	0.055	0.036	0.100	0.300	0.0	0.0	0.0	0.0	0.0		33
5	×1	58.000	53.000	2032.000	2216.000	685,000	645.000	705.000	0.0	0.0	0.0		31
12	Х3.	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
9 :	GR	575.000	1000.000	566.700	1023.000	549.900	1067.000	537.400	1086.000	535.400	1090.000		arco Bu
ŞI	GR	533.800	1094.000	533.800	1300.000	533.800	1548.000	533.800	1572.000	532.400	1585.000		14- day
#15	GR	525.700	1601.000	515.500	1616.000	506.100	1639.000	505.300	1653.000	501.300	1664.000		
0	GP	500.000	1668.000	500.000	1670.000	500.000	1675.000	501.300	1678.000	504.100	1684.000		2 3
17	GR	506.000	1704.000	506-600	1753.000	508.400	1811.000	509.500	1882.000	509.300	1942.000		31
	GR	507.400	1978.000	506.400	2015.000	506.100	2032.000	502.000	2045.000	500.800	2052.000		
	GR	496.500	2075.000	496.500	2113.000	496.500	2113.000	500.800	2170.000	501.300	2177.000		"9
	GR	501.900	2197.000	507.000	2216.000	508.300	2237.000	511.200	2266.000	510.600	2306.000		

	GR GR	510.900 511.600	2366.300	512.600 514.600	2417.000 2625.000	512.600 520.700	2481.000 2636.000	513.700 520.700	2552.000	515.460 525.100	2593.000 2804.000	80	•
	GR NC	550.600	2837.000	562.300	2857.000	575.600	2878.000	0.0	0.0	0.0	0.0		
	ET	0.100	0.055	0.036	0.100	0.300	0.0	0.0	0.0	0.0	0.0		•
	X1 GR	59.000 575.400	69.000	3263.000	3437.000	400.000	330.000	360.000	0.0	0.0	0.0		
	SR	543.400	1000.000	565.700 543.400	1042.000	552.500 543.400	1086.000	543.400 543.400	1119.000	543.400 542.500	1200.000 2180.000		, 0
	GR	539.400	2200.000	542.700	2219.000	543.200	2230.000	543.200	2258.000	540.500	2267.000		
	GR GR	535.300	2280.000	525.600	2297.000	514.300	2325.000	507.700	2337.000	505.500	2343.000		•
	GR	502.000	2349.000	501.500 505.700	2350.000	501.500 505.100	2356.000	501.500 505.700	2361.000	502.000	2363.000 2556.000		- 1 ·
	GR	505.700	2619.000	506.300	2687.000	506.500	2770.000	508.300	2845.000	508.500	2926.000		''●
	GR GR	508.500	3001.000	509.300	3081.000	508.200	3110.000	509.500	3131.000	508.900	3149.000		
	GR	508.500 508.000	3188.000	507.300	3204.000 3278.000	505.500 501.500	3208.000	506.000 498.000	3222.000 3310.000	507.800 498.000	3248.000 3352.000		,1 ₀
	GR	498.000	3414.000	501.500	3418.000	504.300	3420.000	507.200	3437.000	508.400	3473.000		
	GR	510.800	3512.000	511.500	3574.000	511.500	3613.000	513.900	3644.000	514.700	3673.000		1,_
	GR GR	515.700 523.800	3703.000 3950.000	515.200 550.300	3730.000 3982.000	513.200 562.100	3743.000 4004.000	514.200 574.800	3749.000 4031.000	523.800	3761.000		10
	NC	0.100	0.055	0.038	0.100	0.600	0.0	0.0	0.0	0.0	0.0		
	ET	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		12
	X1	60.000	30.000	4190.000	4378.000	460.000	410.000	410.000	0.0	0.0	0.0		113_
	GR CR	574.800 512.700	1000.000	550.300 512.400	2496.000 3539.000	515.400 512.000	3371.000 3596.000	515.500 511.500	3393.000 3654.000	514.900 510.900	3422.000		•
	GR	509.000	3751.000	507.200	3774.000	505.800	3813.000	505.100	3838.000	509.800	3713.000 3867.000		
	GR	511.100	3933.000	511.200	3992.000	511.700	4064.000	511.100	4120.000	509.600	4141.000		1.0
gar/Attention	GR GR	506.500 495.900	4160.000	506.000 495.900	4190.000	504.700	4212.000	502.500 505.900	4225.000 4378.000	495.900 528.000	4262.000 4379.000		18
	EU	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		"• g
		0-4-1	-0,0					4.0					READ
				2002.200	(4) 6.1 65	40,000	35,000	41,686	100				70
		476,460									7501 705		21
		220200				333-256				347.049	72468,078		. 22
				0.00.000			2497,000 3687,000				2001.000		27
	100	505.304	2024 000	0.000.000	3059.000	517 400	1979(350	314,700	11/04 11/0	819,700			24
				535,1934									25
													26
		519,565	3155,000	867,200		505,806	3823,467	508,046	7630,000		7,000		77
				511.000 000 000			3544,000						70
		552,565		445,2460		446.310	013839280X	1995 903		4952355			100
		085,980					4,000						
										0.00			30
													33
		3,202	1	12.111		307.640	20,000		9,818	508,900	564(355)		32 5
													23
													34
					4,4	0.5	1000						35
				#31,490									34
		8.13.864	1.75 8.4	19860 (Ut)	SAME SAME	9,	State Action	351,284.5		110062000		_ \	
													19
		9122117						0.2 3 9	3,279,250	572.755			
			619.507			195.3 1975.3	4550; 501 520, 300	0.6		4653.066 520#600			39
			COLOR WAS							4 6			West Control of the C

	GR	510.900	2366.000	512.600	2417.000	512,600	2481.000	513.700	2552.000	515.400	2593.000	0.4
	GR	511.600	2614.000	514.600	2625.000	520.700	2636.000	520.700	2800.000	525.100	2804.000	81 •
	GR	550.600	2837,000	562.300	2857.000	575.600	2878.000	0.0	0.0	0.00	0.0	
	NC ET	0.100	0.055	0.036	0.100	0.300 40.400	0.0	0.0	0.0	0.0	0.0	•
		380,396	2330,000	300000	<u> </u>	979,789	74.67.700	3,079,2799	1510.00		18177.000	
	X1 GR	59.000 575.400	69.000	3263.000 565.700	3437.000	400.000	330.000 1086.000	360.000 543.400	1119.000	0.0 543.400	1200.000	\ ' @
	GR	543.400	1600.000	543.400	1800.000	543.400	2140.000	543.400	2171.000	542.500	2180.000	
	GR	539.400	2200.000	542.700	2219.000	543,200	2230.000	543.200	2258.000	540.500	2267.000	* \ *
(GR	535.300	2280.000	525.600	2297.000	514.300	2325.000	507.700	2337.000	505.500	2343.000	
	GR	502.000	2349.000	501.500	2350.000	501.500	2356.000	501.500	2361.000	502.000	2363.000	
7	GR	503.900	2369.000	505.700	2386.000	505.100	2429.000	505.700	2492.000	506.000	2556.000	
	GR	505.700	2619.000	506.300	2687.000.	506.500	2770.000	500 300	2845.000	508.500	2926.000	
	GR GR	508.500 508.500	3001.000	509.300	3081.000	508.200 505.500	3110.000	509.500	3131.000	508.900 507.800	3149.000 3248.000	•
4	GR	508.000	3263.000	504.600	3278.000	501.500	3293.000	498.000	3310.000	498.000	3352.000	'
-12	. GR	498.000	3-14.000	501.500	3418.000	504.300	3420.000	507.200	3437.000	508-400	3473.000	
10	GR	510.000	3512.000	511.500	3574.000	511.500	3613.000	513.900	3644.000	514,700	3673.000	
(GR	515.700	3703.000	515.200	3730.000	513.200	3743.000	514.200	3749.000	523.800	3761-000	
15	GR_	523.800	3950,000	550,300	3982,000	562,100	4004-000	574.800	4031.000	0.0	0.0	
	NC	0.100	0.055	0.038	0.100	0.600	0.0	0.0	0.0	0.0	0.0	n n
	ET	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	3843,040	· n
10	X1	60.000	30.000	4190.000	4378.000	460.000	410.000	410.000	0.0	0.0	0.0	
(≥ 72)	GR	574.800	1000.000	550.300	2496.000	515.400	3371.000	515.500	3393.000	514.900	3422.000	
21	GR	512.700	3483.000	512.400	3539.000	512.000	3596.000	511.500	3654.000	510.900	3713.000	"
22	GR	509.000	3751.000	507.200	3774.000	505.800	3813.000	505.100	3838.000	509.800	3867.000	15
	GR GR	511.100	3933.000	511.200	3992.000 4190.000	511.700 504.700	4064.000 4212.000	511.100 502.500	4120.000 4225.000	509.600 495.900	4141.000 4262.000	14
25	GR	506.500 495.900	4160.000	506.000 495.900	4338.000	502.500	4364.000	505.900	4378.000	528.000	4379.000	
(3)	NC	0.0	0.0	0.0	0.400	0.600	0.0	0.0	0.0	0.0	0.0	"• _•
27	NH	3.000	0.100	4141.000	0.039	4378.000	0.060	4721.000	00	0.0	0.0	II. N
98	ET	0.0	0.0	0.0	0.0	8.400	0.0	0.0	0.0	0.0	0.0	17_ 84
(3)	X1	60.100	75.000	3944.000	4378.000	80.000	35.000	41.000	0.0	0.0	0.0	•
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	525.000	516.500	0.0	
	GR	574.800	1000.000	550.300	2496.000	550.300	2525.000	526.100	2534.000	520.600	2561.000	¹¹ • 1
	GR	520.400	2600.000	513.200	2669.000	517.500	2749.000	517.000	2835.000	517.500	2888.000	n
31	GR	519.600	2928.000	520.800	2949.000	520.300	2957.000	513.700	2977.000	506.900	2991.000	73
0	GR	504.900	2999.000	503.200.	3006.000	503.200	3007.000	503.200	3009.000	504.900	3013.000	
Part I	GR	509.000	3024.000	518.900	3058.000	517.500	3070.000	518.700	3096.000	519.700	3130.000	
•	GR	517.900	3151.000	515.900	3169.000	513.000	3178.000	503.200	3209.000	503.200 514.900	3230.000	25
	GR GR	513.000 512.700	3338.000 3483.000	514.200 512.400	3351.000 3539.000	515.400 512.000	3371.000 3596.000	515.500 511.500	3393.000 3654.000	510.900	3'22.000 3713.000	25
	GR	509.000	3751.000	507.200	3774.000	505.800	3813.000	505.100	3838.000	509.800	3867.000	
0	GR	511.100	3933.000	511.200	3944.000	511.200	3944.000	511.700	4064.000	511.100	4123.000	"*
17	GR	511.100	4123.000	509.600	4141.000	506,500	4160.000	506.000	4190.000	504.700	4212.000	
0	GR	502.500	4225.000	495.900	4262.000	495.900	4262.000	495.900	4295.000	495.900	4334.000	79,00%
	GR	495.900	4338.000	502.500	4364.000	505.900	4378.000	505.900	4378.000	507.400	4395.000	
5	GR	508.900	4440.000	509.700	4518.000	510.400	4560.000	512.400	4601.000	512.400	4618.000	
(2)	GR NH	514.200	4627.000	524.300	4633.000 0.039	550.000 4378.000	4668.000 0.060	560.600 4721.000	4694.000	575.300 0.0	4721.000	11
a	SB	3.000 1.200	0.100 1.500	2.900	0.039	467.000	74.000	6760.000	0.670	504.500	504.500	n I
6	080		1040000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			11.000	3,30,000				n_ *
9 17	X1	60.200	0.0	0.0	0.0	12.000	12.000	12.000	0.0	0.0	0.0	
9	X5	0.0	0.0	1.000	524.500	517.500	0.0	0.0	0.0	0.0	0.0	
	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	530.000	517.500	0.0	15 8
, a	BT	28.000	3012.000	537.900	0.0	3118.000 535.400	537.000	0.0 3357.000	3197.000 534.900	536.500	0.0 3457.000	и
33 [ET	3259.000 533.800	535.900	0.0 3569.000	3303.000 532.300	0.0	3668.000	531.700	0.0	3836.000	530.400	
(P)	BT	0.0	3944.000	530.000	511.200	3944.000	530.000	524.500	4123.000	529.600	524.100	"•1
91	BT	4123.000	529.600	520.600	4262.000	529.200	520.200	4262.000	529.200	521.700	4378.000	3 *
u u	BT	528.000	519.300	4378.000	528.000	505.900	4500.000	526.700	0.0	4653.000	525.300	19
9 *	BT	0.0	4817.000	523.300	0.0	4917.000	522.300	0.0	5056.000	520.600	0.0	
	BT	5105.000	519.700	0.0	5209.000	518.200	0.0	5276,000	517.500	0.0	5336.000	

										5000		The Control of the Co	
	81	517.500	0.0	5376.000	525.700	0.0	0.0	0.0	0.0	0.0	0.0	82	
3	NC	0.100	0.050	0.039	0.400	0.600	0.0	350.000	0.0	0.0	0.0		
	ET	0.0	0.0	0.0	0.0	9.100	0.0	> 0.0	0.0	3538.000	4375.000		
-	• •			2504 000	2000 000	304 000	49E 000	417.000	0.0	0.0	0.0		
0	X)	62.000	44.000	3596.000	3809.000	306.000 529.700	495.000 3488.000	529.700	3510.000	524.100	3518.000		
	GR	540.600	1000.000 3538.000	529.700 509.300	3488.000 3555.000	509.400	3583.000	509.700	3596.000	505.800	3604.000		
•	GR	511.200	3611.000	504.500	3615.000	504.500	3681.000	504.500	3739.000	505.000	3746.000		' 💣 i
	GR	505.500	3752.000	508.000	3781.000	507.900	3788.000	505.600	3792.000	505.600	3801.000		2
	GR	508.600	3809.000	509.300	3826.000	507.700	3845.000	505.500	3861.000	507.400	3872.000		
•	GR	511.200	3887.000	511.400	3911.000	512.500	3949.000	512.200	4012.000	511.200	4089.000		
	GR	511.200	4172.000	511.300	4253.000	510.200	4285.000	506.300	4313.000	506.200	4332.000		_ 1
	GR	505.800	4344.000	506.200	4352.000	506.200	4396.000	511.600	4428.000	511.600	4442.000		5
(a)	GR	513.500	4448.000	525.300	4463.000	549.300	4482.000	575.100	4512.000	0.0	0.0		
9	NC ·	0.100	0.060	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		•
10	ET	0.0	0.0	0.0	0.0	13.400	0.0	0.0	0.0	0.0	0.0		. 1
1 1				51.4	3665, 655	545 000	1100 000	F44 000	• •	0.0	0.0		
12	X1	63.000	58.000	3392.000	3623.000	545.000	1180.000	544.000.	0.0	511.800	3258.000		
	GR	535.400	3142.000	525.900	3161.000 3356.000	512.100 514.000	3187.000 3392.000	511.100 508.200	3217.000 3406.000	505.600	3411.000		'•
	GR	511.900	3317.000	513.800	3419.000	505.600	3423.000	507.000	3435.000	508.000	3447.000		10 .
	GR GR	505.000	3412.000	505.000 505.800	3493.000	505.000	3502.000	505.000	3540.000	505.000	3583.000		10
(2)	GR	505.800	3586.000	509.000	3596.000	512.300	3623.000	512.500	3678.000	511.000	3701.000		
	GR	511.200	3739.000	511.000	3787.000	509.800	3803.000	508.000	3810.000	507.200	3813.000		17
8	GR	508.000	3827.000	509.000	3845.000	508.300	3867.000	508.300	3883.000	510.300	3898.000		13 _
() 77	GR	513.600	3944.000	514.000	3975.000	513.200	4106.000	512.400	4287.000	511.900	4508.000		•
	GR	512.600	4646.000	512.400	4831.000	511.500	5003.000	511.300	5094.000	512.000	5162.000		14
2.0	GR	510.600	5208.000	507.300	5277.000	506.200	5295.000	507.900	5318.000	506.900	5352.000		15
(GR	507.000	5363.000	509.200	5373.000	509.200	5395.000	509.900	5402,000	525,200	5421.000		
7 × 1	GR	550.900	5444.000	567.500	5453.000	575.700	5465,000	0.0	0.0	0.0	0.0		· ·
2	NC	0.100	0.060	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		17
10 14	ET	0.0	\\0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0			18
2	٧,	64 000	E2 000	2562.000	2803.000	400.000	750.000	499.000	0.0	0.0	0.0		
(8.2	GR ·	64.000 539.000	52.000	539.000	2218.000	518.600	2244.000	514.800	2290.000	513.400	2424.000		"0"
	GR	511.700	2498.000	513.300	2520.000	512.000	2562.000	509.700	2588.000	508.100	2622.000		70
	GR	507.006	2634.000	505.300	2652.000	505.300	2700.000	505.300	2741.000	507.000	2754.009		71
()	GR	508.800	2768.000	511.100	2803.000	510.300	2861.000	511.100	2902.000	512.400	2969.000		•
r!	GR	511.000	3040.000	510.900	3110.000	510.200	3169.000	508.700	3209.000	506.700	3231.000	8	22
31	GR	511.100	3260.000	512.400	3310.000	515.100	3441.000	515.000	3563.000	515.400	3680.000		11 300
	GR	510.400	3774.000	509.600	3800.000	508.900	3819.000	509.700	3847.000	511.200	3908.000		
9	GR	511.100	3997.000	510.900	4095.000	510.100	4202.000	509.800	4271.000	509.600	4340.000		17
D .	GR	509.400	4363.000	508.900	4376.000	509.600	4385.000	509.900	4408.000	513.500	4420.000		25
	GR	513.500	4440.000	515.000	4448.000	527.300	4468.000	546.200	4515.000	546.200	4548.000		7.6
37	GR	554.900	4573,000	575.500	4627.000	0.0	0.0	0.0	0.0	0.0	0.0		
0	NC	0.060	0.060	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		"
	٧,	4E 800	83.000	2131.000	2313.000	392.000	325.000	380.000	0.0	0.0	0.0		78
43	X1 GR	65.000 569.800	1000.000	567.200	1052,000	564.800	1116.000	558.100	1214.000	551.800	1307.000		. 29
	GR	549.100	1381.000	545.900	1416.000	540.300	1435.000	543.200	1467.000	542.300	1508.000		
	GR	544.100	1532.000	544.100	1554.000	537.800	1576.000	532.800	1607.000	525.300	1656.000		30
- 46	GR	522.300	1675.000	523.900	1693.000	523.900	1711.000	520.200	1728.000	515.500	1766.000		31
	GR	513.900	1770.000	511.900	1778.000	511.000	1782.000	511.000	1788.000	511.000	1796.000		•
6.	GR	511.900	1797.000	515.700	1802.000	517.400	1814.000	517.900	1840.000	516.800	1868.000	and the same of th	31
e [GR	516.200	1947.000	515.700	2051.000	515.400	2105.000	510.600	2131.000	509.100	2135.000		33 (23)
	GR	507.500	2142.000	500.200	2174.000	500.200	2187.000	500.200	2187.000	507.500	2241.000		
	GR	508.900	2253.000	509.700	2279.000	511.000	2313.000	511.000	2368.000	511.700	2441.000		
22	GR	513.200	2508.000	512.400	2573.000	511.100	2634.000	512.500	2663.000	512.300	2782.000		15 🚗
	GR	514.000	2869.000	514.800	2987.000	514.900	3075.000	510.900	3134.000	509.500	3154.000		36
4	GR	510.200	3215.000	509.800	3260.000	511.100	3292,000	511.400	3405.000	511.800	3503.000		
51	GR	511.800	3595.000	510.400	3692.000	509.900	3754.000	509.000	3783.000	507.900	3795.000 3931.000		37
	GR	509.000	3810.000	509.500	3864.000	510.300	3900.000	514.300	3909.000	514.300	4022.000		18
	GR	515.000	3937.000	526.000	3954.000	536.000	3981.000	527.300	4012.000	524.600 556.400	4115.000		
	GR	527.500 557.300	4031.000	534.400	4046.000	550.200	4080.000	551.400	4095.000	0.0	0.0		39
•	GR		4132.000	569.400	4159.000	575.200	4178.000	0.0	0.0	0.0	NATIONAL PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PARTY OF THE		

					14.75 (6.45)				美国共享 。然此我	4.8.23	1465,655	00	
0	X1	66.000	82.000	1832.000	1995.000	350.000	337.000	350.000	0.0	0.0	120.0	83	
	GR	575.200	1000.000	572.000	1059.000	567.100	1123.000	563.700	1187.000	559.900	1262.000		
	GR	555.000	1327.000	549.700	1355.000	549.700	1381.000	547.400	1412.000	545.700	1454.000		_
•	GR	543.000	1482.000	535.100	1503.000	534.400	1540.000	530.000	1574.000	526.400	1585.000		
pro	GR	525.700	1605.000	523,900	1620.000	523.500	1626.000	520.800	1633.000	514.200	1645.000		
_ 1	GR	511.500	1650.000	510.500	1652.000	510.500	1659.000	510.500	1665.000	511.400	1666.000		1.0
	GR	514.000	1671.000	519.400	1680.000	519.400	1707.000	518.100	1717.000	516.900	1751.000		
	GR	516.600	1802.000	516.300	1832.000	512.300	1842.000	509.300	1850.000	508.000	1855.000		2
	GR	505.700	1863.000	505.700	1890.000	505.700	1890.000	508.000	1920.000	508.500	1929.000		344
•	GR	509.000	1962.000	510.500	1995.000	511.200	2039.000	512.000	2111.000	512.800	2158.000		•
	GR	513.200	2182.000	512.500	2235.000	512.200	2277.000	510.700	2318.000	515.500	2358.000		4
7	GR	517.400	2390.000	516.900	2437.000	516.500	2499.000	515.400	2556.000	513.300	2636.000		5.
(GR	511.900	2661.000	512.500	2739.000	512.500	2821.000	512.500	2912.000	512.400	3043.000		
	GR	512.100	3119.000	512.000	3241.000	511.600	3354.000	510.800	3410.000	510.100	3477.000		5 .
15	GR	509.800	3519.000	509.800	3541.000	509.600	3564.000	508.700	3571.000	509.200	3578.000		7
(t	GR	512.200	3593.000	515.900	3606.000	515.900	3623.000	518.800	3631.000	526.100	3645.000		
	GR	535.700	3669.000	544.000	3697.000	546.300	3736.000	549.700	3769.000	559.200	3809.000		THE
10	GR	569.900	3859.000	574.100	3881.000	0.0	0.0	0.0	0.0	0.0	0.0		1
	NC	0.070	0.070	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0		10
18	X1	67.000	89.000	2461.000	2664.000	635.000	400.000	680.000	0.0	0.0	0.0		
(IZ	GR	610.200	1000.000	606.200	1100.000	601.600	1167.000	596.800	1234.000	590.600	1303.000		•
18	GR	584.700	1364.000	574.100	1407.000	573.300	1474.000	570.500	1499.000	568.600	1510.000		12
19	GR	566.900	1517.000	566.100	1526.000	565.300	1533.000	558.100	1544.000	554.500	1562.000		
0 =	GR	554.600	1594.000	554.800	1608.000	549.100	1655.000	546.600	1684.000	541.700	1709.000		
	GR	537.500	1730.000	530.700	1738.000	530.700	1758.000	523.800	1773.000	524.000	1787.000		14
2	GR	515.800	1798.000	512.700	1805.000	512.000	1816.000	511.000	1822.000	512.000	1831.000		
(a) 23	GR	513.000	1840.000	515.000	1864.000	516.600	1882.000	516.600	1905.000	518.600	1927.000		•
21	GR	521.000	1964.000	515.700	1985.000	512.800	2008.000	512.700	2053.000	513.700	2085.000		16
45	GR	514.400	2123.000	514.800	2184.000	515.500	2214.000	515.500	2229.000	514.700	2240.000		
(0)	GR	514.200	2272.000	513.200	2314.000	510.300	2371.000	512.400	2390.000	511.600	2413.000		
v v	GR	512.600	2434.000	514.400	2461.000	512.900	2475.000	511.800	2496.000	510.100	2512.000		18
100	GR	506.000	2550.000	506.000	2574.000	506.000	2597.000	510.100	2638.000	511.300	2651.000		70
	GR	513.900	2664.000	514.300	2691.000	513.900	2740.000	513.500	2777.000	512.900	2822.000		
	GR	512.200	2874.000	511.900	2968.000	512.000	3056.000	512.800	3153.000	513.000	3236.000		20
ä	GR	513.700	3290.000	514,600	3373.000	514.700	3450.000	514.300	3542.000	514.700	3617.000		n
	GR	514.800	3672.000	515.200	3712.000	514.800	3737.000	514.700	3795.000	514.800	3861.000		
n	GR	515.300	3924.000	517.100	3948.000	517.100	3969.000	519.200	3978.000	525.800	3993.000		27
21	GR	540.500	4019.000	555.300	4045.000	567.300	4097.000	573.500	4121.000	0.0	0.0		73
	NC	0.075	0.045	0.042	0.100	0.300	0.0	0.0	0.0	9.0.0	0.0		•
18	E7	0.0	0.0	0.0	0.0	12.400	0.0	0.0	0.0	0.0	0.0		24
-		40.000		2127 222	2227 000	300 000	1150 000	725 000	0.0	0.0	0.0		25
	GR GR	63.000	68.000	2127.000	2327.000	300.000 593.400	1150.000 1085.000	725.000 585.700	1125.000	575.500	1169.000		26
		600.000	1000.000	597.500	1048.000			555.400	1283.000	553.900	1299.000		
14	GR	555.200	1205.000	555.200	1242.000	557.800	1262.000	521.600	1347.000	521.500	1363.000		"0
/	GR GR	550.400	1312.000	538.000	1324.000	526.700	1340.000	513.400	1420.000	512.600	1428.000		79
66	GR	523.200	1375.000	520.600	1391.000	515.300 514.000	1414.000	513.400	1454.000	512.700	1460.000		
	GR	512.000 513.900	1433.000	512.600	1438.000 1491.000	516.200	1534.000	516.000	1604.000	515.900	1659.000		"•
- 6	GR			515.400		515.300	1785.000	515.300	1846.000	515.800	1888.000		39
, L		515.500	1700.000	515.600	1738.000				2127.000	513.300	2162.000		
	GR GR	516.600	1956.000	516.200 513.000	2023.000	515.600 506.500	2071.000 2250.000	514.800 513.000	2287.000	513.900	2295.000		"0
41	GR	513.200 515.500	2199.000	515.900	2390.000	516.200	2459.000	516.200	2547.000	515.700	2627.000		32
45	GR	516.000	2677,000	516.200	2778.000	516.400	2856,000	516.600	2959.000	516.700	3056.000		
					3118.000	521.000	3150.000	523.900	3160.000	523.900	3171.000		37
	GR GR	517.300	3080.000	518.000	3189.000	536.400	3209.000	549.100	3221.000	574.500	3266.000		34
		523.900	3179.000	524.800		626.000	3386.000	0.0	0.0	0.0	0.0		
(A)	GR	599.800	3307.000	616.400	3343.000			0.0	0.0	0.0	0.0		35
	NC	0.100	0.055	0.042	0.100	0.300	0.0		0.0	0.0	0.0		38
86	ET	0.0	0.0	0.0	0.0	9.400	0.0	0.0	0.0	0.0	1400 000		77
	X1	69.000	74.000	1851.000	2191.000	220.000	378.000	425.000	0.0	0.0	0.0		
я	GR	599.700	1000.000	593.500	1047.000	585.100	1092.000	575.900	1121.000	565.400	1146.000		38
. 58	GR	560.800	1150.000	560.400	1175.000	556.600	1189.000	555.900	1202.000	551.700	1213.000		14
	GR	546.500	1224.000	524.800	1253.000	520.900	1293.000	520.900	1322.000	520.900	1341.000		0
Bridge H	GR	517.000	1363.000	515.200	1382.000	514.300	1393.000	513.600	1398.000	513.000	1404.000		

												^ 4
	GR	513.600	1409.000	514.200	1415.000	515,300	1429.000	515.600	1453,000	515.300	1468.000	84
•	GR	513.900	1480.000	513.400	1489.000	514.500	1496.000	515.400	1500.000	515.400	1524.000	
	GR	518.500	1548.000	520.400	1570.000	520.700	1591.000	519.500	1621.000	519.200	1543.000	
	GR	517.900	1704.000	517.200	1751.000	516.400	1772.000	516.500	1802.000	517.100	1825.000	
	GR	516.900	1851.000	515.600	1862.000	514.500	1876.000	513.000	1896.000	513.000	2019.000	
	GR	513.000	2153.000	514.500	2164.000	514.900	2167.000	517.000	2191.000	518.000	2252.000	
	GR	519.000	2305.000	519.000	2366.000	518.700	2444.000	518.400	2516.000	517.900	2612.000	
	GR	518.300	2725.000	518.900	2767.000	519.400	2854.000	520.500	2941.000	522.500	2983.000	· • •
	GR	525.500	3029.000	530.700	3050.000	531.000	3062.000	532.200	3076.000	539.100	3094.000	2 8
	GR	551.100	3124.000	551.300	3183.000	560.200	3220.000	561.300	3261.000	572.100	3280.000	
•	GR	574.400	3302.000	584.800	3338.000	597.000	3380.000	599.100	3406.000	0.0	0.0	
	NC	0.100	0.055	0.042	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
	ET	0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	7 0 0 0	0.0	
(a)												
No.	X1	70.000	79.000	1960.000	2114.000	640.000	920.000	641.000	0.0	0.0	0.0	•
14	GR	600.200	1000.000	593.600	1020.000	584.800	1033.000	583.900	1056.000	557.800	1080.000	1_
(t	GR	557.800	1095.000	556.400	1103.000	550.400	1120.000	537.400	1150.000	522.400	1177.000	
	GR	520.500	1190.000	516.100	1195.000	515.100	1202.000	514.200	1209.000	515.100	1214.000	
13	GR	516.200	1226.000	517.200	1259.000	518.100	1300.000	520.400	1331.000	520.900	1381.000	1
W H	GR	520.700	1430.000	520.000	1464.000	519.300	1497.000	521.500	1519.000	521.500	1530.000	,
19	GR	515.300	1550.000	516.100	1573.000	51.7.000	1596,000	521.100	1638.000	522.100	1720.000	" a
	GR	521.900	1786.000	521.500	1850.000	519.500	1880.000	515.600	1897.000	517.100	1906.000	11
□ 1	GR	520.000	1918.000	520.600	1932.000	521.100	1953.000	520.600	1960.000	516.800	1969.000	12
	GR	515.400	1975.000	510.000	2000.000	510.000	2032.000	510.000 518.800	2066.000	515.400 516.800	2089.000	
•	GR	517.400	2098.000	520.300	2114.000	516.200	2139.000	515.900	2264.000	517.200	2274.000	\ " \
	GR	516.700	2234.000	516.000	2241.000	514.700 521.500	2255.000 2411.000	521.800	2503.000	522.000	2611.000	in the second se
	GR	520.000	2299.000	520.800	2335.000	522.200	2971.000	522.500	3063.000	523.000	3157.000	
•	GR GR	522.100	2732.000	522.000	2859.000 3239.000	526.200	3254.000	526.200	3262.000	529.700	3273.000	15
	GR	522.700 540.900	3209.000 3284.000	526.200 550.200	3303.000	557.200	3338.000	564.000	3371.000	575.500	3419.000	16
15	GR	577.000	3439.000	585.200	3464.000	591.600	3486.000	598.400	3503.000	0.0	0.0	
	NC	0.060	0.050	0.042	0.100	0.600	0.0	0.0	0.0	0.0	0.0	" a _
77	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1850.000	2900.000	13 8
21			1254.054			Section Section						
(a	X1	71.000	47.000	2253.000	2467.000	480.000	440.000	501.000	0.0	0.0	0.0	"•
	GR	599.100	1000.000	592.700	1041.000	584.600	1058.000	584.600	1079.000	576.000	1087.000	20
	GR	560.900	1106.000	560.900	1115.000	556.200	1127.000	545.600	1149.000	535.500	1181.000	21
() :	GR	525.500	1207.000	525.500	1300.000	525.500	1500.000	525.500	1800.000	525.500	2198.000	
	GR	525.500	2209.000	520.600	2218.000	516.500	2230.000	515.300	2233.000	516.500	2245.000	n ·
4	GR	517.300	2253.000	517.000	2263.000	516.500	2272.000	512.500	2341.000	512.500	2367.000	77
	GR	512.500	2435.000	516.500	2457.000	518.300	2467.000	520.800	2497.000	521.900	2530.000	
35	GR	522.400	2581.000	522.900	2641.000	523.000	2725.000	522.900	2799.000	523.100	2858.000	- 24
27	GR	523.100	2922.000	523.400	3063.000	523.700	3166.000	523.900	3273.000	526.400	3287.000	25
0 :	GR	526.400	3307.000	528.600	3315.000	548.500	3346.000	563.200	3374.000	578.200	3398.000	•
7.1	GR	590.500	3443.000	600.200	3477.000	0.0	0.0	0.0	0.0	0.0	0.0	18
ap ap	NC	0.060	0.050	0.044	0.100	0.300	0.0	0.0	0.0	0.0	0.0	77
00	ET	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	
*				A 2 - 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			100 000					"
	X1	72.000	64.000	2430.000	2718.000	410.000	734.000	790.000	0.0	0.0	0.0	n _o
	GR	600.100	1000.000	588.400	1014.000	577.900	1032.000	578.800	1048.000	560.900	1064.000	M
40	GR	560.900	1074.000	555.300	1086.000	544.500	1106.000	527.100	1123.000	527.100	2289.000	
	GR	527.100	1400.000	527.100	1700.000	527.100	2000.000	527.100	2278.000	526.300	2362.000	11
	GR	521.600	2312.000	521.300	2335.000	518.700	2352.000	516.000	2359.000	515.000 522.000	2430.000	77
	GR	515.000	2392.000	516.000	2396.000	517.400	2403.000	520.800 512.300	2484.000	519.000	2524.000	
	GR	520.400	2438.000	519.400	2445.000	519.000	2450.000	518.400	2554.000	519.000	2577.000	»
	GR	519.700	2531.000	519.700	2538.000	519.000	2546.000		2669.000	518.200	2703.000	ц.
	GR	519.500	2596.000	519.500	2624.000	519.500	2649.000	519.000	2773.000	519.400	2801.000	. /
	GR	519.000	2710.000	519.900	2718.000	520.600	2748.000	520.600 519.900	2869.000	523.700	2905.000	35
	GR	519.000	2820.000	518.400	2847.000	519.000	2856.000		3231.000	525.200	3307.000	36
	GR	523.800	2952.000	523.900	3043.000	524.200	3143.000	524.600 529.700	3384.000	550.000	3402.000	
	GR	525.900	3350.000	528.100	3362.000	528.100 590.800	3476.000	599.400	3508.000	0.0	0.0	"@]
	GR	564.100	3420.000	580.500	3445.000	0.300	0.0	0.0	0.0	0.0	0.0	и .
	NC	0.050	0.060	0.039	0.100	0.300	V•V	0.0	V.			
	V1	73.000	56.000	2690.000	2855.000	950.000	490.000	575.000	0.00	0.0	0.0	3
STATE OF THE PARTY	K1 GR	575.500	1000.000	569.500	1013.000	569.500	1023.000	564.400	1035.000	558.100	1047.000	

	GR	558.100	1056.000	549.100	1067.000	540.800	1088.000	536.600	1096.000	530,900	1106 000		
•	GR	530.900	2446.000	525.300	2462.000	523.800	2474.000	519.700	2493.000	517.400	1106.000 2500.000	85	
	GR	516.400	2503.000	516.400	2525.000	517.400	2537.000	518.300	2547.000	521.200	2575.000	OU	
	GR	521.700	2614.000	521.000	2657.000	520.900	2690.000	520.200	2705.000	517.000	2773.000		
	GR	517.000	2773.000	517.000	2793.000	520.200	2834.000	521.800	2855.000	521.900	2906.000		•
	GR	522.000	2966.000	523.100	3036.000	520.800	3080.000	521.500	3114.000	520.200	3154.000		
d d	GR	518.500	3206.000	520.200	3246.000	521.200	3285.000	521.300	3325.000	520.300	3371.000		3
•	GR	519.400	3388.000	524.700	3406.000	525.700	3457.000	526.000	3537.000	525.800	3624.000		
	GR	526.000	3747.000	526.200	3853.000	526.900	3951.000	527.400	3978.000	530.200	3999.000		2 2
	GR	530.200	4015.000	530.700	4022.000	550.200	4034.000	575.100	4063.000	584.800	4081.000		- 5
•	GR	600.400	4098.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		•
	NC	0.050	0.060	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		4
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2291.000	3436.000		
							1,700,304	See The see	- 12-1 THE		1.14		`●
9	XI	74.000	58.000	2556.000	2796.000	970.000	230.000	640.000	0.0	0.0	0.0		6
10	GR	574.500	1000.000	566.200	1040.000	561.600	1052.000	560.100	1089.000	558.600	1161.000		
(11 ·	GR	557.200	1209.000	556.500	1229.000	556.500	1291.000	556.500	1414.000	555.800	1491.000		•
n_	GR	555.400	1595.000	552.300	1660.000	549.000	1716.000	526.200	1750.000	526.200	1933.000		
- 13	GR	526.400	2014.000	526.900	2079.000	525.600	2096.000	525.900	2120.000	526.300	2154.000		
€ 14	GR	526.600	2205.000	525.900	2291.000	525.400	2402.000	524.900	2493.000	521.000	2510.000		9
8	GR	521.900	2536.000	523.200	2556.000	522.700	2562.000	521,000	2568.000	518.400	2576.000		10
14	GR	518.400	2656.000	518.400	2721.000	521.000	2738.000	523.100	2752.000	525.500	2796.000		11_
O P	GR	525.100	2839.000	520.700	2883.000	521.000	2909.000	524.700	2943.000	525.600	2969.000		9
	GR	524.400	2999.000	520.900	3029.000	525.500	3063.000	525.700	3104.000	525.800	3173.000		12
0	GR GR	526.200	3262.000	526.500	3366.000	526.900	3465.000	527.300	3574.000	527.800	3698.000		13
	GR	530.300	3789.000	531.000	3804.000	531.000	3821.000	531.900	3828.000	538.800	3835.000		
		549.800	3849.000	574.400	3890.000	600.900	3917.000	0.0	0.0	0.0	0.0		
(A)	NC ET	0.050	0.055	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		15
	155	0.0	0.0	0.0	0.0	5.400	0.0	0.0	0.0	0.0	0.0		15
21	X1	75.000	57.000	2589.000	2803.000	790.000	320.000	640.000	0.0	0.0	0.0		
(n	Х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		• • •
20	GR	600.900	1000.000	590.300	1043.000	583,900	1061.000	579.100	1074.000	577.000	1094.000		12 12
74	GR	571.500	1134.000	562.800	1157.000	565.300	1180.000	562.300	1241.000	560.200	1260.000		19 2
	GR	557.400	1326.000	555.300	1404.000	552.200	1501.000	551.000	1621.000	550.500	1711.000		
	GR	550.200	1769.000	550.300	1771.000	550.700	1805.000	550.500	1946.000	549.300	1986.000		
12	GR	545.200	2023.000	534.300	2072.000	532.100	2085.000	532.100	2100.000	532.100	2150.000		21
	GR	532.100	2174.000	530.600	2206.000	530.300	2282.000	528.500	2397.000	527.200	2504.000		
70	GR	528.200	2569.000	529.400	2589.000	525.700	2601.000	524.000	2607.000	521.500	2612.000)**
(2)	GR GR	516.000	2623.000	516.000	2702.000	516.000	2759.000	521.500	2790.000	523.900	2803.000		23
	GR	526.300 527.400	2834.000 3460.000	526.600 528.000	2906.000 3479.000	526.800 528.000	3009.000	527.100 529.400	3167.000	527.200 530.000	3316.000		24
p. [7]	GR	531.600	3630.000	531.700	3646.000	534.200	3500.000 3672.000	535.000	3553.000 3679.000	545.200	3605.000 3699.000		
(0)	GR	554.500	3715.000	571.000	3740.000	0.0	0.0	0.0	0.0	0.0	0.0		25
я .	NC	0.040	0.040	0.039	0.300	0.500	0.0	0.0	0.0	0.0	0.0		76
- 5	ET	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		
						-0.700	•••		٠.٠	٠.٠			
在	X1	77.010	48.000	2343.000	2573.000	120.000	150.000	130.000	0.0	0.0	0.0		79
0	X	10.000	0.0	0.0	0.0	0.0	0.0	0.0	531.500	530.200	0.0		79
0"	GR	625.300	1000.000	610.500	1049.000	598.400	1086.000	586.200	1125.000	580.300	1135.000		
- 6	GR	580.300	1144.000	547.100	1199.000	550.300	1226.000	550.300	1267.000	548.800	1276.000		30
	GR	553.200	1313.000	553.100	1391.000	551.700	1491.000	549.700	1548.000	549.700	1574.000		31
()	GR	549.800	1610.000	546.500	1647.000	545.900	1706.000	543.500	1746.000	535.500	1783.000		•
4	GR	531.000	1904.000	528.600	1970.000	528.200	2094.000	528.500	2262.000	533.800	2290.000		32 3
- 6	GR	533.800	2309.000	530.800	2343.000	523.700	2363.000	522.000	2367.000	517.500	2380.000		33
(P 50	GR	517.500	2450.000	517.500	2503.000	522,000	2530.000	523.600	2540.000	524.600	2573.000		
	GR	525.400	2637.000	525.900	2754.000	526.100	2882.000	526.600	3099.000	526.900	3158.000		34 5
10	GR	527.200	3252.000	528.900	3276.000	542.200	3309.000	549.700	3332.000	562.900	3349.000		35 8
•	GR	574.700	3364.000	584.200	3378.000	600.100	3391.000	0.0	0.0	, 0.0	0.0		Bus
	SB	0.900	1.500	3.000	0.0	160.000	6.000	3320.000	5.000	517.500	517.500		36
(3) 10	X1	77.020	0.0	0.0	0.0	50.000	50.000	50.000	0.0	0.0	0.0		37 Om
9	X5	0.0	0.0	1.000	535.100	530.700	0.0	0.0	0.0	0.0	0.0		35 >
. 18	X3	10.000	0.0	. 0.0	0.0	0.0	0.0	0.0	532.000	530.700	0.0		
0	BT	23.000	1614.000	545.500	0.0	1686.000	542.000	0.0	1746.000	539.700	0.0		
	BT	1796.000	537.400	0.0	1870.000	535.600	0.0	1950.000	534.600	0.0	2025.000		

												9.0	
_	BT	532.800	0.000	2085.000	532.000	0.0	2225.000	534.700	0.0	2384.000	539.000	00	
	BT	0.0	2487.000	539.000	0.0	2607.000	539.000	0.0	2786.000	537.400	0.0		
	BT	2984.000	534.900	0.0	3144.000	533.600	0.0	3223.000	533.100	0.0	3285.000		
-	ВТ	532.800	0.0	3354.000	531.100	0.0	3403.000	531.000	0.0	3506.000	530.700		
	BT	0.0	3516.000	530.700	0.0	3527.000	532.500	0.0	3553.000	549.000	0.0		
	NC	0.040	0.040	0.039	0.300	0.500	0.0	0.0	0.0	0.0	0.0		
	ET	0.0	0.0	0.0	0.0	18.400	0.0	0.0	0.0	0.0	0.0		
•					J				4.4	1,4			
	XI	77.000	48.000	2343.000	2'573.000	80.000	40.000	60.000	0.0	0.0	0.0		2 0
(2)	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
	GR	625.300	1000.000	610.500	1049.000	598.400	1086.000	586.200	1125.000	580.300	1135.000		•
	GR	580.300	1144.000	547.100	11.99.000	550.300	1226.000	550.300	1247.000	548.800	1276.000		
•	GR GR	553.200 549.800	1313.000	553.100	1391.000	551.700	1491.000	549.700	1548.000	549.700	1574.000		5.
	GR	531.000	1610.000	546.500	1647.000	545.900	1706.000	543.500	1746.000	535.500	1783.000		
	GR	533.800	2309.000	528.600 530.800	1970.000 2343.000	528.200 523.700	2094.000	528.500	2262.000	533.800	2290.000		
a 0	GR	517.500	2450.000	517.500	2503.000	522.000	2363.000	522.000 523.600	2367.000	517.500	2380.000		1
n in	GR	525.400	2637.000	525.900	2754.000	526.100	2882.000	526.600	2540.000 3099.000	524.600 526.900	2573.000 3158.000		
n[]	GR	527.200	3252.000	528.900	3276.000	542.200	3309.000	549.700					
(14 Ja	GR	574.700	3364.000	584.200	3378.000	600.100	3391.000	0.0	3332.000	562.900 0.0	3349.000		'0
15	NC	0.040	0.040	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		10
16	ET	0.0	0.0	0.0	0.0	15.400	0.0	0.0	0.0	0.0	0.0	- n	
		1000	1116,000	537,435	1024.000	989,400	1148,199	386,800	1000	538,853	1368, 968		".
9	X1	78.000	45.000	1739.000	1955.000	740.000	710.000	735.000	0.0	0.0	0.0		12
19	GR	600.000	1000.000	575.000	1033.000	549.900	1071.000	537.500	1096.000	537.500	1100.000		
() E	GR	537.500	1150.000	537.500	1158.000	536.800	1166.000	534.900	1183.000	534.900	1216.000		
地	GR	532.700	1220.000	528.300	1232.000	526.800	1262.000	527.300	1320.000	527.300	1368.000		14
12	GR	527.900	1412.000	527.000	1457.000	527.400	1509.000	529.200	1564.000	530.100	1658.000		16
	GR	530.000	1721.000	527.900	1739.000	525.000	1754.000	521.600	1768.000	522.900	1780.000		
	GR	521.200	1787.000	519.300	1795.000	519.300	1872.000	519.300	1940.000	521.200	1945.000		16
	GR	524.300	1955.000	526.200	1984.000	525.800	2056.000	526.000	2126.000	525.100	2214.000		17
19 19	GR	525.100	2269.000	526.600	2327.000	529.000	2396.000	529.000	2464.000	529.300	2507.000		9,7
-	GR	529.900	2548.000	530.000	2563.000	550.700	2593.000	575.100	2625.000	600.000	2655.000		II Z.R
(a)	FT	0.0	0.0	0.0	0.0	16.400	0.0	0.0	0.0	0.0	0.0		19
	X1	79.000	40,000	1602.000	1823.000	755.000	620.000	710 000	0.0	0.0	0.0		10
34	GR	600.000	1000.000	575.000	1070.000	550.600	1132.000	710.000	0.0	0.0	0.0		
(22 m	GR	536.100	1203.000	536.000	1227.000	533.400	1248.000	536.100 533.000	1168.000	536.100 530.100	1184.000		21
11	GR	529.200	1411.000	529.200	1464.000	531.000	1531.000	531.000	1597.000	530.100	1342.000 1602.000		21
34	GR	525.000	1610.000	522.000	1626.000	520.200	1636.000	520.200	1684.000	520.200	1711.000		
0	GR	522.000	1753.000	522.500	1764.000	523.500	1792.000	526.200	1823.000	523.700	1844.000		11
35	GR	523.900	1854.000	529.500	1885.000	530.700	1907.000	529.400	1950.000	529.500	2015.000		34
	GR	530.000	2063.000	529.800	2109.000	529.100	2152.000	528.000	2197.000	528.700	2257.000		
9 2	GR	529.600	2294.000	530.100	2308.000	550.300	2343.000	575.300	2380.000	600.100	2428.000		15
10	NC	0.040	0.040	0.043	0.100	0.300	0.0	0.0	0.0	0.0	0.0		26
19	FT	0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	0.0	0.0		27
(A			3,150	0.051									•
42	X1	80.000	32.000	1449.000	1767.000	460.000	412.000	430.000	0.0	0.0	0.0		78
13	GR	600.000	1000.000	575.000	1064.000	550.000	1125.000	539.000	1142.000	539.000	1152.000		79
•	GR	539.000	1178.000	535.000	1198.000	533.400	1261.000	532.000	1329.000	531.000	1366.000		
*12	GR	531.400	1420.000	531.400	1449.000	525.000	1463.000	522.700	1476.000	518.800	1499.000		28
	GR	518.800	1527.000	518.800	1688.000	522.700	1718.000	523.900	1728.000	525.200	1737.000		31
	GR	527.400	1767.000	529.400	1792.000	531.700	1802.000	531.900	1846.000	529.400	1898.000		
	GR	527.900	1918.000	527.100	1936.000	529.800	1953.000	530.500	1963.000	564.400	1997.000		12 0
0	GR	588.700	2025.000	600.000	2045.000	0.0	0.0	0.0	0.0	0.0	0.0		13.0
	NC	0.040	0.090	0.043	0.100	0.300	0.0	0.0	0.0	0.0	0.0		1,9
	E!	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1424.000	1815.000		J" ;
0	X1	91 000	36 000	1434 000	101E 000	365 000	240.000	250 000					35 70
	X3	81.000	36.000	1424.000	1815.000	365.000	340.000	350.000	0.0	0.0	0.0		, 1
5 [3	GR	10.000	1000 000	0.0 575 100	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
0	GR	539.800	1000.000	575.100 539.800	1086.000	572.600 537.900	1108.000	554.400	1133.000	554.500	1155.200		31
2	GR	531.700	1304.000	530.500	1356.000	531.600	1222.000	535.900	1235.000	534.800	1273.000		32 >
20	GR	524.800	1451.000	523.500	1455.000	523.500	1405.000	534.400 524.800	1424.000	530.500	1431.000		
	GR	527.100	1511.000	528.800	1533.000	524.800	1549.000	523.500	1483.000 1554.000	525.400 523.500	1491.000 1625.000		. 37
	GR	523.500	1690.000	524.800	1768.000	525.000	1780.000	527.600	1797.000	529.300	1815.000		

									· /				AND DESCRIPTION OF THE PARTY OF
-	GR	532.200	1845.000	534.000	1867.000	534.500	1880.000	550.000	1915.000	575,000	1951.000	8/	
	GR	600.000	1997.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
	NC	0.040	3000.090	0.043	0.100	0.300	0.0	0.000	0.0	0.0	0.0		
(B)	NH	5.000	0.075	1432.000	0.045	1507.000	0.090	1582.000	0.041	1738.000	0.100		
	NH	1842.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		•
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1265.000	1738.000		
17		2004000											1
	X1	82.000	33.000	1582.000	1738.000	690.000	660.000	685.000	0.0	0.0	0.0		, e
	GR	600.100	1000.000	586.800	1038.000	574.500	1068.000	558.000	1114.000	543.800	1141.000		2 05
6	GR GR	544.100	1168.000	535.800	. 1198.000	535.800	1220.000	535.800	1268.000	535.700	1310.000		, ,
	GR	535.700	1355.000	529.700	1376.000	527.700	1411.000	529.100	1422.000	527.900	1432.000		•
	GR	526.200	1446.000	523.100	1471.000	526.200	1497.000	527.300	1507.000	527.900	1520.000		,
A	GR	526.800 522.800	1548.000	529.700	1582.000	527.200	1607.000	526.200	1624.000	522.800	1673.000		150
	GR	550.100	1673.000	522.800	1727.000	526.200	1733.000	528.500	1738.000	537.800	1764.000		9
16	NC	0.055	0.100	575.400 0.039	1807.000	600.600	1842.000	0.0	0.0	0.0	0.0		6
(A)	NH	5.000	0.055	1124.000	0.100	0.300	0.0	0.0	0.0	0.0	0.0		7
	NH	2058.000	0.0	0.0	0.045	1212.000	0.100	1865.000	0.039	1990.000	0.100		
	ET	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0		
(II	100		•	•••	0.0	9.100	0.0	0.0	0.0	1135.000	1990.000		1_1
12	X1	83.000	44.000	1865.000	1990.000	935.000	957.000	950.000	0.0	0 0	0.0		
H	GR	600.300	1000.000	598.000	1015.000	569.700	1039.000	552.600	0.0 1070.000	0.0 552.600	0.0		10
	GR	537.600	1115.000	537.600	1124.000	528.000	1140.000	528.000	1149.000	528.000	1092.000	. /	11.
	GR	528.000	185.000	528.900	1188.000	534.500	1212.000	535.400	1250.000	535.300	1284.000		11
19	GR	535.400	1312.000	536.400	1327.000	534.600	1349.000	527.000	1362.000	524.500	1366.000		
(TS	GR	527.000	1381.000	528.900	1392.000	532.300	1432.000	532.000	1465.000	527.800	1489.000		
- 22	GR	527.800	1505.000	532.800	1529.000	531.800	1566.000	532.300	1592.000	532,700	1636.000		14
22	GR	533.200	1659.000	533.300	1713.000	532.900	1770.000	531.500	1833.000	532.800	1865.000	~	Take and the same
•	GR	527.000	1878.000	523.000	1888.000	523.000	1923.000	523.000	1954.000	527.000	1966.000		15
94	GR	528.900	1971,000	534.200	1990.000	550.400	2030.000	575.300	2058.000	0.0	0.0		14
23	NH	5.000	r.085	1260.000	0.045	1338.000	0.100	1992.000	0.041	2191.000	0.100		
(B	NH	2268.000	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		"•_
17	ET	0.0	0.0	0.0	0.0	9,100	0.0	0.0	0.0	1175.000	2191.000		18 19
4		541,560							1646,460	5,0			REA
(a	X1	84.000	53.000	1992.000	2191.000	490.000	730.000	700.000	0.0	0.0	0.0		, e
	GR	600.800	1000.000	574.400	1040.000	550.100	1084.000	544.100	1099.000	544.100	1130.000		73
	GR	538.100	1158.000	536.700	1170.000	534.600	1195.000	532.800	1232.000	533.100	1260.000		21
	GR	530.000	1274.000	529.100	1290.000	528.400	1302.000	529.100	1309.000	530.500	1325.000		
	GR	531.700	1338.000	533.800	1361.000	532.100	1369.000	534.400	1387.000	533.600	1408.000		22
(A)	GR GR	535.500	1427.000	535.700	1458.000	535.400	1481.000	530.700	1488.000	531.700	1499.000		73
	GR	534.400 534.000	1522.000	534.300	1564.000	533.200	1608.000	532.200	1620.000	534.000	1642.000		
n f	GR		1692.000	532.900	1729.000	530.500	1748.000	533.200	1771.000	533.900	1790.000		24
12	GR	533.300 535.800	1826.000	532.000	1842.000	534.500	1869.000	536.300	1891.000	536.400	1930.000		25
30	GR	525.000	2118.000	534.300 525.000	1992.000	529.700	2003.000	528.000	2010.000	525.000	2022.000		
4	GR	550.100	2228.000	575.400	2173.000	528.000 599.600	2178.000	529.900	2181.000	532.800	2191.000		
(2) (1)	NC	0.090	0.100	0.041	0.100	0.300	2268.000	0.0	0.0	0.0	0.0		27
Al	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	0.0 1260.000	0.0 2255.000		79
- 0				Teratria a series	0.0	9.100	0.0	0.0	0.0	1200.000	2233.000		
() H	X1	85.000	58.000	2026.000	2255.000	210.000	250.000	245.000	0.0	0.0	0.0		29
45	GR	599.600	1000.000	574.400	1042.000	548.600	1096.000	548.200	1106.000	544.300	0.0	/ /	30
	GR	542.000	1147.000	542.000	1158.000	542.000	1191.000	535.200	1200.000	534.500	1219.000	//	
0	GR	530.400	1230.000	538.700	1243.000	537.000	1268.000	534.300	1291.000	534.700	1343.000		51
	GR	535.400	1425.000	534.900	1465.000	533.700	1496.000	535.100	1518.000	536.200	1529.000		32
47	GR	533.000	1544.000	532.000	1567.000	531.200	1576.000	530.400	1585.000	531.200	1593.000		×
() ·	GR	532.900	1611.000	534.000	1658.000	534.500	1719.000	531.900	1752.000	531.300	1781.000		u e
11	GR	530.700	1806.000	531.300	1810.000	532,600	1818.000	534.700	1848.000	535.900	1888.000		34
- 52	GR	534.500	1914.000	533.500	1928.000	535.600	1948.000	536.100	1977.000	534.700	1997.000		Uan
(S)	GR	536.000	2020.000	534.800	2026.000	530.700	2035.000	529.100	2046.000	526.500	2063.000		20 00
31	GR	526.500	2099.000	526.500	2125.000	529.100	2148.000	530.100	2156.000	532.500	2174.000		36
14	GR	532.200	2189.000	530.000	2208.000	529.300	2224.000	530.100	2236.000	534.000	2255.000		. /3
() a	GR	551.600	2294.000	574.200	2329.000	600.100	2366.000	0.0	0.0	0.0	0.0		3/01
21	NC	0.070	0.110	0.038	0.100	0.300	0.0	0.0	0.0	0.0	0.0		38 >
53	NV	6.000	0.038	534.000	0.038	541.000	0.042	543.000	0.042	543.800	0.040		
	NV	543.900	0.040	560.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		10
	ET	0.0	0.0	0.0	0.0	9,100	0.0	0.0	0.0	1265.000	1915.000		

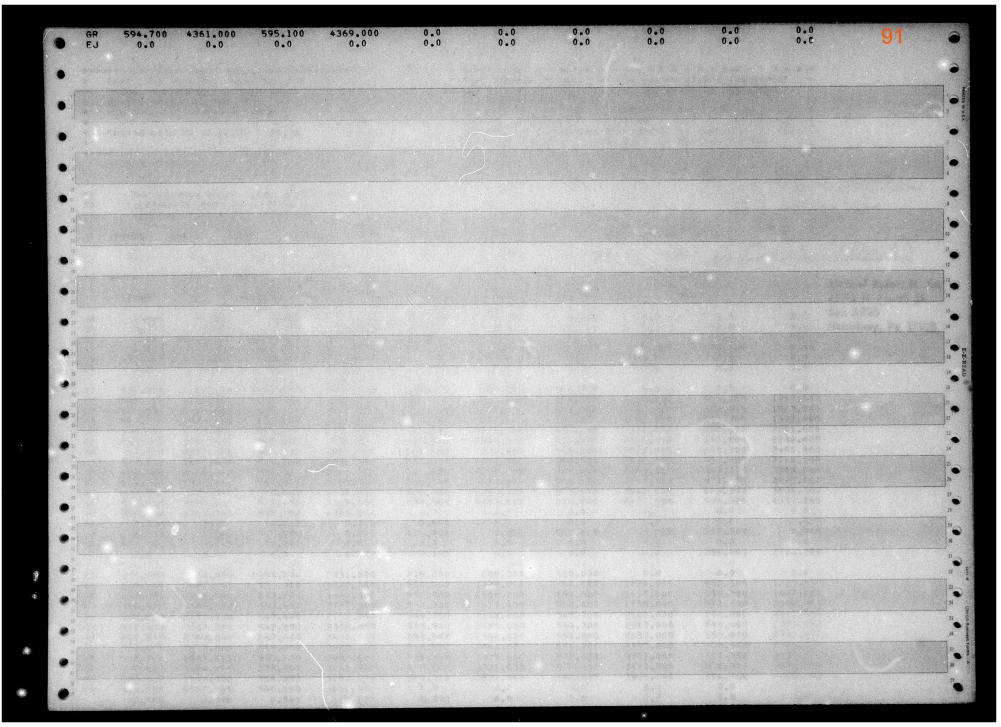
	Constitution of Car		STATE OF THE PARTY	CAR ENGINEERING AND ADVISOR TO SEASON	MANAGEMENT STATES AND TOWNS AND THE STATES AND THE			and the second second second second second	Management and a security of the control of the security of th	Carlottanon como como como como como como como c	The second secon	THE RESERVE AND THE PROPERTY AND THE PARTY A	ale maissairme-mir m
		大阪海水工作的	1984,660	538,608			10000		1954, 390	537.765		88	
	XI	86.000	31.000	1777.000	1915.000	1038.000	895.000	905.000	0.0	0.0	1700.000	00	•
	GR	600.100	1000.000	575.500	1046.000	568.100	1064.000	554.600	1082.000	554.600	1107.000		
	GR	536.100	1149.000	535.900	1161.000	535.100	1167.000	536.100					
•	GR	536.200							1174.000	536.000	1257.000		-
			1318.000	539.100	1333.000	536.000	1343.000	536.000	1437.000	535.500	1527.000		
	GR	534.700	1581.000	534.100	1612.000	535.700	1646.000	537.100	1711.000	537.100	1757.000		
	GR	533.500	1777.000	532.100	1812.000	531.000	1833.000	526.500	1871.000	531.000	1908.000		30
	GR	533.200	1915.000	551.100	1955.000	562.900	1986.000	564.200	2001.000	575.300	2025.000		, e
	GR	600.500	2083.000	7.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		7 0
	NC	0.060	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
	NV	6.000	0.038	536.000	0.038	542.000	0.042	542.500	0.042	544.400	0.040		3 🚗
	NV	544.500	0.040	560,000	0.0	0.0							
	ET	0.0					0.0	0.0	0.0	0.0	0.0		
	51	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1276.000	1919.000		5
	XI	87.000	27.000	1623.000	1919.000	250.000	260.000	270.000	0.0	0.0	0.0		4
	GR	600.400	1000.000	574.400	1035.000	558.800	1065.000	558.800	1090.000	536.800	1132.000		1.
	GR	536.000	1144.000	535.600	1152.000	536.000	1160.000	535.500	1252.000	535.900	1328.000		•
	GR	540.700	1350.000	540.700	1358.000	535.500	1371.000	535.900	1501.000	536.400	1574.000		
13	GR	536.900	1623.000	532.700	1656.000	531.600	1678.000	530.800	1694.000	530.800	1785.000		
3 14	GR	530.800	1904.000	531.600	1907.000	532.800	1910.000	537.000	1919.000	550.400	1946.000		'•
15	GR	575.000	1973.000	600.100	2000.000	0.0	0.0	0.0	0.0	0.0	0.0		19
	NC	0.060	0.087	0.038	0.0								
	NV	6.000	0.038		0.0	0.0	0.0	0.0	0.0	0.0	0.0		11
	NV			536.000	0.038	543.000	0.045	545.000	0.045	545.700	0.043		
		545.800	0.043	560.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		12
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1178.000	1855.000		13
													•
	XI	88.000	34.000	1410.000	1604.000	925.000	860.000	920.000	0.0	0.0	0.0		14
	GR	600.100	1000.000	574.700	1047.000	551,100	1087.000	551.100	1111.000	536.600	1140.000		
	GR	536.100	1147.000	536.700	1154.000	537.700	1234.000	539.000	1308.000	540.600	1353.000		15
	GR	540.400	1384.000	538.400	1410.000	535.700	1424.000	534.000	1428.000	532.200	1434.000		
	GR	530.700	1438.000	530.700	1496.000	530.700							
•	GR	537.300	1604.000				1552.000	532.200	1560.000	534.300	1570.000		17
				537.700	1658.000	537.900	1711.000	535.800	1726.000	534.500	1737.000		
	GR	534.000	1742.000	534.000	1763.000	534.000	1779.000	534.500	1781.000	536.500	1791.000		11 N
	GR	541.500	1841.000	550.200	1877.000	575.100	1914.000	599.900	1946.000	0.0	0.0		EA
	NC	0.060	0.080	0.038	0.0	0.0	0.0	0.0	0.0	0.0	0.0		90
	NV	6.000	0.038	538.000	0.038	544.000	0.045	546.500	0.045	547.400	0.043		70
	NV	547.500	0.043	565.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
•	FT	0.0	0.0	0.0	0.0	9,100	0.0	0.0	0.0	1241.000	1845.000		2 0
21			TENNES OF THE PARTY OF THE PART		11 12 16 3 17 17	6 4 4 6 5				1241.000	1545.000		22
24	X1	89.000	32.000	1487.000	1699.000	766.000	754.000	760.000	0.0	0.0	0.0		
	GR	603.500											23
	GR		1000.000	574.700	1065.000	555.800	1127.000	554.300	1146.000	554.300	1159.000		
		554.300	1168.000	538.500	1201.000	538.000	1208.000	538.800	1215.000	539.500	1322.000		
	GR	539.100	1438.000	539.500	1487.000	536.800	1500.000	534.600	1542.000	534.000	1562.000		25
	GR	532.600	1609.000	532.600	1615.000	532.600	1648.000	534.000	1667.000	534.900	1678.000		
	GR	538.500	1699.000	538.500	1751.000	534.900	1780.000	534.500	1790.000	534.300	1795.000		76
4	GR	534.300	1802.000	534.300	1808.000	534.500	1811.000	535.200	1820.000	550.100	1860.000		77
	GR	575.600	1894.000	599.800	1932.000	0.0	0.0	0.0	0.0	0.0	0.0		
4	NC	0.060	0.110	0.038	0.100	0.300	0.0	0.0	0.0	0.0	0.0		78
	NV	6.000	0.038	538.000	0.038	544.500	0.045	547.000	0.045	547.700	0.043		
	NV	547.800	0.043	565.000	0.0	0.0	0.045	0.0	0.045				29
	FT	0.0								0.0	0.0		30
		0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1221.000	1795.000	- /	
•	٧.		2 1 2 2 2 2 2 2										11
	X1	90.000	24.000	1471.000	1726.000	150.000	150.000	150.000	0.0	0.0	0.0		1
10	GR	601.600	1000.000	585.100	1057.000	554.700	1122.000	554.700	1140.000	539.900	1174.000		30 -
	GR	539.200	1185.000	539.700	1194.000	539.500	1254.000	538.700	1365.000	539.700	1441.000		33 -
W 12	GR	539.700	1471.000	535.800	1504.000	534.500	1513.000	533.800	1518.000	533.800	1600.000		•
9.1	GR	533.800	1658.000	534.500	1678.000	534.900	1689.000	539.000	1726.000	537,100	1762.000		34
	GR	536.500	1781.000	549.200	1819,000	575.500	1850.000	599.200	1912.000	0.0	0.0		Uar
	NC	0.060	0.110	0.038	0.100	0.300	0.0						35 m 8
	NV	6.000						0.0	0.0	0.0	0.0		
			0.038	539.000	0.038	546.000	0.045	548.500	0.045	549.300	0.043		
(0)	NV	549.400	0.043	565.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		37 . 9
	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1273.000	1704.000		
													38
	X1	91.000	22.000	1520.000	1704.000	910.000	908.000	905.000	0.0	0.0	0.0		10
9	GR	590.300	1000.000	575.500	1039.000	549.300	1091.000	549.300	1112.000	548.500	1130.000		9
	GR	546.600	1176.000	544.800	1218.000	543.200	1333.000	542.700	1451.000	543.200	1501.000		

de

	GR	544.100	1520.000	538.000	1537.000	536.000	1544.000	532.700	1554.000	532.700 549.900	1617.000 1757.000	0.0	•
	GR	532.700	1680.000	537.000	1696.000	539.100	1704.000	542.000	1728.000	0.0	0.0	89	
	GR	575.800	1808.000	600.200	1854.000	0.0	0.0	0.0	0.045	551.700	0.043		
	NV	6.000	0.038	541.500	0.038	548.000 0.0	0.045	551.000	0.0	0.0	0.0		•
	NV	551.800	0.043	565.000	0.0	7.400	0.0	0.0	0.0	0.0	0.0		
	ET	0.0	0.0	0.0	V•V		Ŭ•Ŭ						
•	X1	92.000	30.000	1785.000	1975.000	935.000	900.000	905.000	0.0	0.0	0.0		•
	GR	585.400	1000.000	577.700	1069.000	569.200	1140.000	560.400	1164.000	554.900	1199.000		12
	GR	555.300	1227.000	555.300	1248.000	555.300	1263.000	549.600	1291.000	548.900	1353.000		
•	GR	547.600	1438.000	545.100	1498.000	542.300	1567.000	543.100	1635.000	545.500	1696.000		
	GR	545.800	1737.000	544.900	1776.000	543.900	1785.000	540.000	1794.000	537.000	1804.000		,
	GR	532.400	1818.000	532.400	1877.000	532.400	1936.000	537.000	1951.000	538.700	1956.000		300
	GR	542.700	1975.000	545.700	1995.000	557.600	2020.000	575.600	2039.000	599.300	2087.000		
	NC	0.070	0.110	~ 0.038	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
	NV	6.000	0.038	542.000	0.038	549.000	0.045	552.000	0.045	552.900	0.043		6
	NV	553.000	0.043	570.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
	FT	0.0	0.0	0.0	0.0	3.400	0.0	0.0	0.0	V.V			
- 11				1722 000	1050 000	765.000	803.000	795.000	0.0	0.0	0.0		
	X1	93.000	34.000	1722.000	1858.000 1044.000	574.000	1068.000	563.200	1108.000	560.900	1122.000		10
	GR	585.200	1000.000	575.700 557.000	1151.000	554.600	1169.000	552.000	1177.000	552.000	1223.000		11
	GR GR	551.800	1242.000	551.800	1314.000	552.000	1353.000	551.200	1370.000	548.000	1402.000		
	GR	544.800	1441.000	544.500	1520.000	545.600	1569.000	549.900	1590.000	542.300	1611.000		17
30	GR	541.100	1633.000	543.100	1649.000	547.600	1691.000	544.700	1722.000	539.800	1743.000		11300
	GR	538.000	1755.000	533.000	1790.000	533.000	1802,000	533.000	1841.000	538.000	1852.000		
71	GR	540.900	1858.000	561.700	1876.000	575,000	1890.000	599.700	1923.000	0.0	0.0		1"
	NC	0.070	0.110	0.040	0.100	0.300	0.0	0.0	0.0	0.0	0.0		15
	NV	6.000	0.040	543.500	0.040	550.000	0.055	554.000	0.055	554.800	0.045		10
24	NV	554.900	0.045	570.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
25	FT	0.0	0.0	0.0	0.0	12.400	0.0	0.0	0.0	0.0	0.0		170
2 26					1000 000	425 000	440 000	445.000	0.0	0.0	0.0		18
21	X1	94.000	30.000	1820.000	1930.000	435.000	448.000	569.500	1227.000	564.300	1240.000		
- 22	GR	595.100	1000.000	585.800	1096.000	578.300	1196.000	553.500	1338.000	550.300	1368.000		100
•	GR	564.300	1254.000	559.300	1286.000	552.000 550.200	1540.000	550.500	1567.000	546.600	1598.000		70
	GR	547.300	1430.000	547.900	1509.000	545.100	1767.000	545.100	1792.000	540.300	1820.000		71
	GR	545.400	1667.000	544.000 538.500	1706.000	534.000	1884.000	534.000	1884.000	534.000	1910.000		
•	GR	539.500	1828.000	540.500	1930.000	549.400	1942.000	574.500	1970.000	600.400	1993.000		n
	GR NC	538.500	0.110	0.042	0.0	0.0	0.0	0.0	0.0	0.0	0.0		23
•	NV	6.000	0.042	545.500	0.042	552.000	0.060	555.000	0.060	556.000	0.050		•
26	NV	556.100	0.050	570.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		24
- 17	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1489.000	2150.000		В.,
11	X1	95.000	41.000	1782.000	2147.000	115.000	520.000	380.000	0.0	0.0	0.0		11
	GR	594.800	1000.000	585.800	1086.000	577.500	1166.000	574.400	1199.000	568.500	1208.000		27
	GR	568.500	1223.000	559.600	1265.000	552.000	1286.000	553.400	1323.000	550.200	1348.000		28
42	GR	548.700	1425.000	548.600	1478.000	551.800	1503.000	550.200	1518.000	546.400	1548.000		
- 63	GR	546.400	1622.000	546.500	1691.000	547.400	1747.000	545.000	1782.000	540.900 540.700	1866.000		
	GR	538.700	1820.000	536.700	1835.000	538.700	1848.000	540.400	1858.000	544.800	1958.000		36
43	GR	538.800	1877.000	531.700	1904.000	538.800	1928.000	540.200	1933.000	539.200	2129.000		77
45	GR	541.700	1985.000	539.700	2013.000	539.200	2032.000	534.000	2190.000	576.100	2208.000		•
	GR	540.200	2137.000	542.900	2147.000	547.400	2164.000	563.600	0.0	0.0	0.0		32
-	GR	600.000	2242.000	0.0	0.0	0.0	0.0	0.0 555.500	0.060	556.300	0.050		n
•	.NV	6.000	0.042	545.500	0.042	552.000	0.060	0.0	0.0	0.0	0.0		•
	NV	556.400	0.050	570.000	0.0	9.100	0.0	0.0	0.0	1405.000	2290.000		34
	FT	0.0	0.0	0.0	0.0	7.100	J. U						35
	X1	96.000	42.000	1562.000	1819.000	140.000	200.000	300.000	0.0	0.0	0.0		
	GR	595.000	1000.000	585.100	1076.000	579.900	1134.000	578.100	1156.000	574.600	1181.000		36
	GR	563.100	1207.000	559.600	1226.000	552.100	1257.000	553.100	1289.000	550.700	1321.000		37
● 15	GR	548.900	1390.000	549.400	1405.000	551.900	1420.000	551.900	1430.000	547.900	1469.000		
57	GR	546.900	1497.000	545.200	1562.000	540.600	1584.000	542.800	1630.000	541.400	1664.000		1
N.	GR	540.100	1679.000	537.900	1705.000	537.900	1735.000	537.900	1782.000	540.100	1796.000		39
	GR	541.500	1805.000	544.700	1819.000	545,900	1845.000	544.700	1910.000	544.300	1945.000		
0.000	GR	544.900	2044.000	543.600	2131.000	544.500	2210.000	543.800	2243.000	540.300	2261.000	The second secon	

8.3

•	GR	539.700	2264.000	540.300	2275.000	540.800	2284.000	542.000	2303.000	550.200	2328.000	00	EN
	GR	575.000	2360.000	599.700	2401.000	0.0	0.0	0.0	0.0	0.0	0.0	90	•
	NC	0.080	0.100	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
	NV	6.000	0.039	546.000	0.039	552.500	0.055	556.000	0.055	556.700	0.047		571
•	NV	556.800	0.047	570.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1368.000	2360.000		7 3
	.,	07 000	45 000	1268 000	1478.000	530.000	250.000	540.000	0.0	0.0	0.0		100
	X1	97.000	45.000	1368.000	1079.000	617.400	1103.000	611.000	1143.000	599.600	1219.000		2 6
	GR	624.900	1000.000	574.100	1299.000	553,600	1315.000	553.600	1344.000	551.300	1349.000		
•	GR GR	592.100 550.400	1263.000	541.000	1384.000	538.200	1389.000	538.200	1423.000	538.200	1467.000		
	GR	541.000	1471.000	544.500	1478.000	546.800	1505.000	545.100	1543.000	545.400	1559.000		4
	GR	547.400	1614.000	546.500	1660.000	546.500	1697.000	546.600	1710.000	545.200	1738.000		1,
	GR	544.400	1777.000	542.300	1834.000	541.800	1893.000	541.500	1929.000	541.800	1937.000		•
	GR	543.000	1971.000	545.100	2008.000	550.400	2044.000	551.300	2109,000	549.800	2177.000] •
10.	GR'	547.400	2233.000	546.400	2307.000	544.800	2392.000	544.200	2403.000	545.000	2428.000		1
• 11	GR	545.500	2456.000	554.700	2484.000	575.500	2540.000	587.500	2593.000	595.700	2633.000		
u u	NV	6.000	0.039	546.000	0.039	553,000	0.055	556.000	0.055	557.000	0.045		7
10	NV	557.100	0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		'
● H	ET	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1113.000	2360.000		10
15	٠,	98,000	47.000	1113.000	1243.000	300.000	140.000	300.000	0.0	0.0	0.0		11
A 17	K1 GR	624.600	1000.000	600.400	1031.000	574.900	1054.000	555.800	1071.000	555.800	1101.000		•
	GR	551.900	1113.000	541.600	1122.000	538.000	1126.000	538.000	1161.000	538.000	1171.000		12
19	GR	541.600	1197.000	543.100	1208.000	546.100	1243.000	547.800	1289.000	549.000	1319.000		13
	GR	547.600	1379.000	549.000	1437.000	549.000	1519.000	548.200	1628.000	547.800	1697.000		130
11	GR	545.800	1720.000	545.800	1756.000	546.200	1798.000	544.100	1815.000	543.900	1828.000		J"
- 72	GR	543.700	1838.000	543.900	1841.000	544.700	1851.000	545.700	1906.000	549.400	1929.000		15
	GR	549.700	1973.000	550.700	2009.000	550.700	2076.000	549.400	2159.000	548.000	2253.000		
11	GR	546.500	2312.000	545.200	2361.000	546.100	2400.000	546.900	2426.000	546.500	2435.000		1
25	GR	545.500	2445.000	546.100	2452.000	551.300	2501.000	575.100	2569.000	588.500	2634.000		100
● 18	GR	593.800	2672.000	599.900	2707.000	0.0	0.0	0.0	0.0	0.0	0.0		18 %
77	NC	0.090	0.0	0.0	0.0	0.0	0.0	0.0	0.0	557.300	0.045		RE
	NV	6.000	0.039	547.000	0.039	553.500	0.055	556.500 0.0	0.055 0.0	0.0	0.0		" AB
	NV	557.400	0.045	575.000	0.0	0.0 11.400	0.0	0.0	0.0	0.0	0.0		20
	ET.	0.0	0.0	0.0	0.0	11.400	V • V						21
	X1	99.000	52.000	1489.000	1681.000	420.000	180.000	340.000	0.0	0.0	0.0		
33	GR	625.100	1000.000	599.000	1026.000	575.600	1061.000	557.400	1073.000	557.400	1101.000		177
F 11	GR	555.600	1117.000	549.000	1148.000	547.400	1162.000	548.200	1170.000	548.500	1241.000		23
•	GR	550.100	1349.000	547.500	1389.000	547.200	1420.000	547.300	1489.000	545.000	1508.000		
35	GR	542.100	1522.000	540.600	1529.000	540.600	1574.000	540.600	1616.000	542.100	1626.000		-1
n n	GR	544.200	1639.000	547.900	1681.000	547.100	1733.000	547.100	1799.000	546.500	1902.000		25
●2	GR	548.000	1984.000	546.000	5055.000	545.600	2074.000	545.600	2149.000	545.800	2210.000		24
9	GR	547.000	2240.000	546.900	2270.000	545.200	2276.000	543.300	2282.000	545.200	2289.000 2565.000		Al .
	GR	546.500	2294.000	548.400	2310.000	549.000	2372.000	549.100	2465.000	547.800 554.900	2901.000		21
•	GR	546.300	2674.000	546.300	2793.000	547.800	2829.000	551.000 566.000	2871.000 2976.000	575.900	3016.000		12
40	GR	554.200	2911.000	555.100	2917.000	561.000	2949.000	0.0	0.0	0.0	0.0		140
	GR	587.400	3081.000	599.600 0.037	3154.000 0.100	0.0	0.0	0.0	0.0	0.0	0.0		
	NC NV	0.070	0.080	547.000	0.037	554.000	0.055	557.000	0.055	557.700	0.045	·	36
	NV	6.000 557.800	0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		31
● 0	ET	0.0	0.045	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		•
6			•										" "
· *	X1	100.000	57.000	2217.000	2371.000	800.000	620.000	550.000	0.0	0.0	0.0		23
	GR	599.900	1000.000	570.600	1051.000	550.400	1091.000	551.300	1149.000	551.300	1 57.000		24
9.	GR	552.000	1350.000	552.000	1439.000	552.500	1524.000	553.300	1543.000	552.700	1567.000		
. 57	GR	550.700	1591.000	549.400	1635.000	550.100	1692.000	550.600	1743.000	550.700	1813.000 2201.000		35
• 0	GR	550.400	1940.000	551.100	2058.000	551.100	2124.000	551.600	2171.000	550.400 541.500	2282.000		36
, st	GR	548.100	2217.000	545.100	2223.000	543.000	2230,000	541.500 548.000	2235.000	548.100	2440.000		
	GR -	541.500	2319.000	543.000	2329.000	544.600	2339.000	550.700	2662.000	551.000	2740.000		"•
•	GR	547.000	2481.000	547.000	2536.000	546.400 549.600	2610.000	548.800	2993.000	549.700	3000.000		38 3
1	GR	551.000	2823.000	550.300	2880.000	566.100	3141.000	566.100	3154.000	571.000	3173.000		39
	GR	555.100	3046.000	557.000 575.400	3107.000 3236.000	576.300	3325.000	576.400	3442.000	575.300	3636.000		•
	GR GR	572.500 575.200	3201.000 3785.000	575.400	3907.000	580.500	4013,000	590.200	4207.000	594.700	4337.000		



Macan out on										-	STATES AND DESIGNATION OF THE	ASSESSMENT OF THE PARTY OF THE
			AND THE RESERVE	. 1		1,1				8.2	9	2
						9.46			1834,308		_	
**			****									
4			THRU 09R2	1974 #				BY THE UNITED				
	MODIFICATI			A 19 . 050		DEPARTMENT			ALL SOL ENGIN	100000		'6
•	MBJ UPDATE	D 07/20/7	6 0830	4 1 1 1 1				EVISED BY MIC]2
	TODAYS DAT	F TS 04/26	/77 17.35	2138#980				SE ON THEIR C				1.0
	1	81,75,850		21 8 2 4 9 8 6	549,388*			DROLOGIC ENGI				,
*	2.553 SFC		******	*******	10 H 1 H 1 H 1 H 1 H 1 H 1 H 1 H 1 H 1 H	* * * * * *				Sala ast		5
	2.333.360						1000000		Tion	1/1/0	COFFIN	
10	CUCOUS		D DICEN CONNE	CCTON					T 151	11NG	CREEK	- 1,
T			CK-CHICKSHIND						_			
		IG CREEK -	100 YEAR FLOO	io oi	7747		1000,000	7.77	100	LOOF	WAT	
J	1 TCHECK	TNO	NINV IDI	R STRT	METRIC	HVINS	0	WSEL FO		- T		
10	. Tomeon								101	11-	1450	11
17	10.00	4.	0.	0. 0.0	0.0	0.0	0. 5	59.167 0.	0 /0/	· · · · ·	179.0	
18 19 J	NPROF	TPL07	PREVS XSE	CV XSECH	FN	ALLDC	IBW	CHNIM	RACE	75 TO P. 10		
11	r mariner	19-9-96	1 000		469 See	0.0	0.0	0.0	0.0 5 66	1837,659	Michael Baker, J	
21	1.000	0.0	-1.000	0.0	0.0	0.0	0.0		V.V		2763 N. Fourth	St*
13 J	3 1.000	34.000		4.000	27.000	28.000	9.000	2100.0	9.0.00	0.0	Box 3225	15
24 N		0.080		0.100	0.300	0.0 87000.000	0.0	0.0	0.0	0.0	Harrisburg, Pa. 17	/105 15
23 N		20000.000	Marine William International Confession Conf	48800.000	554.000	0.055	557.000	0.055	557.700	0.045		"
27 N		0.045		0.0	0.0	0.0	0.0	0.0	0.0	0.0		19
28 F	r 0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0		19
29 X	1 100.000	57.000	2217.000	2371.000	800.000	620.000	550.000	0.0	0.0	0.0		20
31 GI		1000.000		1051.000	550.400	1091.000	551.300	1149.000	551.300	1257.000		
12 G		1350.000		1439.000	552.500 550.100	1524.000	553.300 550.600	1543.000 1743.000	552.700 550.700	1567.000 1813.000		
3 6		1591.000		1635.000	551.100	2124.000	551.600	2171.000	550.400	2201.000		
35 GI		2217.000		2223.000	543.000	2230.000	541.500	2235.000	541.500	5585.000		"
36 G		2319.000		2329.000	544.600 546.400	2339.000	548.000 550.700	2371.000	548.100 551.000	2740.000		24
21 G		2823.000		2536.000	549.600	2982.000	548.800		549.700	3000.000		23
G		3046.000	557.000	3107.000	566.100	3141.000	566.100	3154.000	571.000	3173.000		le de
40 G		3201.000		3236.000 3907.000	576.300 580.500	3325.000 4013.000	576.400 590.200	3442.000 4207.000	575.300 594.700	3636.000 4337.000		n_{μ}
41 G		3785.000 4361.000		4369.000	0.0	0.0	0.0	0.0	90.0	0.0		73
N	0.070	0.070	0.037	0.100	0.400	0.0	0.0	0.0	0.0	0.0		
N		0.040		0.040	554.000	0.055	557.000 0.0	0.055	557.900	0.045		9
F		0.0	0.0	0.0	9.100	0.0	0.0	0.0	1246.000	2703.000		
67					4.35		1.0	1.7	0.0	5.0		14
AS X		52.000		2331.000	215.000 550.500	200.000	180.000		0.0 552.100	1223.000		32 A
e G		1319.000		1431.000	552.000	1568.000	552.600		555.300	1667.000		33
G		1690.000		1727.000	553.500	1817.000	550.400	1955.000	552.300	2048.000		14
S G		2130.000		2153.000	544.700	2162.000	543.300 544.200		542.800 548.900	2171.000		15
s GI		2237.000		2300.000	543.300 552.600	2502.000	551.800		550.400	2761.000		36
S G		2813.000		2828.000	549.800	2844.000	554.200	2895.000	558.100	2942.000		1,
G		2983.000		2990.000	578.300	3017.000	578.400 575.900		577.300 576.300	3091.000		1.4
GI		3184.000		3266.000 3790.000	575.800 589.300	3331.000	592.800		594.700	4055.000		
s GI	594.700	4082.000	595.100	4094.000	0.0	0.0	0.0	0.0	0.0	0.0		"1
N	0.080	0.070	0.040	0.100	0.300	0.0	0.0	0.0	0.0	0.0		

	NV	5.000	0.036	549,500	0.036	556,000	0.055	558.000	0.055	558,900	0.045	00	
	NV	559.000	0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	93	•
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1334.000	2491.000		
•	X J	102.000	53.000	2116.000	2391.000	695.000	665.000	740.000	0.0	0.0	0.0		
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	551.000	555.000	0.0		
	GR	599.900	1000.000	575.500	1065.000	551.300	1155.000	552.500	1209.000	552.800	1304.000		
_	GR	553.800	1405.000	553.700	1511.000	554.400	1603.000	552.900	1630.000	554.200	1654.000		' (a)
	GR	554.200	1672.000	551.700	1680.000	552.600	1720.000	553.300	1791.000	552.700	1850.000		1 6
	GR	553.900	1909.000	554.700	1939.000	554.000	1992.000	554.900	2030.000	555.400	2083.000		,
_	GR	555.400	2116.000	550.200	2138.000	551.000	2151.000	549.800	2162.000	546.400	2169.000		3 13
	GR	544.700	2175.000	542.300	2183.000	542.300	2238.000	542.300	2321.000	544.700	2332.000		
	GR	546.300	2339.000	550.500	2362.000	558.600	2391.000	556.800	2480.000	555.100	2573.000		
	GR			552.800	2725.000	560.600	2753.000	575.200	2791.000	578.300	2810.000		1
•		553.600	2633.000		2972.000	579.100	3065.000	579.400	3179.000	579.600	3273.000		
	GR	578.300	2825.000	578.400		583.100	3434.000	583.100	3456.000	586.200	3491.000		
	GR	579.800	3355.000	581.400	3421.000			0.0	0.0	0.0	0.0		7.3
	GP	592.600	3521.000	594.300	3571.000	600.700	3646.000			0.0	0.0		
	, NC	0.080	0.070	0.037	0.100	0.300	0.0	0.0	0.0			orner en	
1	NV	6.000	0.036	550.000	0.036	556.000	0.053	558.500	0.053	559.400	0.045		19 70
•	NV	559.500	0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		•
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1351.000	2397.000		10
	16.										4.6		N CONTRACTOR
	xl	103.000	49.000	2102.000	2357.000	280.000	290.000	285.000	0.0	0.0	0.0		
	х3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	553.000	555.000	0.0		12
	GR	600.600	1000.000	585.700	1072.000	570.400	1127.000	554.600	1186.000	554.700	1253,000		
•	GR	554.800	1350.000	555.200	1443.000	555.200	1534.000	555.100	1609.00.0	556.800	1637.000		
	GR	555.800	1660.000	555.600	1717.000	551.900	1727.000	551.400	1744.000	553.500	1755.000		14
	GR	552.900	1829.000	551.900	1883.000	552.300	1923.000	553.400	1994.000	555.300	2052.000		
/	GR	556.600	2065.000	556.600	2085.000	553.000	2102.000	548.800	2128.000	545.500	2138.000		
	GP	545.000	2140.000	545.000	2228.000	545.000	2310.000	545.500	2320.000	547.900	2332.000		14
	GR	558.800	2357.000	557.300	2471.000	555.500	2597.000	554.100	2710.000	553.100	2772.000		
			2793.000	559.500	2814.000	562.000	2870.000	562.000	3002.000	565.300	3025.000		
•	GR	553.100 574.500	3109.000	576.700	3118.000	576.700	3138.000	579.700	3158.000	589.900	3251.000		10 2
						594.900	3350.000	600.200	3428.000	0.0	0.0		- 2
	GR	589.900	3268.000	594.600	3293.000				0.0	0.0	0.0		19 🕳 8
	NC	0.080	0.100	0.037	0.100	0.700	0.0	0.0			0.045		9
	NV	6.000	0.037	550.500	0.037	557.000	0.053	559.000	0.053	560.200			20
	NV	560.300	0.045	575.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		di
	FT	0.0	0.0	0.0	0.0	4.400	0.0	0.0	0.0	0.0	0.0		
													11
	x1	104.000	41.000	2193.000	2405.000	330.000	450.000	380.000	0.0	0.0	0.0		71
(x3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		•
	GP	600.200	1000.000	590.000	1139.000	583.600	1202.000	575.300	1264.000	567.700	1318.000		H
	GR	560.500	1361.000	558.600	1418.000	557.900	1511.000	559.000	1656.000	557.700	1732.000		
0	GR	558.400	1754.000	558.800	1769.000	559.200	1820.000	559.900	1873.000	559.900	1902.000		
	GR	558,000	1951.000	555.600	2004.000	553.900	2063.000	552.200	2122.000	554.600	2141.000		31
	GR	557.500	2155.000	557.500	2175.000	555.700	2193.000	550.600	2216.000	548.800	2555.000		
	GP	546.500	2228.000	543.000	2236.000	543.000	2293.000	543.000	2352.000	546.500	2367.000		
	6.0	549.500	2380.000	555.300	2405.000	556.000	2455.000	558.900	2484.000	564.700	2530.000		18
	GH	568.400	2577.000	569.200	2632.000	577,900	2651.000	586.500	2697.000	596.500	2755.000		
	GR	600.500	2795.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		29
	NC NC			0.0	0.300	0.800	0.0	0.0	0.0	0.0	0.0		
		0.0	0.0		0.330	557.000	0.052	560.000	0.052	560.700	0.045		220
	NV	6.000	0.037	550.500		0.0	0.0	0.0	0.0	0.0	0.0		11
	NV	560.800	0.045	575.000	0.0				0.0	1655.000	2059.000		
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1033.000			
						150 000	127 000	14E 000	0.0	-0.500	0.0		13 _ §
	X1	106.010	24.000	1913.000	2059.000	150.000	137.000	145.000	0.0				9
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	556.000	559.200	. 0.0		1
	GR	600.800	1000.000	590,600	1136.000	585.000	1199.000	583.900	1262,000	579.600	1321.000		
	GR	562.800	1367.000	550.200	1437.000	560,600	1454.000	560.100	1551.000	558.900	1633.000		0
	GR	556.100	1674.000	555.900	1731.000	555.900	1756.000	555.100	1800.000	555.000	1869.000		4
	GR	550.300	1913.000	541.500	1963.000	541.500	2044.000	549.000	2059.000	570.300	2097.000		
	GR	570.800	2105.000	571.100	2121.000	574.400	2128.000	601.600	2167.000	0.0	0.0		
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1655.000	2059.000		10
						144.000	7.500	1815.000	0.0	544.500	544.500		
	SB	0,900	1.500	3.000	0.0	177.000	• 500	10 . 10	to the				37.00
0	9	· ·				20.000	20.000	20.000	0.0	0.0	0.0		
Market Co.	X1	106.020	0.0	0.0	0.0	30.000	30.000	30.000	0.0	0.0	V. V		

									·				
	XS.	0.0	0.0	1.000	557.900	557.100	0.0	0.0	0.0	0.0	0.0	Q <u>4</u>	
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	557.100	562.000	0.0	VT	
	RT	12.000	1325.000	579.400	0.0	1373.000	561.800	0.0	1444.000	560.200	0.0		
	RT	1504.000	560.500	0.0	1645.000	557.100	0.0	1668.000	557.100	0.0	1794.000		
	RT	557.500	0.0	1857.000	557.900	0.0	1925.000	562.000	0.0	2069.000	562.000		•
	RT	0.0	5105.000	563.000	0.0	2125.000	563.200	0.0	2155.000	575.100	0.0		
1	NC	0.045	0.100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2059.000		1, 1
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1655.000	2039.000		- 3
						135 000	00 000	100.000	0.0	0.500	0.0		
	×1	106.000	0.0	0.0	0.0	125.000	90.000	0.0	0.0	0.0	0.0		163
	NC	0.050	0.100	0.041	0.100	0.300 9.400	0.0	0.0	0.0	0.0	0.0		
	FT	0.0	0.0	0.0	0.0	7.400							
	X1	107.000	29.000	1837.000	2071.000	570.000	810.000	755.000	0.0%	0.0	0.0		10
	x3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
1	GR	600.300	1000.000	589.700	1122.000	580.500	1282.000	574.600	1310.000	568.600	1321.000		
	GR	558.500	1358.000	557.000	1419.000	555.800	1471.000	557.600	1499.000	557.600	1538.000		'0
	GR	557.600	1634.000	557.700	1703.000	556.800	1738.000	554.300	1769.000	554.900	1797.000		
	GR	561.400	1837.000	555.500	1858.000	550.400	1891.000	549.600	1936.000	549.000	1946.000	<i>f</i>	
	GR	547.000	1978.000	547.000	2006.000	547.000	2043.000	549.000	2056.000	550.400	2066.000		0
	GR	557.000	2071.000	575.700	2087.000	575.700	2109.000	599.900	2138.000	0.0	0.0		10
	NC	0.060	0.060	0.041	0.0	0.0	0.0	0.0	0.0	0.000	0.0		11 4
	FT	0.0	130.00	0.0	0.0	10.400	0.0	0.0	0.0	0.00	1760.000		
	1		1776.000	56.00, 320		200			2470,000	2 1 6 g 2 G 2 C	1674.000	Vicinia de la companya della companya della companya de la companya de la companya della company	12
1	, X1	108.000	24.000	1703.000	1919.000	200.000	415.000	350.000	0.0	0.0	0.0		13
	. X3	10.000	0.0	0.0	0.0	0.0	1148,000	0.0 574.200	0.0 1181.000	560.500	1239.000		•
1	GR	599.300	1000.000	589.100	1084.000	580.400 557.400	1491.000	554.700	1556.000	553.500	1622.000		ad'
	GR	558.100	1303.000	558.100	1388.000	550.800	1738.000	549.800	1767.000	549.500	1775.000		15
	GR	553.100	1663.000	561.100	1703.000	550.600	1905.000	555.100	1919.000	560.700	2009.000		16
	GR	546.500	1836.000	549.500	1891.000	575.700	2081.000	600.700	2117.000	0.0	0.0		
. 2	NC	562.100	0.080	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0		ľa.
•	FT	0.055	0.080	0.041	0.0	9.400	0.0	0.0	0.0	0.0	0.00		13 8
			- 4						777 1778		9.000		13
	. X1	109.000	27.000	1458.000	1709.000	250.000	410.000	365.000	1410.000	90.0	1880.000		0 8
	. x3	10.000	0.0	%00.00A	1690.000	0.0	0.0	0.0	0.0	0.0	0.0		70
	CP	600.5 30	1000.000	575.000	1121.000	560.200	1189.000	559.700	1229.000	558.600	1304.000		h, 3
	GR	559.000	1371.000	556.900	1387.000	553.900	1418.000	554.200	1435.000	562.500	1458.000		
	GI5	550.400	1487.600	550.000	1492.000	550.000	1496.000	550.000	1582.000	550.000	1701.000		pr
1	GP .	550.500	1703.000	552.100	1709.000	552.400	1761.000	559.700	1783.000	560.300	1849.000 2028.000		73
	GP	560.900	1950.000	555.600	1969.000	565.600	2008.000	565.600	2019.000	565.600 0.0	0.0		
1 / 3	GR	574.500	2049.000	600.400	2101.000	0.0	0.0	0.0	0.0	0.0	0.0		"
	NE	0.080	0.090	0.041	0.100	0.300 6.400	0.0	0.0	0.0	0.0	0.0		25
	FT	0.0	0.0	0.0	0.0	0.400	0.0	S 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•		0.0		7.
	y 3	110.000	33.000	1095.000	1378.000	500.000	570.000	580.000	0.0	0.0	0.0	4	
	GR GR	605.300	1000.000	604.000	1009.000	585.200	1038.000	575.200	1054.000	565.300	1073.000		" >
	GR	555.800	1095.000	553.700	1101.000	552.500	1108.000	549.800	1124.000	549.800	1147.000		23
	GR	549.800	1175.000	552.500	1201.000	554.100	1217.000	552.800	1266.000	552.200	1303.000		
	GR	551.500	1328.000	551.000	1346.000	551.500	1357.000	552.000	1369.000	554.000	1378.000 .		r's
	GR	552.900	1391.000	555.500	1421.000	556.000	1464.000	556.000	1506.000	555.100	1529.000		20
	GR	560.300	1589.000	560.400	1654.000	560.700	1734.000	555.600	1754.000	570.500	1789.000		11
_	GR	570.500	1809.000	575.000	1820.000	599.400	1854.000	0.0	0.0	0.0	0.0		
	NC	0.100	0.100	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0		37
	FT	0.0	0.0	0.0	0.0	12.400	0.0	0.0	0.0	0.0	0.0		23 9
	e die	274425609			4		410.000	550 000	0.0	0.0	0.0		0
5	X 1	111.000	33.000	1327.000	1507.000	570.000	410.000	550.000	0.0	0.0 554.900	1112.000		
3	GR	625.000	1000.000	600.000	1033.000	575.000	1065.000	557.500	1099.000	555.400	1186.000		35
	GR	554.600	1119.000	554.600	1119.000	554.600	1119.000	554.900	1284.000	555.200	1309.000		
	GR	558.000	1229.000	559.900	1245.000	555.100	1270.000	557.500 554.500	1456.000	555.100	1466.000		
5	GR	554.900	1327.000	554.500	1342.000	551.700 557.600	1392.000	556.500	1709.000	557.200	1787.000		P
	GR	556.700	1507.000	556.400	1570.000	560.200	1880.000	570.200	1921.000	570.200	1940.000		
3	GR	560.700	1841.000	561.300 600.300	1975.000	625.200	2024.000	0.0	0.0	0.0	0.0		
\$	GR	574.600	0.100	0.041	0.100	0.300	0.0	0.0	0.0	0.0	0.0		No.
0 5	NC	0.100	0.100	1433.000	0.041	1625.000	0.100	1666.000	0.050	1713.000	0.100		•
	NH	5.000	0.100	1433.000	0,041	1023,000	0.100						

											Sandraker and an a track a family and an extension of the sandraker and the sandrake	CONTRACTOR (CONTRACTOR CONTRACTOR	Maditimizacion/For
•	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1169.000	1940.000	95	•
	xı	112.000	31.000	1433.000	1625.000	330.000	375.000	405.000	0.0	0.0	0.0		
	GR	624.800	1000.000	600.200	1030.000	574.700	1055.000	556.800	1102.000	557.900	1170.000		
	GR	561.200	1241.000	560.100	1328.000	556.400	1340.000	557.700	1372.000	557.300	1433.000		
4	GR	556.000	1457.000	553.100	1496.000	553.100	1496.000	553.100	1590.000	556.000	1610.000		
	GR	558.300	1625.000	560.600	1656.000	556.000	1666.000	553.100	1672.000	553.100	1685.000		6
	GR	553.100	1685.000	556.000	1703.000	557.500	1713.000	560.400	1903.000	561.000	1879.000		7
4	GR	562.504	1978.000	570.500	1998.000	570.500	2018.000	574.300	2036.000	599.300	2077.000		
	GR	624.760	211000	0.0	0.00	0.0	1280.00	0.0	3790.000	0.004	0.0		
4	NC	0.100	0.100	0.041	0.100	0.500	0.0	0.0	0.0	0.0	0.0 1830.000		4
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1160.000	0.100		10
•	NH	5.000	0.100	1400.000	0.041	1535.000	0.100	1719.000	0.0	0.0	0.0		
	NH	1978.000	- 0.0	0.0	0.0						THE STATE OF A		
	X1	113.000	38.000	1400.000	1535.000	95.000	250.000	100.000	0.0	0.0	0.5		70
	GR	624.700	1000.000	600.600	1029.000	574.800	1056.000	557.100	1099.000	560.000	1140.000		
1	GR	561.100	1205.000	561.400	1257.000	560.300	1349.000	558.400	1400.000	557.200	1430.000		
	GR	556.400	1438.000	551.500	1477.000	551.500	1477.000	551.500	1496.000	556.400	1529.000		
1	GR	557.200	1535.000	560.800	1560.000	560.600	1600.000	560.400	1640.000	558.100	1659.000		te de
111	GR	556.500	1670.000	552.200	1699.000	556.300	1712.000	558.700	1719.000	558.300	1740.000		11
	GR	556.700	1748.000	556.200	1750.000	556.200	1754.000	556.200	1761.000	556.700 570.500	1762.000		•
16	GR	560.000	1770.000	560.300	1800.000	560.900	1840.000	570.500	1852.000	0.0	1874.000		12
4	GR	575.000	1889.000	600.400	1936.000	624.800 0.300	0.0	0.0	0.0	0.0	0.0		do
. •	NC FT	0.100	0.100	0.041	0.0	9.100	0.0	0.0	0.0	1256.000	2000.000		
, .	NH	5.000	0.100	1278.000	0.041	1424.000	0.100	1920.000	0.050	1982.000	0.100		
• 2	NH	2118.000	0.0	0.0	2260.000	0.0	0.0	0.0	0.0	0.0	0.0		15
	×1	114.000	39.000	1278.000	1424.000	460.000	660.000	550.000	0.0	0.0	0.0		
	GR	625.300	1000.000	598.900	1046.000	575.500	1099.000	560.200	1172.000	560,600	1180.000		
	GR	560.500	1189.000	561.400	1225.000	560.300	1254.000	558.500	1278.000	558.000	1288.000		10
	GR	557.600	1295.000	558.000	1302.000	558.400	1311.000	557.700	1315.000	551.700	1349.000		19
	GP	551.700	1360.000	551.700	1390.000	557.700	1409.000	558.800	1413.000	560.000	1424.000		•
31	GP	565.000	1454.000	565.500	1486.000	565.000	1518.000	563.100	1604.000	565.300	1680.000		29
- 3	GP	566.300	1741.000	564.100	1810.000	562.400	1875.000	559.500	1920.000	558.400	1930.000		n S
	GR	556.000	1952.000	556.000	1952.000	556.000	1977.000	558.400	1982.000	570.500	2003.000		•
	GR	577.700	2022.000	574.800	2040.000	598.500	2070.000	624.100	2118.000	0.0	0.0		
	NC	0.100	0.100	0.041	0.100	0.300	0.0	0.0	0.0	0.0 1189.000	2230.000		13
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0 2150.000	0.050	2220.000	0.100		
5.0	NH	5.000	0.100	1189.000	0.041	0.0	0.0	0.0	0.0	0.0	0.0		
	IV.	2355.000		V•V	•								10
	X1	115.000	35.000	1189.000	1342.000	480.000	255.000	510.000	0.0	0.0	0.0		26
	GR	625.300	1000.000	615.300	1079.000	611.800	1110.000	599.500	1132.000	574.300	1175.000		77
	GR	565.000	1189.000	560.100	1196.000	559.500	1208.000	555.500	1251.000	559.500	1300.000		•
	GR	560.200	1312.000	565.300	1342.000	566.100	1382.000	566.400	1455.000	565.800	1520.000		13
	GR	566.100	1590.000	566.500	1655.000	567.100	1734.000	566.300	1801.000	563.400	1850.000		129
	GR	564.100	1875.000	563.700	1935.000	563.000	2020.000	561.500	2100.000	559.500	2150.000		•
45	GR	558.600	2157.000	555.000	2180.000	558.600	2209.000	560.000	2320.000	562.300 625.300	2232.000		713h
1000	GR	570.500	2259.000	570.500	2280.000	574.800 0.300	0.0	0.0	0.0	0.0	0.0		31
e 0	NC E.T	0.080	0.080	0.041	0.100	9.100	0.0	0.0	0.0	1283.000	2705.000		79
dig.	NH	5.000	0.080	1283.000	0.041	1375.000	0.100	2639.000	0.050	2691.000	0.100		1
	NH	2942.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		"0
			F4 444	1202 000	1275 000	350 000	300 000	36E 000	0.0		0.0		34
- 6	X1	116.000	56.000	1283.000	1375.000	250.000	280.000	265.000	0.0	0.0 615.100	0.0		15
	GP	624.800	1000.000	624.200	1012.000	623.500	1021.000	620.000	1038.000	575.400	1238.000		
	GP	605.200	1150.000	604.400	1165.000	604.100	1172.000	600.000 553.000	1196.000	553.000	1331.000		
35	GR GR	562.400	1283.000	561.500 560.600	1290.000	560.600 563.800	1375.000	567.000	1399.000	566.600	1423.000		Pi N
(P)	GR	553.000 565.800	1346.000	567.700	1493.000	570.100	1541.000	570.500	1620.000	570.300	1674.000		
	GR	568.400	1747.000	567.800	1794.000	565.400	1850.000	564.000	1903.000	563.400	1950.000		
	GR	564.100	1988.000	564.400	2052.000	564.800	2112.000	565.200	2192.000	565.100	2308.000		"6
2	GR	564.700	2351.000	564.400	2402.000	564.000	2444.000	563.100	2509.000	563.800	2542.000		

CONTRACTOR OF THE		Marie and all a better to the property	Design of a state of the state		2611.000	559.700	2639.000	559,000	2641.000	556.000	2647.000		SSECRETARIA
	GR	562.300	2569.000	560.800	2670.000	559.000	2684.000	560.300	2691.000	570.700	2730.000	96	6
	GR	556.000	2662.000	556.000	2783.060	575.300	2804.000	599.600	2835.000	610.900	2880,000		
	GR	570.700	2750.000	571.800			0.0	0.0	0.0	0.0	0.0		
	GR	625.300	2942.000	0.0	30.00.0	0.0		3802.000	0.050	3870.000	0.080		
•	NH	5.000	0.080	2303.000	0.041	2473.000	0.080		0.0	0.0	0.0		
	NH	3992.000	0.0	0.0	0.0	0.0	0.0	0.0		2303.000	3870.000		300 3
.00	FT	.0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2303.000	3670.000		1 3
•				ANN ARTS							0.0		
	X1	117.000	67.000	2303.000	2473.000	650,000	175.000	525.000	0.0	0.0			353
	GR	624.600	1000.000	620.100	1071.000	600.400	1150.000	600.400	1150.000	600.200	1166.000		1
	GR	595.300	1207.000	592.400	1241.000	589.800	1281.000	589.800	1295.000	584.900	1402.000		•
	GR	588.300	1416.000	588.400	1450.000	586.000	1481.000	585.300	1562.000	575.400	1595.000		-1
	GR	573.200	1644.000	572.600	1662.000	572.600	1820.000	571.500	1833.000	571.500	1922.000		5
7			1963.000	571.500	2048.000	571.500	2070.000	571.500	2080.000	570.500	2103.000		
•	GR	571.500		568.300	2203.000	568.300	2266,000	567.500	2303.000	565.300	2351.000		
,	GR	570.100	2164.000	562.000	2359.000	553.700	2370.000	553.700	2381.000	553.700	2381.000		
18	GR	56%.200	2356.000		2410.000	565.100	2420.000	570.000	2473.000	570.300	2522.000		0
11	GR	562.000	2402.000	564.300		570.100	2700.000	569.400	2755.000	568.800	2830.000		1
12	GR	571.100	2580.000	570.300	2620.000		2990.000	566.000	3040.000	567.500	3100.000		
13	GR	560.600	2894.000	566.400	2943.000	565.800	3400.000	566.500	3600.000	565.800	3788.000		10
•	GR	566.000	3150.000	-567.500	3201.000	566.500	3822.000	557.000	3835.000	557.000	3842.000		10
152	GR	565.000	3802.000	560.500	3814.000	559.200		572.500	3890.000	575.000	3904.000		
TA.	GP	557.000	3856.000	559.200	3858.000	572.500	3870.000	0.0	0.0	0.0	0.0		11
	GR	574.800	3931.000	625.300	3992.000	0.0	0.000		0.0	0.0	0.0		12
	NC	0.100	0.100	0.041	0.100	0.300	0.0	0.0	0.050	3723.000	0.090		
10	NH	5.000	0.080	2041.000	0.039	2242.000	0.080	3615.000		0.0	0.0		11
	NH	3835.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0		3723.000		
	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	2041.000	3123.000		
- 4										0.0	0.0		В
. "	x1	118.000	48.000	2041.000	2242.000	270.000	250.000	265.000	0.0	0.0			
	GR	625.200	1000.000	616.300	1041.000	604.300	1105.000	604.100	1108.000	604.100	1142.000		- "
24	GR	601.300	1151.000	595.100	1205.000	592.800	1267.000	592.800	1277.000	591.100	1296.000		17
25	GR	586.200	1391.000	586.200	1422.000	584.300	1439.000	582.500	1501.000	581.800	1551.000		• 7
● 26	GR	574.800	1591.000	573.800	1600.000	574.900	1603.000	576.100	1621.000	574.200	1644.000		
27		570.100	1682.000	574.100	1722.000	574.100	1743.000	572.800	1762.000	570.500	1800.000		19 2
23	GR	572.300	1891.000	572.100	1903.000	570.900	1958.000	572.100	2000.000	571.900	2041.000		• 9
9 : 21	GR			564.500	2068.000	562,500	2072.000	560.700	2077.000	560.700	2210.000		20
30	GR	570.100	2050.000	570.500	2455.000	570.000	2668.000	566.000	3348.000	568.000	3595.000		21
31	GR	5/10.000	2242.000	560.000	3644.000	558.000	3670,000	558.000	3705.000	568.000	3723.000		
32	GR	568.000	3615.000		3760,000	625.000	3835.000	0.0	0.0	0.0	0.0		92
33	GR	575.000	3736.000	575.000		0.300	0.0	0.0	0.0	0.0	0.0		
34	NC	0.080	0.080	0.039	0.100		0.0	0.0	0.0	0.0	0.0		
35	FT	0.0	0.0	0.0	0.0	11.400	0.0						24
35					-110	435.000	390.000	420.000	0.0	0.0	0.0		
37	X1	119.000	60.000	1892.000	2103.000			0.0	573.100	560.000	0.0		"N
. 15	X3	10.000	0.0	0.0	0.0	0.0	0.0	603.500	1179.000	603.500	1195.000		26
76	GR	625.300	1000.000	611.100	1104.000	605.400	1166.000	589.700	1412.000	586.200	1468.000		
	GR	600.300	1275.000	594.800	1325.000	592.500	1371.000		1607.000	579.800	1635.000		21
	GR	580.300	1544.000	579.800	1551.000	579.800	1603.000	579.800	1712.000	572.500	1751.000		77
	GR	577.200	1644.000	577.200	1681.000	577.000	1690.000	574.600		565.400	1917.000		
	GR	572.500	1763.000	570.500	1810.000	571.100	1881.000	573.100	1892.000	563.400	2037.000		10_
	GR	563.400	1928.000	561.400	1940.000	561.400	1982.000	561.400	2022.000		2709.000		•
* "	GR	564.200	2044.000	572.500	2103.000	571.300	5511.000	570.000	2350.000	567.900			
45	GP	566.700	2944.000	567.600	3022.000	568.100	3167.000	567.900	3182.000	562.300	3209.630		31
46	GR	560.700	3214.000	559.200	3219.000	559.200	3230,000	559.200	3238.000	560.700	3247.000		•
• 4		561.900	3254.000	567.500	3282.000	567.000	3396.000	566.800	3437.000	566.400	3593.000		22
45	GR			560.800	3727.000	559.700	3735.000	560.300	3743.000	574.500	3772.000		n i
44	GR	564.700	3672.000	576.300	3802.000	582.600	3812.000	599.300	3828.000	626.100	3874.000		
● 10	GP	574.500	3792.000			16.400	0.0	0.0	0.0	0.0	0.0		34
- 51	FT	0.0	0.0	0.0	0.0	10.400							
53	Europe					705 000	660 000	765.000	0.0	0.0	0.0		
	X1	120.000	53.000	1379.000	1569.000	795.000	660.000		1087.000	611.000	1099.000		26
	GP	625.600	1000.000	616.300	1029.000	614.100	1068.000	611.200		593.100	1252.000		
- 51	GR	597.500	1140.000	597.300	1163.000	595.700	1166.000	594.700	1201.000		1379.000		20
55	GR	576.500	1296.000	576.500	1308.000	576.500	1314.000	576.500	1340.000	575.200			
● 56	GP	568.900	1401.000	565.800	1418.000	563.000	1433.000	563.000	1468.000	563.000	1500.000		
. 57				566.900	1528.000	573.500	1569.000	572.900	1720.000	572.000	1912.000		39
56	GR	565.800	1520.000		2380.000	567.300	2417.000	564.600	2440.000	563.400	2444.000		
-	GR	569.800 560.800	2206.000	566.000 560.800	2460.000	560.800	2460.000	563.400	2473.000	564.200	2480.000		

A STATE OF	GR	568.200	2499.000	567,400	2609.000	568.100	5640.000	565.300	2804.000	564.400	2829.000		
	GR	566.300	2851.000	568.300	3022.000	566.100	3198.000	565.600	3262.000	562.700	3314.000	07	
•	GR	560.800	3319.000	561.500	3323.000	562.700	3388.000	573.100	3431.000	573.300	3451.000	97	1
	GR	576.700	3459.000	599.400	3483.000	626.100	3535.000	0.00	7100.0cm	0.0	0.0		
	NC	0.080	0.080	0.039	0.100	0.300	0.000	0.0	3300.030	0.0	0.0		9 7
•	FT	0.0	0.0	0.0	0.0	11.400	0.0	0.0	4.6.0.000	0.0	0.0		1
	1	VENEZUE KAROLE				950 000	780 000	840.000	0.0	0.0	0.0		1
	x !	121.000	45.000	1244.000	1379.000	850.000	780.000		1127.000	599,200	1157.000		1
	GR	625.400	1000.000	612.100	1052.000	601.900	1105.000	599.700	1249.000	564.000	1250.000		7 5
	GB	580.400	1187.000	580.400	1194.000	568.900	1244.000	564.500	1379.000	572.800	1404.000		3
-	GR	564.000	1311.000	564.000	1370.000	564.500	1371.000	570.000		574.100	2109.000		
	GR	571.400	1563.000	570.500	1748.000	571.200	1897.000	572.800	1953.000	564.000	2399.000	The state of the s	1
	GR	572.800	5515.000	570.800	2325.000	567.700	2364.000	564.800	2390.000	566.800	2550.000		5
•	GR	562.100	2418.000	564.000	2437.000	564.800	2445.000	567.200	2477.000 -	567.200	3145.000		1
	GP	564.600	2616.000	566.900	2667.000	567.500	2802.000	568.000	2998.000	567.300	3455.000		
	ER .	568.200	3398.000	570.600	3434.000	568.300	3442.000	566.800	3449.000	624.700	3561.000		100
	GR	577.900	3472.000	577.900	3488.000	580.100	3500.000	601.300	3522.000	0.0	0.0		3
,	12 NC	0.080	0.000	0.039	0.100	0.300	87000 000	0.0	0.0	0.0	0.0		7
1	ОТ		20000.000	38000.000	48800.000	48800.000	87000.000	0.0	0.0	0.0	0.0		19
	FT	0.0	0.0,	0.0	0.0	10.400	0.0	0.0	0.0	F13	A S VIII NO B		10
	13 200	100	111111111111111111111111111111111111111	1261 262	1352 000	720.000	650.000	715.000	0.0	0.0	0.0		1)
	X1	122.000	51.000	1261.000	1352.000		1074.000	602.800	1094.000	582.700	1128.000		"
	# GR	624.300	1000.000	605.300	1067.000	602.800 572.800	1176.000	576.700	1231.000	574.800	1252.000		12
	GR	582.600	1135.000	581.100	1150.000	572.800 565.000	1278.000	565.000	1303.000	565.000	1325.000	The second second	
)	GR	573.400	1261.000	570.500	1267.000	565.000 575.200	1383.000	576.700	1432.000	573.800	1530.000		
. •	GR	570.500	1342.000	573.600	1352.000	575.200 575.600	1383.000	574.800	2066.000	574.100	2200.000		4
	GR	575.500	1575.000	576.100	1789.000	575.600 568.900	2533.000	563.200	2567.000	570.800	2590.000		16
	a GR	573.800	2301.000	571.900	2450.000	568,900	2619.000	563.200	2628.000	563.000	2638.000		
	a) GR	567.100	2603.000	565.500	2609.000	563.000 572.300	2710.000	568.800	2750.000	569.200	2879.000		14
	, GR	565.500	2648.000	568.100	2658.000	572.300 570.100	3358.000	578.200	3412.000	581.300	3448.000		1
	GR	567.200	3066.000	568.300	3188.000		3512.000	598.100	3530.000	599.800	3537.000		
	GP	580.200	3464.000	580.300	3483.000	598.100	0.0	0.0	0.0	0.0	0.0		N N
7	GR	624.700	3597.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10 2
	NC	0.080	0.080	0.039	48800.000	42400.000	87000.000	0.0	0.00	0.0	0.0		
	OT	5.000	20000,000	38000.000	0.0	17.400	0.0	0.0	0.0	0.0	0.0		20
	FT	0.0	0.0	0.0	0.0	11.400	THE REPORT OF THE PARTY OF THE	THE RESERVE OF THE PERSON NAMED IN		46.00	1700 March 1880		7)
	W.3	122 000	42 000	1328.000	1502.000	550.000	600.000	545.000	0.0	0.0	0.0		
	M X1	123.000	43.000	610.300	1039.000	608.200	1073.000	603.100	1105.000	594.600	1199.000		p A
	GP GP	624.800		594.800	1239.000	574.600	1278.000	573.900	1311,000	573.300	1328.000		II .
	S GR	594.600	1222.000	567.000	1350.000	567.000	1408.000	567.000	1470.000	571.100	1478.000		
. •	s GP	571.100 575.200	1335.000	578.300	1502.000	576.100	1575.000	574.100	1648.000	573.500	1950.000		A.
1	GP	575.200	2200.000	573.500	2450.000	574.200	2738.000	573.500	2922.000	572.000	3100.000		22
		574.000	3132.000	567.000	3147.000	564.700	3156.000	564.700	3167.000	564.700	3178.000		
	GR		3188.000	568.800	3195.000	573.100	3218.000	571.400	330000	571.500	3400.000		Wat .
	GP	573.100	3550.000	582.100	3580.000	582.100	3601.000	582.100	3629.000	583.500	3675.000		11
	GR	584.100	3709.000	599.800	3738.000	624.800	3778.000	0.0	0.004	0.0	0.0		•
	M GR	0.080	0.080	0.039	0.100	6,300	0.0	0.00	0.0.0	0.0	0.0		21
	OT	5.000	17200.000	32900.000	42400.000	42400.000	77000.000	0.0	0.0	0.0	0.0		25
	ET	0.0	0.0	0.0	0.0	11.400	0.0	0.0	0.0	0.0	0.0		
	1	0.00					w0.48 (96)		1100000	Part of the second	0.0		Operation of
	×1	123.500	34.000	1328.000	1545.000	300.000	1500.000	300.000	0.0	0.0	0.0		31
	. X3	10.000	0.0	0.0	7 0 . 0	0.0	0.0	0.0	573.300	579.000	0.0		•
	GR	624.800	1000.000	610.300	1039.000	608.200	1073.000	603.100	1105.000	594.600	1199.000		4 4
	GR	594.600	1555.000	594.800	1239.000	574.600	1278.000	573.900	1311.000	573.300	1328.000		10
	GP	571.100	1335.000	567.000	1350.000	567.000	1408.000	567.000	1470.000	571.100	1478.000		•
	GR	575.200	1487.000	581.000	1545.000	580.000	1580.000	575.000	1880.000	573.500	2580.000		ar A
	GR	575.000	2700.000	573.500	2850.000	575.000	2930.000	572.000	3170.000	575.000	3500.000		25
_	GR	580.000	3700.000	578.000	4100.000	580.000	4270.000	580.000	4470.000	590.000	4680.000		
	GP	590.000	4710.000	595.000	5450.000	600.000	5580.000	625.000	5700.000	0.0	0.0		
	NC	0.080	0.080	0.039	0.300	0.800	0.0	0.0	0.0	0.0	0.0		St.
	FT	0.080	0.0	0.0	0.0	8.400	0.0	0.0	0.0	0.0	0.0		
	GI STATE OF	0.0	1977 1889					500,000	1955		0.0		T'
	s X1	124.000	39.000	1266.000	1556.000	320.000	350.000	320.000	0.0	0.0	0.0		21
_	50 X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	592.800	579.500	0.0		
•	GR	629.300	1000.000	611.800	1056.000	599.800	1075.000	583.000	1095.000	583.000	.000		
					1111 666	***					1		

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ALCOHOL:	Dr. Ta Mark	Section when I retrieve to the selection	andrea, in the his second in the second	MANAGEMENT	amounts in 10 do , water , w , w , water	The same of the parameter		575,700	1187.000	580.300	1196.000	CALLED BY A THE WILLIAM A CALLED BACK	
	GR	575.300	1127.000	580.500	1160.000	577.100	1326.000	580.700	1350.000	575.700	1371.000	98	
	GR	592.800	1266.000	590.700	1310.000	568.000	1443.000	568.000	1502.000	571.800	1513.000	- 00	
	GR	571.800	1387.000	568.000 585.500	1403.000 1556.000	587.000	1856.000	582,500	2101.000	581.000	2400.000		
	GR	574.100	1520.000	573.000	2830.000	575.000	2930.000	580.000	3300.000	580.000	3480.000		
•	GR	575.000	2700.000	580.000	3730.000	581.000	4050.000	585.000	4480.000	590.000	4530.000		
	GR	577.500	3650,000	595.000	5200.000	600.000	5330.000	625.000	5520.000	0.0	0.0		
	· · ·	340.000	4560.000	193.000	3200.000	000.000	2000.000	673.155	500,500	175 - 58	1835,058		
2	×1	124.100	0.0	0.0	0.0	115.000	350.000	115.000	0.0	0.600	13 0.00		2
	x3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	593.400	580.100	0.0		
-	NC	0.080	0.080	0.041	0.300	0.800	0.0	0.0	0.0	0.0	0.0		10
	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	5 0.0	0.0		4
	P STATE OF		7.00000000			CONTRACTOR CONTRACTOR		1.000.000	18,000,000				11. 14
	X1	126.010	39.000	1269.000	1425.000	115.000	350.000	115.000	0.0	0.0	0.0		,0
	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	591.000	581.500	0.0		6
	GR	630.400	1000.000	630.200	1009.000	624.400	1029.000	600.500	1100.000	594.200	1108.000		7
6 11	GR	580.700	1138.000	581.700	1238.000	581.700	1251.000	575.900	1269.000	575.900	1269.000		9
	GR	568.000	1334.000	568.000	1347.000	568.000	1393.000	576.600	1408.000	577.600	1425.000		
- 17	GR	577.600	1425.000	580.000	1440.000	580.000	3590.000	592.000	3618.000	592.000	3638.000		9
	GB	592.300	3655.000	593.900	3691.000	594.100	3814.000	594.500	3913.000	594.700	4001.000		9
1	GR	594.800	4071.000	594.900	4144.000	594.800	4231.000	594.500	4333.000	594.600 599.800	4782.000		
16	GR	594.900	4481.000	597.600	4558.000	598.900	4653.000	598,900	4744.000	0.0	0.00		H 🛌
9 13	GR	603.800	4843.000	609.600	4901.000	620.500	4960.000	630.200	1.280	568.000	568.000		
11	, SR	0.900	1.500	3.000	0.0	106.000	6.000	2470.000	1.200	505.000	300000		
11		104 000		0.0	0.0	80.000	80,000	80.000	0.0	0.00	0.0		13
9 21	X1	126.020	0.0	1.000	584.700	585.500	0.0	0.0	0.0	0.0	0.0		1,
2	X3	10.000	0.0	0.0	0.0	0.0	0.0	0.0	593.100	585.500	0.0		
1	RT.	42.000	1157.000	595.300	0.0	1184.000	590.500	0.0	1216.000	594.200	0.0		15
2	RT	1239.000	594.200	0.0	1335.000	593.700	0.0	1508.000	592.500	0.0	1594.000		18
7	RT	592.100	0.0	1667.000	591.900	0.0	1716.000	591.700	0.0	1813.000	591.500		
2	BT	0.0	1883.600	591.200	0.0	1932.000	590.700	0.0	2043.000	589.500	0.0		"e .
9 2	RT	2184.000	589.200	0.0	2312.000	588.500	0.0	2418.000	587.900	0.0	2567.000		18: 8
2	RT	587.100	0.0	2727.000	586.700	0.0	2814.000	586.400	0.0	2912.000	586.10.0		10
	BT	0.0	3051.000	585.900	0.0	3161.000	585.500	0.0	3374.000	585.500	0.0		0
	BT	3497.000	585.500	0.0	3612,000	585 500	0.0	3745.000	585.500	0.0	3869.000		20
	RT	586.100	0.0	3967.000	586.600	0.0	4057.000	588.000	0.0	4210.000	592.000		21
	AT	0.0	4227.000	592.300	0.0	4263.000	593.900	0.0	4386.000	594.100	0.0		0
1	RT	4485.000	594.500	0.0	4573.000	594.700	0.0	4643.000	594.800	0.0	4716.000		[17] [17]
. 3	RT	594.900	0.0	4803.000	594.800	0.0	4905.000	594.500	0.0	5002.000	594.600		23
	RT	0.0	5053.000	594.900	0.0	5130.000	597.600	0.0	0.0	0.0	0.0		G. 8
1 3	NC NC	0.100	0.060	0.039	0.300	0.800	0.0	0.0	0.0	0.0	0.0		74
3	FT	0.0	0.0	0.0	0.0	8.400	0.0	0.0	0.0	0.0	1001.000		25
		127 000	40.000	1103 000	1254.000	900.000	100.000	835.000	0.0	0.0	0.0		26
3	X1	127.000	42.000	1103.000	1047.000	582.800	1087.000	582.800	1103.000	575.700	1117.000		
4	GR	630.400 574.500	1000.000	570.500	1160.000	570.500	1176.000	570.500	1179.000	574.500	1228.000		11
	GR	575.400	1239.000	578.900	1254.000	581.000	1295.000	580.900	1392.000	581.900	1524.000		28
	GP	580.500	1632.000	581.300	1674.000	580.100	1730.000	579.600	1805.000	584.500	1895.000		
	GR	584.500	3065.000	592.000	3093.000	592.000	3113.000	592.300	3702.000	593.900	3738.000		121
. 4	GR	594.100	3861.000	594.500	3960.000	594.700	4048.000	594.800	4118.000	594.900	4191.000		100
	CP	594.800	4278.000	594.500	4380.000	594.600	4477.000	594.900	4528.000	597.600	4605.000		45
	GR	598.900	4700.000	598.900	4791.000	599.800	4829.000	603.800	4890.000	609.600	4948.000		•
	GR	620.500	5007.000	630.200	5079.000	0.0	0.0	0.0	0.0	0.0	0.0		32
	NC	0.100	0.080	0.039	0.100	0.300 ·	0.0	0.0	0.0	0.0	0.0		13
	FT	0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0		•
									2017 000		1000,000		2834
51	X1	128.000	50.000	1111.000	1250.000	750.000	350.000	750.000	0.0	0.0	0.0		33
9 5	GR	650.300	1000.000.	625.600	1027.000	600.200	1066.000	583.400	1092.000	583.400	1111.000		9
51	GR	576.200	1129.000	572.000	1139.000	572.000	1189.000	572,000	1226.000	576.200	1454.000		36
51	GR	577.600	1250.000	581.200	1278.000	582.300	1323.000	583.100	1394.000	583.300 580.600	1721.000		87
● 50	GP	583.500	1509.000	580.100	1522.000	580.100	1580.000	580.300	1642.000	580.100	1960.000		9
57	GR	582.200	1801.000	583.100	1877.000	583.800	1892.000	583.000 585.500	2551.000	592.000	2579.000		
	GR	580.700	2025.000	582.800	2066.000	585.500	2116.000	594.100	3347.000	594.500	3446.000		37
6 51	GR	592.000	2599.000	592.300	3188.000	593.900 594.900	3224.000 3677.000	594.800	3764.000	594.500	3866.000		3
	GP	594.700	3534.000	594.800	3604.000	554.900	3011.000	334.000	31375003				

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	NO.	594.600	3963,000	594.900	4014.000	597.500	4091.000	598.900	4186.000	598.900	4277.000	99	ATT CHICAGO
	GR	599.800	4315.000	603.800	4376.000	609.600	4434.000	620.500	4493.000	630.200	4565.000	33	0
	NC	0.100	0.090	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0		
	ET	0.0	0.0	0.000	0.0	6.400	0.0	0.0	0.0	0.0	0.0		
•	X1	129.000	44.000	1144.000	1265.000	390.000	475.000	415.000	0.0	0.0	1160.000		
	GR	650.300	1000.000	625.600	1039.000	599.000	1083.000	585.300	1103.000	585.300	1122,000		
•	GR	578.500	1144.000	576.600	1158.000	573.500	1180.000	573.500	1200.000	573.500	1220.000		10
	GR	576.500	1251.000	577.900	1265.000	579.800	1298.000	581.600	1332.000	579.100	1357.000		
	GR	578.400	1377.000	581.000	1424.000	581.500	1476.000	582.400	1503.000	580.100	1532.000		
4	GR	581.100	1578.000	582.700	1649.000	581.900	1707.000	582.300	1815.000	582.500	2002.000		10
	. GR	583.900	2092.000	584.300	2225.000	582.700	2302.000	592.200	2346.000	592.200	2368.000		
	GR	594.100	2383.000	594.400	2511.000	594.700	2689.000	594.800	2835.000	594.900	2933.000		
•	GR	594.800	3081.000	594.900	3151.000	598.000	3242.000	598.100	3344.000	598.400	3415.000		
	GR	602.500	3479.000	609.900	3551.000	621.500	3632.000	630.600	3736.000	0.0	0.0		
	, NC	0.100	0.090	0.041	0.100	0.300	0.0	0.0	0.0	0.0	13:0.00		
	, FT	0.0	0.0	0.0	0.00	8.400	0.0	0.0	0.000	0.0	0.0		0
1	×ı	130.000	57.000	1066.000	1180.000	620.000	880.000	632.000	0.0	0.0	0.0		779
	GR	650.500	1000.000	625.600	1015.000	600.200	1024.000	589.400	1042.000	589.100	1057.000		'-
	GR	584.200	1066.000	578.000	1073,000	572.000	1104.000	578.000	1141.000	579.200	1154.000		
	GR	583.000	1180.000	578.700	1200.000	583.200	1237.000	584.700	1281.000	584.700	1355.000		
-	GR	584.500	1416.000	584.900	1487.000	584.600	1564.000	584.900	1612.000	584.900	1669.000		
	GR	585.800	1719.000	585.400	1781.000	586.100	1827.000	587.500	1887.000	586.400	1946.000		12
	GR	587.000	2001.000	587.400	2058.000	587.700	2118.000	584.800	2193.000	584.400	2270.000		18 . 8
	GR	584.100	2372.000	585.300	2468.000	585.800	2561.000	586.100	2660.000	586.300	2765.000		
	GR	586.100	2803.000	595.300	2827.000	595.300	2850.000	595.300	2885.000	595.300	2975.000		4
	GR	603.800	3000.000	605.200	3052.000	606.400	3133.000	604.900	3207.000	604.900	3255.000		15
	GR	606.000	3276.000	607.800	3382.000	608.100	3450.000	609.700	3514.000	610.800	3589.000		
	H GR	614.000	3633.000	614.800	3660.000	616.400	3686.000	625.200	3747.000	627.700	3772.000		14
	GR	636.400	3800.000	649.800	3853.000	0.0	0.0	0.0	0.0	0.0	0.0		
	NC	0.050	0.090	0.041	0.100	0.300	3740.00	0.0	3 20 . 0	0.0	0.0		0,
	FT	0.0	0.0	0.0	0.0	10.400	74 70.004	0.0	0.0	0.0	0.0		2-RI
-	X1	131.000	69.000	1943.000	2075.000	500.000	550.000	800.000	0.0	0.0	0.0		IT ON
	GR	635.100	1000.000	624.900	1024.000	607.000	1073.000	589.400	1113.000	589.400	1122.000		11
	GR	579.700	1137.000	577.000	1141.000	579.700	1150.000	582.900	1161.000	586.600	1191.000		
-	GR	586.600	1296.000	586.900	1417.000	586.900	1546.000	588.000	1631.000	588.200	1755.000		Ta l
	GR	589.500	1841.000	589.000	1923.000	584.700	1943.000	581,600	1955.000	577.000	1974.000		10
	GR	577.000	2005.000	577.000	2019.000	581.600	2063.000	582.800	2075.000	584.900	2103.000		
(0)	, GR	584.900	2161.000	584.900	2218.000	583.700	2244.000	584.600	2282.000	582.000	2304.000		0
	GP GP	584.700	2325.000	586.700	2348.000	585.500	2377.000	585.100	2396.000	586.600	2416.000		21
	GP	588.000	2435.000	585.600	2455.000	587.000	2487.000	587.000	2535.000	586.400	2581.000		
	GP	586.400	2640.000	587.400	2701.000	587.800	2774.000	588.600	2822.000	587.700	2937.000		0
	GR	587.900	3006.000	587.900	3076.000	590.200	3138.000	589.800	3189.000	588.200	3227.000		
	GR	596.600	3251.000	596.600	3256.000	600.700	3273.000	600.200	3302.000	600.800	3330.000		и .
	GR	604.400	3350.000	605.600	3412.000	606.900	3526.000	608.000	3618.000	612.500	3751.000		9
	GR	612.900	3824.000	613.500	3882.000	613.300	3897.000	613.800	3923.000	614.900	3967.000		. 1
	GR	615.700	3988.000	625.200	4030.000	636.500	4072.000	650.600	4135.000	0.0	0.0		29
	NC FT	0.050	0.090	0.041	0.100	7.400	0.0	0.0	0.0	0.0	0.0		
0	×1	132.000	69.000	2301.000	2492.000	340.000	250.000	550.000	0.0	0.0	0.0		· o .
	GR	637.400	1000.000	614.800	1033.000	589.700	1090.000	589.700	1102.000	582.400	1117.000		12 014
	GR	580.500	1121.000	582.400	1131.000	585.400	1148.000	586.800	1200.000	587.300	1269.000		
	GR	588.200	1344.000	588.100	1451.000	588.500	1585.000	589.700	1688.000	589.600	1768.000		O NRC
	GR	587.400	1847.000	586.900	1878.000	589.600	1930.000	588.400	2005.000	587.400	2086.000		34 0
4	GR	586.600	2132.000	587.400	2146.000	589.400	2198.000	589.800	2284.000	589.400	2301.000		T) TE
	GR	586.600	2315.000	584.500	2322.000	580.000	2339.000	584.500	2360.000	586.000	2371.000		0 3
	GR	586.300	2372.000	584.500	2379.000	580.000	2395.000	580.000	2417.000	580.000	2430.000		11 1
	GR	584.500	2470.000	586.000	2483.000	586.800	2492.000	587.400	2565.000	588.300	2597.000		. 6
	GR	587.200	2684.000	585.600	2715.000	588.000	2755.000	587.500	2819.000	589.200	2872.000		9
5	GR	590.200	2941.000	590.800	3001.000	590.600	3089.000	590.400	3130.000	587.100	3173.000		38 10
51	GR	587.600	3194.000	606.000	3254.000	606.600	3332.000	607.600	3373.000	606.000	3386.000		- 19
20 S	GR	606.000	3413.000 3670.000	605.600	3422.000 3803.000	608.300	3455.000 3905.000	617.200	3538.000 4005.000	609.900	3595.000 4036.000		9
	GR	612.200											

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						À					The state of the s	PROPERTY AND THE PROPERTY OF T	
	GR	613.500	4056.000	625.900	4075.000	637.400	4112.000	549.800	4154.000	0.0	7770.077	100	
•	NC	0.060	0.100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
			SAPER CORN		3279,000			EAS . OUR	3万年李子斯安斯		474 475		
	X1	133.000	92.000	3156.000	3387.000	345.000	210.000	560.000	0.0	0.0	0.0		
•	GR	635.400	1000.000	613.800	1033.000	599.900	1059.000	588.000	1087.000	588.000	1102.000		•
	GR	584.900	1118.000	584.500	1134.000	583.800	1148.000	583.100	1162.000	583.800	1168.000		
	GR	585.400	1183.000	587.500	1209.000	589.800	1292.000	589.500	1382.000	589.800	1453.000		
6 2	GR	589.800	1571.000	589.800	1663.000	589.900	1767.000	589.300	1868.000	588.800	1968.000		0
	GR	590.400	2045.000	591.100	2078.000	589.600	2124.000	589.200	2144.000	590.600	2170.000		
	GR	591.600	2216.000	590.100	2272.000	589.200	2337.000	589.100	2388.000	590.400	2454.000		
•	GR	590.800	2534.000	591.000	2566.000	589.200	2590.000	587.000	2600.000	586.400	2603.000		· •
	GR	586.400	2642.000	587.000	2646.000	589.600	2666.000	591.300	2692.000	589.300	2733.000		4
7	GR	595.100	2775.000	593.100	2816.000	591.600	2887.000	590.800	2896.000	586.500	2910.000		
•	GR	586.400	2911.000	586.400	2925.000	586.500	2926.000	587.200	2937.000	589.600	2950.000		0
,	GR	587.800	2976.000	589.400	2997.000	589.300	3048.000	589.300	3127.000	587.800	3156.000		6
10	GR	586.400	3165.000	587.700	3174,000	586.200	3190.000	580.800	3260.000	586.200	3316.000		7
•	GR	586.600	3323.000	587.100	3337.000	586.200	3356.000	585.500	3372.000	586,200	3375.000		
12	GR	588.900	3387.000	590.700	3414.000	590.500	3503.000	590.500	3599.000	586.100	3664.000		8
13	GR GR	586.100	3680.000	595.800	3730.000	596.200 605.300	3775.000	596.800 610.700	3800.000	604.700	3837.000 4021.000		
9 16	GR	605.400	3882.000 4048.000	604.700	3932.000 4107.000	610.400	4160.000	614.200	4215.000	612.600 614.800	4292.000		
15	GR	615.700	4397.000	616.500	4478.000	620.100	4494.000	620.100	4513.000	625.800	4533.000		111111111111111111111111111111111111111
16	GR	637.000	4572.000	650.500	4619.000	0.0	0.0	0.0	0.0	0.0	0.0		11
12	NC	0.080	-0.060	0.039	0.100	0.300	8-0.0	610.000	0.0	0.0	0.0		
18									7777 F 10 10 10 10 10 10 10 10 10 10 10 10 10	- ENR. 208	The state of the s		".
	X1	134.000	61.000	3259.000	3372.000	200.000	920.000	865,000	0.0	0.0	0.0		3
	GR	637.800	1000.000	625.200	1018.000	600.300	1057.000	589.400	1091.000	589.400	1105.000		
	GR	584.800	1122.000	584.200	1132.000	583.800	1139.000	584.200	1146.000	585.200	1160.000		
	GR	588.300	1184.000	587.500	1308.000	588.300	1371.000	589.700	1450.000	590.400	1531.000		15
	GR	591.000	1648.000	590.800	1718.000	591.900	1833.000	592.800	1889.000	590.200	1934.000		16
25	GR	591.300	2018.000	591.900	2049.000	590.700	2075.000	590.700	2140.000	591.100	2159.000		
2 21	GR	590.200	2175.000	591.000	2190.000	592.400	2241.000	591.500	2333.000	589.600	2378.000		"9
71	GR	590.400	2406.000	589.400	2441.000	590.700	2490.000	591.200	2550.000	590.100	2600.000		18
	GR	588.700	2616.000	587.400	2627.000	586.200	2638.000	587.400	2650.000	589.400	2670.000		
20 20	GR	589.700	2705.000	588.200	2742.000	592.100	2790.000	595.700	2846.000	589.900	2946.000		"0
32	GR	591.500	3072.000	591.400	3156.000	590.900	3239.000	589.600	3259.000	588.700	3272.000		20
31	GR	581.000	3318.000	588.800	3363.000	592.200	3372.000	610.300	3410.000	611.900	3432.000		
22	GR	609.300	3458.000	610.800	3499.000	610.800	3518.000	625.000	3544.000	636.400	3582.000		l'o
37	GP	650.200	3623.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		27
30	NC	0.0	0.070	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		.,
25	FT	0.0	0.0	0.0	0.0	5.400	0.0	0.0	.0.0	0.0	0.0		
26		198439		40.000		10.000.800		600,300					24
37	× 1	135.000	60.000	3257.000	3387.000	600.000	645.000	625.000	0.0	0.0	0.0		75
9 12	GR	638.600	1000.000	625.800	1034.000	599.700	1095.000	590.800	1131.000	590.800	1146.000		0
31	GB	590.100	1169.000	590.800	1225.000	592.600	1304.000	591.900	1373.000	591.000	1407.000		" "
40	CB	591.500	1457.000	592.300	1515.000	592.700	1612.000	592.900	1668.000	591.600	1717.000		η
9 a	GR	589.300	1727.000	588-600	1730.000	589.300	1752.000	590,000	1775.000 2081.000	592.400 595.000	1831.000 2150.000		0
47	GR	593.800	1862.000	593 000	1935.000	590.860 591.100	2026.000	593.100 589.700	2537.000	588.500	2559.000		18
63	GR	594.100	2575.000	592.000	2586.000	589.800	2602.000	592.000	2637.000	592.900	2660.000		10
1 41	GR	590.300	2678.000	588.900	2696.000	588.400	27/2.000	588.900	2711.000	590.200	2734.000		9
6	GR	595.300	2778.005	595.600	2882.000	596.000	2979.000	595.500	3095.000	595.100	3107.000		100
41	GR	596.100	3138.000	595.700	3204.000	594.900	3257.000	593.300	3278.000	590.700	3288.000		3)
0	GR	585.000	3312.000	585.000	3336.000	585.000	3359.000	590.700	3378.000	593.300	3387.000		
	GR	616.400	3425.000	618.900	3449.000	618.900	3458.000	625.300	3474.000	650.600	3512.000		- "
47	NC	0.0	0.090	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		33
100	FT	0.0	0.0	0.0	0.0	4.400	0.0	0.0	0.0	0.0	0.0		
57		and the second second								Contract Adjust	1495,045		
	X1	136.000	60.000	2989.000	3168.000	380.000	635.000	575.000	0.0	0.0	0.0		35
	GR	637.300	1000.000	624.800	1058.000	599.600	1106.000	593.200	1152.000	593.200	1166.000		16
	GR	591.100	1196.000	593.900	1285.000	592.500	1408.000	593.200	1547.000	592.900	1630.000		
	GR	589.200	1719.000	590.000	1790.000	589.600	1809.000	588.600	1816.000	586.000	1834.000) P (0)
	GR	586.000	1841.000	588.600	1853.000	591.400	1866.000	594.800	1900.000	592.800	1948.000		38
	GP	592.100	2031.000	594.000	2092.000	595.600	2185.000	595.200	2240.000	593.800	2324.000		
	GR	593.800	2410.000	593.000	2454.000	589.000	2475.000	592.900	2511.000	588.800	2569.000		39
	GR	591.300	2599.000	593.200	2630.000	588.000	2650.000	592.200	2675.000	595.200	2722.000		

											and the second of the second s	
	GR	595.300	2837.000	595.200	2930.000	595.100	2970.000	593.800	2989.000	592.000	3002.000	101
	GR	586.000	3045.000	586.000	3075.000	586.000	3076.000	592.000	3150.000	593.500	3168.000	IUI 🧑
	GR	593.800	3215.000	605.000	3270.000	605.200	3290.000	608.000	3297.000	611.100	3346.000	
	GR	612.900	3447.000	614.600	3509.000	614.600	3547.000	615.500	3568.000	616.800	3621.000	
•	GR	619.700	3665.000	619.700	3677.000	622.000	3700.000	637.000	3746.000	649.300	3795.000	
	NC	0.060	0.350	0.039	40.100	0.300	0.0	0.0	0.0	599.376	0.00	
1	FT	0.0	0.0	0.0	0.0	8.400	0.0	0.0	0.0	0.00	0.0	
•		127 000	FO	0474 000	0470 000	210 000				399 399		0
	X1 GR	137.000	52.000	2476.000	2678.000	310.000	580.000	600.000	0.000	0.0	0.000	2
		637.700	1000.000	624.800	1058.000	600.300	1100.000	596.200	1117.000	596.200	1140.000	, _
•	GR	594.100	1192.000	594.600	1307.000	594.700	1413.000	594.800	3519.000	594.400	1620.000	
	GR	594.800	1706.000	593.200	1725.000	592.700	1791.000	593.100	1828.000	590.200	1847.000	
	GR	590.200	1861.000	592.600	1878.000	593.700	1891.000	592.800	1922.000	594.300	1967.000	
•	GR	594.300	2028.000	594.800	2090.000	595.500	2150.000	595.500	2 72.000	595.300	2296.000	9
	GR	595.100		595.200	2431.000	594.800	2476.000	593.600	2489.000	592.400	2503.000	16
-11	GR	586.500 595.100	2572.000	592.400	2637.000	595.300	2678.000	595.900	2777.000	595.700	2867.000	1_
	GR	600.300	2898.000 3069.000	594.100 601.300	2930.000 3128.000	592.900 605.300	2949.000 3192.000	594.400	2961.000	596.200	3004.000	
	GR	610.300	3304.000	612.200				605.300	3205.000	607.100	3246.000	The second secon
	GR	630.200		649.700	3389.000	612.200	3415.000	614.400	3459.000	615.600	3515.000	
•	NC	0.070	3588.000 0.050	0.039	3653.000 0.100	0.0	0.0	0.0	0.0	0.0	0.0	9
	FT	0.0	0.050	0.0	0.0	9.100	0.0	0.0	0.0	1375.000	2535.000	-
Jan 1		19050333	1498, 556	1705 J. A. 8505	1444 Oct	544 240	1501 000	246 254	10.75.500	13/3.000	2333.000	11
	X1	138.000	56.000	1999.000	2180.000	365.000	650.000	615.000	0.0	0.0	0.0	. 9
	GR	639.000	1000.000	624.800	1062.000	598.500	1101.000	597.700	1128.000	592.200	1159.000	and the second second
•	GR	594.100	1212.000	595.200	1289.000	594.900	1374.000	594.500	1449.000	594.500	1559.000	
	GP	593.900	1624.000	594.800	1689.000	594.100	1770.000	592.200	1788.000	591.000	1803.000	
	GP	590.200	1818.000	594.900	1844.000	595.500	1897.000	593.900	1912.000	595.100	1950.000	
	GR	594.800	1999.000	593.900	2012.000	592.900	2021.000	588.500	2075.000	592,900	2146.000	15
·	GR	593.300	2158.000	594.700	2180.000	594.800	2191.000	593.100	2199.000	588.800	2218.000	, ,
	GR	593.100	2234.000	594,400	2239.000	595.100	2255.000	595.100	2292.000	595.500	2369.000	THE RESIDENCE THE PARTY OF THE PARTY.
•	GR	595.000	2449.000	593.000	2464.000	594.700	2478.000	596.100	2530.000	600.300	2602.000	// A
	GR	595.600	2657.000	596.200	2709.000	600,800	2790.000	600.500	2882.000	600.300	2956.000	14
	GR	600.100	3027.000	596.800	3088.000	596.800	3134.000	596.800	3167.000	598.300	3180.000	
	GR	594.200	3196.000	606.600	3220.000	606.600	3254.000	619.400	3287.000	630.100	3328.000	1,41
	GR	650.200	3393.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	140.000	20
	NC	0.050	0.060	0.0	0.000	0.0	0.0	0.0	0.0	0.0	0.0	
	FT	0.0	0.0	0.0	0.0	9.100	1990.0	0.0	0.000	1285.000	2370.000	l'en
					F 92.700	16 m 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1277.00					hz hz
2	X1	139.000	54.000	1518.000	1724.000	585.000	490.000	590.000	0.0	0.0	0.0	
	GR	642.700	1000.000	625.800	1057.000	600.800	1094.000	600.800	1111.000	595.600	1132.000	"0)
24	GR	598.300	1169.000	600.200	1232.000	599.800	1273.000	600.300	1328.000	598.900	1401.000	H .
	GR	600.500	1451.000	599.800	1489.000	599.400	1518.000	596.400	1542.000	594.200	1564.000	
	GR	593.400	1571.000	589.000	1611.000	589.000	1626.000	589.000	1665.000	593.400	1696.000	fo
1	GR-	594.800	1706.000	596.100	1724.000	595.600	1755.000	595.500	1784.000	593.600	1801.000	la la
46	GR	591.600	1817.000	593.600	1825.000	595.800	1834.000	595.400	1866.000	595.100	1917.000	11
	GR	594.000	1947.000	594.200	1962.000	595.300	1998.000	597.800	2070.000	600.300	2138.000	
1	GR	500.500	2168.000	600.500	2189.000	600.900	2251.000	600.100	2336.000	597.000	2389.000	- 16
47	GR	597.300	2423.000	600.300	2477.000	600.800	2545.000	600.100	2659.000	597.500	2733.000	19
(A)	GR GR	595.900	2828.000	596.000	2887.000	598.400	2900.000	595.700	2907.000	606.200	2928.000	9
45	NC	0.085	2957.000	0.039	0.100	0.300	2982.000	0.0	3025.000	0.0	0.0	10
- 15	FT	0.085	0.050	0.039	0.100	9.100				1310.000	2355.000	n _
	6.80	959 2 60			V • U 11 11 11 11 11 11 11 11 11 11 11 11 1	661.666	0.0	0.0	0.0	1310.000	2333.000	9
	x 1	140.000	53.000	1396.000	1587.000	375.000	335.000	385.000	0.0	0.0	0.0	
W.	GR	649.900	.000.000	637.000	1049.000	625.100	1097.000	598.200	1157.000	598.500	1187.000	b_1
4	GR	597.700	1207.000	601.100	1229.000	601.100	1246.000	600.300	1268.000	601.100	1346.000	9
	GR	600.900	1376.000	598,800	1396.000	594.500	1407.000	593.500	1416.000	589.500	1455.000	³⁴
	GR	589.500	1471.000	589.500	1508.000	593.500	1532.000	594.400	1537.000	593.500	1543.000	3 _
	GR	591.600	1553.000	591.600	1553.000	591.600	1557.000	593.500	1568.000	594.600	1574.000	9
	GR	597.500	1587.000	595.700	1610.000	595.900	1669.000	598.000	1726.000	596.400	1812.000	and the second second second
	GR	595.500	1851.000	595.600	1925.000	600.200	2013.000	601.000	2068.000	600.300	2141.000	
0	GR	599.400	2218.000	598.400	2269.000	596.500	2296.000	597.700	2342.000	601.300	2408.000	9
-52	GR	601.600	2492.000	601.200	2558.000	600.100	2632.000	598.100	2733.000	596,400	2833.000	
50	GR	597.200	2886.000	599,900	2897.000	597.000	2905.000	605.100	2923.000	605.100	2955.000	39
1	GR	607.300	2959.000	625.600	2995.000	650.500	3023.000	0.0	0.0	0.0	0.0	· "•

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* 100 King Aug 18	SHE ALL DESCRIPTION	0.080	0.050	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	SERVICE STREET, STREET
	OT	5.000	17200.000	32900.000	42400.000	42400.000	77000.000	0.0	0.0	0.0	0.0	102 🧸
	FT	0.0	0.0	10.00.000	0.0	9.100	0.0		0.0	1128.000	2315.000	
			7-1000,000			931,186	1984, 220	436,275	1175,644	172.465	1.64.25	
6	XI	141.000	46.000	1252.000	1408.000	940.000	620.000	890.000	0.0	90.00	0.0	O
	GR	650.500	1000.000	634.300	1044.000	606.300	1104.000	606.300	1114.000	594.300	1127.000	
	GR	592.100	1129.000	594.300	1160.000	594.900	1169.000	596.400	1203.000	597.400	1221.000	
6	GR	595.200	1252.000	594.100	1264.000	590.500	1303.000	590.500	1316.000	590.500	1356.000	0)
	GR	594.100	1379.000	595.400	1388.000	602.800	1408.000	601.700	1441.000	601.100	1497.000	
	GR	602.200	1571.000	601.100	1641.000	600.000	1731.000	597.500	1791.000	595.600	1839.000	
5	GR	596.100	1880.000	600.400	1943.000	600.800	2051.000	601.500	2161.000	602.500	2263.000	30
	, GR	602.700	2351.000	603.000	2451.000	601.900	2563.000	600.500	2644.000	598.800	2769.000	
	GP	598.300	2845.000	599.900	2878.000	598.000	2885.000	604.100	2917.000	604.100	2939.000	
	GR	604,100	2946.000	604.100	2985.000	607.400	2994.000	607.400	3009.000	625.900	3043.000	50
2 / 3	GR	650.700	3093.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6
н	NC	0.095	0.050	0.039	0.100	0.300	0.0	0.0	0.0	0.0	0.0	
•	FT	0.0	0.0	0.0	0.0	9.100	0.0	0.0	0.0	1220.000	2335.000	'
11	1						/					1
	XI	142.000	50.000	1277.000	1446.000	365.000	350.000	365.000	0.0	0.0	0.0	
16	GR	650.600	1000.000	638.400	1061.000	629.100	1104.000	625.50.0	1136.000	601.100	1184.000	(0)
1	GR	601.100	1210.000	595.700	1227.000	597.100	1248.000	597.200	1277.000	595.200	1298.000	,
1	GP	594.800	1306.000	592.000	1353.000	592.000	1353.000	592.000	1387.000	594.800	1412.000	
6	GR	595.700	1420.000	598.400	1446.000	598.400	1501.000	596.400	1512.000	599.100	1534.000	"0
1	GR	598.500	1566.000	598.700	1597.000	598.700	1655.000	598.100	1718.000	598.200	1787.000	12
1	GR	598.700	1847.000	599.100	1928.000	600.100	1999.000	598.700	2065.000	600.200	2103.000	
0 2	GR	600.700	2197.000	601.300	2298.000	601.700	2453.000	602.000	2563.000	601.900	2662.000	(6)
1	GR	601.700	2763.000	600.600	2869.000	599.600	2924.000	601.400	2949.000	603.000	2965.000	1 The second
. 2		599.800	2974.000	603.700	3000.000	604.700	3024.000	604.700	3039.000	604.700	3190.000	1 N 2
•	GR NC	614.800	3209.000	614.800	3222.000	625.400	3239.000	637.300	3277.000	649.900	3314.000	"0
2	FT	0.0	0.0	0.0	0.100	0.600	0.0	0.0	0.0	0.0	0.0	IS .
2		0.0	0.0	0.0	0.0	7.400	0.0	0.0	0.0	0.0	0.0	ln_
● 2	×1	143.010	50.000	1222.000	1385.000	260.000	267.000	267.000		-0.700		0
1	GR	650.000	1000.000	637.800	1058.000	626.700	1115.000	625.700	0.0 1179.000		0.0	
	GR	604.800	1214.000	598.500	1222.000	595.800	1228.000	592.000	1236.000	604.800 592.000	1204.000	11
•	GR	592.000	1272.000	595.800	1330.000	596.900	1351.000	600.000	1385.000	601.400	1444.000	
	GR	602.600	1460.000	601.800	1477.000	601.800	1509.000	602.200	1608.000	602.700	1650.000	29
	GR	602.700	1755.000	602.200	1807.000	602.600	1835.000	601.600	1864.000	602.100	1921.000	n 🦡
•	GR	602.200	2003.000	602.600	2102.000	602.800	2223.000	602.400	2319.000	602.000	2433.000	
	GR	602.800	2523.000	603.700	2656.000	604.900	2739.000	604.900	2815.000	606.300	2882.000	
	GR	607.100	2911.000	610.300	2925.000	610.300	2935.000	610.300	2940.000	610.300	2959.000	22 🦡
	GR	612.400	2980.000	612.400	3008.000	613.500	3066.000	613.700	3115.000	614.200	3156.000	11
	GR	614.700	3238.000	615.200	3325.000	616.300	3367.000	627.300	3403.000	650.100	3463.000	
6	NC	0.0	0.0	0.0	0.100	0.300	0.0	0.0	0.0	0.0	0.0	* 5
	FT	0.0	0.0	0.0	0.0	6.400	0.0	0.0	0.0	0.0	0.0	
4												
6 4	×1	143.000	0.0	0.0	0.0	260.000	268.000	268.000	0.0	0.700	0.0	"
47	NC NC	0.0	0.060	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	23
43	FT	0.0	0.0	0.0	0.0	10.400	0.0	0.0	0.0	0.0	0.0	
10 44												r'o.
45	X1	144.000	66.000	1606.000	1796.000	570.000	330.000	600.000	0.0	0.0	0.0	10
- 46	GP	650.100	1000.000	636.400	1067.000	629.200	1126.000	625.800	1163.000	604.800	1195.000	
Ø 97	GR	604.800	1208.000	599.400	1229.000	598,400	1245.000	597.900	1254.000	598.500	1260.000	"0
41	GR	599.600	1271.000	602.200	1328.000	601.600	1379.000	599.300	1419.000	602.900	1453.000	37
- 40	GP	600.400	1482.000	598.900	1506.000	599.200	1526.000	602.300	1566.000	601.600	1606.000	
(0 50	GR	598.900	1638.000	598.000	1646.000	597.000	1656.000	597.000	1700.000	597.000	1754.000	r'a
51	GR	598.000	1759.000	599.600	1767.000	603.500	1796.000	603.500	1831.000	604.400	1888.000	ja ja
- 51	GR	604.000	1939.000	604.600	2008.000	603.000	2068.000	602.100	2106.000	596.300	2143.000	
Ø 53	GR	596.700	2169.001	604.900	2186.000	603.200	2246.000	602.100	2309.000	603.000	2397.000	
31	GR	603.500	2480.000	603.400	2545.000	603.500	2625.000	605.600	2678.000	606.600	2756.000	В.
53	GP	607.900	2840.000	609.000.	2932.000	608.800	2982.000	611.000	3006.000	611.000	3014.000	The state of the s
€ 56	GR	611.000	3034.000	614.400	3049.000	614.400	3070.000	616.000	3091.000	616.900	3149.000	
57	GP	617.300	3229.000	617.100	3301.000	615.600	3313.000	616.300	3349.000	616.800	3422.000	
1	GP	617.600	3489.000	618.300	3571.000	620.100	3621.000	622.900	3644.000	633.100	3683.000	
(59	GR	650.100	3732.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	"0
Side of the	NC	0.0	0.050	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

	ET	0.0	0.0	0.0		0.0	5,400		0.0	0.0	0.0	0	0.0	0.0	103	
5	XI GR GR GR GR GR GR GR GR GR GR GR GR GR	145.000 650.100 608.200 599.300 600.400 604.100 597.800 607.300 613.000 616.700 618.700 649.900	56.000 1000.000 1211.000 1273.000 1450.000 1669.000 2011.000 2340.000 2695.000 3106.000 3313.000 3723.000	1669.000 639.700 608.200 601.306 599.300 600.500 599.000 608.400 613.300 615.700 621.200		860.000 050.000 226.000 298.000 476.000 690.000 821.000 061.000 2419.000 0730.000 146.000 401.000	375.000 637.100 599.300 604.500 604.500 599.000 600.200 608.400 611.400 613.500 614.900 624.600	6 10 12 13 15 16 18 20 24 28	20.000 80.000 47.000 54.000 02.000 99.000 32.000 99.000 77.000 25.000 67.000 0.000	560.000 630.700 597.800 604.100 604.700 597.800 604.400 608.800 610.600 614.400 629.200 0.0	0.0 1135.000 1251.000 1414.000 1572.000 1707.000 1860.000 2128.000 2552.000 2923.000 3181.000 3557.000	622 597 604 604 597 604 607 611 616 617	2.400 7.800 .800 .400 .400 .400 .400 .100 .900 .500	0.0 1188.000 1255.000 1431.000 1618.000 1771.000 1912.000 2230.000 2637.000 3010.000 3241.000 3629.000	100	0 0 6 0 0
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IOA	1000 FEET				HEC-2 a	1000 900 00 00 00 00 00 00 00 00 00 00 00		loodplair	SA AMERICA STREETS	PROFILES	MULTIPLE P	INTOUT FOR	SUMMARY P
		= NGVI = 467.9	,	+ (datu + (- 0.7	NAVD29 468.69		WSEL	loodway	F	C (Carotico 29 63		FFK 100 YFA	
	WSELK	STENCR	STENCL	TOPWID	EG	VSEL	CWSEL Known V	DISCHARGE %CFS<	MIN EL GROUND			HANNEL MIN ENGTH ROAD	
High Water Ma	460.70 461.70	0.0 5243.00	0.0	371.86 343.00	467.10 467.14	680.32	462.24 462.14	58500.00 58500.00		0.0	0.0	0.0	1.01
	0.0	0.0 5283.00	0.0	750.83 453.00	468.98 469.07	2966.91 12893.66		58500.00 58500.00		0.0	0.0	450.00 450.00	1.02
	0.0	0.0 5285.00	0.0 4656.00	1052.12 629.00	470.14 470.24	16061.32 15979.25		58500.00 58500.00		0.0	0.0	680.00 680.00	XS A 1.00
	0.0	0.0 5509.00	0.0 4530.00	2361.30 673.66	471.51 472.22	10181.03		58500.00 58500.00		0.0	0.0	700.00 700.00	B 1.10
	0.0	0.0 5545.00	0.0 4160.00	3443.27 1385.00	471.92 472.79	22346.64 21525.43		58500.00 58500.00		0.0	0.0	230.00	C 5.00
	0.0 0.0	0.0 5689.00	0.0	4087.02 1549.00	472.03 472.91	22891.14 20743.62		58500.00 58500.00		0.0	0.0	125.00 125.00	3.01 3.01
	0.0	0.0 5689.00	0.0	4083.86 1549.00	472.16 473.08	20190.35		58500.00 58500.00		476.10 476.10	467.60 467.60	10.00	3.02 3.02
	0.0	0.0 5689.00	0.0 4140.00	4094.98 1549.00	472.18 473.11	20288.28 18017.59		58500.00 58500.00		476.10 476.10	467.60 467.60	21.00	3.10 3.10
	0.0	0.0 5689.00	0.0	4389.82 1549.00	472.29 473.24	24756.82 22081.39		58500.00 58500.00		0.0	0.0	10.00	3.20 3.20
	0.0	0.0 6100.00	0.0 3850.00	5438.82 2200.39	472.47 473.45	39567.16 39308.01		58500.00 58500.00		0.0	0.0	30.00 30.00	4.01 4.01
	0.0	0.0	0.0 3850.00	5439.61 2200.85	472.47 473.46	39610.01 39341.90		58500.00 58500.00		0.0	0.0	15.00 15.00	4.02 4.02
	0.0	0.0	0.0 3850.00	5811.43 2250.00	475.87 476.02	72525.81 53725.77		58500.00 58500.00		476.00 476.00	474.10 474.10	17.00 17.00	4.10 4.10
	0.0	0.0	0.0 3850.00	5812.21 2250.00	475.87 476.03	72631.94 53792.48		58500.00 58500.00		0.0	0.0	66.00 66.00	4.20 4.20
	0.0	0.0 5918.00	0.0 3540.00	4722.04 1551.59	475.98 476.57	27192.71 15756.96		58500.00 58500.00		484.30 484.30	482.20 482.20	5.00 5.00	5.01 5.01
	0.0	0.0 5918.00	0.0 3540.00	4723.08 1564.60	475.99 476.60	27222.12 15841.16		58500.00 58500.00		484.30 484.30	482.20 482.20	18.00 18.00	5.10 5.10
	0.0	0.0 5821.00	0.0	5355.43 2841.00	476.05 476.91	56191.27 46700.09		58500.00 58500.00		0.0	0.0	5.00 5.00	6.01 6.01
	0.0	0.0 5821.00	0.0	5357.25 2841.00	476.06 476.93	56345.55 46857.13		58500.00 58500.00		0.0	0.0	205.00	D 6.00
	0.0	0.0 5394.00	0.0	5130.95 2554.00	476.09 476.98	56346.86 44941.11		58500.00 58500.00		0.0	0.0	680.00 680.00	E 7.00

	SECTION	CHANNEL MIN	FL OF MA	X FL OF	MIN EL DISCHA	RGF CWSFL	то	EG	TOPWID	STENCL	STENCR	WSELK	105	0
		LENGTH ROAL		W CHORD	GROUND %CFS	<					* .	4		
J	8.00	725.00	0.0	0.0	456.00 58500. 456.00 58500.		57974.20 48733.07	476.13 477.05	4821.38	2480.00	5042.00	0.0		5.01
	G 9:00	30.00	0.0	0.0	456.00 58500.	.00 476.08	56406.45	476.14	4817.53	0.0	0.0	0.0		10
建二十	9.00	30.00	0.0	0.0	456.00 58500	.00 476.95	48126.94	477.06	2577.00	2465.00	5042.00	0.0		1
1	H10.00		0.0	0.0	456.70 58500		51415.77	476.24		0.0	0.0	0.0		'O
7			0.0	0.0	456.70 58500	•00 4//•11	49167.54	477.18	2931.00	1830.00	4761.00	0.0		- '
8	11.00		0.0	0.0	459.40 58500. 459.40 58500.		44880.45	476.30 477.24	4321.93	0.0	0.0	0.0		10
	11.10	75.00	0.0	0.0										
Market In	11.10		0.0	0.0	459.40 58500. 459.40 58500.		44730.84	476.33 477.27	4248.57 3191.00	0.0	0.0 4911.00	0.0		9
	12.01	5.00	480.00	476.90	452.90 58500.	00 476-25	32609.55	476.34	4036.19	0.0	0.0	0.0		0
	12.01		480.00	476.90			31119.73	477.28	3230.89	1670.00	5092.00	0.0		10
	12.10		480.00	476.90			32774.10	476.37	4041.75	0.0	0.0	0.0		110
	12.10	110.00	480.00	476.90	452.90 58500.	.00 477.23	31271.95	477.32	3234.41	1670.00	5092.00	0.0		18
	13.10		0.0	0.0	460.00 58500.		35740.82	476.38		0.0	0.0	0.0		150
	13.10	5.00	0.0	0.0	460.00 58500.	.00 477.22	35420.55	477.33	3356.86	1650.00	5148.00	0.0		
	J13.20		0.0	0.0	460.00 58500.		35992.40	476.41		0.0	0.0	0.0		0
THE REAL PROPERTY.	13.20		0.0	0.0	460.00 58500.	477.25	35997.37	477.36	3377.36	1630.00	5148.00	0.0		16
See	K14.00	635.00	0.0	0.0	456.00 58500.		39976.17	476.45	4236.61	0.0	0.0	0.0		"O.
Still Ma	14.00	0.35.00	0.0	0.0	456.00 58500.	.00 477.29	39507.46	477.42	3228.91	1620.00	4976.00	0.0		ZARE
	16.01 16.01		0.0	0.0	458.00 58500.		27905.69	476.58	3794.65	0.0	0.0	0.0		17/10/0
Tilde.	16.01	654.00	0.0	0.0	458.00 58500.	477.28	27467.27	477.54	2946.19	1545.00	4621.00	0.0	100000000000000000000000000000000000000	75
	16.02		485.70	494.60	458.00 58500.		25448.70	476.59	3277.09	0.0	0.0	0.0		210
***	10.02	10.00	485.70	494.60	458.00 58500.	00 477.28	23544.60	477.55	2308.02	1645.00	4721.00	0.0		
	16.03		485.70	494.60	458.00 58500.		25623.45	476.63	3280.08	0.0	0.0	0.0		D(•)
11211	16.03	76.00	485.70	494.60	458.00 58500.	.00 477.33	23701.59	477.59	2308.25	1645.00	4721.00	0.0		N T
	16.04		0.0	0.0	458.00 58500.		28320.40	476.65	3802.30	0.0	0.0	0.0		80
	16.04	10.00	0.0	0.0	458.00 58500.	00 477.34	27732.50	477.60	2947.29	1545.00	4621.00	0.0		26
	16.00		0.0	0.0	459.00 58500.		33240.89	476.68	4282.23	0.0	0.0	0.0		"O
	16.00	60.00	0.0	0.0	459.00 58500.	00 477.44	30793.43	477.63	2949.29	1585.00	4661.00	0.0	25	78
	18.01		0.0	0.0	459.00 58500.	00 476.75	24640.36	477.03	3696.41	0.0	0.0	0.0		70
TE SERVICE	18.01	738.00	0.0	0.0	459.00 58500.	00 477.70	23972.79	478.01	2627.31	1490.00	4154.00	0.0		20
	18.02		473.10	478.50	459.00 58500.	00 476.91	20408.50	477.05	3711.95	0.0	0.0	0.0		n 🔿
	18.02	10.00	473.10	478.50	459.00 58500.		19442.61	478.03	2630.07	1490.00	4154.00	0.0		37
	18.03	27.00	473.10	478.50	459.00 58500.	00 476-93	20489.92	477.07	3713.83	0.0	0.0	0.0		la o
	18.03		473.10	478.50	459.00 58500.		19515.18	478.05	2630.41	1490.00	4154.00	0.0		м
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		CHANNEL			MAX EL		MIN EL GROUND	MISCHARGE ACES	CWSEL	то	EG	TOPWID	STENCL	STENCR	WSELK		
	18.04		.00	0.0		0.0		58500.00	476.85	25144.52	477.11	3706.09	0.0	0.0	0.0		0
a E	18.04	4 10	•00	0.0		0.0	459.00	58500.00	477.80	24418.22	478.10	2629.06	1490.00	4154.00	0.0		
9	M18.00	0 55	.00	0.0		0.0	459.00	58500.06	476.94	25137.30	477.15	3714.62	0.0	0.0	0.0		10
	18.00		.00	0.0		0.0		58500.00		24431.14	478.13	2630.55	1490.00	4154.00	0.0		1,
	N 19.00			0.0		0.0		58500.00		18708.96	478.50 479.55	3342.07 1821.26	0.0	0.0	0.0		•
7						0.0	460.10	36300.00	410.04	10000.05	419.55	1021.20	2650.00	4535.00	0.0		1
	19.10			0.0		0.0		58500.00	478.79	11320.66	480.41	2136.32	0.0	0.0	0.0		6
1	19.10	0 805	.00	0.0		0.0	461.90	58500.00	479.69	11405.36	481.50	1150.62	2070.00	3291.00	0.0		
1.11	020.00	0 805	-00	0.0		0.0	461-40	58500.00	490.91	10256.30	483.48	2014.26	0.0	0.0	0.0		100
112	20.00			0.0		0.0		58500.00		10634.38	484.44	470.37	2811.63	3282.00	480.81		1
13																	
154	P21.00			0.0		0.0		58500.00		15009.24	484.74	1281.43	0.0	0.0	0.0		0
15	21.00	0 323	•00	0.0		0.40	402.00	36300.00	404.00	14914.00	485.66	367.00	2225.00	2592.00	483.31		110
147	23.01			0.0		0.0		58500.00	483.46	14422.87	486.00	669.83	0.0	0.0	0.0		"0
18	23.01	1 445	•00	0.0		0.0	458.30	58500.00	484.35	15248.57	486.72	276.00	1299.00	1575.00	0.0		
7 25	23.07	2 30	.00	482.5	0 48	35.00	458-30	58500.00	484.64	16099.46	486.81	832.15	0.0	0.0	0.0		12
21	23.02			482.5		35.00		58500.00		16299.26	487.42	276.00	1299.00	1575.00	0.0		14
(2)				7												un es companya de la	11
24	Q23.00	0 55	.00	0.0		0.0		58500.00		17415.54	487.04	841.12	0.0	0.0	0.0		0
25		,	• 00	•		0.0	456.30	36300.00	403.94	17396.73	487.63	276.00	1299.00	1575.00	0.0		
125	R 24.00	0 370		0.0		0.0		58500.00	485.37	13574.36	487.81	946.12	0.0	0.0	0.0		"6
77	24.00	0 370	•00	0.0		0.0	462.80	58500.00	485.76	12880.69	488.50	223.53	1239.00	1472.00	0.0	•	15
29	c 25.00	750	-00	0.0		0.0	465.20	58500.00	48B 70	21180.36	489.44	1384.59	0.0	0.0	0.0		
36	5 25.00	750		0.0		0.0		58500.00		17386.29	490.25	525.00	1365.00	1890.00	0.0		20
31																	71
31	T 26.00			0.0		0.0		58500.00		16448.24	490.31	942.09	0.0	0.0	0.0		
34	20.00	0 450	•00	0.0		0.0	465.50	58500.00	489.38	15801.37	491.01	495.00	1445.00	1940.00	0.0		
35	U27.00	540	.00	0.0		0.0	467.80	58500.00	489.77	19453.89	490.88	733.77	0.0	0.0	0.0		^D •
34	27.00	0 540	.00	0.0		0.0	467.80	58500.00	490.01	16263.53	491.72	340.00	1490.00	1830.00	0.0		24
31	V 28.00	940	. 0.0	0.0		0.0	469 50	58500.00	400 40	14875.47	492.17	592.05	0.0				25
39	V 28.00	940		0.0		0.0		58500.00		14957.45	493.11	320.00	1780.00	0.0	0.0		26
A)																	77 _
	W29.00	790		0.0		0.0		58500.00		20790.27	493.10	1037.87	0.0	0.0	0.0		2
40.07			• 00	0.0		0.0	4/0.10	58500.00	493,41	19907.10	494.10	724.80	1568.20	2293.00	492.43		78
4	X 30.00	410	.00	0.0		0.0	471.00	58500.00	492.87	24675.47	493.38	1018.34	0.0	0.0	0.0		170
45	30.00	410	.00	0.0		0.0	471.00	58500.00	493.84	25335.13	494.38	799.16	1518.94	2321.00	492.87		30
e7	V31.00	575	.00	0.0		0.0	472 00	58500.00	402 10	22809.90	402.70	1251 70			0.0		33
42	Y31.00			0.0		0.0		58500.00		23507.11	493.70	1251.78	0.0	0.0	0.0 493.18		п
4																	32
30	Z 32.00	630.		0.0		0.0		58500.00		15834.91	494.53	913.49	0.0	0.0	0.0		9
2	32.00	6.30	• 00	0.0		0.0	470.80	58500.00	494.33	15662.37	495.45	780.03	1313.00	2093.04	493.34		
																	35

13 🔿

15 A

	MANNEL MIN		X EL OF	MIN EL GROUND	DISCHARGE %CFS<	CWSEL	то	EG	TOPWID	STENCL	STENCR	WSELK	
	380.00	0.0	0.0		58500.00	494 17	22434.83	494,86	1160.05	0.0	0.0	0.0	
AA33.00	380.00	0.0	0.0		58500.00		23318.57	495.76	966.00	1280.00	2246.00	0.0	
AD34-00	480.00	0.0	0.0	475-40	58500.00	494 45	17182.77	495.30	1055.67	0.0	0.0		
AB34.00	480.00	0.0	0.0		58500.00		17417.21	496.20	831.18	1345.28	2176.47	0.0 494.45	
AC35.00	720.00	0.0	0.0	477-60	58500.00	405 37	16453.04	496.12	1548.90	0.0	0.0		
AC35.00	720.00	0.0	0.0		58500.00		16688.48	497.00	1113.39	1235.03	2349.22	0.0 495.37	
AD36.00	740.00	0.0	0.0	474.20	58500.00	496-03	13175.85	497.87	385.17	0.0	0.0	0.0	
AD36.00	740.00	0.0	0.0		58500.00		14029.82	498.55	350.00	2870.00	3220.00	0.0	
36.10	60.00	0.0	0.0	475.00	58500.00	495.85	9094.88	498.39	374.12	0.0	0.0	0.0	
36.10	60.00	0.0	0.0		58500.00		9905.41	498.99	329.32	2629.00		0.0	
36.20	10.00	513.00	532.00	475.00	58500.00	495.93	9168.10	498.44	374.75	0.0	0.0	0.0	
36.20	10.00	513.00	532.00		58500.00		9959.70	499.03	329.52	2629.00		0.0	
36.30	130.00	513.00	532.00	475.00	58500.00	496.80	10007.84	499.01	381.85	0.0	0.0	0.0	
36.30	130.00	513.00	532.00	475.00	58500.00		10608.22	499.50	331.93	2629.00		0.0	
36.40	10.00	96 0.0	0.0	475.00	58500.00	496.85	10044.53	199.05	382.16	0.0	0.0	0.0	
36.40	10.00	0.0	0.0	475.00	58500.00		10640.04	499.54	332.05	2629.00	3130.00	0.0	
38.00	100.00		0.0	476.50	58500.00	498.40	18317.72	499.54	391.05	0.0	0.0	/0.0	
38.00	100.00	0.0	0.0	476.50	58500.00	498.90	18987.16	499.98	365.00	2265.00	2630.00	0.0	
39.00	315.00	0.0	0.0	. 477.60	58500.00	499.54	23146.87	499.97	852.26	0.0	0.0	0.0	
39.00	315.00	0.0	0.0	477.60	58500.00	499.85	20997.67	500.38	699.00	2151.00		0.0	
AE40.00	410.00	0.0	0.0	478.60	58500.00	500.01	50628.57	500.10	1813.74	0.0	0.0	0.0	
40.00	410.00	0.0	0.0	478.60	48800.00		21896.92	500.64	685.00	1780.00	2465.00	0.0	
AF41.00	460.00	0.0	0.0	478.80	58500.00	500.10	63092.50	500.15	2711.76	0.0	0.0	0.0	
41.00	460.00	0.0	0.0	478.80	48800.00	500.64	31928.38	500.81	1205.00	1525.00	2730.00	0.0	
42.01	250.00	0.0	0.0	477.00	58500.00	500.11	41802.78	500.20	2896.01	0.0	0.0	0.0	
42.01	250.00	0.0	0.0	477.00	48800.00	500.67	20387.65	500.99	1270.00	1490.00	2760.00	0.0	
42.02	25.00	0.042	0.0		58500.00	500.12	41937.76	500.21	2896.02	0.0	0.0	0.0	
42.02	25.00	0.0	0.0	477.00	48800.00	500.68	20530.22	501.01	1270.00	1490.00	2760.00	0.0	
42.10	25.00	492.00	493.00	477.00	58500.00	500.12	34587.50	500.22	2896.00	0.0	0.0	0.0	
42.10	25.00	492.00	493.00	477.00	48800.00	500.68	20536.67	501.01	1270.00	1490.00	2760.00	0.0	
42.20	50.00	0.0	0.0		58500.00		41924.42	500.23	2896.07	0.0	0.0	0.0	
42.20	50.00	0.0	0.0	477.00	48800.00	500.73	20580.62	501.05	1270.00	1490.00	2760.00	0.0	
G 43.00	230.00	0.0	0.0		58500.00		67731.44	500.26	3338.24	0.0	0.0	0.0	
43.00	230.00	0.0	0.0	481.00	48800.00	501.01	32173.24	501.14	1460.00	1520.00	2980.00	0.0	
H 44.00	415.00	0.0	0.0		48800.00		18298.09		1621.36	0.0	0.0	0.0	
44.00	415.00	0.0	0.0	480.60	48800.00	501.11	17672.61	501.61	1045.00	1495.00	2540.00	0.0	

													100
UMBER LEN	NNEL MIN EL	/ LOW	EL OF CHORD	GROUND	%CFS<	· CWSEL	TQ	EG	TOPWID	STENCL	STENCR	WSELK	
45.00	420.00	0.0	0.0		48800.00		11911.60	501.19	1238.01	0.0	0.0	0.0	
45.00	420.00	0.0	0.0	481.50	48800.00	501.24	12012.13	502.20	894.00	1780.00	2674.00	0.0	
46.00	565.00	0.0	0.0	482-20	48800.00	501.38	15602.67	501.92	1239.34	0.0	0.0	0.0	
46.00	565.00	0.0	0.0		48800.00		15867.06	502.91	915.00	1645.00	2560.00	0.0	
47.00 47.00	630.00	0.0	0.0		48800.00		13850.42	502.46 503.49	1165.89 780.00	0.0	0.0	0.0	
41.00	030.00	J. U	0.0	404.00	40000.00	302.10	13411.11	303.49	700.00	1310.00	2330.00	0.0	
48.00	610.00	0.0	0.0		48800.00		12099.34	503.36	938.65	0.0	0.0	0.0	
48.00	610.00	0.0	0.0	486.00	48800.00	503.51	12584.90	504.36	595.00	1580.00	2175.00	0.0	
49.00	555.00	0.0	0.0	486.30	48800.00	503.48	13178.26	504.19	723.82	0.0	0.0	0.0	
49.00	555.00	0.0	0.0		48800.00		11934.48	505.27		1503.34	1998.00	503.48	
E0 00	445 00			404.00	40000 05	E00.00	11410 47		FF2 07				
50.00	465.00 465.00	0.0	0.0		48800.00		11412.67	505.05 506.22	553.87 378.91	0.0	2190-00	0.0 503.83	
	.00.00	Mar U	0.0	100.50		304.01	11023.01	200.62		.011.09	2173.00	200.00	
SECTION	DISCHARGE	CWSEL			CWSEL D		EL-WSELK	TOPWID	T.W. D	IFF LEN	IGTH	0.5	
NUMBER 1.010	CFS 58500.000	462	.239	EACH G	FACH SE		0.0	371.863	0.0		0.0		
1.010	58500.000		.136	-0.103			0.0	343.000	28.8		0.0		
	1885 D												
1.020	58500.000		.984	0.0	4.7		0.0	750.832	0.0		0.000		
1.020	58500.000	467	.016	0.032	4.8	50	0.0	453.000	297.8	32 45	50.000		
1.000	58500.000		.694	0.0	1.7		0.0	1052.117	0.0		0.000	,	
1.000	58500.000	468	.755	0.060	1.7	39	0.0	629.000	423.1	17 68	0.000		
1.100	58500.000	470	.087	0.0	1.3	92	0.0	2361.301	0.0	7.0	0.000	- 15 per 4 8 15 per	
1.100	58500.000		.613	-0.474	0.8		0.0	673.660	1687.6		0.000		
					48-00.00								
2.000	58500.000 58500.000		.152	0.0	1.00		0.0	3443.270	0.0		0.000		
2.000	38500.000	4/1	.927	0.775	2.3		0.0	1385.000	2058.2	70 23	0.000		
3.010	58500.000		.415	0.0	0.2		0.0	4087.016	0.0		25.000		
3.010	58500.000	472	.181	0.766	0.2	54	0.0	1549.000	2538.0	16 12	25.000		
3.020	58500.000	471	.299	0.0	-0.1	16	0.0	4083.863	0.0	1	0.000		
3.020	58500.000		.025	0.726	-0.1		0.0	1549.000	2534.8		0.000		
	e27584							100,00	10000				
3.100	58500.000		.329	0.0	0.0		0.0	4094.977	0.0		21.000		
3.100	58500.000	4/2	.058	0.729	0.0	33	0.0	1549.000	2545.9	11 6	21.000		
3.200	58500.000	471	.773	0.0	0.4	44	0.0	4389.816	0.0	i	0.000		
3.200	58500.000	472	•595	0.822	0.5	37	0.0	1549.000	2840.8	16 1	0.000		
4.010	58500.000	673	.314	0.0	0.5	6.1	0.0	5438.816	0.0		30.000		
4.010	58500.000		.260	0.946	0.6		0.0	2200.387	3238.4		30.000		
4.020	58500.000		.318	0.0	0.0		0.0	5439.609	0.0		5.000		
4.020	58500.000	473	.263	0.945	0.0	0.3	0.0	2200.848	3238,7	62 l	5.000		
4.100	58500.000	475	.825	0.0	3.5	08	0.0	5811.430	0.0	1	7.000		
4.100	58500.000		.912	0.086	2.6		0.0	2249.996	3561.4		7.000		
	E0500 055		0.00			0.4	100	E014 015			6 000		
4.200	58500.000 58500.000		.920	0.0	0.0		0.0	5812.215	3562.2		66.000		
	0200000			3.070					,				
5.010	58500.000		.724	0.0	-0.1		0.0	4722.043	0.0		5.000		
5.010	58500.000	475	.386	-0.338	-0.5	34	0.0	1551-586	3170.4	57	5.000		

O

		950, 271, 451, 455		
FISHING	CDEEK	100	VEAD	1

	NNEL MIN EL			DISCHARGE %CFS<	CWSEL	ТО	FG	TOPWID	STENCL	STENCR	WSELK	
50.00 50.00	465.00 465.00	0.0 0.		48800.00 48800.00		11411.62		553.87 378.88	0.0	0.0	503.83 503.83	
51.00 51.00	225.00	0.0 0.		48800.00 48800.00		11155.47		481.02 339.96	0.0	0.0	0.0 504.11	
52.00 52.00	225.00	0.0 0.		48800.00 48800.00	504.27 505.17	9428.89	506.37	391.76 273.81	0.0	0.0	0.0	
52.10 52.10	275.00 275.00	0.0 0.	0 489.60	48800.00 48800.00	504.67 505.64	7462.70	508.51	302.55	0.0	0.0	0.0	
53.00 53.00	275.00 275.00	0.0 0.	0 489.90	48800.00 48800.00	505.78 506.64	7289.76	509.92	294.84	0.0	0.0	0.0 505.78	
54.00 54.00	805.00	0.0 0.	0 491.50	48800.00 48800.00	509.86	8835.27	512.97 513.42	299.20	0.0	0.0	0.0	
55.00 55.00	655.00 655.00	0.0 0.	0 491.80	48800.00 48800.00	512.26	11203.93	514.60	339.30	0.0	0.0	0.0	
56.00 56.00	380.00 380.00	0.0 0.	0 491.70	48800.00 48800.00	513.09	10193.99	515.13 515.40 516.14	195.00 479.61	0.0	0.0	0.0	
57.00 57.00	500.00	0.0 0.	0 493.40	48800.00 48800.00	515.20	13059.20	516.14 516.39 517.29	267.72 693.07 481.26	0.0	0.0	0.0	
58.00 58.00	705.00 705.00	0.0 0.	0 496.50	48800.00 48800.00	516.20	12022.93	517.46	1012.91	0.0	0.0	0.0	
59.00 59.00	360.00 360.00	0.0 0.	0 498.00	48800.00	517.44	16693.35	517.96	1435.84	0.0	0.0	0.0	
60.00	410.00	0.0 0.	0 495.90	48800.00	517.60	12437.23	519.14	1062.63	0.0	0.0	0.0	
SECTION	01SCHAPGE	0.0 0.	CWSFL DIF	48800.00 F CWSEL DI	FF CWS	12333.40 EL-WSFLK	519.92	627.05 T.W. DI	3750.94 4		517.60	
50.000 50.000	CFS 48800.000 48800.000	503.831 504.810	0.0 0.979	0.0 0.0	TION	0.0	553.869 378.877	0.0	465. 91 465.		•	
51.000 51.000	48800.000 48800.000	504.115 505.065	0.0	0.28		0.0	481.018 339.962	0.0	225.	000		
52.000 52.000	48800.000 48800.000	504.267 505.166	0.0	0.15		0.0	391.756 273.807	0.0 117.95	225.	000		
52.100 52.100	48800.000 48800.000	504.667 505.635	0.0	0.40		0.0	302.549	0.0 95.66	275.	000		
53.000 53.000	48800.000 48800.000	505.782 506.636	0.0 0.854	1.11		0.0	294.840	0.0	275.	000		1
54.000 54.000	48800.000 48800.000	509.860 510.150	0.0	4.07		0.0	299.196	0.0	805.			1146.30

TION	CHANNEL MIN EL	OF MA)	C EL OF	MIN EL C	SCES<	CWSEL	> ТО	EG	TOPWID	STENCL	STENCR	WSELK	
50.00		0.0	0.0		48800.00 48800.00		11411.62	505.05 506.23	553.87 378.88	0.0	0.0	503.83	
50200	`						11155.47	505.51	481.02	0.0	0.0	0.0	
51.00		0.0	0.0		48800.00		11129.67	506.73	339.96	1727.41	2061.38	504.11	
52.00	225.00	40	0.0		48800.00		9428.89	506.37	391.76	2023.19	0.0	0.0 504.27	
52.00	225.00	0.0	0.0	489.30	48800.00	505.18	9446.60	507.64	273.81	ZUZ3.19	2231.00	30-02-	
52.10	275.00	0.0	0.0		48800.00		7462.70	508.51	302.55	0.0 1942.51	2149.40	0.0 504.67	7
52.10		0.0	0.0	489.60	48800.00	505.65	7992.05	509.43	206.88	1942.51	2147.40	304.07	
53.00	275.00	0.0	0.0	489.90	48800.00	505.78		509.92	294.84	0.0	0.0	0.0	
53.00		0.0	0.0	489.90	48800.00	506.64	7830.68	510.59	202.00	2107.00	2309.00	505.78	
54.00	805.00	0.0	0.0	491.50	48800.00	509.86		512.97	299.20	0.0	0.0	0.0 509.86	
54.00		0.0	0.0	491.50	48800.00	576 15	8832.00	513.42	195.00	2148.00	2343.00	509.66	
55.00	655.00	0.0	0.0	491.80	48809.00	512.26	11203.93	514.60	339.30	0.0	0.0	0.0	
55.00	*CHRORESPECTORNIA GRADA (TORONICO PERMINA) NO RENOZIONE DE CONTRACA (CONTRACA PERMINA DE CONTRACA PORTA (CONTRACA PERMINA PERM	0.0	0.0	491.80	#800.00	512.29	10506.4	515.13	195.00	1848.00	2043.00	512.26	
F . 0/	380.00	0.0	0.0	191.70	48800.00	513.09	10193.99	515.40	479.61	0.0	0.0	0.0	
56.00		0.0	0.0		48800.00		9163.98	516.14	267.72	1668.00	1935.72	513.09	
			/	403 40	48800.00	515.20	13059.20	516.39	693.07	0.0	0.0	0.0	
57.00		0.0	0.0		48800.00		12948.86	517.29	481.26	1529.00	2010.27	515.20	
						E14 20	12022.93	517.46	1012.91	0.0	0.0	0.0	
58.00		0.0	0.0		48800.00		11905.80	518.39	674.87	1690.30	2365.17	516.20	
50.00	/							517.96	1435.84	0.0	0.0	0.0	
59.00		0.0	0.0		48800.00		16693.35	519.14	645.50	2791.50	3437.00	517.44	
59.00	360.00	0.0	0.0			CONTRACTOR STATE OF THE STATE OF STATE	O NORTH CONTRACTOR TO THE PROPERTY OF THE PROP		1042 62	0.0	0.0	0.0	
60.00		0.0	0.0		48800.00		12437.23	518.92 519.92	1062.63	3750.94	4378.00	517.60	
60.00	410.00	0.0	0.0	493.70	48000.00							0.0	
60.10		0.0	0.0		48800.00		14227.79	519.22	685.55 536.12	3944.00	0.0	518.50	
60.10	41.00	0.0	0.0	495.90	48800.00	519,43	14402.54						
60.2	12.00	0.0	0.0		48800.00		15840.39	520.07 521.06	686.13 550.52	3944.00	0.0	9.0 519.46	
60.21	12.00	0.0	0.0	495.90	48800.00	520.41	16086.64	521.00	350.32	3744.00	117,100		
62.0	417.00	0.0	0.0		48800.00		16570.73	520.53	932.15	0.0	0.0	0.0	
62.0		0.0	0.0	504.50	48800.00	521.06	17477.47	521.52	837.00	3538.00	4375.00	0.0	
63.0	0 544.00	0.0	0.0	505.00	48800.00		26891.23	521.04	2245.33	0.0	0.0	0.0	
63.0		0.0	0.0		48800.00		25373.39	522.03	1785.79	3392.00	5177.80	520.93	
		0.0	0.0	505-30	48800.00	521.19	26329.00	521.26	2217.24		0.0	0.0	
64.0		0.0	0.0		48800.00	[[지사장시아] (1000년][[[[[[[[[[[[[[[[[[[[[[[[[[[[[[[[[[3 26059.95	522.27	1709.08	2562.00	4271.09	521.15	
				E00 30	48800.00	521 - 26	5 25308.73	521.39	2223.61	0.0	0.0	0.0	
65.0		0.0	0.0		48800.00		5 25282.70	522.40	1674.94	2121.45	3796.40	521.26	

110

SECTION NUMBER	CHANNEL			K EL OF	MIN EL GROUND	DISCHARGE %CFS<	CWSEL	TQ	EG	TOPWID	STENCL	STENCR	WSELK	
66.00	350	.00	0.0	0.0	505.70	48800.00 48800.00		18073.69 17905.72	521.58 522.59	2004.54	0.0	0.0 3439.20	0.0 521.41	
67.00 67.00			0.0	0.0		48800.00 48800.00		18083.60 18014.34		2193.85 1625.71	0.0 2067.31	0.0 3693.04	0.0 521.77	
68.00 68.00			0.0	0.0		48800.00 48800.00		12535.21 11990.98		1799.83 1237.58	0.0 1666.49	0.0 2904.06	0.0 522.48	
69.00			0.0	0.0		48800.00 48800.00		8976.00 9154.21	523.68 524.86	1717.83 1129.81	0.0 1535.76	0.0 2665.57	0.0 522.95	*
70.00			0.0	0.0		48800.00 48800.00	525.11 526.04	8759.41 8461.13	525.90 527.15	2057.61 1193.63	0.0 1509.84	0.0 2703.47	0.0 525.11	
71.00 71.00			0.0	0.0		48800.00 48800.00		7741.78 8414.61	528.04 529.02	2102.83 1050.00	0.0 1850.00	0.0	0.0	
72.00 72.00			0.0	0.0		48800.00 48800.00		12549.10 12099.65	529.81 530.75	2262.33 1064.58	0.0 2005.77	0.0 3070.34	0.0 529.41	
73.00 73.00			0.0	0.0		48800.00 48800.00		13958.73 13707.32	530.66 531.63	1568.74 1065.67	0.0 2532.96	0.0 3598.64	0.0 530.30	
74.00 74.00			0.0	0.0		48800.00 48800.00		12744.30 11655.42	531.43 532.46	2078.28 1145.00	0.0	0.0 3436.00	0.0	
75.00 75.00			0.0	0.0		48800.00 48800.00		9244.13 10116.89	532.85 533.79	1440.67 892.17	0.0 2497.31	0.0 3389.48	0.0 531.47	
77.0 77.0			0.0	0.0		48800.00 48800.00		13651.52 12892.33	533.35 534.21	1394.59 905.26	0.0 2173.10	0.0 3102.65	0.0 532.80	
77.02			0.0	0.0		48800.00 48800.00		22272.90 21237.18	535.61 536.35	1505.11 1080.17	0.0 2065.98	0.0 3146.16	0.0 535.35	
77.00 5 77.00		ARREST SERVICE CONTROL CONTROL	0.0	0.0		48800.00 48800.00		22378.24 19050.27	535.64 536.43	1505.92 917.56	0.0 2154.90	0.0 3072.46	0.0 535.38	
78.00 78.00			0.0	0.0		48800.00 48800.00		21869.45 19784.94	536.00 536.90	1395.74	0.0 1393.51	0.0 2336.73	0.0 535.73	
79.00 79.00			0.0	0.0		48800.00 48800.00		13902.55	536.61 537.71	1091.13 681.73	0.0 1468.65	0.0 2150.38	0.0 535.99	
80.00			0.0	0.0		48800.00 48800.00		13372.29	537.22 538.36	777.91 473.05	0.0 1406.98	0.0	0.0 536.40	
81.00 81.00			0.0	0.0		48800.00 48800.00		9134.52 9090.87	538.02 539.18	655.43 391.00	0.0 1424.00	0.0 1815.00	0.0	
82.00 82.00			0.0	0.0		48800.00 48800.00		7825.70 8764.66	540.46 541.27	577.30 473.00	0.0 1265.00	0.0 1738.00	0.0	

TAMES TO SEE

<u> </u>														-112
		HANNEL MIN EL		EL OF CHORD	MIN EL GROUND	DISCHARGE %CFS<	CWSEL	TO,	EG	TOPWID	STENCL	STENCR	WSFLK	
	83.00 83.00	950.00 950.00	0.0	0.0	523.00	48800.00		11415.58	542.97 543.43	901.29	0.0 1135.00	0.0	0.0	
	84.00	700.00	0.0	0.0	525.00	48800.00	543.23	14902.75	543.82	1079.28	0.0	0.0	0.0	
	84.00	700.00	0.0	0.0	525.00	48800.00	543.64	15536.73	544.20	1016.00	1175.00	2191.00	0.0	
ă.	85.00 85.00	245.00 245.00	0.0	0.0		48800.00 48800.00		12620.32	544.12 544.49	1132.95 995.00	0.0	0.0 2255.00	0.0	
	86.00.	905.00	0.0	0.0		48800.00		9935.07	546.05	812.80	0.0	0.0	0.0	
1 E	86.00	905.00	0.0	0.0	526.50	48800.00	545.41	9076.29	546.62	650.00	1265.00	1915.00	0.0	
	87.00	270.00	0.0	0.0		48800.00		14869.37	546.50 547.14	822.38	0.0 1276.00	0.0 1919.00	0.0	
	87.00	270.00	0.0	0.0	530.60	48800.00	540,40	13/41.61	547.14	643.00	12/0.00		0.0	
H	88.00 88.00	920.00	0.0	0.0		48800.00		10252.64	548.00 548.68	744.71 677.00	0.0 1178.00	0.0 1855.00	0.0	
16											Project is the control			
11	89.00	760.00 760.00	0.0	0.0		48800.00		10881.20	549.63 550.21	676.81 604.00	0.0	0.0 1845.00	0.0	
19.00	90.00	150.00	0.0	0.0	533.80	48800.00	549.03	11121.40	549.94	665.45	0.0	0.0	0.0	
21	90.00	150.00	0.0	0.0		48800.00		11303.24	550.51	574.00	1221.00	1795.00	0.0	
13	91.00	905.00	0.0	0.0		48800.00		9157.83	552.26	669.95	0.0	0.0	0.0	
150	91.00	905.00	0.0	0.0	532.70	48800.00	551.06	8648.07	552.96	431.00	1273.00	1704.00	0.0	
124	92.00	905.00	0.0	0.0		48800.00		12283.77	554.22	737.20	0.0	0.0	0.0	
27	92.00	905.00	0.0	0.0	532.40	48800.00	553.93	12050.60	555.07	482.37	1492.63	1975.00	553.16	
j 29	93.00	795.00	0.0	0.0		48800.00		8905.57	556.11	699.67	0.0	0.0	0.0	
Marie	93.00	795.00	0.0	0.0	533.00	48800.00	555.24	9198.00	556.88	455.40	1402.60	1858.00	554.29	
137	94.00	445.00	0.0	0.0		48800.00		9244.63	557.42	654.93	0.0	0.0	0.0	
	94.00	445.00	0.0	0.0	5.34.00	48800.00	556.48	8161.72	558.34	415.66	1514.34	1930.00	555.92	
135	95.00	380.00	0.0	0.0		48800.00		18644.06	557.89	909.52	0.0	0.0	0.0	
	95.00	380.00	0.0	0.0	531.70	48800.00	558.47	18932.01	558.87	661.00	1489.00	2150.00	0.0	
	96.00	300.00	0.0	0.0		48800.00		16632.36	558.09	1104.17	0.0	0.0	0.0	
0	96.00	300.00	0.0	0.0	537.90	48800.00	558.16	17068.89	559.07	885.00	1405.00	2290.00	0.0	
4	97.00	540.00	0.0	0.0		48800.00		14174.32	558.49	1181.84	0.0	0.0	0.0	
	97.00	540.00	0.0	0.0	538.60	48800.00	559.10	14075.35	559.46	992.00	1300.00	2300.00	0.0	
la li	98.00	300.00	0.0	0.0		48800.00		14386.18	558.72 559.68	1452.58	0.0	2360.00	0.0	
	98.00	300.00	0.0	0.0	538.00	48800.00	559.35	14049.20	237.00	1247.00	1113.00	2300.00	0.0	
47 0	99.00	340.00	0.0	0.0		48800.00 48800.00		19991.29	558.93 559.90	1864.74	0.0	0.0 2732.25	0.0 558.77	
e9 (10)	99.00	340.00	0.0	0.0										
	100.00	550.00 550.00	0.0	0.0		48800.00		18853.70 18655.71	559.35 560.32	2041.46	0.0	0.0	0.0 559.17	
5	100.00													
H .	SECTION	DISCHARGE	CWSEL		CWSEL DIF	F CWSEL D		EL-WSELK	TOPWID	T.W. D	IFF LEN	NGTH		
56 j	50.00	0 48800.000	503.	831	0.0	0.0		0.0	553.869	0.0		55.000		
57	30,000	48800.000	504.	823	0.992	0.0		0.0	378.877	174.9	191 46	55.000		
N II	51.000		504.		0.0	0.2		0.0	481.018	0.0	INTO A STATE OF THE PERSON NAMED AND ADDRESS OF THE PERSON NAM	25.000	29	
	51.000	48800.000	505.	077	0.962	0.2	54	0.963	339.962	141.0	20	25.000		

							TANKERS JOHN	original and the				77.0
ISHING CRE	FK 100 YEA	P F			ANAGS . OF	The Constitution	11969 and	374.06	(154.6) 有些			
	HANNEL MIN			MIN EL I	%CFS<	CWSEL	70	F6	TOPWID	STENCL	STENCE	WSFLK
100 00	EE0 00	0 0	0.0	541.50	48800.00	559-17	18851.92	559.35	2041.46	0.0	0.0	559.17
100.00	550.00 550.00	0.0	0.0		48800.00		18660.13	560.32	1577.18	1283.24	2860.43	559.17
100.00									- 44			
101.00	180.00	0.0	0.0		48800.00		15580.47	559.56	1885.41	0.0	0.0	0.0
101.00	180.00	0.0	0.0	542.80	48800.00	560.17	15018.75	560.55	1457.00	1246.00	2703.00	0.0
				E / O 30	48800.00	EE0 05	12496.16	560.48	1649.06	0.0	0.0	0.0
102.00	740.00	0.0	0.0		48800.00		12056.91	561.58	1157.00	1334.00	2491.00	0.0
102.00	740.00	0.0	0.0	542.30	4000.00	300.00	12.050.01	30				
103.00	285.00	0.0	0.0	545.00	48800.00	560.35	11293.14	561.00	1668.56	0.0	0.0	0.0
103.00	285.00	0.0	0.0	545.00	48800.00	561.29	11034.38	562.13	1046.00	1351.00	2397.00	0.0
								545 O4	11/1 /2	0.0	0.0	0.0
104.00	380.00	0.0	0.0		48800.00		7695.59	562.94	699.81	1705.19	2405.00	560.93
104.00	380.00	0.0	0.0	543.00	48800.00	561.92	A234.01	203.01	099.01	1103.17	2405.00	
	145 00	0.0	0.0	541 00	48800.00	561.36	7531.61	564.17	689.58	0.0	0.0	0.0
106.01	145.00	0.0	0.0		48800.00	562.34		564.86	404.00	1655.00	2059.00	0.0
106.01	145.00	•										
106.02	30.00	557.10	557.90	541.00	48800.00	562.76		564.83	718.69	0.0	0.0	0.0
106.02	30.00	557.10	557.90	541.00	48800.00	562.87	8228.50	565.18	404.00	1655.00	2059.00	0.0
							10000 70	565.35	723.02	0.0	0.0	0.0
106.00	100.00	0.0	0.0		48800.00		12000.70	565.72	404.00	1655.00	2059.00	0.0
106.00	100.00	0.0	0.0	541.50	48800.00	304.20	10303.10	900.12		1,000.00		
107.00	755.00	0.0	0.0	547-00	48800.00	565.64	13315.87	566.40	746.55	0.0	0.0	0.0
107.00	755.00	0.0	0.0		48800.00	566.10	12376.76	567.04	582.72	1488.28	2071.00	565.64
10,000	133.00											0.0
108.00	350.00	0.0	0.0		48800.00		13687.47	566.80	858.02	0.0	0.0	0.0 566.11
108.00	350.00	0.0	0.0	546.50	48800.00	566.61	12990.66	567.49	589.69	1348.07	1937.76	300.11
				550.00		644 40	13316.17	567.27	870.00	0.0	0.0	0.0
109.00	365.00	0.0	0.0		48800.00		12785.90	568.00	556.09	1280.06	1836.16	566.49
109.00	365.00	0.0	00	550.00	48800.00	30.00	جسرت المسا					
110.00	580.00	0.0	0.0	549.80	48800.00	567.19	12511.01	568.13	711.89	0.0	0.0	0.0
110.00	580.00	0.0	0.0	549.80	48800.00	567.86	12323.36	568.88	508.94	1095.00	1603.94	567.19
									004 50	0.0	0.0	0.0
111.00	550.00	0.0	0.0		48800.00		10558.88	569.06	834.59 603.61	1164.16	1767.76	568.20
111.00	550.00	0.0	0.0	551.70	48800.00	568.76	9779.16	569.95	003.01	1104.10	1.0.	
			0.0	553 10	48800.00	569-03	11583.23	569.81	924.43	0.0	0.0	0.0
112.00	405.00	0.0	0.0		48800.00		12047.24	570.75	771.00	1169.00	1940.00	0.0
112.00	405.00	0.0	0.0	333•10	400000							
113.00	100.00	0.0	0.0	551.50	48800.00	569.12	8662.97	570.38	780.47	0.0	0.0	0.0
113.00	100.00	0.0	0.0	551.50	48800.00	570.01	9125.93	571.29	670.00	1160.00	1830.00	0.0
								F70 00	000 01	0.0	0.0	0.0
114.00	550.00	0.0	0.0		48800.00	570.75		572.08	882.01 744.00	1256.00	2000.00	0.0
114.00	550.00	0.0	0.0	551.70	48800.00	571.50	9573.15	572.91	144.00	1250.00	2000.30	
	510 OF		0.0	CEE 00	48800.00	572.33	9725.49	573.15	1108.86	0.0	0.0	0.0
115.00	510.00	0.0	0,0		48800.00		10872.74	573.86	1041.00	1189.00	2230.00	0.0
115.00	510.00	0.0	0.10	333.00	1000000							
116.00	265.00	0.0	0.0	553.00	48800.00		10925.59	573.79		0.0	0.0	0.0
116.00	265.00	0.0	0.0	553.00	48800.00	573.85	11881.51	574.38	1422.00	1283.00	2705.00	6.90
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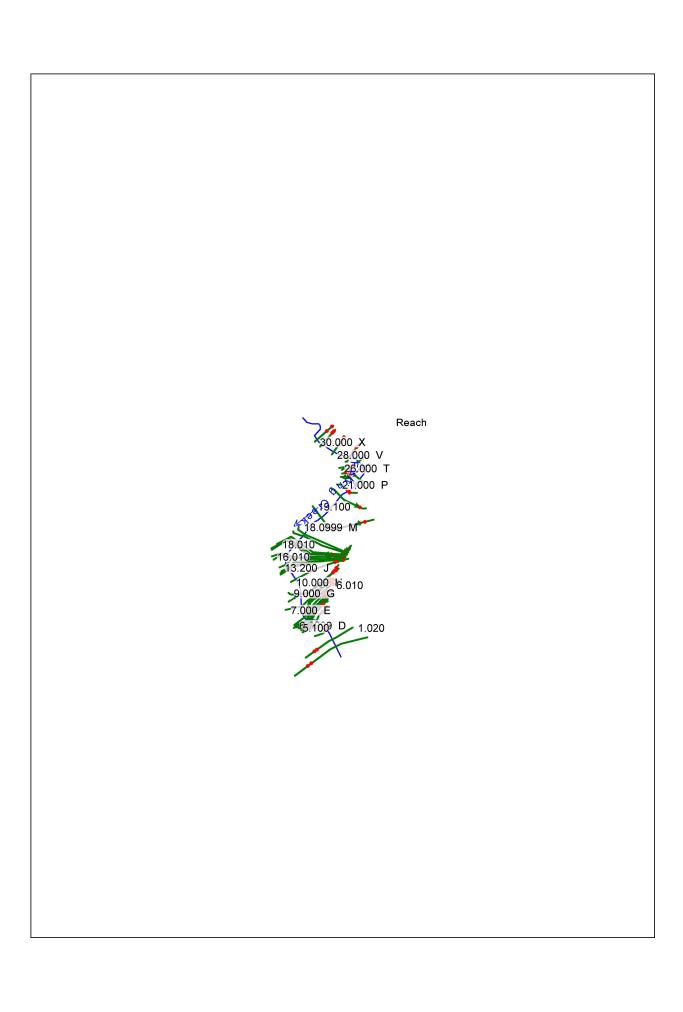
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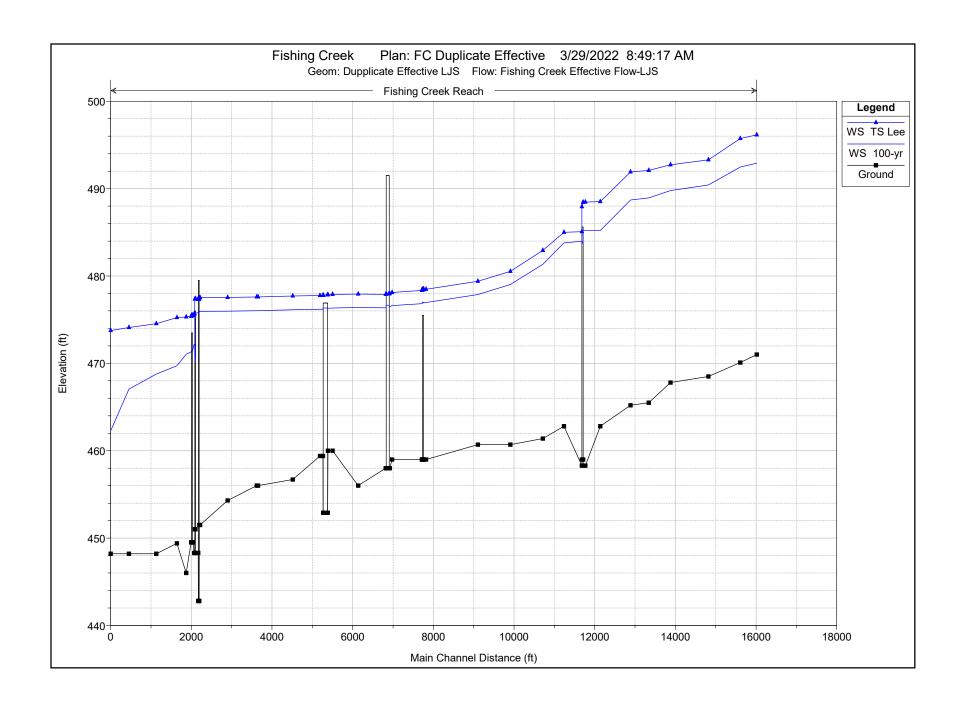
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2		HANNEL MIN F		C EL OF	GROUND	DISCHARGE *CFS<	CWSEL	то	FG	TOPWID	STENCL	STENCE	WSELK
18	117.00	525.00	0.0	0.0		48800.00		11774.34	574.36	2272.73	0.0	0.0	0.0
•	117.00	525.00	0.0	0.0	553.70	48800.00	574.49	11924.07	574.86	1566.99	2303.00	3870.00	0.0
					FF0 00		F74 2F	12622 68	574.80	2099.04	0.0	0.0	0.0
	118.00	265.00	0.0	0.0		48800.00		12622.48	575.26	1681.99	2041.00	3723.00	0.0
0	118.00	265.00	0.0	0.0	558.00	48800.00	5/4.83	13410.00	3/3.20	1001.99	2041.00	3723.00	••
A	119.00	420.00	0.0	0.0	559.20	48800.00	575.10	13608.56	575.37	2087.97	0.0	0.0	0.0
	119.00	420.00	0.0	0.0		48800.00	575.45	11810.41	575.86	1615.96	1892.00	3507.96	575.10
	120.00	765.00	0.0	0.0	560.80	48800.00		14201.91	576.23	2103.10	0.0	0.0	0.0
•	150.00	765.00	0.0	0.0	560.80	48800.00	576.69	11929.97	577.04	1656.19	1379.00	3035.19	576.02
12							F76 00	15250 10	577.10	2261.07	0.0	0.0	0.0
1 1	121.00	840.00	0.0	0.0		48800.00		15358.18	578.11	1844.72	1244.00	3088.72	576.88
e is	121.00	840.00	0.0	0.0	502.10	48800.00	511.00	14021.30	370.11	1044.12	1244.00	3000.12	3,0.00
	122.00	715.00	0.0	0.0	563-00	48800.00	577.76	10122.26	578.11	2248.59	0.0	0.0	0.0
b		715.00	0.0	0.0		48800.00		10100.05	579.17	1852.05	1261.00	3113.05	577.76
			J										
	123.00	545.00	0.0	0.0	564.70	48800.00		10671.24	579.42	2300.24	0.0	0.0	0.0
	123.00	545.00	0.0	0.0	564.70	42400.00	579.99	9020.65	580.54	1630.28	1328.00	2958.29	579.01
								10051 10	501 11	3218.24	0.0	0.0	0.0
	123.50	300.00	0.0	0.0		42400.00		12851.13	581.11	1833.30	1328.00	3161.30	580.90
•	123.50	300.00	0.0	0.0	567.00	42400.00	581.90	12400.01	302.10	1033.30	1320.00	3101.30	500.70
	124.00	320.00	0.0	0.0	568.00	42400.00	581.33	5994.19	582.78	1945.82	0.0	0.0	0.0
•	124.00	320.00	0.0	0.0		42400.00	582.33	6354.89	583.87	1055.84	1266.00	2989.62	581.33
		• • • • • • • • • • • • • • • • • • • •											
	124.10	115.00	0.0	0.0		42400.00	582.94		583.80	2259.84	0.0	0.0	0.0
	124.10	115.00	0.0	0.0	568.60	42400.00	583.89	8210.98	584.79	1286.95	1266.00	3138.20	582.94
30							F03 (F	7102 06	584.68	2329.50	0.0	0.0	0.0
	126.01	115.00	0.0	0.0		42400.00	583.65 584.47		585.85	1401.06	1269.00	2670.06	583.65
. 3	126.01	115.00	0.0	0.0	200.00	7 42400.00	304.41	0922.02	505.05	1401.00	1207.00	20.0.00	
	126.02	80.00	0.0	0.0	568-00	42400.00	587.48	17223.13	587.67	2338.46	0.0	0.0	0.0
	126.02	80.00	0.0	0.0		42400.00		16756.82	588.53	1830.84	1269.00	3099.85	587.48
	127.00	835.00	0.0	0.0		42400.00		10617.04	588.35	1998.18	0.0	0.0	0.0
	127.00	835.00	0.0	0.0	570.50	0 42400.00	588.61	10599.63	589.30	1139.76	1103.00	2242.76	587.75
20							588.52	9239.14	589.44	1479.91	0.0	0.0	0.0
40	128.00	750.00	0.0	0.0		0 42400.00	589.40		590.38	892.73	1111.00	2003.73	588.52
() N	128.00	750.00	0.0	0.0	512.01	7 42400.00	369.40	73.70.00	390.30	0,2.13	1111.00	2005.75	
	129.00	415.00	0.0	0.0	573.5	42400.00	589.57	9119.10	590.40	1237.10	0.0	0.0	0.0
	129.00	415.00	0.0	0.0		42400.00	590.53		591.31	941.66	1144.00	2085.66	589.57
	130.00	632.00	0.0	0.0		0 42400.00	591.48		592.11	1778.53	0.0	0.0	0.0
	130.00	632.00	0.0	0.0	572.0	0 42400.00	592.30	8967.89	592.98	1335.98	1066.00	2401.98	591.48
	401.00				527 0		E02 00	12110.71	593.14	2134.88	0.0	0.0	0.0
	131.00	800.00	0.0	0.0		0 42400.00		11748.30	594.07	1478.78	1233.66	2712.44	592.80
C 130	131.00	800.00	0.0	0.0	311.01	3 42400 . 00	373.03	-17-55-50	3,4.01				
	132.00	550.00	0.0	0.0	580.00	0 42400.00	593.33	10720.20	593.67	2130.94	0.0	0.0	0.0
	132.00	550.00	0.0	0.0		0 42400.00		11274.75	열시는) 전력을 참 없어 맛있다면 선택되었다.	1554.16	1185.50	2739.66	593.33
•	1000	42875.53	6 SAR	39.1	7,1								

	CHANNEL MIN EL		OW CHORD	GROUND	%CFS<	CWSEL	ТО	EG	TOPWID	STENCL	STENCR	WSEL
133.00	560.00 560.00	0.0	0.0		42400.00		10545.95	594.30 595.22	2618.27 2122.06	0.0 1259.86	0.0 3387.00	0.0 594.0
134.00	865.00	0.0	0.0	581.00	42400.00	594.82	6816.21	595.34	2274.60	0.0	0.0	0.0
134.00	865.00	0.0	0.0		42400.00	595.63		596.19	2043.33	1326.24	3372.00	594.8
135.00	625.00	0.0	0.0	585.00	42400.00	597.13	6934.07	597.65	2287.90	0.0	0.0	0.0
135.00	625.00	0.0	0.0	585.00	42400.00	597.82	7265.91	598.35	1993.27	1393.73	3387.00	597.1
136.00	575.00	0.0	0.0	586.00	42400.00	598.49	9298.87	598.85	2124.04	0.0	0.0	0.0
136.00	575.00	0.0	0.0	586.00	42400.00	599.09	9679.76	599.46	1814.61	1353.39	3168.00	598.4
137.00	600.00	0.0	0.0	586.50	42400.00	599.38	8614.41	599.81	1950.40	0.0	0.0	0.0
137.00	600.00	0.0	0.0		42400.00	599.88	7992.56	600.49	1387.48	1377.98	2765.46	599.3
138.00	615.00	0.0	0.0	588.50	42400.00	600.55	9448.60	600.92	2029.66	0.0	0.0	0.0
138.00	615.00	0.0	0.0	588.50	42400.00	601.21	8781.35	601.77	1160.00	1375.00	2535.00	0.0
139.00	590.00	0.0	0.0	589.00	42400.00	601.65	6854.02	602.57	1826.18	0.0	0.0	0.0
139.00	590.00	0.0	0.0		42400.00	602.40	6569.57	603.68	1085.00	1285.00	2370.00	0.0
140.00	385.00	0.0	0.0	589.50	42400.00	602.99	9410.84	603.58	1771.99	0.0	0.0	0.0
140.00	385.00	0.0	0.0		42400.00	603.99			1045.00	1310.00	2355.00	0.0
141.00	890.00	0.0	0.0	590.50	42400.00	604.59	8544.65	605.30	1870.47	0.0	0.0	0.0
141.00	890.00	0.0	0.0		42400.00	605.58		606.41	1187.00	1128.00	2315.00	0.0
142.00	365.00	0.0	0.0	592.00	42400.00	605.61	12101.39	605.94	2016.60	0.0	0.0	0.0
142.00	365.00	0.0	0.0		42400.00		12023.70	607.04	1115.00	1220.00	2335.00	0.0
143.01	267.00	0.0	0.0		42400.00		8077.52	606.75	1689.75	0.0	0.0	0.0
143.01	267.00	0.0	0.0	591.30	42400.00	606.87	8502.29	607.77	1067.46	1222.00	2289.46	605.8
143.00	268.00	0.0	0.0		42400.00	606.62			1691.41	0.0	0.0	0.0
143.00	268.00	0.0	0.0	592.00	42400.00	607.59	8762.01	608.43	1115.48	1222.00	2337.48	606.6
144.00	600,00	0.0	0.0	596.30	42400.00	608.16	8488.36	608.72	1671.90	0.0	0.0	0.0
144.00	600.00	0.0	0.0	596.30	42400.00	608.83	7941.61	609.64	1053.38	1406.73	2460.12	608.1
145.00	560.00	0.0	0.0		42400.00	609.10		611.22	1203.16	0.0	0.0	0.0
145.00	560.00	0.0	0.0	597.80	42400.00	610.01	5712.21	612.11	685.16	1279.49	1964.66	609.1
SECTION NUMBER	DISCHARGE	CWS	Marin Control of the State of t	CWSEL DIF	F CWSEL I		EL-WSFLK	TOPWID	T.W. (DIFF LEN	NGTH	216.5
100.0	00 48800.000		59.167	0.0	0.	0	0.0	2041.458	0.0		50.000	
100.0	00 48800.000	5	60.103	0.936	0.	0	0.0	1577.181	464.7	277 55	50.000	
101.0	00 48800.000	5	59.254	0.0	0.	088	0.0	1885.409	0.0		30.000	
101.00	00 48800.000	5	60.169	0.914	0.0	066	0.0	1456.999	428.4	10 18	30.000	
102.00	00 48800.000		59.952	0.0	0.0	698	0.0	1649.057	0.0		40.000	
102.00	00 48800.000	5	60.878	0.926	0.	709	0.0	1156.999	492.0	058 74	40.000	
103.00	00 48800.000	5	60.351	0.0	0.	399	0.0	1668.560	0.0		85.000	
103.00	00 48800.000	5	61.294	0.943	0.	417 700	0.0	1045.999	622.5	561 28	35.000	
104.00	00 48800.000	5	60.926	0.0	0.	575	0.0	1141.621	0.0	0 38	30.000	
104.00		5	61.921	0.995	0.	626	0.995	699.813	441.	308 31	80.000	
106.01	10 48800.000	_	61.365	0.0	0	439	0.0	689.575	0.0	n 1,	45.000	

D.2 Effective Model in HEC-RAS Model Output



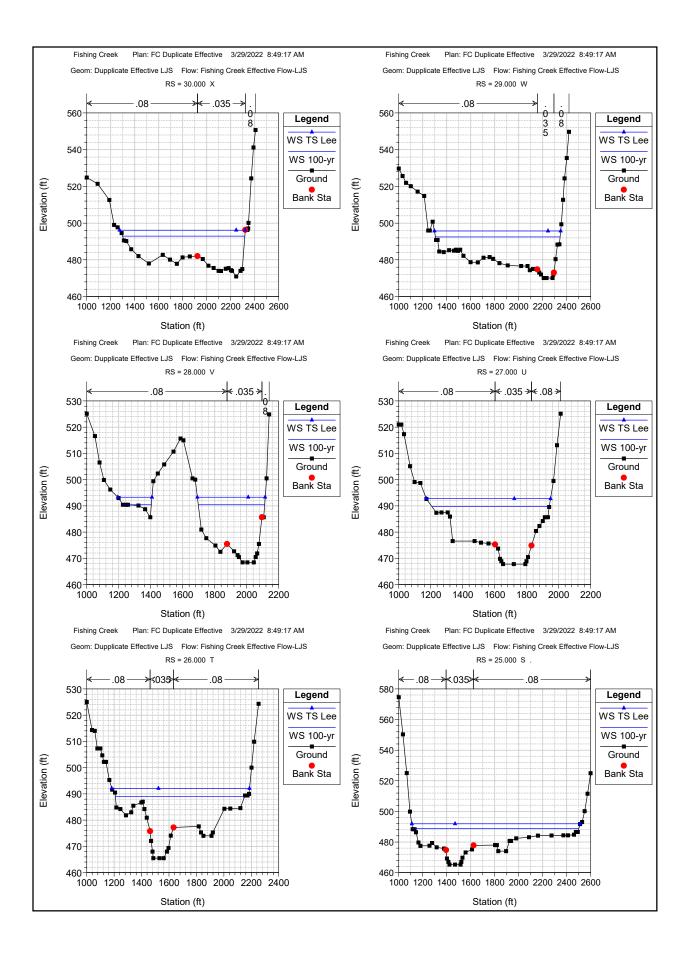


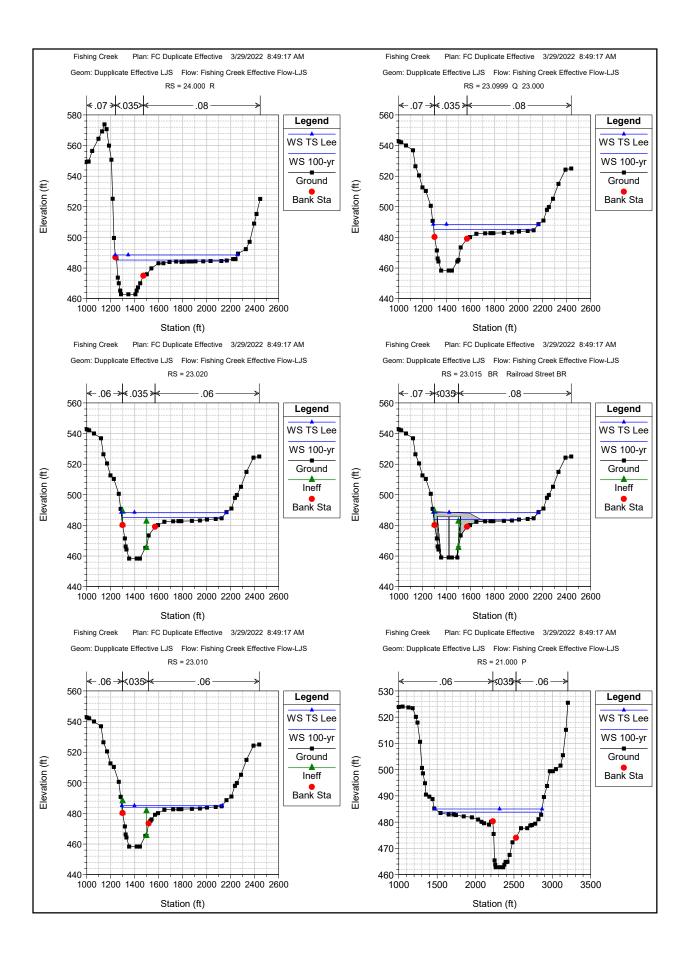
Reach 3 Reach 2 Reach 2	River Sta 30.000 X 30.000 X 30.000 X 29.000 W 29.000 W 28.000 V 27.000 U 27.000 U 27.000 T 26.000 T 25.000 S 25.000 S 24.000 R	Profile 100-yr TS Lee 100-yr TS Lee	Q Total (cfs) 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	Min Ch El (ft) 471.00 471.00 470.10 470.10 468.50 468.50 467.80 465.50 465.50	W.S. Elev (ft) 492.92 496.15 492.47 495.73 490.42 493.29 489.78 492.73	Crit W.S. (ft)	E.G. Elev (ft) 493.42 496.73 493.15 496.47 492.21 495.50	E.G. Slope (ft/ft) 0.000564 0.000530 0.000797 0.000760 0.001563 0.001642	Vel Chnl (ft/s) 6.53 7.06 9.20 9.87 11.72 13.21	Flow Area (sq ft) 13507.38 16839.80 13798.48 17201.74 6773.32 8536.08	Top Width (ft) 1018.62 1047.34 1038.03 1052.55 592.31 637.04	0.28 0.28 0.35 0.35 0.48
Reach 3 Reach 2	30.000 X 29.000 W 29.000 W 28.000 V 28.000 V 27.000 U 27.000 U 26.000 T 26.000 T 25.000 S 24.000 R	TS Lee 100-yr TS Lee	\$8900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	471.00 471.00 470.10 470.10 468.50 468.50 467.80 465.50	492.92 496.15 492.47 495.73 490.42 493.29 489.78 492.73	(II)	493.42 496.73 493.15 496.47 492.21 495.50	0.000564 0.000530 0.000797 0.000760 0.001563 0.001642	6.53 7.06 9.20 9.87 11.72 13.21	13507.38 16839.80 13798.48 17201.74 6773.32 8536.08	1018.62 1047.34 1038.03 1052.55 592.31 637.04	0.28 0.35 0.35
Reach 3 Reach 2	30.000 X 29.000 W 29.000 W 28.000 V 28.000 V 27.000 U 27.000 U 26.000 T 26.000 T 25.000 S 24.000 R	TS Lee 100-yr TS Lee	78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	471.00 470.10 470.10 468.50 468.50 467.80 465.50	496.15 492.47 495.73 490.42 493.29 489.78 492.73		496.73 493.15 496.47 492.21 495.50 490.91	0.000530 0.000797 0.000760 0.001563 0.001642	7.06 9.20 9.87 11.72 13.21	16839.80 13798.48 17201.74 6773.32 8536.08	1047.34 1038.03 1052.55 592.31 637.04	0.28 0.35 0.35
Reach 2	29.000 W 29.000 W 28.000 V 28.000 V 27.000 U 27.000 U 26.000 T 26.000 T 25.000 S 24.000 R	100-yr TS Lee	58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	470.10 470.10 468.50 468.50 467.80 465.50	492.47 495.73 490.42 493.29 489.78 492.73		493.15 496.47 492.21 495.50 490.91	0.000797 0.000760 0.001563 0.001642	9.20 9.87 11.72 13.21	13798.48 17201.74 6773.32 8536.08	1038.03 1052.55 592.31 637.04	0.35 0.35
Reach 2	29.000 W 28.000 V 28.000 V 27.000 U 27.000 U 26.000 T 26.000 T 25.000 S 25.000 S 24.000 R	TS Lee 100-yr TS Lee	78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	470.10 468.50 468.50 467.80 467.80 465.50	495.73 490.42 493.29 489.78 492.73		496.47 492.21 495.50 490.91	0.000760 0.001563 0.001642	9.87 11.72 13.21	17201.74 6773.32 8536.08	1052.55 592.31 637.04	0.35
Reach 2	29.000 W 28.000 V 28.000 V 27.000 U 27.000 U 26.000 T 26.000 T 25.000 S 25.000 S 24.000 R	TS Lee 100-yr TS Lee	78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	470.10 468.50 468.50 467.80 467.80 465.50	495.73 490.42 493.29 489.78 492.73		496.47 492.21 495.50 490.91	0.000760 0.001563 0.001642	9.87 11.72 13.21	17201.74 6773.32 8536.08	1052.55 592.31 637.04	0.35
Reach 2	28.000 V 27.000 U 27.000 U 28.000 T 28.000 T 25.000 S 25.000 S 24.000 R	100-yr TS Lee	78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	467.80 467.80 465.50 465.50	493.29 489.78 492.73 488.94		495.50 490.91	0.001642	13.21	8536.08	637.04	0.48
Reach 2	28.000 V 27.000 U 27.000 U 28.000 T 28.000 T 25.000 S 25.000 S 24.000 R	TS Lee 100-yr TS Lee 100-yr TS Lee 100-yr TS Lee 100-yr TS Lee	78700.00 58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	467.80 467.80 465.50 465.50	493.29 489.78 492.73 488.94		495.50 490.91	0.001642	13.21	8536.08	637.04	
Reach 2	27.000 U 27.000 U 26.000 T 26.000 T 25.000 S 25.000 S 24.000 R	100-yr TS Lee 100-yr TS Lee 100-yr TS Lee	58900.00 78700.00 58900.00 78700.00 58900.00 78700.00	467.80 467.80 465.50 465.50	489.78 492.73 488.94		490.91					0.50
Reach 2	27.000 U 26.000 T 26.000 T 25.000 S 25.000 S 24.000 R	TS Lee 100-yr TS Lee 100-yr TS Lee	78700.00 58900.00 78700.00 58900.00 78700.00	467.80 465.50 465.50	492.73 488.94			0.000045				1
Reach 2	27.000 U 26.000 T 26.000 T 25.000 S 25.000 S 24.000 R	TS Lee 100-yr TS Lee 100-yr TS Lee	78700.00 58900.00 78700.00 58900.00 78700.00	467.80 465.50 465.50	492.73 488.94			0.000045				
Reach 2	26.000 T 26.000 T 25.000 S 25.000 S 24.000 R 24.000 R	100-yr TS Lee 100-yr TS Lee	58900.00 78700.00 58900.00 78700.00	465.50 465.50	488.94			0.000915	9.60	9470.83	733.90	0.37
Reach 2	26.000 T 25.000 S 25.000 S 24.000 R 24.000 R	TS Lee 100-yr TS Lee 100-yr	78700.00 58900.00 78700.00	465.50			494.09	0.000961	10.75	11696.03	776.33	0.39
Reach 2	26.000 T 25.000 S 25.000 S 24.000 R 24.000 R	TS Lee 100-yr TS Lee 100-yr	78700.00 58900.00 78700.00	465.50								
Reach 2 Reach 2 Reach 2 Reach 2 Reach 2 Reach 2	25.000 S 25.000 S 24.000 R 24.000 R	100-yr TS Lee	58900.00 78700.00		492.09		490.33	0.001284	11.27	9780.41	942.04	0.44
Reach 2 Reach 2 Reach 2 Reach 2 Reach 2	25.000 S 24.000 R 24.000 R	TS Lee 100-yr	78700.00	465.20			493.54	0.001194	11.95	12864.01	1004.77	0.43
Reach 2 Reach 2 Reach 2 Reach 2 Reach 2	25.000 S 24.000 R 24.000 R	TS Lee 100-yr	78700.00	465.20	400.00		400.44	0.000775	0.40	40000.04	4004.50	0.04
Reach 2 Reach 2 Reach 2 Reach 2	24.000 R 24.000 R	100-yr		465.00	488.69		489.44	0.000775	8.46	13606.04	1384.56	0.34
Reach 2 Reach 2 Reach 2	24.000 R			465.20	491.91		492.65	0.000681	8.79	18082.22	1404.59	0.33
Reach 2 Reach 2 Reach 2	24.000 R		58900.00	462.80	485.19	478.93	487.74	0.001954	13.11	5625.45	935.28	0.53
Reach 2 Reach 2			78700.00	462.80	488.52	470.55	491.06	0.001804	13.64	8943.82	1017.58	0.52
Reach 2			10100.00	102.00	100.02		101.00	0.001001	10.01	00.10.02	1011.00	0.02
Reach 2	23.0999 Q	100-yr	58900.00	458.30	485.24		486.93	0.001186	10.59	6730.50	839.00	0.42
	23.0999 Q	TS Lee	78700.00	458.30	488.45		490.36	0.001152	11.53	9487.83	876.01	0.42
Reach 2	23.020	100-yr	58900.00	458.30	485.18	475.66	486.86	0.001202	10.60	6630.86	838.30	0.42
	23.020	TS Lee	78700.00	458.30	488.45	478.92	490.23	0.001112	11.28	9404.02	875.98	0.41
Reach 2	23.015		Bridge									
	23.010	100-yr	58900.00	458.30	483.98	475.67	486.20	0.001459	12.20	5661.51	740.58	0.47
Reach 2	23.010	TS Lee	78700.00	458.30	485.08	478.92	488.44	0.002108	15.17	6544.26	837.13	0.56
	21.000 P	100-yr	58900.00	462.80	483.80		485.15	0.001287	9.96	8339.94	1331.05	0.43
Reach 2	21.000 P	TS Lee	78700.00	462.80	485.00		486.83	0.001659	11.84	9980.52	1394.43	0.49
Booch 2	20.000 O	100-yr	58900.00	461.40	481.34	481.34	484.09	0.002405	15.03	7545.80	2024.54	0.60
	20.000 O	TS Lee	78700.00	461.40	482.93	482.93	485.66	0.002405	16.02	10789.25	2024.54	0.60
Treacii 2	20.000 0	10 Lee	70700.00	401.40	402.93	402.93	403.00	0.002400	10.02	10703.23	2034.59	0.02
Reach 1	19.100	100-yr	58900.00	460.70	479.02	472.96	479.40	0.000551	6.43	20218.30	3664.80	0.28
	19.100	TS Lee	78700.00	460.70	480.54	475.39	480.92	0.000556	6.85	25845.75	3757.01	0.28
		1.2.2.2										
Reach 1	19.000 N	100-yr	58900.00	460.70	477.87	472.95	478.48	0.000884	7.76	16229.94	3338.01	0.35
	19.000 N	TS Lee	78700.00	460.70	479.40	476.39	479.98	0.000849	8.10	21593.80	3700.87	0.35
Reach 1	18.0999 M	100-yr	58900.00	459.00	476.96	474.81	477.21	0.000525	6.48	23499.09	3716.78	0.27
Reach 1	18.0999 M	TS Lee	78700.00	459.00	478.47	474.81	478.73	0.000524	6.84	29237.44	3868.15	0.28
	18.040	100-yr	58900.00	459.00	476.93	474.71	477.18	0.000532	6.52	23373.94	3713.52	0.28
Reach 1	18.040	TS Lee	78700.00	459.00	478.44	474.71	478.70	0.000530	6.87	29109.95	3864.96	0.28
D h	40.000	400	50000.00	450.00	470.00	474.74	477.40	0.000504	0.50	00050 44	0740.04	0.00
	18.030 18.030	100-yr TS Lee	58900.00 78700.00	459.00 459.00	476.92 478.43	474.71 474.71	477.18 478.70	0.000534 0.000531	6.52 6.88	23352.41 29086.95	3712.94 3864.36	0.28 0.28
Reacti	10.030	13 Lee	78700.00	459.00	470.43	4/4./1	476.70	0.000551	0.00	29000.93	3004.30	0.20
Reach 1	18.025		Bridge									
Reach 1	18.020	100-yr	58900.00	459.00	476.83	474.61	477.10	0.000554	6.62	23023.97	3704.08	0.28
	18.020	TS Lee	78700.00	459.00	478.35	474.61	478.62	0.000547	6.96	28768.52	3856.11	0.28
Reach 1	18.010	100-yr	58900.00	459.00	476.83	474.61	477.09	0.000555	6.63	23001.71	3703.48	0.28
Reach 1	18.010	TS Lee	78700.00	459.00	478.35	474.61	478.61	0.000548	6.97	28745.81	3855.52	0.28
	16.0999 L	100-yr	58900.00	459.00	476.61	471.93	476.75	0.000305	4.68	29020.44	4292.82	0.21
Reach 1	16.0999 L	TS Lee	78700.00	459.00	478.12	474.20	478.27	0.000318	5.07	35654.21	4502.95	0.21
	10.010	400						0.5		00	4	
	16.040	100-yr	58900.00	458.00	476.48	472.36	476.72	0.000421	6.09	23580.70	4273.25	0.25
Reach 1	16.040	TS Lee	78700.00	458.00	477.98	474.21	478.24	0.000440	6.56	29419.54	4487.15	0.26
Pooch .	16.020	100	E0000 00	450.00	470 51	470 51	470.70	0.000540	F 00	20074 00	2000.00	0.00
	16.030 16.030	100-yr TS Lee	58900.00 78700.00	458.00 458.00	476.51 478.01	472.51 474.01	476.70 478.22	0.000512 0.000542	5.39 5.75	22671.96 27705.68	3286.66 3411.08	0.22 0.23
i teacii 1	10.030	13 Lee	10100.00	458.00	4/8.01	4/4.01	418.22	0.000542	5.75	21105.08	3411.08	0.23
Reach 1	16.025		Bridge									
. touoti I	. 5.020		bridge									
Reach 1	16.020	100-yr	58900.00	458.00	476.43	472.51	476.62	0.000528	5.46	22399.62	3279.91	0.22
	16.020	TS Lee	78700.00	458.00	477.97	474.01	478.18	0.000550	5.79	27543.39	3407.10	0.23
			1									
Reach 1	16.010	100-yr	58900.00	458.00	476.36	472.36	476.61	0.000440	6.20	23124.49	4255.85	0.25
	16.010	TS Lee	78700.00	458.00	477.90	474.01	478.16	0.000453	6.63	29089.08	4477.51	0.26
Reach 1	14.000 K	100-yr	58900.00	456.00	476.39	469.69	476.49	0.000234	3.91	28986.30	4240.59	0.17

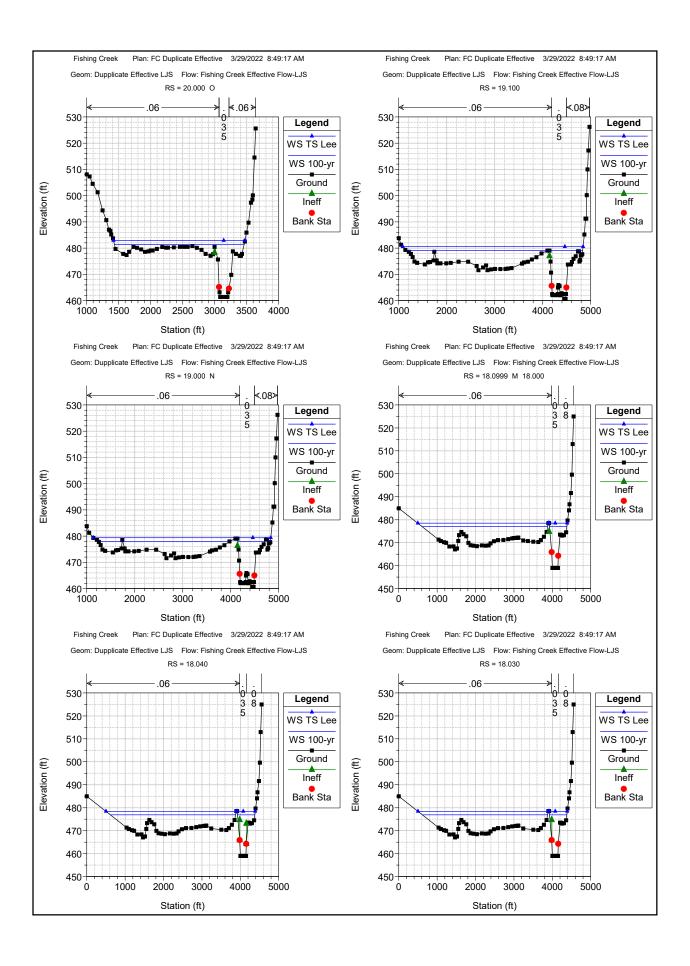
Reach	Plan: FC Duplicate Eff River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach	14.000 K	TS Lee	78700.00	456.00	477.93	471.06	478.04	0.000239	4.19	35659.46	4390.48	0.18
Reach	13.200 J	100-yr	58900.00	460.00	476.34	470.44	476.44	0.000295	4.12	27118.14	4245.36	0.19
Reach	13.200 J	TS Lee	78700.00	460.00	477.89	471.50	478.00	0.000288	4.35	33863.21	4427.62	0.19
Reach	13.100	100-yr	58900.00	460.00	476.30	470.44	476.41	0.000299	4.14	26982.44	4240.97	0.19
Reach	13.100	TS Lee	78700.00	460.00	477.86	471.50	477.97	0.000292	4.37	33725.85	4424.33	0.19
Reach	12.100	100-yr	58900.00	452.90	476.29	470.09	476.40	0.000274	4.34	26813.94	4043.40	0.18
Reach	12.100	TS Lee	78700.00	452.90	477.84	471.35	477.97	0.000279	4.58	33345.60	4362.96	0.18
Reach	12.015		Bridge									
Reach	12.010	100-yr	58900.00	452.90	476.19	470.10	476.31	0.000284	4.40	26416.23	4023.37	0.18
Reach	12.010	TS Lee	78700.00	452.90	477.77	471.34	477.90	0.000285	4.63	33043.36	4348.42	0.19
Reach	11.100	100-yr	58900.00	459.40	476.21	470.00	476.28	0.000176	3.56	33083.96	4319.33	0.16
Reach	11.100	TS Lee	78700.00	459.40	477.80	470.77	477.88	0.000181	3.85	39894.33	4504.08	0.16
Reach	11.000 I	100-yr	58900.00	459.40	476.18		476.25	0.000176	3.55	33286.38	4316.08	0.16
Reach	11.000 I	TS Lee	78700.00	459.40	477.76		477.84	0.000181	3.84	40245.63	4499.33	0.16
Reach	10.000 H	100-yr	58900.00	456.70	476.13		476.19	0.000133	3.09	37349.86	4653.96	0.14
Reach	10.000 H	TS Lee	78700.00	456.70	477.71		477.78	0.000141	3.38	44853.07	4843.49	0.14
Reach	9.000 G	100-yr	58900.00	456.00	476.03		476.09	0.000112	3.08	38750.25	4810.68	0.13
Reach	9.000 G	TS Lee	78700.00	456.00	477.60		477.67	0.000120	3.37	46468.77	4998.72	0.13
Reach	8.000 F	100-yr	58900.00	456.00	476.02		476.08	0.000106	3.02	39318.10	4813.99	0.12
Reach	8.000 F	TS Lee	78700.00	456.00	477.60		477.67	0.000115	3.32	47041.16	5002.69	0.13
Reach	7.000 E	100-yr	58900.00	454.30	475.98		476.04	0.000111	3.16	39957.93	5124.54	0.13
Reach	7.000 E	TS Lee	78700.00	454.30	477.55		477.62	0.000118	3.43	48169.94	5313.65	0.13
Reach	6.0999 D	100-yr	58900.00	451.50	475.95		476.01	0.000108	3.31	40609.99	5351.07	0.12
Reach	6.0999 D	TS Lee	78700.00	451.50	477.52		477.59	0.000113	3.55	49195.93	5540.00	0.13
Reach	6.010	100-yr	58900.00	451.50	475.95	466.80	476.01	0.000108	3.30	40603.63	5350.93	0.12
Reach	6.010	TS Lee	78700.00	451.50	477.52	469.59	477.59	0.000113	3.54	49188.97	5539.85	0.13
Reach	5.100	100-yr	58900.00	442.80	475.68	464.88 468.44	475.95	0.000480	5.68 5.45	22706.31	4707.49	0.21
Reach	5.100	TS Lee	78700.00	442.80	477.34	400.44	477.55	0.000419	5.45	30809.85	5056.57	0.19
Reach	5.015		Bridge									
Reach Reach	5.010 5.010	100-yr TS Lee	58900.00 78700.00	442.80 442.80	475.67 477.33		475.94 477.54	0.000482 0.000420	5.70 5.46	22653.04 30762.48	4702.46 5054.37	0.21 0.19
rteacii	3.010	10 Lee	70700.00	442.00	477.55		411.54	0.000420	3.40	30702.40	3034.37	0.19
Reach	4.200	100-yr	58900.00	448.30	475.78	463.41	475.82	0.000067	2.85	46651.49	5807.50	0.10
Reach	4.200	TS Lee	78700.00	448.30	477.41	466.34	477.46	0.000074	3.12	56222.23	5944.09	0.11
Danah	4.400	100	E0000 00	440.20	475 77	462.42	475.00	0.000067	2.05	46605.07	E007.44	0.40
Reach Reach	4.100 4.100	100-yr TS Lee	58900.00 78700.00	448.30 448.30	475.77 477.40	463.42 466.35	475.82 477.45	0.000067 0.000074	2.85 3.12	46625.07 56192.31	5807.11 5943.66	0.10 0.11
												•
Reach	4.025		Bridge									
Reach	4.020	100-yr	58900.00	448.30	472.20	463.42	472.37	0.000231	4.83	26486.85	5423.42	0.18
Reach	4.020	TS Lee	78700.00	448.30	475.66	466.35	475.74	0.000124	3.87	45944.95	5797.28	0.14
Decel	4.010	400	50000.00	440.00	470.00		470.07	0.000231	4.04	00405 50	F 400 00	0.40
Reach Reach	4.010	100-yr TS Lee	58900.00 78700.00	448.30 448.30	472.20 475.65		472.37 475.74	0.000231	4.84 3.87	26465.50 45933.63	5422.88 5797.12	0.18 0.14
Reach	3.200	100-yr	58900.00	449.50	471.59	465.35	472.16	0.000616	8.29	17621.49	4218.00	0.31
Reach	3.200	TS Lee	78700.00	449.50	475.48	470.29	475.66	0.000232	5.67	35756.42	5090.56	0.20
Reach	3.100	100-yr	58900.00	449.50	471.61	463.88	472.13	0.000541	7.50	18299.93	4227.85	0.29
Reach	3.100	TS Lee	78700.00	449.50	475.48	469.88	475.66	0.000213	5.27	36615.28	5090.43	0.19
Reach	3.021		Bridge									
Reach	3.020	100-yr	58900.00	449.50	471.43		472.00	0.000626	8.32	17562.99	4152.52	0.31
Reach	3.020	TS Lee	78700.00	449.50	475.41		475.58	0.000229	5.62	36250.17	5074.23	0.19
Pooch	3.010	100 :==	E0000 00	449.50	474.00	AGE OF	471.97	0.000004	0.70	18506 47	4002.07	0.33
Reach Reach	3.010	100-yr TS Lee	58900.00 78700.00	449.50 449.50	471.32 475.39	465.35 470.29	471.97 475.58	0.000694 0.000239	8.73 5.75	16506.47 35313.59	4093.27 5070.63	0.33
	2.0.0	.0.200	. 57 00.00	++0.00	41 0.00	+1 U.23	47 0.00	5.500208	5.75	55010.08	3070.00	0.20
Reach	2.000 C	100-yr	58900.00	446.00	471.04		471.86	0.000726	8.85	14483.08	3378.55	0.33
Reach	2.000 C	TS Lee	78700.00	446.00	475.30		475.55	0.000258	5.93	32830.11	4924.11	0.20

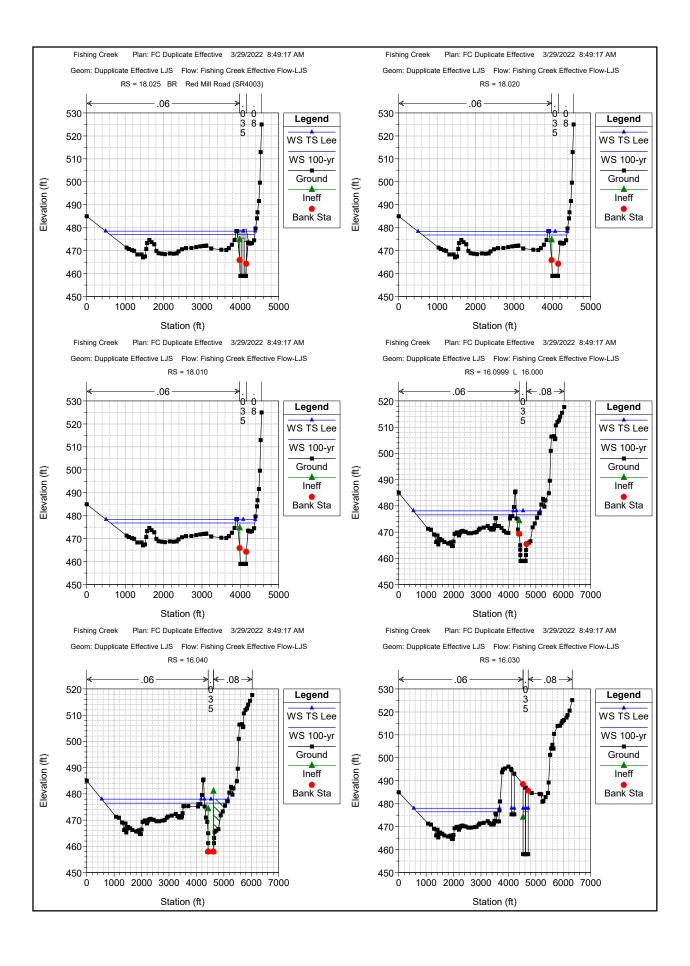
HEC-RAS Plan: FC Duplicate Eff River: Fishing Creek Reach: Reach (Continued)

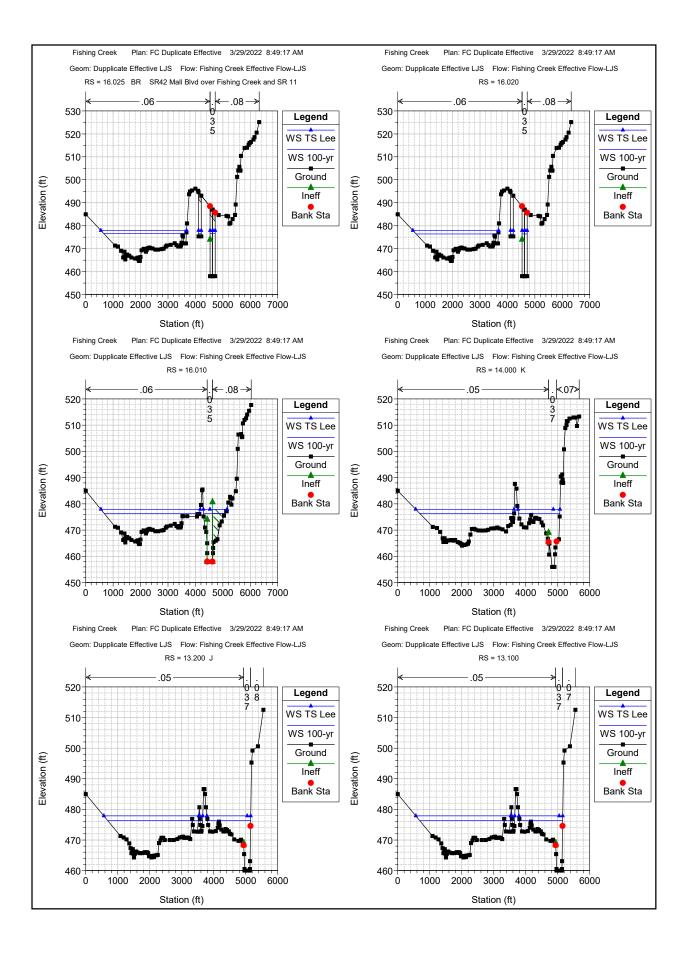
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach	1.100 B	100-yr	58900.00	449.40	469.72	464.20	471.40	0.003829	11.46	7339.74	1772.15	0.48
Reach	1.100 B	TS Lee	78700.00	449.40	475.24		475.41	0.000567	4.89	28415.49	4882.81	0.18
Reach	1.0999 A	100-yr	58900.00	448.20	468.76		470.21	0.001322	10.30	7424.44	1065.56	0.44
Reach	1.0999 A	TS Lee	78700.00	448.20	474.54		475.08	0.000463	7.38	22802.96	4798.27	0.27
Reach	1.020	100-yr	58900.00	448.20	467.06	462.31	469.06	0.002027	11.89	5869.60	766.05	0.53
Reach	1.020	TS Lee	78700.00	448.20	474.10		474.73	0.000538	7.85	20696.31	4751.21	0.29
Reach	1.010	100-yr	58900.00	448.20	462.26	462.26	467.17	0.007714	18.17	3463.22	372.22	0.97
Reach	1.010	TS Lee	78700.00	448.20	473.75	464.72	474.47	0.000604	8.24	19118.47	4288.01	0.31

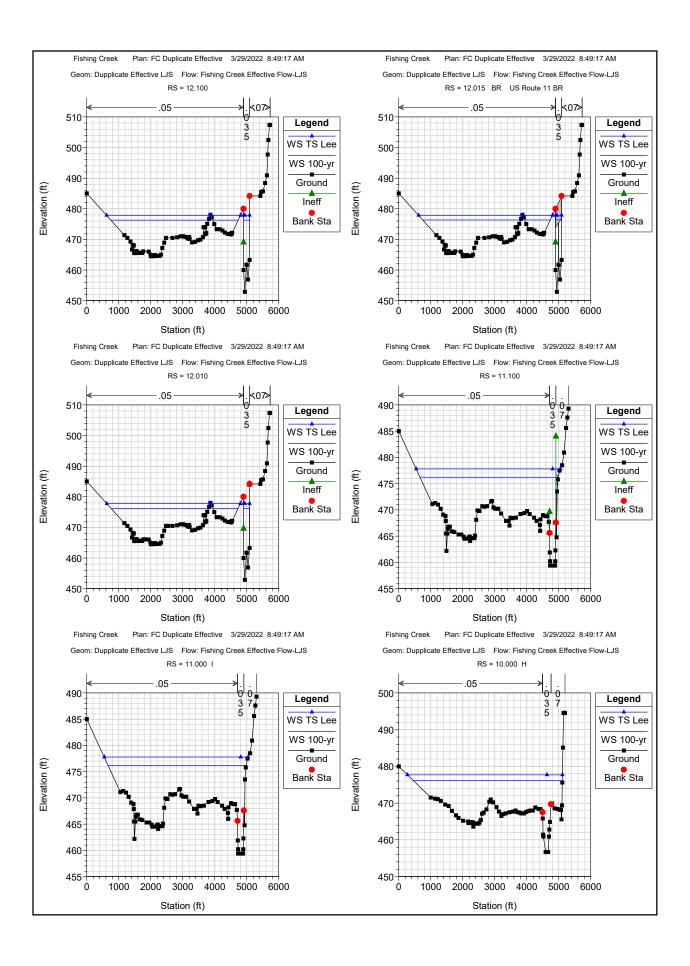


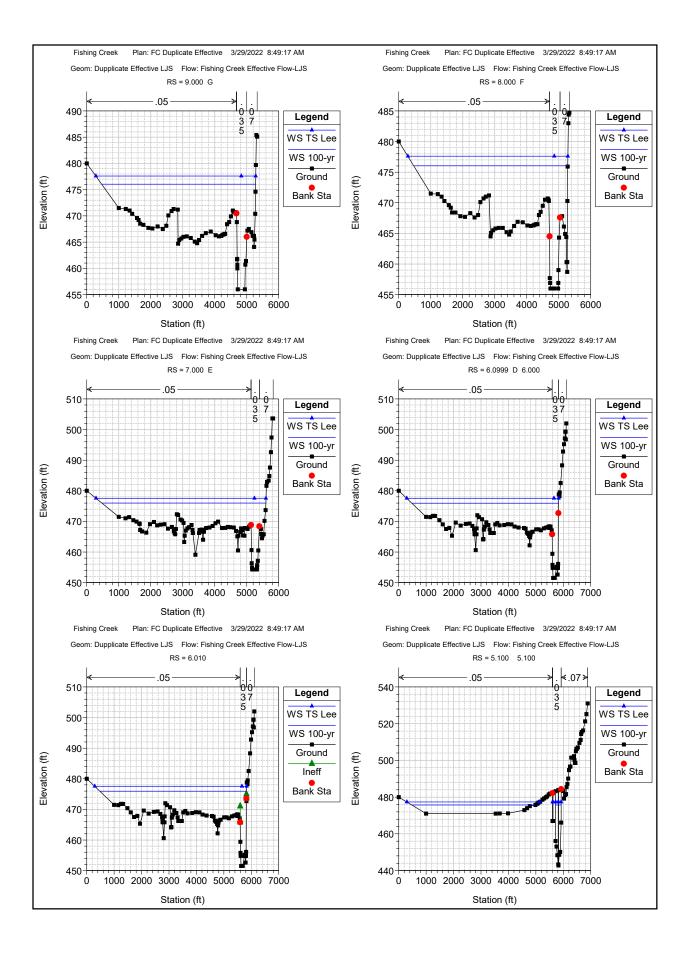


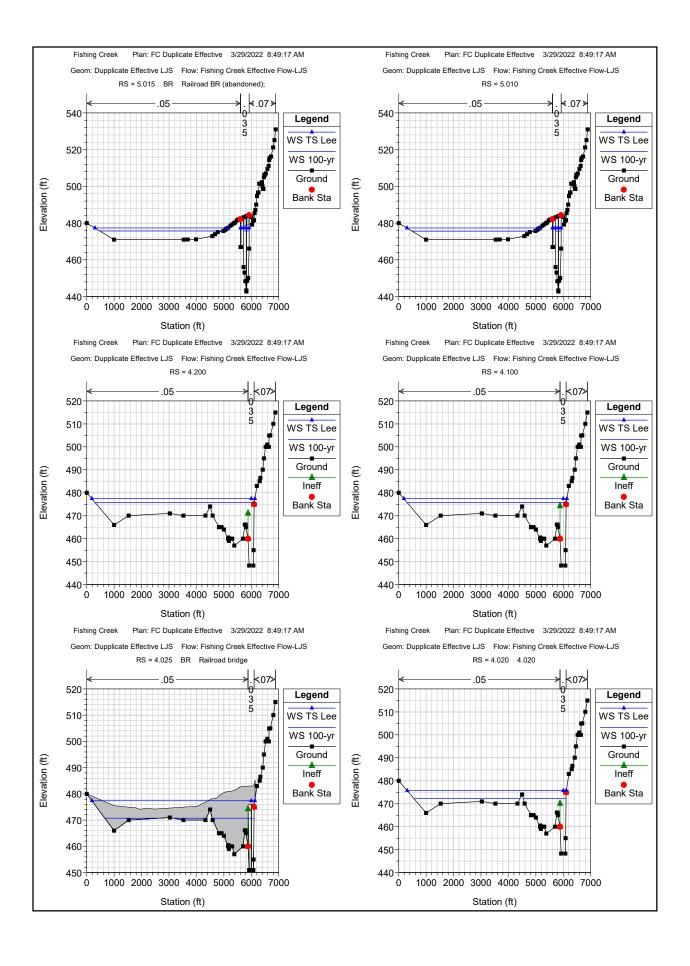


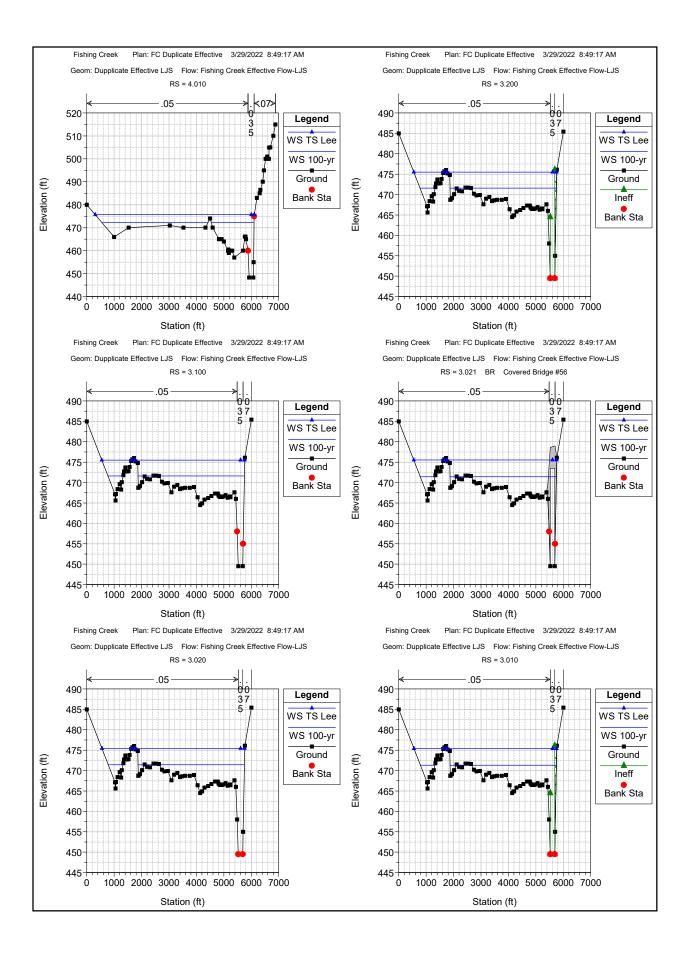


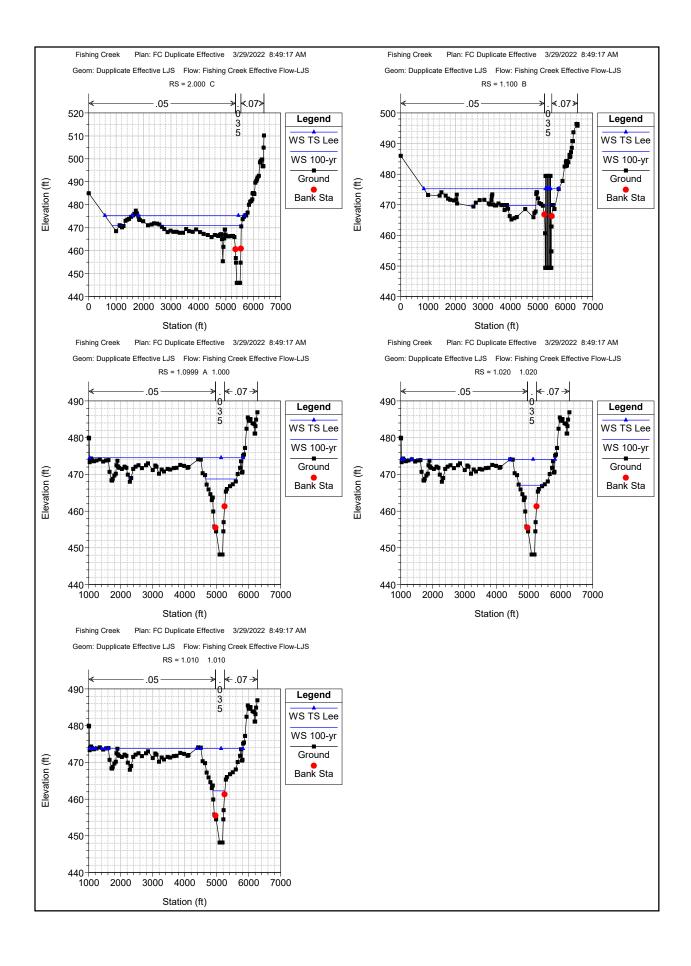




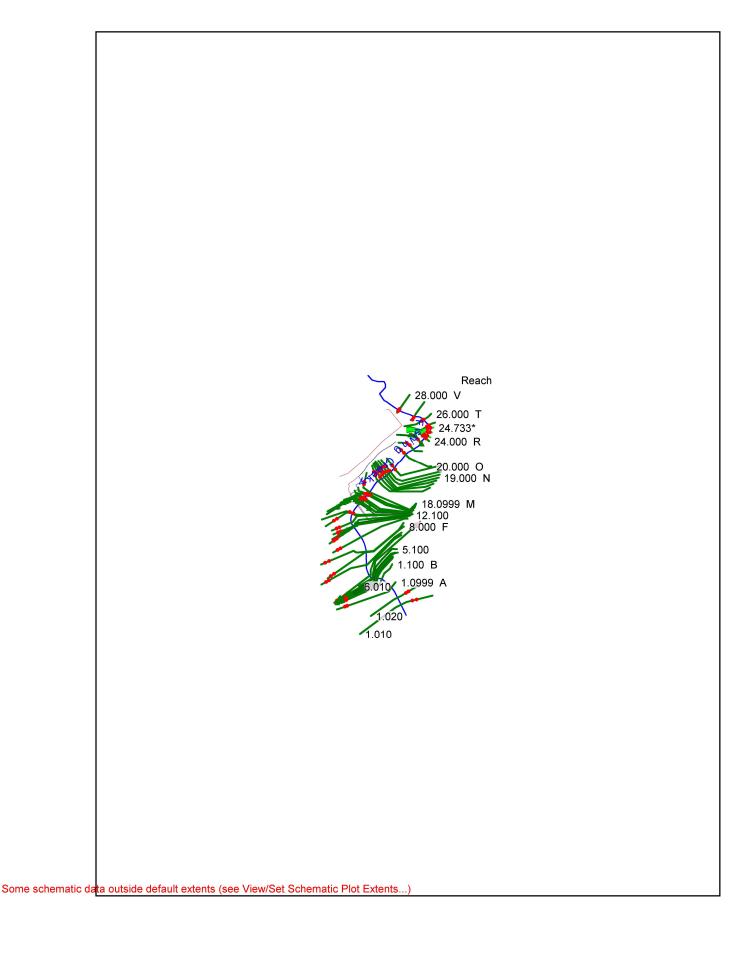


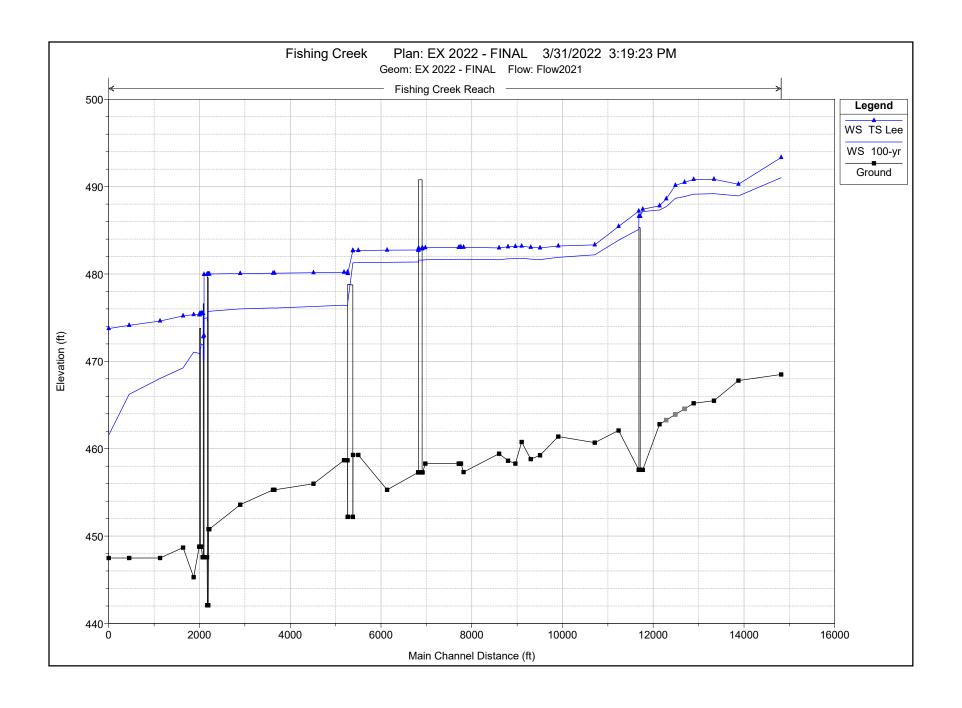






D.3 Existing Condition Model Output



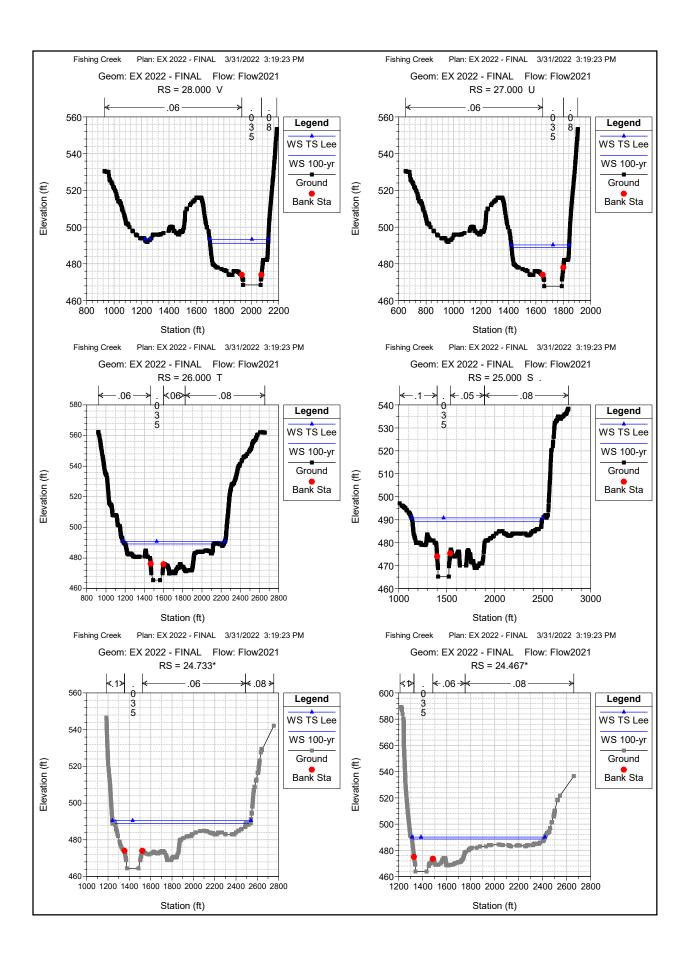


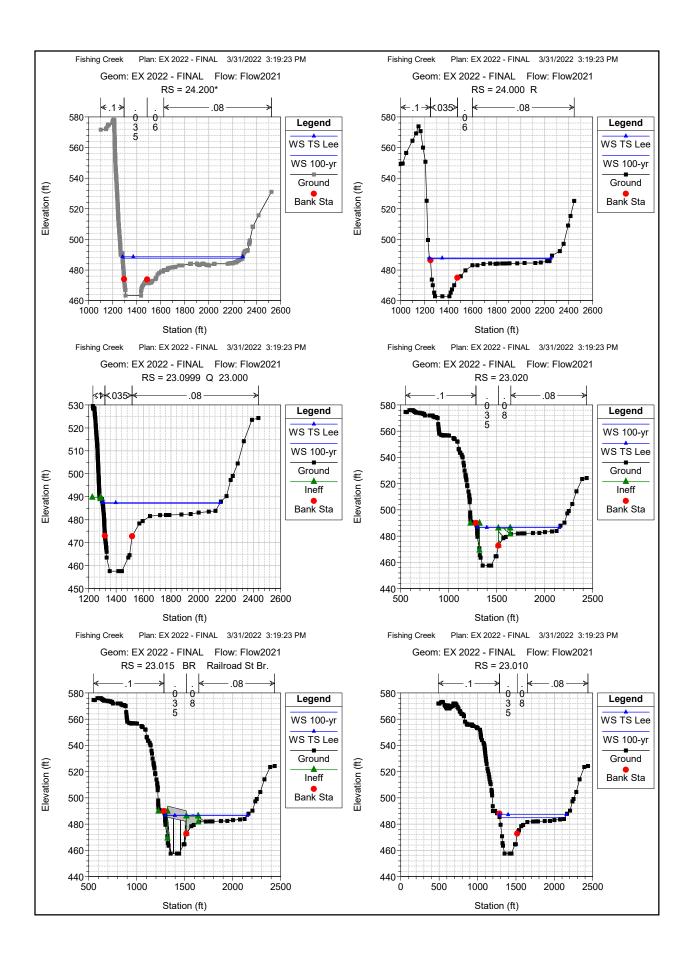
Reach	lan: FINAL River: Fish River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
rteacii	Tivel ola	1 TOTAL	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	7 TOUGE # OIII
Reach	28.000 V	100-yr	58900.00	468.50	491.03	(11)	492.82	0.001465	12.50	6887.95	423.35	0.47
Reach	28.000 V	TS Lee	78700.00	468.50	493.34		495.76	0.001774	14.69	7906.03	468.05	0.52
Reach	27.000 U	100-yr	58900.00	467.80	488.93		491.17	0.002024	13.76	6093.94	418.83	0.54
Reach	27.000 U	TS Lee	78700.00	467.80	490.27		493.62	0.002807	16.90	6657.74	421.68	0.64
Reach	26.000 T	100-yr	58900.00	465.50	489.20		490.08	0.000961	10.03	11107.83	973.07	0.38
Reach	26.000 T	TS Lee	78700.00	465.50	490.84		492.07	0.001255	12.02	12806.97	1063.84	0.44
Reach	25.000 S	100-yr	58900.00	465.20	489.14		489.64	0.000574	7.86	14355.65	1347.23	0.29
Reach	25.000 S	TS Lee	78700.00	465.20	490.82		491.48	0.000724	9.25	16625.94	1372.45	0.33
Decel	04.700*	400	50000.00	404.50	400.07		400.54	0.000040	0.50	40000.00	4040.00	0.00
Reach	24.733* 24.733*	100-yr	58900.00	464.56 464.56	488.87		489.54 491.36	0.000649 0.000801	8.53 9.93	13696.06	1243.88 1299.09	0.32
Reach	24.733	TS Lee	78700.00	404.50	490.49		491.30	0.000601	9.93	15778.71	1299.09	0.30
Reach	24.467*	100-yr	58900.00	463.92	488.67		489.43	0.000753	9.01	11774.03	1101.22	0.33
Reach	24.467*	TS Lee	78700.00	463.92	490.15		491.21	0.001000	10.84	13409.80	1109.31	0.39
rtodon	24.407	10 200	70700.00	400.02	450.10		701.21	0.001000	10.04	10-100.00	1100.01	0.00
Reach	24.200*	100-yr	58900.00	463.28	487.71		489.21	0.001141	10.98	8792.51	997.98	0.41
Reach	24.200*	TS Lee	78700.00	463.28	488.62		490.90	0.001682	13.69	9701.49	1002.70	
Reach	24.000 R	100-yr	58900.00	462.80	487.32		489.03	0.001221	11.07	7729.46	1009.78	0.42
Reach	24.000 R	TS Lee	78700.00	462.80	487.80		490.60	0.001971	14.27	8206.79	1012.85	0.54
Reach	23.0999 Q	100-yr	58900.00	457.59	487.14		488.62	0.000771	10.22	8746.05	855.59	0.35
Reach	23.0999 Q	TS Lee	78700.00	457.59	487.41		489.95	0.001316	13.44	8975.08	858.99	0.46
Reach	23.020	100-yr	58900.00	457.59	486.80	474.68	488.55	0.000870	10.88	7348.97	859.99	
Reach	23.020	TS Lee	78700.00	457.59	486.59	477.70	489.80	0.001608	14.71	7174.31	857.40	0.51
Decel	00.045		Deleter									
Reach	23.015		Bridge									
Danah	23.010	100	E0000 00	457.50	40E 40		406.07	0.001127	10.05	7202.54	849.60	0.41
Reach Reach	23.010	100-yr TS Lee	58900.00 78700.00	457.59 457.59	485.12 487.19		486.87 489.50	0.001127 0.001386	10.95 12.80	8990.66	871.55	
rteacii	23.010	10 Lee	70700.00	437.55	407.19		403.30	0.001300	12.00	0990.00	07 1.55	0.40
Reach	21.000 P	100-yr	58900.00	462.09	483.87		486.06	0.002216	12.27	7008.84	949.80	0.49
Reach	21.000 P	TS Lee	78700.00	462.09	485.43		488.43	0.002842	14.63	8552.48	1018.21	0.56
Reach	20.000 O	100-yr	58900.00	460.69	482.21	476.68	484.72	0.002809	13.41	8269.48	1764.75	0.54
Reach	20.000 O	TS Lee	78700.00	460.69	483.34	482.58	486.74	0.003707	16.01	10287.99	1791.87	0.63
Reach	19.100	100-yr	58900.00	461.39	481.91		482.86	0.001461	8.97	15946.64	2623.65	0.36
Reach	19.100	TS Lee	78700.00	461.39	483.20		484.40	0.001810	10.41	19374.93	2666.57	0.40
Reach	19.050	100-yr	58900.00	459.25	481.65		482.37	0.001143	7.84	15317.15	2710.17	0.32
Reach	19.050	TS Lee	78700.00	459.25	482.99		483.82	0.001327	8.84	18978.97	2757.94	0.34
	10.005	100	50000.00	450.04	101.70		100.10	2 22222	0.00	10501.00	0007.07	
Reach	19.025 19.025	100-yr	58900.00	458.81	481.70		482.13	0.000902	6.60 7.44	19521.89	3067.67	0.28
Reach	19.025	TS Lee	78700.00	458.81	483.06		483.56	0.001036	7.44	23747.79	3153.56	0.30
Reach	19.000 N	100-yr	58900.00	460.77	481.80		481.98	0.000461	4.81	28681.30	3760.48	0.20
Reach	19.000 N	TS Lee	78700.00	460.77	483.18		483.39	0.000401	5.38	33907.78	3797.56	0.20
rtouon	10.000 14	10 200	70700.00	400.77	400.10		+00.00	0.000022	0.00	00007.70	0707.00	0.21
Reach	18.902	100-yr	58900.00	458.29	481.77		481.95	0.000406	4.79	29013.84	3656.56	0.19
Reach	18.902	TS Lee	78700.00	458.29	483.14		483.36	0.000473	5.41	34076.38	3707.20	
Reach	18.788	100-yr	58900.00	458.62	481.75		481.91	0.000417	4.72	29620.60	3718.29	0.19
Reach	18.788	TS Lee	78700.00	458.62	483.12		483.32	0.000481	5.31	34772.49	3771.21	0.21
Reach	18.649	100-yr	58900.00	459.43	481.63		481.87	0.000334	5.68	30292.85	3791.67	0.22
Reach	18.649	TS Lee	78700.00	459.43	482.98		483.27	0.000398	6.46	35474.79	3858.71	0.24
Reach	18.0999 M	100-yr	58900.00	457.32	481.69		481.76	0.000117	3.69	36120.95	4199.00	
Reach	18.0999 M	TS Lee	78700.00	457.32	483.06		483.15	0.000135	4.12	41966.16	4315.08	0.15
Desert	10.040	400	F0000 5	150.5-	101.5-		404 ==	0.00000	0.5-	00070 57	00015-	
Reach	18.040	100-yr	58900.00	458.29	481.69		481.75	0.000092	3.20	38679.98	3834.80	
Reach	18.040	TS Lee	78700.00	458.29	483.06		483.14	0.000112	3.66	43941.62	3843.64	0.13
Reach	18.03	100-yr	58900.00	458.29	481.68		481.75	0.000099	3.32	37355.25	3829.95	0.12
Reach	18.03	TS Lee	78700.00	458.29 458.29	483.05		481.75	0.000099	3.32	42625.32	3829.95	
i (Cacil	10.00	10 Lee	70700.00	+30.29	403.03		+03.14	0.000119	3.10	72020.32	3000.10	0.14
Reach	18.02	100-yr	58900.00	458.29	481.68		481.74	0.000102	3.39	38116.11	4038.51	0.13
Reach	18.02	TS Lee	78700.00	458.29	483.05		483.13	0.000102	3.83	43674.54	4076.20	
				.00.20	.00.00		100.10	2.300.20	0.50	.207 1.04	.0.0.20	5.14
Reach	18.010	100-yr	58900.00	458.29	481.68		481.74	0.000101	3.37	38367.80	3993.20	0.13
Reach	18.010	TS Lee	78700.00	458.29	483.05		483.12	0.000120	3.83	43874.64	4068.43	
Reach	16.0999 L	100-yr	58900.00	458.29	481.62	473.96	481.71	0.000115	3.57	32524.32	3807.68	0.13
				458.29	483.00	475.68	483.10	0.000123	3.85	40234.56	3969.37	

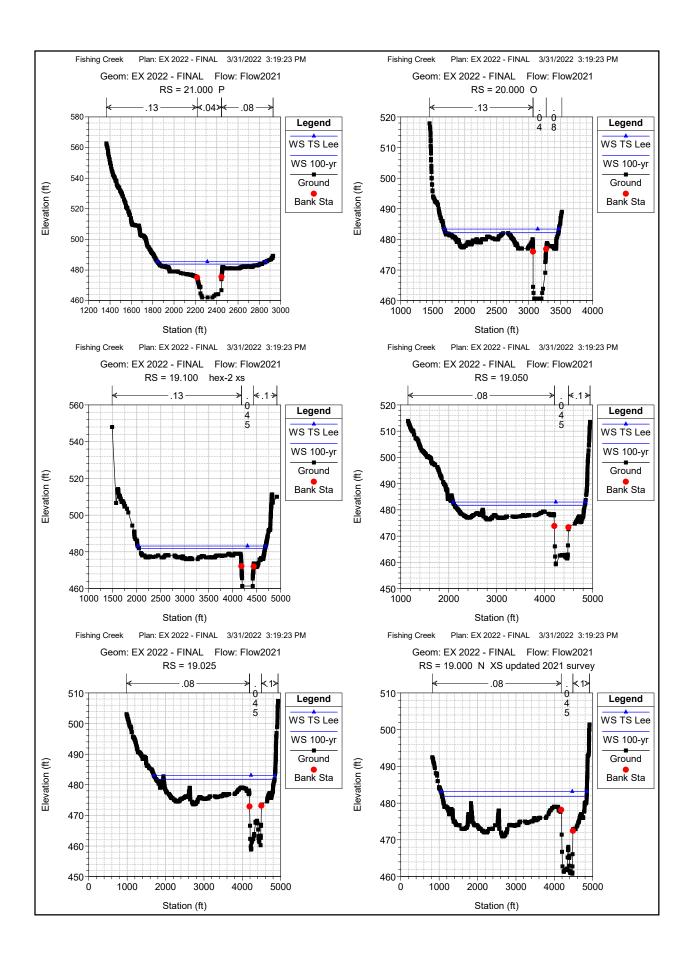
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Froude # Chl	
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach	16.040	100-yr	58900.00	457.29	481.59	473.91	481.70	0.000146	4.01	28322.24	3125.82	0.14
Reach	16.040	TS Lee	78700.00	457.29	482.95	475.85	483.08	0.000175	4.55	32796.02	3292.47	0.16
Reach	16.030	100-yr	58900.00	457.29	481.49	472.85	481.69	0.000287	5.18	25320.21	4498.27	0.19
Reach	16.030	TS Lee	78700.00	457.29	482.88	477.79	483.08	0.000302	5.47	31191.83	4766.38	0.19
Reach	16.025		Bridge									
Reach	16.020	100-yr	58900.00 78700.00	457.29	481.32	473.02	481.53	0.000304	5.30	25078.89 31088.23	4579.28	0.19
Reach	16.020	TS Lee	78700.00	457.29	482.71	477.63	482.92	0.000309	5.51	31088.23	4754.72	0.19
Reach	16.010	100-yr	58900.00	457.29	481.38		481.47	0.000117	3.59	32538.28	3396.50	0.13
Reach	16.010	TS Lee	78700.00	457.29	482.76		482.87	0.000140	4.08	37230.80	3416.21	0.15
Reach	14.000 K	100-yr	58900.00	455.29	481.34		481.43	0.000128	3.73	37587.54	5533.45	0.14
Reach	14.000 K	TS Lee	78700.00	455.29	482.73		482.83	0.000137	4.01	45316.93	5589.24	0.15
Reach	13.200 J	100-yr	58900.00	459.29	481.30		481.39	0.000157	3.94	36921.40	5539.58	0.15
Reach	13.200 J	TS Lee	78700.00	459.29	482.69		482.78	0.000161	4.16	44655.30	5570.03	0.16
Reach	13.100	100-yr	58900.00	459.29	481.29		481.37	0.000148	3.82	37957.67	5565.14	0.15
Reach	13.100	TS Lee	78700.00	459.29	482.68		482.77	0.000148	4.05	45722.82	5593.75	0.15
-		,	1 2. 30.00	.30.20	. 32.00		.52.17	2.220.02			22300	0.10
Reach	12.100	100-yr	58900.00	452.19	481.24	475.28	481.36	0.000194	4.38	32599.27	5554.43	0.16
Reach	12.100	TS Lee	78700.00	452.19	482.68	477.09	482.77	0.000151	4.01	45787.92	5582.37	0.14
Reach	12.015		Bridge									
Dasah	12.010	100	50000 00	452.40	470.05	476.65	470.27	0.004707	10.10	0000.60	4005.07	0.40
Reach Reach	12.010	100-yr TS Lee	58900.00 78700.00	452.19 452.19	476.65 480.05	476.65 477.68	478.37 480.56	0.001797 0.000671	12.10 8.17	9809.68 23009.01	4025.27 5450.77	0.49
rteacii	12.010	10 Lee	70700.00	402.10	400.03	477.00	400.50	0.000071	0.17	23003.01	3430.77	0.30
Reach	11.100	100-yr	58900.00	458.69	476.36		477.08	0.001152	8.80	13992.41	4073.46	0.39
Reach	11.100	TS Lee	78700.00	458.69	480.21		480.40	0.000324	5.41	33390.37	5717.74	0.22
Reach	11.000 I	100-yr	58900.00	458.69	476.43		476.70	0.000576	6.19	22131.63	5367.77	0.28
Reach	11.000 I	TS Lee	78700.00	458.69	480.21		480.29	0.000165	3.84	43558.57	5822.40	0.15
Decel	40.000 11	400 :	50000 00	455.00	470.00		470.44	0.000055	4.40	20040.00	5005.04	0.40
Reach Reach	10.000 H 10.000 H	100-yr TS Lee	58900.00 78700.00	455.99 455.99	476.28 480.15		476.41 480.21	0.000255 0.000095	4.42 3.10	32046.32 54956.46	5825.34 5979.34	0.19 0.12
Reacii	10.000 FI	13 Lee	78700.00	400.88	400.13		400.21	0.000093	3.10	34930.40	3919.34	0.12
Reach	9.000 G	100-yr	58900.00	455.29	476.11		476.26	0.000221	4.45	32822.70	5690.08	0.18
Reach	9.000 G	TS Lee	78700.00	455.29	480.08		480.15	0.000097	3.34	56624.66	6295.39	0.12
Reach	8.000 F	100-yr	58900.00	455.29	476.11		476.24	0.000180	4.18	33187.24	5709.34	0.16
Reach	8.000 F	TS Lee	78700.00	455.29	480.09		480.15	0.000081	3.16	57082.69	6302.69	0.11
Danah	7.000 E	100	58900.00	453.59	476.00		476.14	0.000211	4.47	33520.75	6517.94	0.18
Reach Reach	7.000 E	100-yr TS Lee	78700.00	453.59	480.05		480.10	0.000211	3.16	60278.77	6649.18	0.10
rtcuori	7.000 E	10 200	70700.00	400.00	400.00		400.10	0.000000	0.10	00210.11	0040.10	0.11
Reach	6.0999 D	100-yr	58900.00	450.79	475.72	466.04	476.03	0.000352	6.07	32184.62	6578.88	0.23
Reach	6.0999 D	TS Lee	78700.00	450.79	479.99	471.82	480.08	0.000119	3.96	60391.23	6777.32	0.14
Reach	6.010	100-yr	58900.00	450.79	475.70	466.01	476.02	0.000368	6.17		6562.17	0.23
Reach	6.010	TS Lee	78700.00	450.79	479.98	471.86	480.08	0.000130	4.12	61086.23	6768.17	0.14
Reach	5.100	100-yr	58900.00	442.09	475.72	463.73	475.98	0.000259	5.69	34013.65	6456.41	0.20
Reach	5.100	TS Lee	78700.00	442.09	479.99	469.67	480.06	0.000205	3.76	61942.21	6718.27	0.12
	0.100											****
Reach	5.015		Bridge									
Reach	5.010	100-yr	58900.00	442.09	474.97	465.39	475.32	0.000332	6.34	27406.27	5804.84	0.22
Reach	5.010	TS Lee	78700.00	442.09	479.97	467.28	480.05	0.000095	3.77	58023.35	6645.34	0.12
Reach	4.200	100 :==	58900.00	447.59	474.98	464.42	475.31	0.000306	6.08	27869.11	5546.07	0.22
Reach	4.200	100-yr TS Lee	78700.00	447.59	474.98	464.42	480.04	0.000306	3.78	58639.24	6690.45	0.22
		.0 200	. 57 55.50	++1.55	47 0.30	100.37	100.04	0.000000	0.70	55000.24	3000.40	0.12
Reach	4.100	100-yr	58900.00	447.59	474.91	464.37	475.28	0.000333	6.33	25815.02	4863.60	0.22
Reach	4.100	TS Lee	78700.00	447.59	479.94	467.29	480.03	0.000106	4.04	56010.30	6665.88	0.13
Reach	4.025		Bridge									
Reach	4.020	100-yr	58900.00	447.59	471.89	465.82	472.36	0.000494	7.14	19894.55	4734.58	0.27
Reach	4.020	TS Lee	78700.00	447.59	475.48	468.49	475.65	0.000209	5.10	38972.68	5766.76	0.18
Peach	4.010	100-yr	58900.00	447.59	471.88	462.91	472.36	0.000490	7.11	20399.35	4820.61	0.27
Reach Reach	4.010	TS Lee	78700.00	447.59	471.88	462.91	472.36	0.000490	5.03	39623.91	5776.51	0.27
		.0 200	. 57 55.50	++1.00	47 0.40	100.14	410.00	0.000204	0.00	33020.31	3770.01	0.10
	3.200	100-yr	58900.00	448.79	472.00	468.15	472.22	0.000653	5.47	23240.59	5630.46	0.22

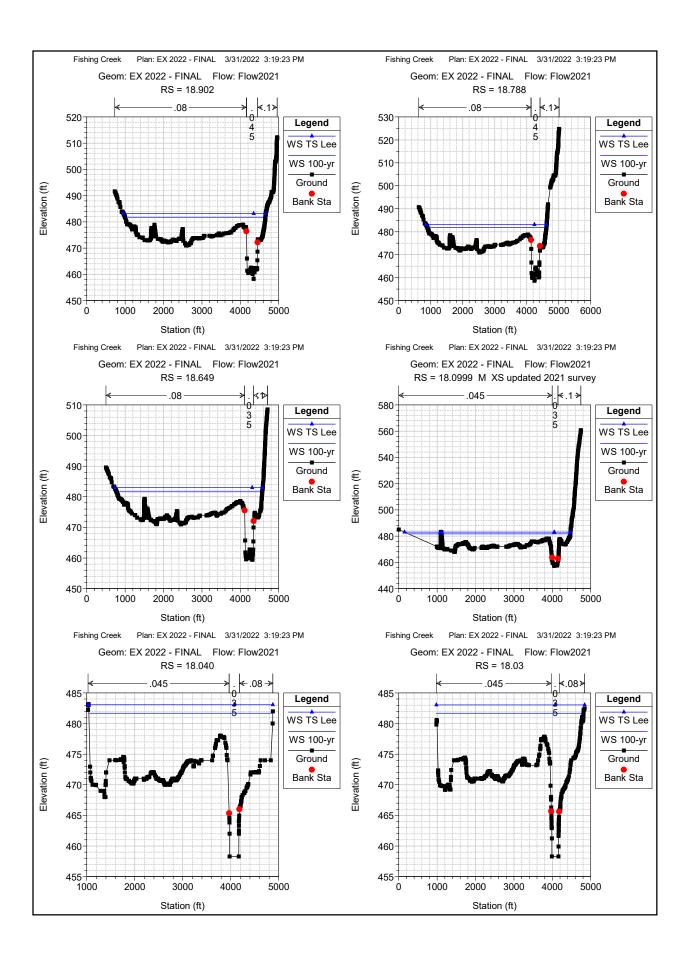
HEC-RAS Plan: FINAL River: Fishing Creek Reach: Reach (Continued)

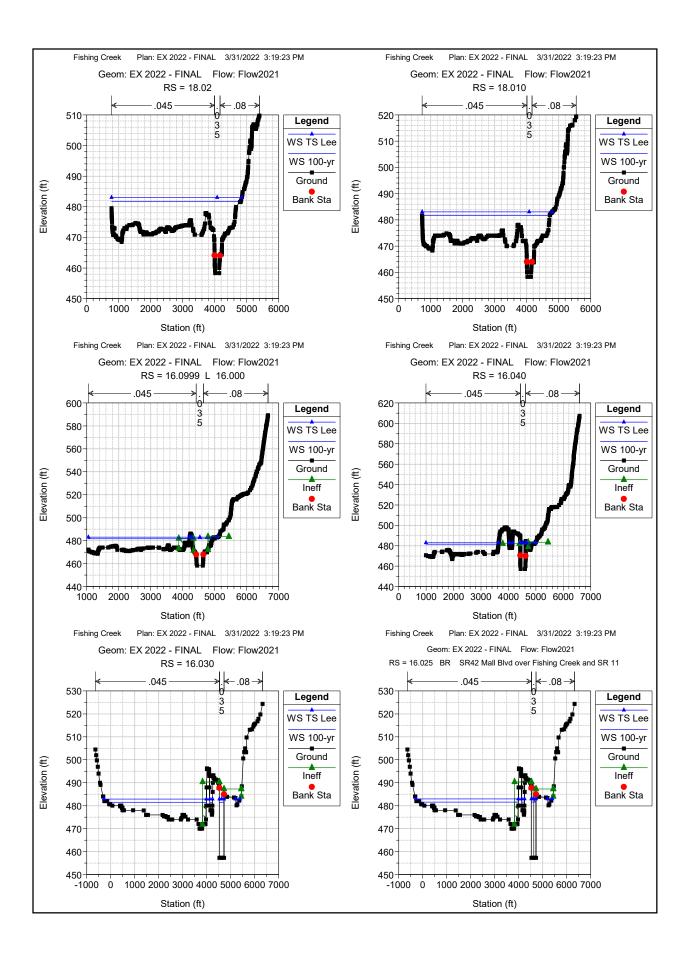
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach	3.200	TS Lee	78700.00	448.79	475.53	469.29	475.60	0.000223	3.38	43496.16	6029.13	0.13
Reach	3.100	100-yr	58900.00	448.79	471.41	470.16	472.07	0.000725	9.15	19243.74	4940.42	0.34
Reach	3.100	TS Lee	78700.00	448.79	475.42	470.94	475.57	0.000216	5.57	41362.22	6014.20	0.19
Reach	3.021		Bridge									
Reach	3.020	100-yr	58900.00	448.79	470.83	469.83	471.74	0.000951	10.29	17115.16	4734.41	0.39
Reach	3.020	TS Lee	78700.00	448.79	475.33	470.90	475.49	0.000223	5.64	40487.60	5813.12	0.19
Reach	3.010	100-yr	58900.00	448.79	470.92	469.28	471.62	0.000714	8.94	18370.34	4664.49	0.34
Reach	3.010	TS Lee	78700.00	448.79	475.33	470.50	475.48	0.000197	5.30	41209.54	5799.19	0.18
Reach	2.000 C	100-yr	58900.00	445.29	471.06		471.34	0.000850	5.76	20021.66	4599.06	0.23
Reach	2.000 C	TS Lee	78700.00	445.29	475.35		475.43	0.000209	3.27	42302.69	5502.65	0.12
Reach	1.100 B	100-yr	58900.00	448.69	469.25		470.84	0.003623	11.21	7716.15	1518.79	0.47
Reach	1.100 B	TS Lee	78700.00	448.69	475.21		475.35	0.000457	4.44	32483.15	5377.91	0.16
Reach	1.0999 A	100-yr	58900.00	447.49	468.04		469.67	0.001444	10.75	7225.60	1129.17	0.46
Reach	1.0999 A	TS Lee	78700.00	447.49	474.61		475.06	0.000382	6.85	27447.36	5941.43	0.25
Decet	4.000	400 :	50000.00	447.40	400.00	404.00	400.40	0.000404	40.04	F77F 00	700.04	0.55
Reach Reach	1.020	100-yr TS Lee	58900.00 78700.00	447.49 447.49	466.22 474.12	461.63	468.40 474.73	0.002194 0.000497	12.31 7.71	5775.62 24184.15	739.21 4800.46	0.55 0.28
Reach	1.010	100-yr	58900.00	447.49	461.53	461.53	466.44	0.007740	18.18	3455.75	371.92	0.98
Reach	1.010	TS Lee	78700.00	447.49	473.75	463.97	474.48	0.000576	8.22	22421.56	4797.66	0.30

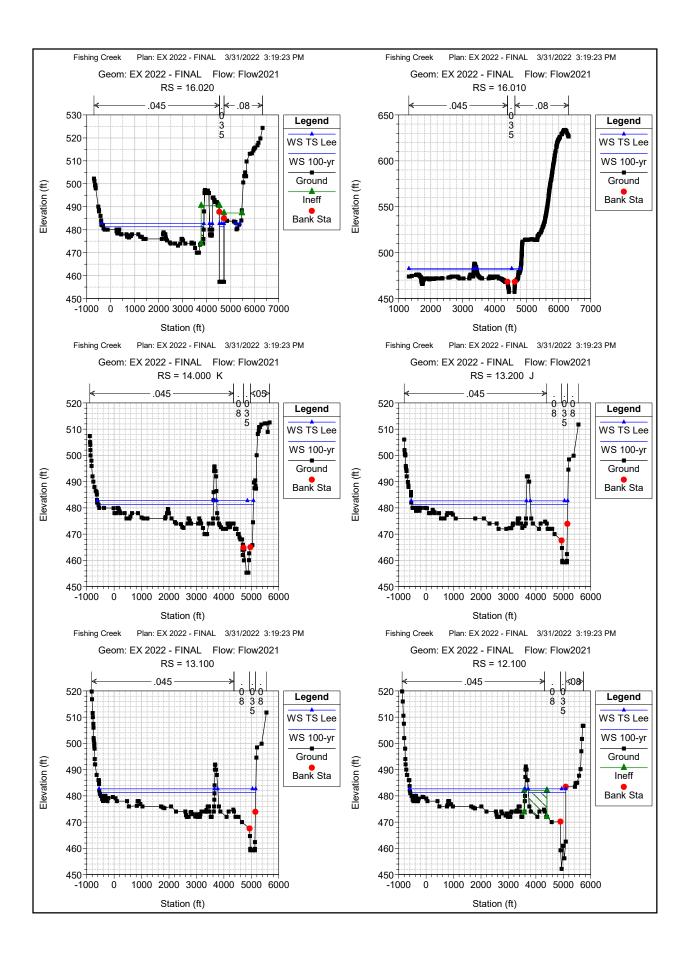


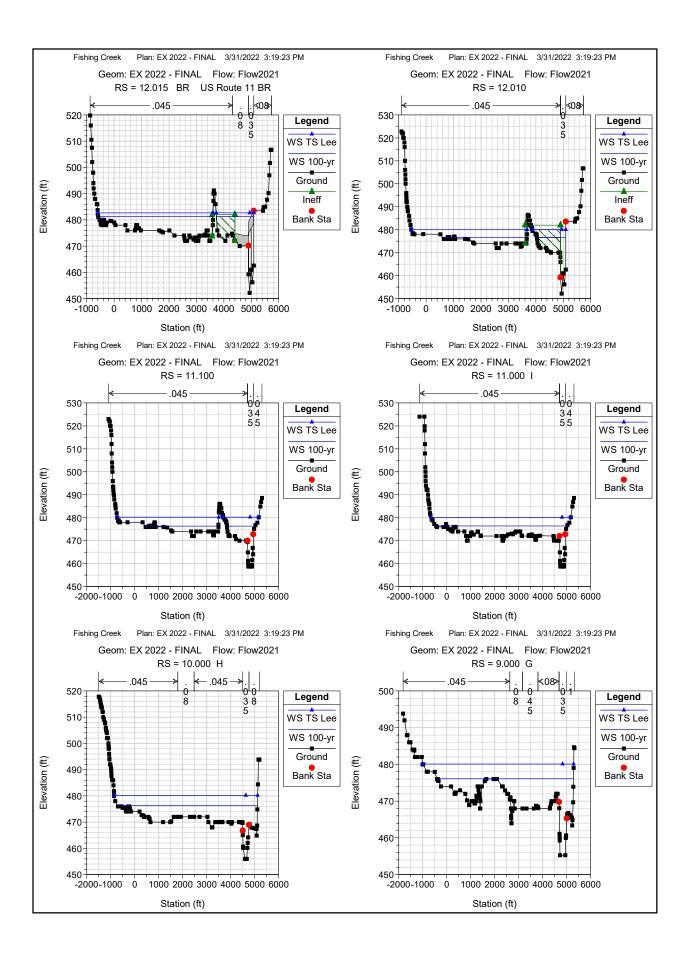


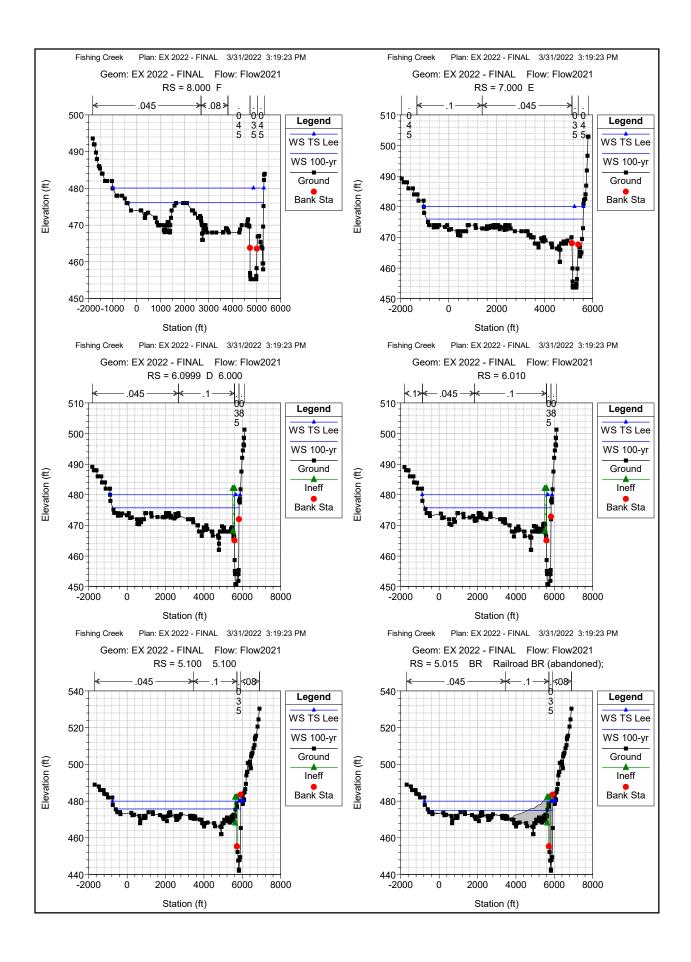


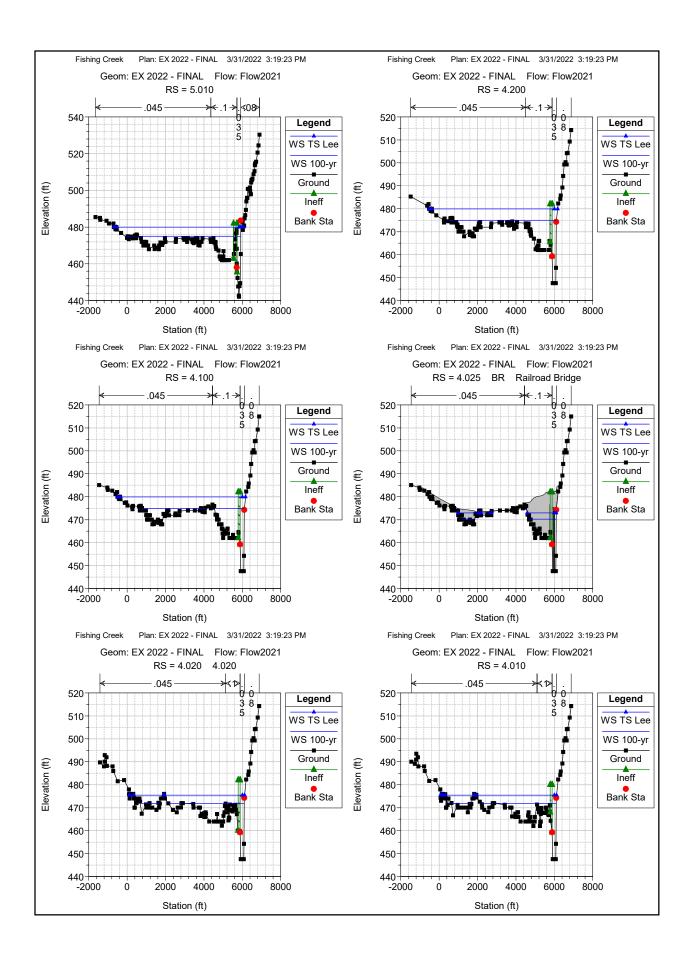


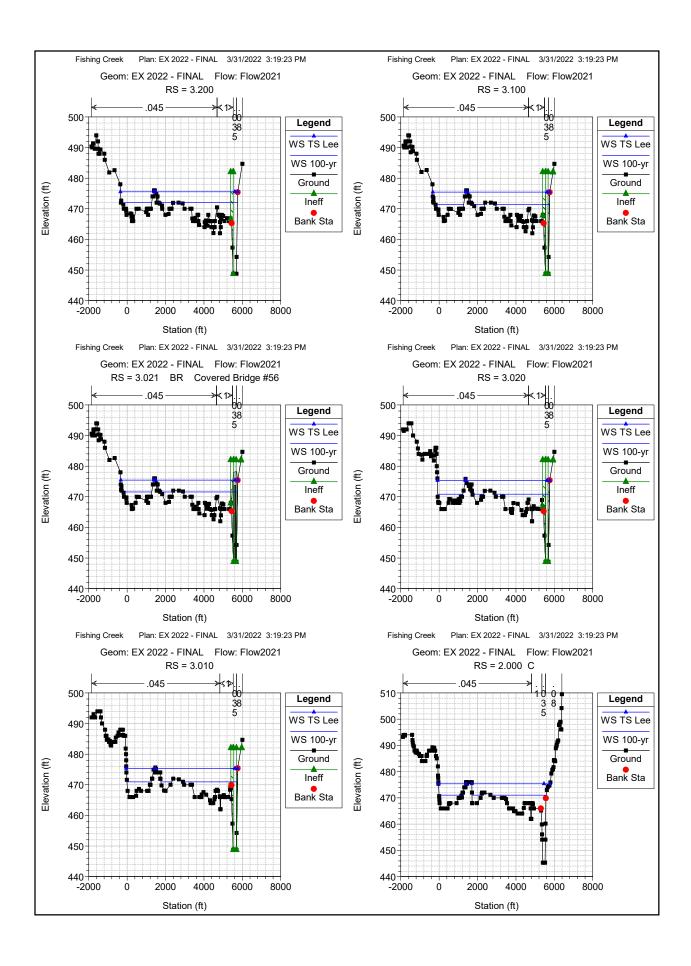


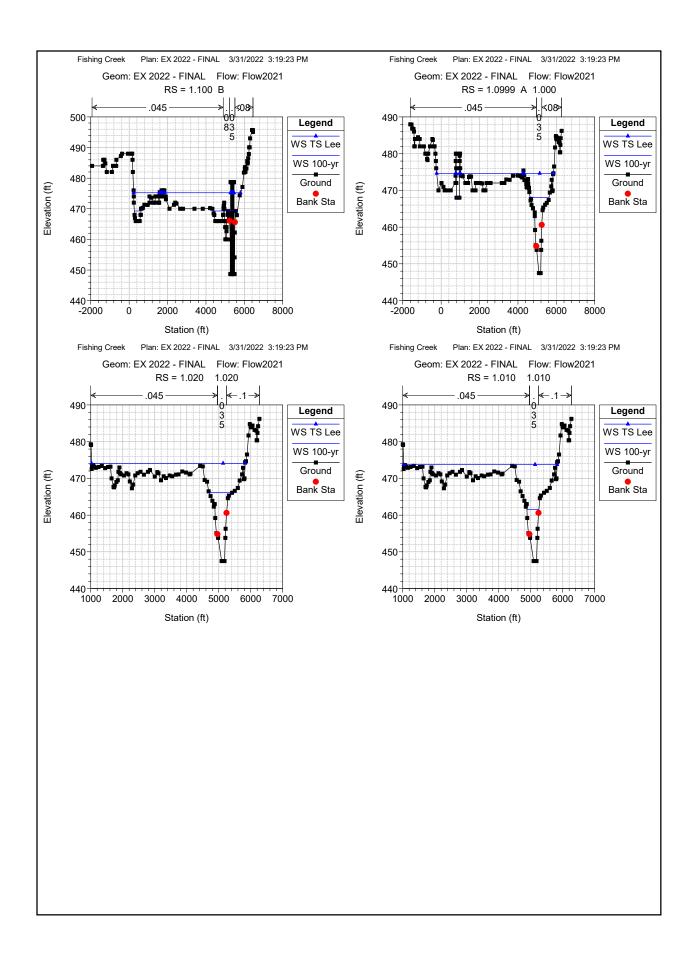








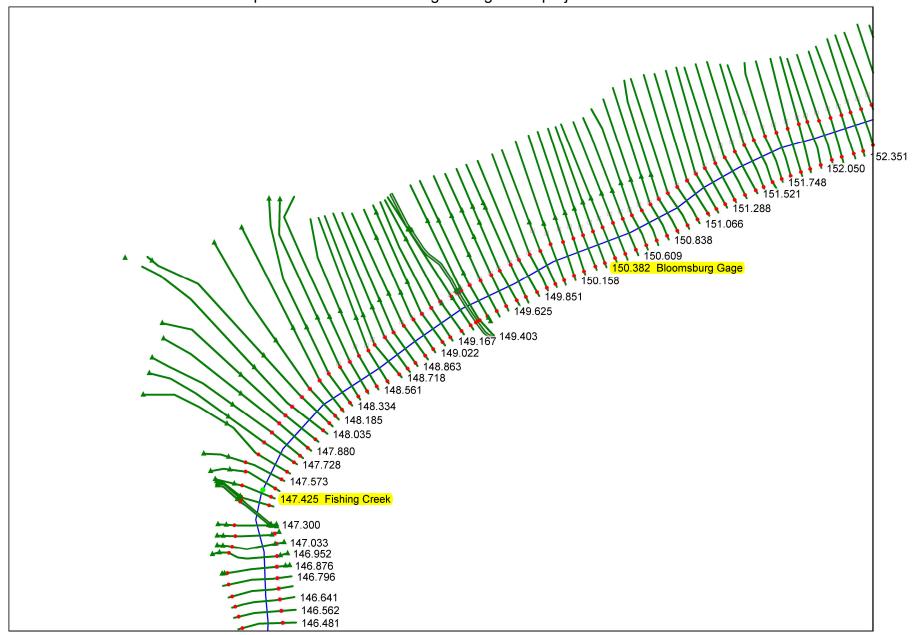


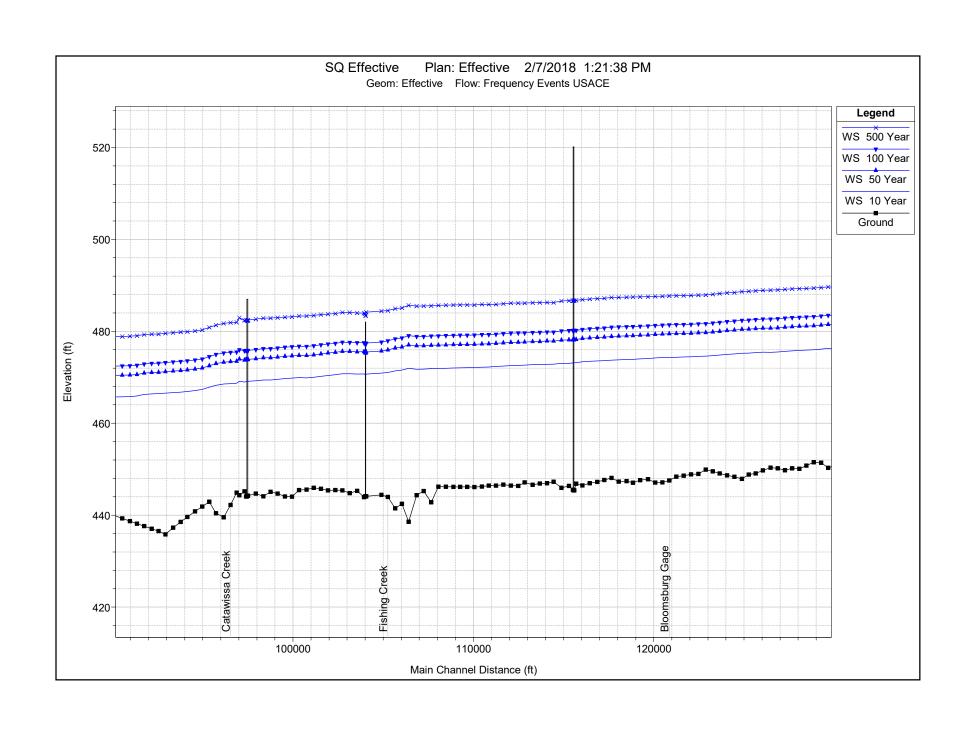


E. Susquehanna River Hydraulic Analysis

E.1 Effective Model Output

Print out is limited to reach of Susquehanna River in the neighboring of the project area.

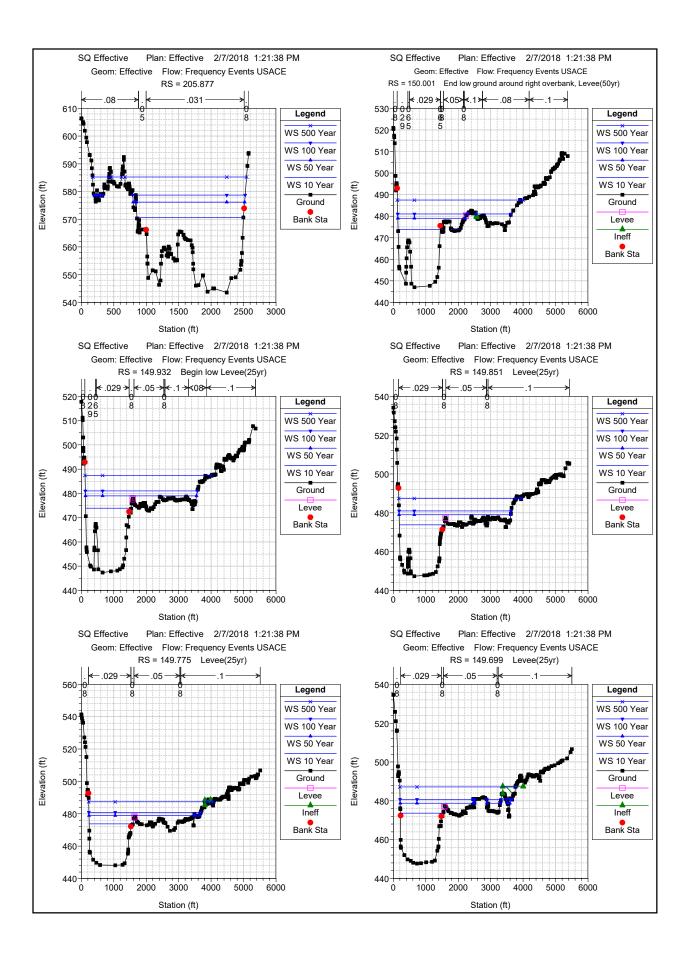


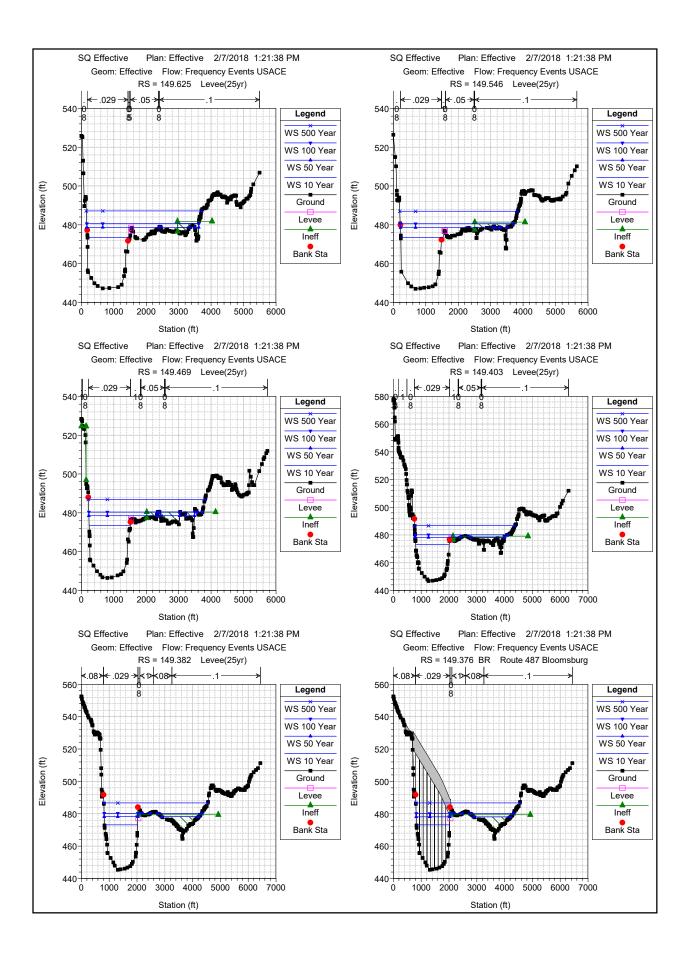


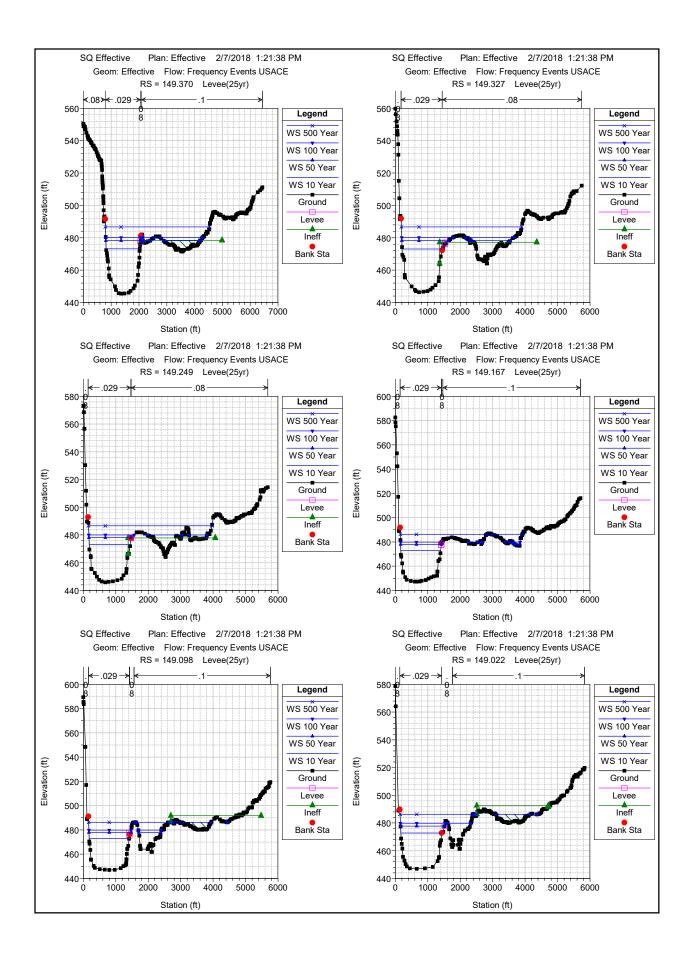
Comparison Com	HEC-RAS Plan: E	Effective Locations Reach		Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
Songerferne Mode Regul (1902) Store 14200 14100	Rivei	Reacii	River Sta	Fiolile										Floude # Cill
Supplement Marke Propose Supplement Marke Supplement Sup	Susquehanna	Middle Reach	150.001	10 Year										0.23
Separation Model Feet 1927 Septem 1970 Septem 1970		Middle Reach	150.001	50 Year					479.77	0.000194				0.23
Appendix	Susquehanna	Middle Reach	150.001	100 Year	277800.00	447.07	481.03	462.04	481.79	0.000189	7.12		3248.02	0.23
Baugarierres Balle Beach 4932 19 Year 2000000 447.3 479.0 469.0 479.0 469.0 479.0 469.0 479.	Susquehanna	Middle Reach	150.001	500 Year	378000.00	447.07	487.46	464.93	488.25	0.000163	7.46	69464.70	3860.88	0.22
Baugarierres Balle Beach 4932 19 Year 2000000 447.3 479.0 469.0 479.0 469.0 479.0 469.0 479.			440.000	40.14	470000 00		470.07	450.04	474.40	2 222424		00055.00	4404.05	0.00
Supplement Marie Reach Marie State M														
Sempendemon Model Febron Select														
Graphener Mode Record 48.85 10 Peru 17900.00 44.72 47.50 49.50 47.50 50.0017 50.00 50.														0.21
Regulation Mode Reum 1867 50 Year 200000 447 3 400 0 416 0 400 0 4			1											
Registration Model Febral 1875 10 Year 27900.00 447 2 44	Susquehanna	Middle Reach	149.851	10 Year	176300.00	447.32	473.81	458.29	474.35	0.000172	5.90	29916.21	1375.98	0.22
Segregation	Susquehanna	Middle Reach	149.851	50 Year	246300.00	447.32	478.96	460.63	479.60	0.000172	6.53	44180.27	3439.67	0.22
Company	Susquehanna													0.22
Supplement	Susquehanna	Middle Reach	149.851	500 Year	378000.00	447.32	487.42	464.28	488.10	0.000140	7.01	73805.20	3641.16	0.21
Supplement														
Suggesterman Mode Reach M														
Supplement														
Segrephannon Mode Reach 148 589 19 Year 1750000 447 67 473 62 468 50 474 50 280019 6.10 2075 50 1914 61 0.2														
Supplementary Mode Report 146900 O Year 249000 44767 47914 480.70 47967 47914 50.00165 7.00 460.40 60.00 0.00 30.00165 7.00 460.40 470.70 446.7	Ousquerianna	Wilddic reach	143.773	Joo Teal	370000.00	440.12	407.00	404.14	400.04	0.000100	0.51	70100.00	5750.72	0.20
Supplementary Mode Report 146900 O Year 249000 44767 47914 480.70 47967 47914 50.00165 7.00 460.40 60.00 0.00 30.00165 7.00 460.40 470.70 446.7	Susquehanna	Middle Reach	149.699	10 Year	176300.00	447.67	473.62	458.50	474.20	0.000183	6.15	28725.03	1314.61	0.23
Suggestern	· ·													0.23
Suggesthamma Mode Rasch 468.65 10 Year 17500.00 447.21 473.65 468.20 477.11 0.000179 0.11 2008156 305.52 0.2								461.69						0.23
Suggestherms	Susquehanna	Middle Reach	149.699	500 Year	378000.00	447.67	487.19	464.44	487.97	0.000154	7.44	66348.77	3562.10	0.22
Suggestherms														
Supplement Mode Reach 48,025 199 Yard 77780.00 447.2 49.04 441.44 441.40 0.000110 7.7 4959.17 3444.44 0.000110 7.7 4959.17 3444.40 0.000110 7.7 4959.17 34														0.22
Supplementary Models Reach 168-255 500 Year 37000 00 447-27 467-37 468-27 477-36 0.000133 7-44 70978-15 3546-56 0.2 Supplementary Models Reach 169-366 10 Year 170000 00 446-27 477-36 468-15 477-40 0.000137 0.10 2095-20 1266-22 0.1 Supplementary Models Reach 169-366 10 Year 277700 00 446-27 477-36 488-15 477-36 0.000137 7-7.20 0.0001														0.23
Marcel Reach 10.548 10 Year 17500.00 446.07 473.40 406.15 473.00 0.001977 6.10 226902.00 12990.07 0.20 12990.07 0.20 12990.07 0.20 12990.07 0.20 12990.07 0.20 12990.07 0.20														0.23
Suggespharms Modelle Reach 48 9-540 50 Year 24600000 44697 479.50 400.41 479.30 0.000186 7.20 30240.80 3199.44 0.000176 7.50 60228 6.00 3837.09 0.00 0.000186 7.20 7.50 60228 6.00 3837.09 0.00 0.000186 7.20 7.50 60228 6.00 3837.09 0.00 0.000186 7.20 6.000186 7.20	ousquenanna	Middle Reach	149.625	ouu Year	3/8000.00	447.23	487.13	464.21	487.91	0.000153	7.44	70878.15	3546.54	0.22
Suggespharms Modelle Reach 48 9-540 50 Year 24600000 44697 479.50 400.41 479.30 0.000186 7.20 30240.80 3199.44 0.000176 7.50 60228 6.00 3837.09 0.00 0.000186 7.20 7.50 60228 6.00 3837.09 0.00 0.000186 7.20 7.50 60228 6.00 3837.09 0.00 0.000186 7.20 6.000186 7.20	Susauchanna	Middle Pooch	1/10 5/16	10 Vecr	176200.00	446.07	472 40	AEQ 4E	474.00	0.000177	£ 10	28082 00	1200 F2	0.22
Siegepatharman Models Reach 149 July 500 Year 27700000 446 97 467 03 461 11 467 30 000107 7.20 4276 33 3470 50 0.2 2 3 3 3 3 5 0.0 2 2 3 3 3 3 3 5 0.0 2 2 3 3 3 3 3 5 0.0 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3														0.22
Suspenharma Middle Reach 149,540 00 Year														0.23
Suspenhamma Middle Reach 149.489 90 Years														0.22
Suspenhamma Middle Reach 149.489 90 Years														
Siegepathname Models Reach 1 149-489 100 Year 277800 00 440-80 400-10 431-26 481-26 0.000199 7.33 3973.77 3372.58 0.2 2	Susquehanna	Middle Reach	149.469	10 Year	176300.00	446.46	473.40	458.04	473.98	0.000184	6.14	28712.81	1269.04	0.23
Staggesharma Medic Reach 169.409 50 Verar 17500.00 446.56 490.54 497.77 0.000160 7.61 66209.38 3901.58 0.2 Staggesharma Medic Reach 169.403 10 Verar 17500.00 446.56 473.16 459.20 473.00 0.000239 6.76 72 25958.16 1200.07 7.00 7.00 7.00 7.00 7.00 7.00 7.0	Susquehanna	Middle Reach	149.469	50 Year	246300.00							36250.65	2967.34	0.24
Sungeshamma Moddle Reach 149,403 10 Year 178000 0 444.08 473.16 499.28 473.00 0.000239 6.79 20969.16 120.807 0.20														0.24
Sugupahama Middle Reach 149.403 59 Year 24530.00 448.68 478.21 461.76 479.12 0.000254 7.67 32206.38 28867.3 202 202 202 7.68 481.16 0.000252 7.68 4220.38 28867.3 202 202 202 7.68 481.16 0.000252 7.68 481.	Susquehanna	Middle Reach	149.469	500 Year	378000.00	446.46	486.94	464.04	487.77	0.000166	7.61	68299.38	3591.58	0.22
Sugupahama Middle Reach 149.403 59 Year 24530.00 448.68 478.21 461.76 479.12 0.000254 7.67 32206.38 28867.3 202 202 202 7.68 481.16 0.000252 7.68 4220.38 28867.3 202 202 202 7.68 481.16 0.000252 7.68 481.			140 400	40.14	470000 00	110.00	170.10	450.00	470.00	2 222222	0.70	05050 40	1000.07	
Suspephanne Middle Reach 149 403 100 Year 277800.00 448 68 480 72 482 76 485 18 487 70 0.000242 7.86 42590.50 3341.17 0.2														
Susquehamn Medie Reach 149.403 00 Year 37500.00 446.80 486.76 465.86 487.70 0.000168 8.12 65006.55 3508.13 0.2														
Surguehama Middle Reach 149.382 10 Year 176300.00 445.38 473.16 498.37 473.86 0.000216 6.1 26657.67 1192.30 0.2 Surguehama Middle Reach 149.382 50 Year 247800.00 445.38 478.21 460.81 479.09 0.000237 7.53 2688.71 2539.33 0.2 Surguehama Middle Reach 149.382 50 Year 277800.00 445.38 486.21 446.87 487.68 0.000199 7.70 4141.20 372.48 0.2 Surguehama Middle Reach 149.382 50 Year 277800.00 445.38 486.71 446.87 487.68 0.000198 8.16 67282.34 3734.83 0.2 Surguehama Middle Reach 149.370 10 Year 176300.00 445.49 473.15 488.22 473.81 0.000214 6.56 28666.94 1211.12 0.2 Surguehama Middle Reach 149.370 10 Year 246300.00 445.49 473.15 488.22 473.81 0.000214 6.56 28666.94 1211.12 0.2 Surguehama Middle Reach 149.370 10 Year 246300.00 445.49 473.15 488.22 473.81 0.000214 6.56 28666.94 1211.12 0.2 Surguehama Middle Reach 149.370 10 Year 246300.00 445.49 480.19 461.68 481.08 0.000223 7.66 43983.30 3712.09 0.2 Surguehama Middle Reach 149.370 10 Year 176300.00 445.89 480.19 461.68 481.08 0.000225 7.66 43983.30 3714.71 0.2 Surguehama Middle Reach 149.327 10 Year 176300.00 446.38 473.05 486.68 464.71 487.64 0.000194 8.00 67445.95 3741.71 0.2 Surguehama Middle Reach 149.327 10 Year 176300.00 446.38 473.05 486.68 467.71 487.64 0.000226 7.79 469.83 1247.04 0.2 Surguehama Middle Reach 149.327 10 Year 176300.00 446.38 473.05 486.68 467.71 487.64 0.000226 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83 0.000276 7.79 469.83														
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Sizeguehanna Middle Reach 149.382 500 Year 37800.00 445.38 446.71 464.87 487.68 0.000168 8.16 67252.34 3734.83 0.2	· ·		149.382			445.38	478.21	460.81	479.09	0.000232	7.53	32688.71	2539.33	0.26
Susquehanna Middle Reach 149.376 Bridge	Susquehanna	Middle Reach	149.382	100 Year	277800.00	445.38	480.22	461.86	481.12	0.000193	7.70	44141.20	3126.58	0.25
Susquehama Middle Rauch 149.370 10 Year 176300.00 445.49 473.15 458.22 473.81 0.000214 6.56 26866.34 1211.12 0.2	Susquehanna	Middle Reach	149.382	500 Year	378000.00	445.38	486.71	464.87	487.68	0.000168	8.16	67252.34	3734.83	0.24
Susquehama Middle Rauch 149.370 10 Year 176300.00 445.49 473.15 458.22 473.81 0.000214 6.56 26866.34 1211.12 0.2														
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Susquehanna Middle Reach 149,249 50 Year 246300.00 445,94 478.07 460.24 478.87 0.000215 7.16 34387.10 1295.02 0.2	Susauchanna	Middle Pooch	1/0 2/0	10 Vecr	176200.00	AAE 04	472.00	457.00	A72 GE	0.000104	6 20	27602 64	1266.06	0.00
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Susquehanna Middle Reach 149.098 50 Year 246300.00 446.96 477.89 460.12 478.64 0.000202 7.04 40715.45 1975.84 0.2 Susquehanna Middle Reach 149.098 100 Year 277800.00 446.96 479.96 461.09 480.68 0.000202 7.36 44639.52 2010.08 0.2 Susquehanna Middle Reach 149.098 500 Year 378000.00 446.96 486.29 463.97 487.27 0.000190 8.10 58723.41 3537.23 0.2 Susquehanna Middle Reach 149.022 10 Year 176300.00 446.89 472.76 457.82 473.37 0.000195 6.27 28097.51 1260.73 0.2 Susquehanna Middle Reach 149.022 50 Year 246300.00 446.89 472.76 460.12 478.56 0.000208 7.15 3470.18 1347.23 0.2 Susquehanna Middle Reach 149.022 100 Year 277800.00 446.89 479.79	Suggisher	Middle Deart	140.000	10 Vaar	170000 00	440.00	470.00	457 77	470.40	0.000400	0.00	07740 40	4000 47	000
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Susquehanna Middle Reach 149.022 500 Year 378000.00 446.89 486.24 463.95 487.18 0.000183 7.96 58701.80 3443.79 0.2 Susquehanna Middle Reach 148.947 10 Year 176300.00 446.62 472.74 457.14 473.28 0.000164 5.88 29996.11 1358.13 0.2 Susquehanna Middle Reach 148.947 50 Year 246300.00 446.62 477.76 459.30 478.45 0.000175 6.67 40045.30 2237.21 0.2 Susquehanna Middle Reach 148.947 100 Year 277800.00 446.62 479.76 460.26 480.50 0.000176 6.98 44172.77 2577.14 0.2 Susquehanna Middle Reach 148.947 500 Year 378000.00 446.62 486.22 462.97 487.09 0.000165 7.65 58803.37 3422.90 0.2 Susquehanna Middle Reach 148.863 10 Year 176300.00 447.12 472.6	Susquehanna										7.15			0.24
Susquehanna Middle Reach 148.947 10 Year 176300.00 446.62 472.74 457.14 473.28 0.000164 5.88 29996.11 1358.13 0.2 Susquehanna Middle Reach 148.947 50 Year 246300.00 446.62 477.76 459.30 478.45 0.000175 6.67 40045.30 2237.21 0.2 Susquehanna Middle Reach 148.947 100 Year 277800.00 446.62 479.76 460.26 480.50 0.000176 6.98 44172.77 2577.14 0.2 Susquehanna Middle Reach 148.947 500 Year 378000.00 446.62 486.22 462.97 487.09 0.000165 7.65 58803.37 3422.90 0.2 Susquehanna Middle Reach 148.863 10 Year 176300.00 447.12 472.64 458.08 473.20 0.000184 6.04 30141.74 1846.18 0.2 Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66														0.24
Susquehanna Middle Reach 148.947 50 Year 246300.00 446.62 477.76 459.30 478.45 0.000175 6.67 40045.30 2237.21 0.2 Susquehanna Middle Reach 148.947 100 Year 277800.00 446.62 479.76 480.26 480.50 0.000176 6.88 44172.77 2577.14 0.2 Susquehanna Middle Reach 148.947 500 Year 378000.00 446.62 486.22 462.97 487.09 0.000165 7.65 58803.37 3422.90 0.2 Susquehanna Middle Reach 148.863 10 Year 176300.00 447.12 472.64 458.08 473.20 0.000184 6.04 30141.74 1846.18 0.2 Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66 460.26 478.36 0.000190 6.78 39949.64 2088.28 0.2	Susquehanna	Middle Reach	149.022	500 Year	378000.00	446.89	486.24	463.95	487.18	0.000183	7.96	58701.80	3443.79	0.24
Susquehanna Middle Reach 148.947 50 Year 246300.00 446.62 477.76 459.30 478.45 0.000175 6.67 40045.30 2237.21 0.2 Susquehanna Middle Reach 148.947 100 Year 277800.00 446.62 479.76 480.26 480.50 0.000176 6.88 44172.77 2577.14 0.2 Susquehanna Middle Reach 148.947 500 Year 378000.00 446.62 486.22 462.97 487.09 0.000165 7.65 58803.37 3422.90 0.2 Susquehanna Middle Reach 148.863 10 Year 176300.00 447.12 472.64 458.08 473.20 0.000184 6.04 30141.74 1846.18 0.2 Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66 460.26 478.36 0.000190 6.78 39949.64 2088.28 0.2			110	40.31										
Susquehanna Middle Reach 148.947 100 Year 277800.00 446.62 479.76 460.26 480.50 0.000176 6.98 44172.77 2577.14 0.2 Susquehanna Middle Reach 148.947 500 Year 378000.00 446.62 486.22 462.97 487.09 0.000165 7.65 58803.37 3422.90 0.2 Susquehanna Middle Reach 148.863 10 Year 176300.00 447.12 472.64 458.08 473.20 0.000184 6.04 30141.74 1846.18 0.2 Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66 460.26 478.36 0.000190 6.78 39949.64 2088.28 0.2														
Susquehanna Middle Reach 148.947 500 Year 378000.00 446.62 486.22 462.97 487.09 0.000165 7.65 58803.37 3422.90 0.2 Susquehanna Middle Reach 148.863 10 Year 176300.00 447.12 472.64 458.08 473.20 0.000184 6.04 30141.74 1846.18 0.2 Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66 460.26 478.36 0.000190 6.78 39949.64 2088.28 0.2														
Susquehanna Middle Reach 148.863 10 Year 176300.00 447.12 472.64 458.08 473.20 0.000184 6.04 30141.74 1846.18 0.2 Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66 460.26 478.36 0.000190 6.78 39949.64 2088.28 0.2														
Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66 460.26 478.36 0.000190 6.78 39949.64 2088.28 0.2	Susquenanna	WILGUIG IXEAUIT	170.547	JUU TEAL	570000.00	440.02	400.22	402.97	401.09	0.000105	7.05	30003.37	J422.8U	0.23
Susquehanna Middle Reach 148.863 50 Year 246300.00 447.12 477.66 460.26 478.36 0.000190 6.78 39949.64 2088.28 0.2	Susquehanna	Middle Reach	148.863	10 Year	176300.00	447.12	472.64	458.08	473.20	0.000184	6.04	30141.74	1846.18	0.23
														0.23
	Susquehanna												2174.03	0.23

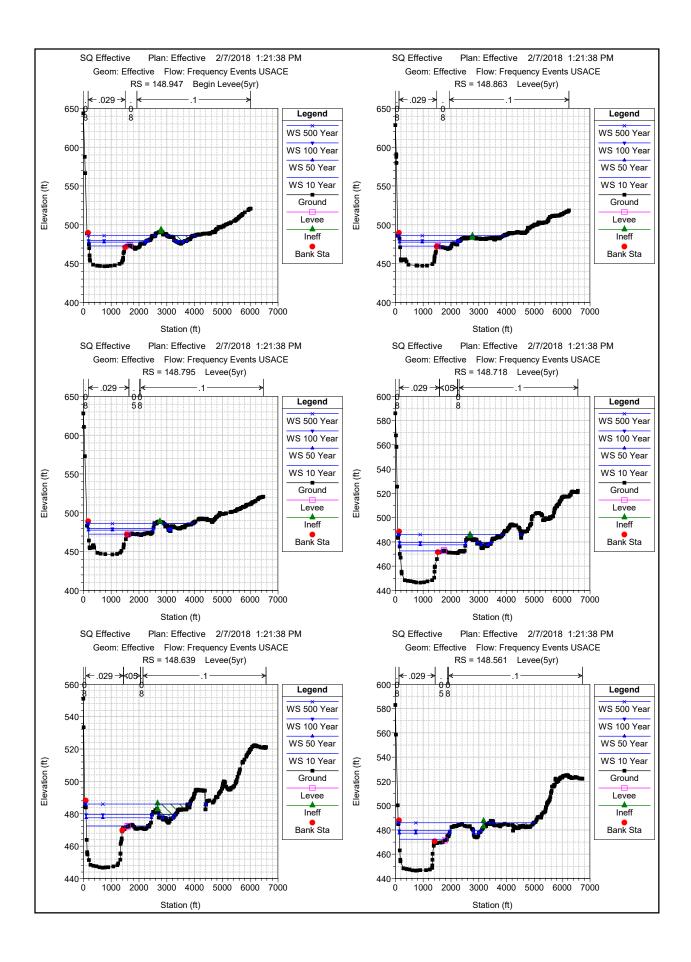
HEC-RAS Plan: Effective Locations: User Defined (Continued)

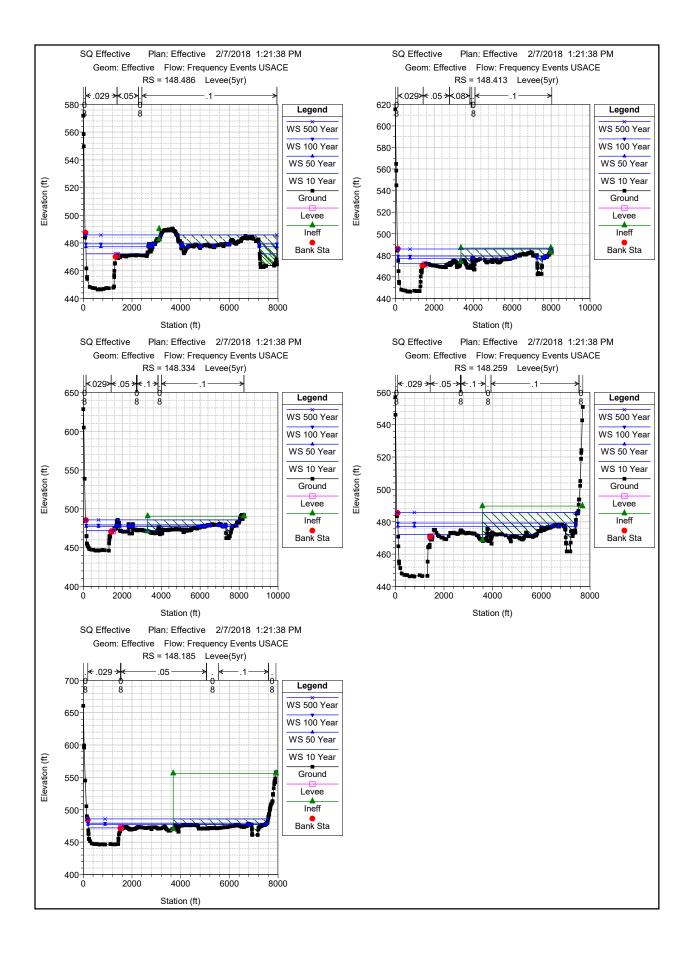
River	Effective Locations Reach	River Sta	, ,	O T-4-1	Min Oh El	W.O. Flan	0-14.141.0	F.O. Fl	F 0 01	V-1.0b-1	F1 A	T 186-185	F
River	Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
		440.000	5001/	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	0.00
Susquehanna	Middle Reach	148.863	500 Year	378000.00	447.12	486.15	463.91	487.02	0.000171	7.66	63681.09	3766.93	0.23
Susquehanna	Middle Reach	148.795	10 Year	176300.00	446.36	472.59	457.80	473.13	0.000178	5.88	30212.50	1826.88	0.22
Susquehanna	Middle Reach	148.795	50 Year	246300.00	446.36	477.63	460.03	478.28	0.000179	6.54	41446.43	2362.45	0.22
Susquehanna	Middle Reach	148.795	100 Year	277800.00	446.36	479.64	460.96	480.34	0.000175	6.79	46117.23	2433.29	0.22
Susquehanna	Middle Reach	148.795	500 Year	378000.00	446.36	486.15	463.64	486.93	0.000175	7.29	61492.92	3414.50	0.22
Susquenanna	Wildule Reach	140.753	Journal	370000.00	440.30	400.13	403.04	400.53	0.000133	1.25	01432.32	3414.30	0.22
Susquehanna	Middle Reach	148.718	10 Year	176300.00	446.43	472.54	456.75	473.05	0.000162	5.73	30900.11	1560.17	0.21
Susquehanna	Middle Reach	148.718	50 Year	246300.00	446.43	477.59	458.96	478.20	0.000162	6.35	43445.37	2647.04	0.21
Susquehanna	Middle Reach	148.718	100 Year	277800.00	446.43	479.61	459.90	480.25	0.000159	6.58	48228.43	2903.38	0.21
Susquehanna	Middle Reach	148.718	500 Year	378000.00	446.43	486.15	462.70	486.85	0.000138	6.98	70892.61	3765.84	0.21
		1											
Susquehanna	Middle Reach	148.639	10 Year	176300.00	446.64	472.45	456.80	472.98	0.000160	5.85	31061.93	2103.49	0.21
Susquehanna	Middle Reach	148.639	50 Year	246300.00	446.64	477.48	459.00	478.13	0.000166	6.54	42659.32	2741.94	0.22
Susquehanna	Middle Reach	148.639	100 Year	277800.00	446.64	479.49	459.92	480.18	0.000164	6.80	47398.78	2977.15	0.22
Susquehanna	Middle Reach	148.639	500 Year	378000.00	446.64	486.01	462.67	486.78	0.000147	7.30	63777.74	3790.02	0.21
Susquehanna	Middle Reach	148.561	10 Year	176300.00	446.44	472.36	456.58	472.91	0.000166	5.95	30477.81	1706.92	0.22
Susquehanna	Middle Reach	148.561	50 Year	246300.00	446.44	477.37	458.84	478.05	0.000175	6.72	39757.69	1998.13	0.22
Susquehanna	Middle Reach	148.561	100 Year	277800.00	446.44	479.37	459.78	480.11	0.000175	7.02	43868.36	2121.23	0.23
Susquehanna	Middle Reach	148.561	500 Year	378000.00	446.44	485.86	462.58	486.71	0.000160	7.61	60457.54	4750.54	0.22
Susquehanna	Middle Reach	148.486	10 Year	176300.00	446.44	472.24	456.91	472.84	0.000180	6.21	30035.60	3229.37	0.23
Susquehanna	Middle Reach	148.486	50 Year	246300.00	446.44	477.29	459.22	477.98	0.000181	6.83	43044.27	3724.58	0.23
Susquehanna	Middle Reach	148.486	100 Year	277800.00	446.44	479.31	460.19	480.03	0.000177	7.06	48479.53	5474.86	0.23
Susquehanna	Middle Reach	148.486	500 Year	378000.00	446.44	485.86	462.99	486.62	0.000152	7.43	67842.97	7224.92	0.22
Susquehanna	Middle Reach	148.413	10 Year	176300.00	446.24	472.18	456.74	472.77	0.000182	6.16	30955.36	3387.10	0.23
Susquehanna	Middle Reach	148.413	50 Year	246300.00	446.24	477.26	459.06	477.90	0.000174	6.64	46712.82	6054.33	0.22
Susquehanna	Middle Reach	148.413	100 Year	277800.00	446.24	479.29	460.02	479.95	0.000167	6.79	53253.55	6560.95	0.22
Susquehanna	Middle Reach	148.413	500 Year	378000.00	446.24	485.88	462.87	486.53	0.000137	6.99	74717.71	7922.09	0.21
Susquehanna	Middle Reach	148.334	10 Year	176300.00	446.14	472.13	456.30	472.68	0.000169	5.96	30835.19	3240.20	0.22
Susquehanna	Middle Reach	148.334	50 Year	246300.00	446.14	477.18	458.57	477.83	0.000171	6.58	44844.64	6104.20	0.22
Susquehanna	Middle Reach	148.334	100 Year	277800.00	446.14	479.20	459.52	479.87	0.000167	6.80	50813.49	7027.16	0.22
Susquehanna	Middle Reach	148.334	500 Year	378000.00	446.14	485.75	462.33	486.47	0.000143	7.16	70952.63	7922.18	0.21
Susquehanna	Middle Reach	148.259	10 Year	176300.00	446.15	472.10	456.01	472.61	0.000156	5.75	32054.11	4131.06	0.21
Susquehanna	Middle Reach	148.259	50 Year	246300.00	446.15	477.15	458.26	477.75	0.000157	6.34	48189.53	6838.98	0.21
Susquehanna	Middle Reach	148.259	100 Year	277800.00	446.15	479.17	459.17	479.79	0.000152	6.51	55210.36	7312.04	0.21
Susquehanna	Middle Reach	148.259	500 Year	378000.00	446.15	485.76	461.92	486.39	0.000127	6.77	78135.33	7449.68	0.20
Susquehanna	Middle Reach	148.185	10 Year	176300.00	446.16	472.05	455.82	472.54	0.000147	5.64	31252.55	1339.13	0.21
Susquehanna	Middle Reach	148.185	50 Year	246300.00	446.16	477.13	458.01	477.67	0.000142	6.09	50189.50	7184.18	0.20
Susquehanna	Middle Reach	148.185	100 Year	277800.00	446.16	479.16	458.94	479.71	0.000136	6.23	57313.82	7344.40	0.20
Susquehanna	Middle Reach	148.185	500 Year	378000.00	446.16	485.77	461.62	486.31	0.000111	6.39	80519.62	7420.10	0.19







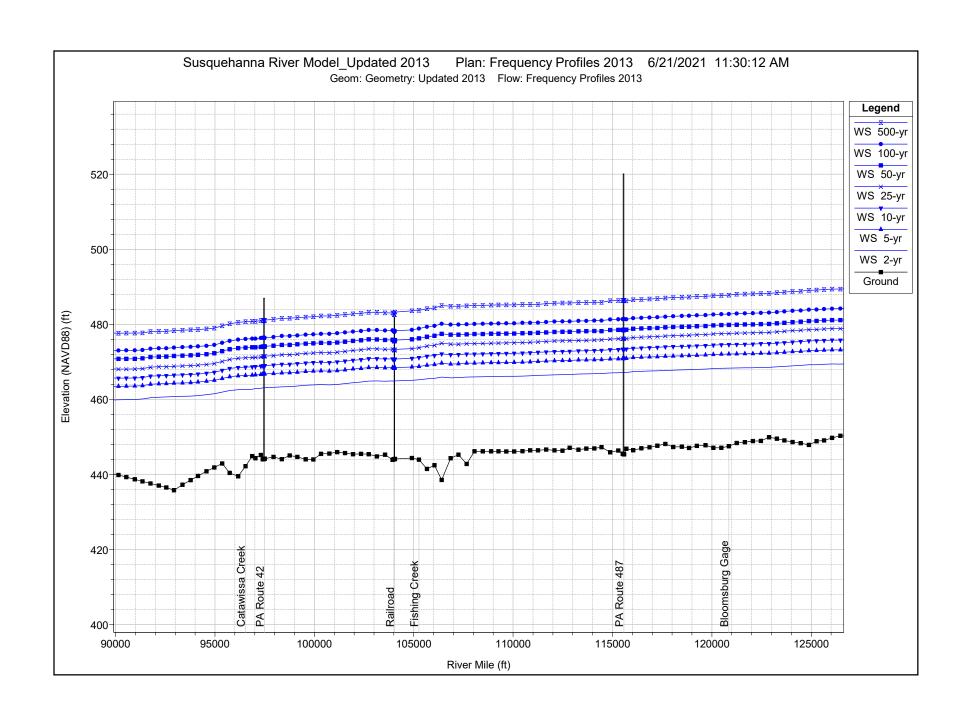




E.2 Preliminary Revised Effective Model Output

Print out is limited to the reach of Susquehanna River in the neighboring of the project area. 151.365 151.144 150.988 148.561 147.425 Fishing Creek **→** 146.562 **→** 146.481

146.328

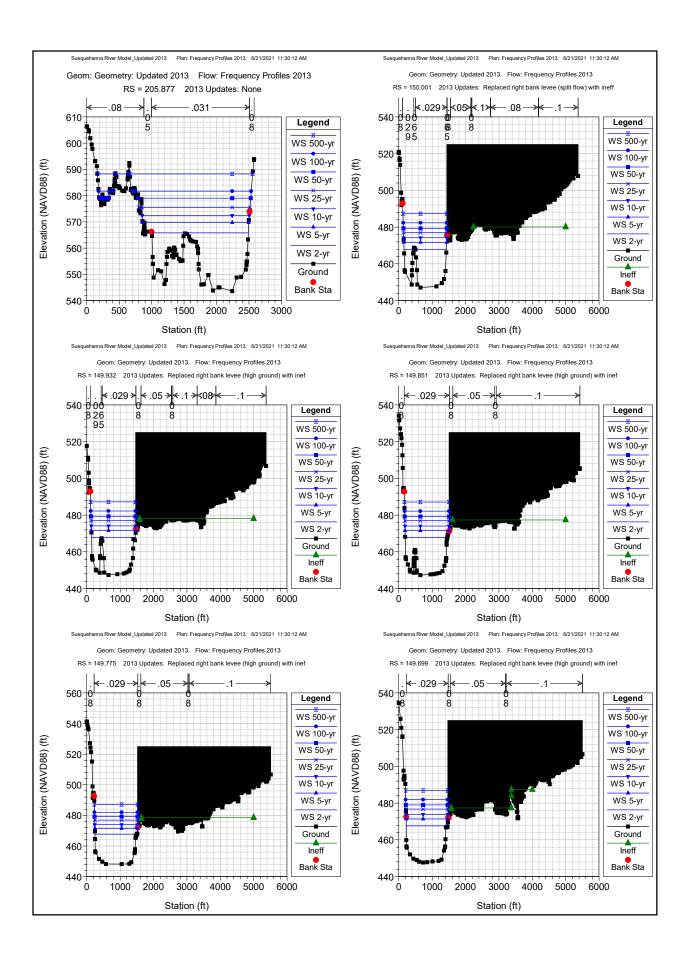


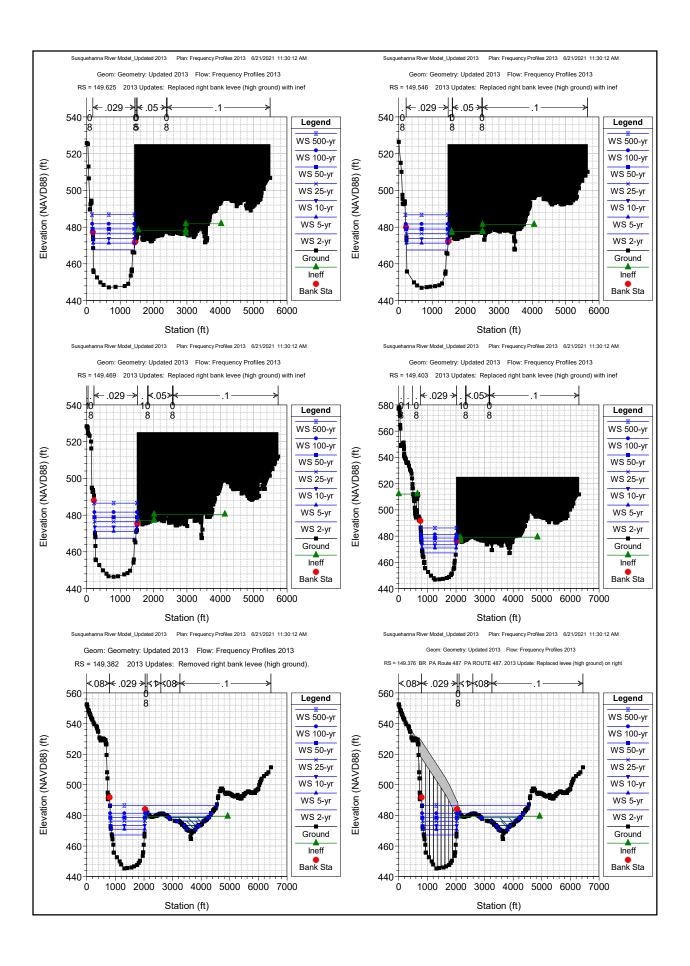
September Sept	HEC-RAS Plan: F River	requency 2013 Lo Reach	cations: User Defined River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
	Curringhama	Middle Desek	450,004	2	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	0.24
Security														
Security														
Separation Sep														
Section Sect														
Page														
Separation Sep	Susquehanna													0.25
Separation Sep	Sucauphanna	Middle Peach	140 032	2-vr	117600.00	447.41	467.86	456.35	468.34	0.000186	5.52	21205.73	1311 30	0.24
Mate March														
Separation Company C														
September Sept														
Manufactures														
Companies Mark Peach Mark														
Separation Marke Presson														
Separate Name Name Person 1489 1997 190000 1472 1773 1774 1														
Secure March Peacl March														
Marchelland														
Separaterian Marie Real M														
Seegentern Month March														
Secretaries Mode Resolt Mode														
Separation Marie Reach 60.778														
Supplement Mode Respon Mode Person M	Susquehanna	Middle Reach	149.851	500-yr	390900.00	447.32	487.15	464.60	488.20	0.000223	8.22	4/535.55	1335.37	0.24
Secure March Reach March														
Section Sect														0.23
Made Roses March Roses M														0.24
Supplement South Research South Re	Susquehanna													0.25
Segenthern	Susquehanna													0.24
Companisment Model Record 149 009 Cyr 11700.00 44 72 467 0 49 53 48 51 0.000191 0.55 218 53 122 60 0.00000000000000000000000000000000														0.24
Soughermon Mode Reach 14,000 1977 1930.00 1477 4773 49.00 477 4770 4730 1500.00 1477 4770 4	Susquehanna	Middle Reach	149.775	500-уг	390900.00	448.12	487.01	464.48	488.10	0.000228	8.39	46589.09	1291.68	0.25
Soughermon Mode Reach 14,000 1977 1930.00 1477 4773 49.00 477 4770 4730 1500.00 1477 4770 4	Susquehanna	Middle Reach	149.699	2-уг	117600.00	447.67	467.64	456.38	468.11	0.000181	5.55	21185.33	1238.48	0.24
Sougembrane Marie Reach 14,000 15,000 147,07 15000.00 147,07														0.24
Sougelearne Model Roach Model Sept 29800.00	Susquehanna													0.24
Suppartername Marie Reach 148-969														0.25
Segregation Medic Reach 148 099		Middle Reach	149.699			447.67	479.07	461.43		0.000196	7.59	35456.70	1258.26	0.25
Supplement Madie Reach 160 525 2y 117900.00 44 72 40 75 455 10 480.04 0.000175 5.50 21300.14 123446 0.2000.00		Middle Reach	149.699		303400.00	447.67	481.90	462.42	482.85	0.000220			1261.84	0.25
Segregations Models Reach 168.055 Syr 160000 0	Susquehanna	Middle Reach	149.699	500-yr	390900.00	447.67	486.83	464.80	488.00	0.000242	8.67	45269.67	1268.04	0.25
Segregations Models Reach 168.055 Syr 160000 0	Curringhama	Middle Desek	440.605	2	117600.00	447.00	467.57	456.40	460.04	0.000475	5.50	24200.44	1004.40	0.22
Singepatherms Mode Reach 168 255 294 239000 447 22 473 61 658 20 475 50 0.000146 0.00014 73 63 63 63 63 63 63 63														
Singesplanners Model Reach 186 186 187														
Suggestharms Models Reach 149 025 0.9y 28800.00 447.23 479.00 481.10 479.00 0.000161 7.55 5509.04 129.04 0.25 0.														
Stageplannya Motile Reach 148,025 100-yr 393400.00 447.23 481.82 482.16 0.00216 6.776 3918.81 21.256.65 0.24														
Suggesterman Models Reach 149,255 90-yr 17700 00 447 23 489 75 495 64 497 30 0.0000001 8.03 4549 13 1275 50 0.25														
Suggesthams Middle Reach 189,548 2-yr 11700.00 448,97 467,00 456,04 467,77 0.000171 0.47 21400.03 1228.03 0.23														
Siegepaharma Models Reach 148,546 Syr 152000 00 446.97 471.26 457.67 471.46 0.000127 0.20 2291297 124.08 0.24 Siegepaharma Models Reach 149,546 259.97 239600 00 446.97 477.62 440.27 477.45 0.000201 7.30 33802.18 1227.18 0.25 Siegepaharma Models Reach 140,546 259.97 239600 00 446.97 477.62 440.27 477.45 0.000201 7.30 33802.18 1227.18 0.25 Siegepaharma Models Reach 140,546 0.000201 7.30 33802.18 1227.18 0.25 Siegepaharma Models Reach 140,546 100-yr 333400 00 446.97 476.12 442.27 0.00027 7.74 392.12.00 1223.14 0.25 Siegepaharma Models Reach 140,546 0.000201 0.000201 7.74 392.12.00 0.25 Siegepaharma Models Reach 140,540 2.9r 117600.00 446.40 447.41 445.29 445.27 0.00027 7.74 392.12.00 1223.14 0.25 Siegepaharma Models Reach 140,440 2.9r 117600.00 446.40 447.41 445.59 447.00 0.00017 5.51 221323.11 1229.17 0.25 Siegepaharma Models Reach 140,440 5.9r 1139500 00 446.40 447.81 445.59 447.00 0.00017 5.51 221323.11 1229.07 0.25 Siegepaharma Models Reach 140,440 5.9r 113950 00 446.40 447.81 445.59 447.40 0.00017 5.51 221323.11 1229.07 0.25 Siegepaharma Models Reach 140,440 5.9r 113950 00 446.40 447.81 445.59 447.40 0.00018 666 22095.50 1269.46 0.25 Siegepaharma Models Reach 140,440 5.9r 5.9r 200800 00 446.40 447.83 445.59 447.70 0.000018 7.55 33881.57 1270.00 2.25 Siegepaharma Models Reach 140,440 5.0r 7.0r 7.0r 3.00000 446.40 447.81 445.90 447.70 0.000018 7.55 33881.57 1272.20 0.25 Siegepaharma Models Reach 140,440 5.0r 7.0r 5.0r 5.0			1.000	1 1 1										
Stagepathrama Modele Reach 146 546 10-yr 195000.00 448 97 478 52 450.00 200001 7.30 30001.01 127.12 10.025 30.00 2001.01 127.14 127.14 10.025 30.00 2001.01 127.14 10.00 2	Susquehanna	Middle Reach	149.546	2-уг	117600.00	446.97	467.50	456.04	467.97	0.000171	5.47	21490.63	1229.63	0.23
Sagageharma Medic Reach 149.546 19.94 19.9500.00 449.97 478.72 459.76 477.42 0.000162 0.02 20217.20 1242.16 0.25 Sagageharma Medic Reach 149.546 30.97 269800.00 449.97 478.92 440.02 477.80 0.0000162 7.30 32091.00 129.114 0.25 Sagageharma Medic Reach 149.546 30.97 269800.00 449.97 478.92 440.02 477.80 0.000102 7.34 39671.00 129.114 0.25 Sagageharma Medic Reach 149.546 30.97 390000.00 449.97 478.92 440.00 477.80 0.000102 7.34 39671.00 129.114 0.25 Sagageharma Medic Reach 149.546 30.97 390000.00 449.97 478.65 444.67 40.000001 5.51 212331 1200.72 0.25 Sagageharma Medic Reach 149.486 349.87 449.80 447.70 447.70 449.80 449.8						446.97								0.24
Stagepathrama Modele Reach 149.546 S0-yr 28980.00 449.07 48.12 49.10 47.750 0.000172 7.54 39571.96 1.251.14 0.25 80sepathrama Modele Reach 149.546 0.00yr 39090.00 449.07 481.74 492.06 44.67 0.000217 7.74 39571.50 1.202.14 0.22 80sepathrama Modele Reach 149.546 0.00yr 39090.00 449.07 481.74 480.05 449.46 487.80 0.000239 8.07 45440.88 1727.62 0.25 80sepathrama Modele Reach 149.469 2yr 11760.00 449.67 487.60 449.67 487.80 0.000239 8.07 45440.88 1727.62 0.25 80sepathrama Modele Reach 149.469 5yr 14050.00 449.46 477.31 455.56 0.477.70 0.000171 5.51 1129.23 1 100.74 0.23 80sepathrama Modele Reach 149.469 10-yr 190500.00 449.46 477.35 455.60 477.70 0.000170 6.06 2909.65 1123.97 0.24 80sepathrama Modele Reach 149.469 10-yr 290500.00 449.46 477.35 490.17 177.000170 6.06 2909.65 1123.97 0.25 80sepathrama Modele Reach 149.469 10-yr 290500.00 449.46 478.35 490.00 477.77 0.000170 6.06 2909.65 1123.97 0.25 80sepathrama Modele Reach 149.469 10-yr 290500.00 449.46 478.35 490.00 477.77 0.000170 7.73 30501.50 1727.74 0.05 80sepathrama Modele Reach 149.469 10-yr 290500.00 449.46 478.35 490.00 477.77 0.000170 7.74 39000.20 177.72 4 0.25 80sepathrama Modele Reach 149.469 10-yr 390500.00 449.46 478.35 490.00 477.77 0.000170 7.74 39000.20 177.72 4 0.25 80sepathrama Modele Reach 149.469 10-yr 390500.00 449.46 478.35 490.00 477.77 0.000170 7.74 39000.20 177.72 4 0.25 80sepathrama Modele Reach 149.409 50-yr 390500.00 449.46 478.55 449.55 449.70 0.000245 8.59 45940.00 1.280.00 0.25 80sepathrama Modele Reach 149.409 50-yr 390500.00 449.46 478.55 449.55 449.70 0.000245 8.59 45940.00 1.280.00 0.25 80sepathrama Modele Reach 149.403 50-yr 290500.00 449.80 478.70 479.70 0.000245 8.57 1228647 1196.00 0.25 80sepathrama Modele Reach 149.403 50-yr 290500.00 449.80 478.25 449.50 477.70 0.000245 8.57 1228647 1196.00 0.25 80sepathrama Modele Reach 149.403 50-yr 290500.00 449.80 478.25 449.50 477.70 0.000245 8.57 1228647 1196.00 0.00024 8.59 1966.00 0.00024 8.59 1966.00 0.00024 8.50 1966.00 0.00024 8.50 1966.00 0.00024 8.50 1966.00 0.00024 8.50 1966.0		Middle Reach	149.546		193500.00	446.97	473.74	458.74	474.42	0.000182	6.62	29217.26	1242.86	0.24
Stangushamma Medile Reach 49.546 100-yr 30000000 446.97 481.74 402.09 442.07 0.000217 7.74 39215.20 1283.41 0.24	Susquehanna	Middle Reach	149.546	25-yr	239600.00	446.97	476.62	460.21	477.45	0.000201	7.30	32802.18	1247.18	0.25
Singqueharman Middle Reach 149,546 500-yr 3900000 446,97 486,85 464,45 487,80 0.000238 8.62 4544,98 1774,52 0.25	Susquehanna	Middle Reach	149.546	50-уг	268800.00	446.97	478.92	461.08	479.80	0.000192	7.54	35671.96	1251.14	0.25
Susqueharma Middle Reach 149.469 Syr 1170000 446.46 447.40 455.89 467.00 0.000176 5.51 21329.31 1208.74 0.23 Susqueharma Middle Reach 149.469 Syr 1620000 446.46 477.16 477.55 471.77 0.000176 6.25 22899.55 1238.97 0.23 Susqueharma Middle Reach 149.469 Syr 1620000 446.46 477.45 477.55 471.77 0.000180 6.65 22899.95 1288.97 0.23 Susqueharma Middle Reach 149.469 25yr 228900.00 446.46 477.55 470.75 0.000208 7.33 32881.53 1270.05 0.25 Susqueharma Middle Reach 149.469 50yr 303400.00 446.46 478.83 446.90 479.72 0.000208 7.74 39200.02 1278.74 0.25 Susqueharma Middle Reach 149.469 50yr 303400.00 446.46 481.65 448.55 446.37 0.000226 7.74 39200.02 1278.24 0.25 Susqueharma Middle Reach 149.469 50yr 303400.00 446.86 448.55 446.37 477.70 0.000246 8.59 4594.90 1278.69 0.25 Susqueharma Middle Reach 149.403 2yr 117000.00 446.86 447.21 456.93 467.81 0.000245 8.59 4594.90 1108.91 0.27 Susqueharma Middle Reach 149.403 5yr 110000 446.86 447.31 456.93 467.81 0.000246 8.59 4594.90 1108.91 0.27 Susqueharma Middle Reach 149.403 5yr 120000 446.86 447.31 459.93 457.71 0.000248 7.38 26234.03 1108.91 0.27 Susqueharma Middle Reach 149.403 5yr 120000 446.86 477.31 459.93 457.71 0.000238 8.97 2256.47 1194.52 0.28 Susqueharma Middle Reach 149.403 5yr 239000.00 446.86 477.25 407.55 477.72 0.00028 8.07 2256.47 1194.52 0.28 Susqueharma Middle Reach 149.403 5yr 239000.00 446.86 478.75 477.57 0.00028 8.07 2256.47 1194.52 0.28 Susqueharma Middle Reach 149.403 5yr 239000.00 446.86 478.75 477.57 0.00028 8.07 2256.47 1194.52 0.28 Susqueharma Middle Reach 149.403 0.00rr 33900000 446.86 478.75 477.57 0.00028 8.07 2256.97 2256.97 2256.00 0.00028 477	Susquehanna	Middle Reach	149.546	100-yr	303400.00	446.97	481.74	462.09	482.67	0.000217	7.74	39215.20	1263.41	0.24
Sungusharman Middle Reach 149.489 Syr 16200.00 444.86 471.16 457.55 471.77 0.000176 6.25 22899.55 1288.97 0.24 0.25 0	Susquehanna	Middle Reach	149.546	500-уг	390900.00	446.97	486.65	464.45	487.80	0.000239	8.62	45449.68	1274.52	0.25
Sungusharman Middle Reach 149.489 Syr 16200.00 444.86 471.16 457.55 471.77 0.000176 6.25 22899.55 1288.97 0.24 0.25 0														
Stangasharana Middel Reach 189 469 10-yr 193500.00 444.64 473.65 458.62 474.34 0.00190 6.66 293085.05 1265.64 0.25 5 120.00 10.00 1446.64 476.85 460.00 147.73 32818.15 1270.05 0.25 5 1270.00 1446.64 476.85 460.00 147.73 1280.00 147.73 1280.00 1480.00 147.73 147.73 10.000208 7.55 35612.76 1273.74 0.25 5 1270.00 1446.64 478.83 460.00 472.00 0.00028 7.55 35612.76 1273.74 0.25 1270.00 1446.64 478.83 460.00 472.00 0.00028 7.74 35020.00 1278.00 0.25 5 1270.00 1446.64 478.83 460.00 472.00 0.00028 7.74 35020.00 1278.00 0.25 1279.00 1446.64 478.83 460.00 472.00 0.00028 7.74 35020.00 1278.00 0.25 1279.00 1446.64 486.55 464.39 487.70 0.000245 0.59 4594.00 1286.00 0.25 1280.00 1446.64 486.55 464.39 487.70 0.000245 0.59 4594.00 1286.00 0.25 1280.00 1446.64 486.55 464.39 487.70 0.000245 0.59 4594.00 1286.00 0.25 1280.00 1446.64 486.55 464.39 487.70 0.000245 0.59 4594.00 1286.00 0.25 1280.00 1446.84 473.00 1486.00 149.00 149.00 149.00 149.00 149.00 149.00 1446.84 470.00 149.0														
Sieguehanna Middel Reach 189.469 25 yr 239800.00 446.46 476.55 460.11 477.37 0.000208 7.33 32881.55 1277.05 0.25 8isquehanna Middel Reach 189.469 10.0 yr 28880.00 446.66 481.65 462.00 482.56 0.000222 7.74 38200.24 1278.24 0.25 8isquehanna Middel Reach 189.469 10.0 yr 30300.00 446.46 481.65 462.00 482.56 0.000222 7.74 38200.24 1278.24 0.25 8isquehanna Middel Reach 189.469 50.0 yr 30300.00 446.66 488.55 462.00 482.56 0.000222 7.74 38200.24 1278.24 0.25 8isquehanna Middel Reach 189.469 50.0 yr 1100.00 446.66 488.55 462.00 482.56 0.000222 7.74 38200.24 1278.24 0.25 8isquehanna Middel Reach 189.403 5.yr 1100.00 446.66 487.21 486.93 467.81 0.000245 6.24 18855.04 1108.91 0.27 8isquehanna Middel Reach 189.403 5.yr 1100.00 446.86 470.33 458.73 477.69 0.000238 6.97 32256.47 1114.52 0.22 8isquehanna Middel Reach 189.403 5.yr 128000.00 446.86 470.33 458.73 477.69 0.000238 6.97 32256.47 1114.52 0.22 8isquehanna Middel Reach 189.403 5.yr 22800.00 446.86 470.25 461.53 477.27 0.000286 8.07 29868.96 1219.44 0.22 8isquehanna Middel Reach 189.403 5.yr 22800.00 446.86 476.55 461.53 477.27 0.000286 8.07 29868.96 1219.44 0.22 8isquehanna Middel Reach 189.403 10.0 yr 28800.00 446.86 481.57 482.99 0.000238 1.20 27 32561.61 1222.22 0.28 8isquehanna Middel Reach 189.403 10.0 yr 28800.00 446.86 481.57 482.99 0.000281 8.83 33975.07 1237.74 0.22 8isquehanna Middel Reach 189.403 10.0 yr 30000.00 446.86 486.24 478.55 462.99 475.62 0.000281 8.83 33975.07 1237.74 0.22 8isquehanna Middel Reach 189.303 10.0 yr 1100.0 yr 1100.														
Sungaphannan Middle Reach 149.469 50-yr 28800.00 446.46 478.85 460.09 479.72 0.000196 7.55 35912.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25 35812.76 1273.74 0.25														
Susqueharinan Middle Reach 149.469 100-yr 303400.00 446.46 441.65 462.00 482.58 0.000222 7.74 30200.24 1278.24 0.25														
Sisaguehanna Middle Reach 149.489														
Sunguehama Middle Reach 149 403 2-yr 117600.00 446.86 467.21 456.93 467.81 0.000245 6.24 18865.04 1168.91 0.27														
Sissquehama Middle Reach 149.403 5-yr 162000.00 446.86 470.93 458.73 471.69 0.000248 6.97 23258.47 1194.52 0.28	Ousquerianna	Wilduic (Caci)	143.403	300-yi	330300.00	110.10	400.00	404.00	407.70	0.000243	0.00	40404.00	1200.03	0.20
Sissquehanna Middle Reach 149.403 10-yr 133300.00 446.86 473.41 459.91 472.25 0.000248 7.38 26234.03 1208.77 0.28	Susquehanna	Middle Reach	149.403	2-уг				456.93	467.81		6.24	18855.04	1168.91	0.27
Sissquehanna Middle Reach 149,403 25-yr 23960.00 446,86 476,25 461,53 477,27 0,000268 8,07 29685.96 1219,44 0,29	Susquehanna													0.28
Susquehanna Middle Reach 149.403 50-yr 28880.00 446.86 478.56 482.49 479.62 0.000253 8.27 32516.18 1229.28 0.28	Susquehanna													0.28
Susquehanna Middle Reach 149.403 100-yr 30340.0 446.86 481.37 483.80 482.47 0.000221 8.43 35976.07 1227.74 0.28	Susquehanna													0.29
Susquehanna Middle Reach 149.403 500-yr 390900.00 446.86 486.24 486.20 487.59 0.000303 9.30 42028.74 1246.31 0.28														
Susquehanna Middle Reach 149.382 2-yr 117600.00 445.38 467.22 456.04 467.78 0.000207 5-98 19664.23 1172.16 0.25														
Susquehanna Middle Reach 149.382 5-yr 162000.00 445.38 470.94 457.84 471.65 0.000212 6.75 23993.54 1498.90 0.26	Susquenaillid	MINUTE IVERCII	. 70.700	300-yi	00.000000	440.00	+00.24	400.20	407.09	0.000303	9.30	+2020.14	1240.37	U.28
Susquehanna Middle Reach 149.382 5-yr 162000.00 445.38 470.94 457.84 471.65 0.000212 6.75 23993.54 1498.90 0.26	Susquehanna	Middle Reach	149.382	2-уг	117600.00	445.38	467.22	456.04	467.78	0.000207	5.98	19664.23	1172.16	0.25
Susquehanna Middle Reach 149.382 10-yr 193500.00 445.38 473.41 459.01 474.22 0.000224 7.18 28933.55 1892.66 0.27	Susquehanna													0.26
Susquehanna Middle Reach 149.382 25-yr 239600.00 445.38 476.26 460.60 477.22 0.000245 7.90 30336.38 2166.33 0.28	Susquehanna													0.27
Susquehanna Middle Reach 149.382 50-yr 268800.00 445.38 478.56 461.56 479.59 0.000232 8.12 33117.50 2584.33 0.27	Susquehanna													0.28
Susquehanna Middle Reach 149.382 100-yr 30340.0 0	Susquehanna	Middle Reach	149.382		268800.00	445.38	478.56	461.56	479.59	0.000232	8.12	33117.50	2584.33	0.27
Susquehanna Middle Reach 149.382 500-yr 399900.00 445.38 486.42 465.24 487.47 0.000244 8.53 66143.31 3728.89 0.26	Susquehanna	Middle Reach	149.382	100-yr	303400.00	445.38	481.44	462.67	482.40	0.000242	8.02	48122.84	3440.25	0.26
Susquehanna Middle Reach 149.370 2-yr 117600.00 445.49 467.19 455.89 467.73 0.000201 5.93 19847.11 1145.94 0.25	Susquehanna	Middle Reach	149.382		390900.00	445.38	486.42	465.24	487.47	0.000244	8.53	66143.31	3728.89	0.26
Susquehanna Middle Reach 149.370 2-yr 117600.00 445.49 467.19 455.89 467.73 0.000201 5.93 19847.11 1145.94 0.25	Susquebanna	Middle Reach	149 376 PA Pouto 497		Bridge									
Susquehanna Middle Reach 149.370 5-yr 162000.00 445.49 470.90 457.68 471.60 0.000207 6.70 24176.80 1184.99 0.26 Susquehanna Middle Reach 149.370 10-yr 193500.00 445.49 473.37 458.84 474.16 0.000223 7.13 27142.09 1686.33 0.27 Susquehanna Middle Reach 149.370 25-yr 23960.00 445.49 478.56 461.41 479.52 0.000226 7.92 39006.63 2904.45 0.27 Susquehanna Middle Reach 149.370 50-yr 268800.00 445.49 478.56 461.41 479.52 0.000226 7.92 39006.63 2904.45 0.27 Susquehanna Middle Reach 149.370 50-yr 268800.00 445.49 481.39 465.06 482.36 0.000224 7.92 39006.63 2904.45 0.26 Susquehanna Middle Reach 149.370 500-yr 390900.00 445.49 486.37	Susquenaillid	MINIONE INCHUIT	. 70.070 FA NOULE 407		Bridge									
Susquehanna Middle Reach 149.370 5-yr 162000.00 445.49 470.90 457.68 471.60 0.000227 6.70 24176.80 1184.99 0.26 Susquehanna Middle Reach 149.370 10-yr 193500.00 445.49 473.37 458.84 474.16 0.000223 7.13 27142.09 1688.33 0.27 Susquehanna Middle Reach 149.370 50-yr 288800.00 445.49 478.56 461.41 479.52 0.000226 7.92 39006.63 2904.45 0.27 Susquehanna Middle Reach 149.370 50-yr 268800.00 445.49 478.56 461.41 479.52 0.000226 7.92 39006.63 2904.45 0.27 Susquehanna Middle Reach 149.370 50-yr 268800.00 445.49 481.39 462.50 482.36 0.000246 7.98 48056.44 3506.46 0.26 Susquehanna Middle Reach 149.370 50-yr 399900.00 445.49 486.37	Susquehanna	Middle Reach	149.370	2-уг	117600.00	445.49	467.19	455.89	467.73	0.000201	5.93	19847.11	1145.94	0.25
Susquehanna Middle Reach 149.370 10-yr 193500.00 445.49 473.37 458.84 474.16 0.000223 7.13 27142.09 1888.33 0.27 Susquehanna Middle Reach 149.370 25-yr 239600.00 445.49 476.21 460.44 477.16 0.000225 7.83 30608.27 2309.94 0.28 Susquehanna Middle Reach 149.370 50-yr 26800.00 445.49 476.21 460.44 477.16 0.000226 7.92 39006.63 2904.45 0.27 Susquehanna Middle Reach 149.370 100-yr 303400.00 445.49 481.39 462.50 482.36 0.000246 7.98 48056.44 3506.46 0.26 Susquehanna Middle Reach 149.370 500-yr 390900.00 445.49 486.37 465.08 487.42 0.000244 8.47 66270.86 3738.68 0.26 Susquehanna Middle Reach 149.327 2-yr 117600.00 446.38 467.10	Susquehanna	Middle Reach	149.370		162000.00	445.49	470.90	457.68	471.60	0.000207	6.70	24176.80	1184.99	0.26
Susquehanna Mddle Reach 149.370 25-yr 23960.00 445.49 476.21 460.44 477.16 0.000245 7.83 30608.27 2309.94 0.28 Susquehanna Middle Reach 149.370 50-yr 268800.00 445.49 478.56 461.41 479.52 0.000226 7.92 39090.63 2904.45 0.27 Susquehanna Middle Reach 149.370 100-yr 303400.00 445.49 486.37 465.08 487.42 0.000246 7.98 48056.44 3506.46 0.26 Susquehanna Middle Reach 149.370 500-yr 399900.00 445.49 486.37 465.08 487.42 0.000244 8.47 66270.86 3738.68 0.26 Susquehanna Middle Reach 149.327 2-yr 11760.00 446.38 467.10 456.43 467.68 0.000220 6.12 19217.98 1378.91 0.26 Susquehanna Middle Reach 149.327 5-yr 162000.00 446.38 470.82	Susquehanna													0.27
Susquehanna Middle Reach 149.370 50-yr 268800.00 445.49 478.56 461.41 479.52 0.000226 7.92 39006.63 2904.45 0.27 Susquehanna Middle Reach 149.370 100-yr 303400.00 445.49 481.39 462.50 482.36 0.000246 7.98 48056.44 3506.46 0.26 Susquehanna Middle Reach 149.370 500-yr 399900.00 445.49 486.74 0.00244 8.47 66270.86 8.77 0.00244 8.47 627 1.0000 446.38 467.10 456.43 467.68 0.000220 6.12 19217.98 1378.91 0.26 Susquehanna Middle Reach 149.327 5-yr 162000.00 446.38 470.82 459.31 471.51 0.000223 6.87 23588.10 1751.04 0.27 Susquehanna Middle Reach 149.327 10-yr 193500.00 446.38 473.29 459.31 471.11 0.000244 7.27 26626.48 186	Susquehanna			25-уг										0.28
Susquehanna Middle Reach 149.370 100-yr 303400.00 445.49 481.39 482.50 482.38 0.000246 7.88 48056.44 3506.46 0.26 Susquehanna Middle Reach 149.370 500-yr 390900.00 445.49 486.37 465.08 487.42 0.000244 8.47 66270.86 3738.68 0.26 Susquehanna Middle Reach 149.327 2-yr 117600.00 446.38 467.10 456.43 467.88 0.000220 6.12 19217.98 1378.91 0.26 Susquehanna Middle Reach 149.327 5-yr 16200.00 446.38 470.82 458.18 471.55 0.000233 6.87 23588.10 1751.04 0.27 Susquehanna Middle Reach 149.327 10-yr 193500.00 446.38 470.29 459.31 477.11 0.000244 7.27 26626.48 1865.33 0.28 Susquehanna Middle Reach 149.327 25-yr 239600.00 446.38 476.18	Susquehanna	Middle Reach	149.370		268800.00	445.49	478.56	461.41	479.52	0.000226	7.92	39006.63	2904.45	0.27
Susquehanna Middle Reach 149.327 2-yr 117600.00 446.38 467.10 456.43 467.68 0.000220 6.12 19217.98 1378.91 0.26 Susquehanna Middle Reach 149.327 5-yr 16200.00 446.38 470.82 458.18 471.55 0.000233 6.87 23588.10 1751.04 0.27 Susquehanna Middle Reach 149.327 10-yr 193500.00 446.38 473.29 459.31 474.11 0.000244 7.27 26626.48 1865.33 0.28 Susquehanna Middle Reach 149.327 25-yr 239600.00 446.38 476.18 460.88 477.09 0.000246 7.74 35480.69 2282.09 0.28 Susquehanna Middle Reach 149.327 50-yr 28800.00 446.38 476.13 461.80 479.46 0.000226 7.86 41400.75 2732.69 0.27 Susquehanna Middle Reach 149.327 100-yr 303400.00 446.38 481.37 462.67 482.29 0.000241 7.89 50002.89 3468.20 0.26	Susquehanna	Middle Reach		100-уг								48056.44		0.26
Susquehanna Middle Reach 149.327 5-yr 162000.00 446.38 470.82 458.18 471.55 0.000233 6.87 23588.10 1751.04 0.27 Susquehanna Middle Reach 149.327 10-yr 193500.00 446.38 473.29 459.31 474.11 0.000244 7.27 26626.48 1865.33 0.28 Susquehanna Middle Reach 149.327 25-yr 239600.00 446.38 476.18 460.88 477.09 0.000246 7.74 35480.69 2282.09 0.28 Susquehanna Middle Reach 149.327 50-yr 26880.00 446.38 476.18 461.80 479.46 0.000226 7.86 41400.75 2732.69 0.27 Susquehanna Middle Reach 149.327 100-yr 303400.00 446.38 481.37 462.87 482.29 0.000241 7.89 50002.89 3468.20 0.26	Susquehanna	Middle Reach	149.370	500-yr	390900.00	445.49	486.37	465.08	487.42	0.000244	8.47	66270.86	3738.68	0.26
Susquehanna Middle Reach 149.327 5-yr 162000.00 446.38 470.82 458.18 471.55 0.000233 6.87 23588.10 1751.04 0.27 Susquehanna Middle Reach 149.327 10-yr 193500.00 446.38 473.29 459.31 474.11 0.000244 7.27 26626.48 1865.33 0.28 Susquehanna Middle Reach 149.327 25-yr 239600.00 446.38 476.18 460.88 477.09 0.000246 7.74 35480.69 2282.09 0.28 Susquehanna Middle Reach 149.327 50-yr 26880.00 446.38 476.18 461.80 479.46 0.000226 7.86 41400.75 2732.69 0.27 Susquehanna Middle Reach 149.327 100-yr 303400.00 446.38 481.37 462.87 482.29 0.000241 7.89 50002.89 3468.20 0.26	Suggishanna	Middle Passh	140 327	2-vr	117600.00	446 20	467.10	4EC 42	467.60	0.000330	6 10	10217.00	1270 04	0.00
Susquehanna Middle Reach 149.327 10-yr 193500.00 446.38 473.29 459.31 474.11 0.000244 7.27 26626.48 1865.33 0.28 Susquehanna Middle Reach 149.327 25-yr 239600.00 446.38 476.18 460.88 477.09 0.000246 7.74 35480.69 2282.09 0.28 Susquehanna Middle Reach 149.327 50-yr 228600.00 446.38 476.18 461.80 479.46 0.000226 7.86 41400.75 2732.69 0.27 Susquehanna Middle Reach 149.327 100-yr 303400.00 446.38 481.37 462.67 482.29 0.000241 7.89 50002.89 3468.20 0.26														
Susquehanna Middle Reach 149.327 25-yr 23960.00 446.38 476.18 460.88 477.09 0.000246 7.74 35480.69 2282.09 0.28 Susquehanna Middle Reach 149.327 50-yr 268800.00 446.38 478.53 461.80 479.46 0.000226 7.86 4140.075 2732.69 0.27 Susquehanna Middle Reach 149.327 100-yr 303400.00 446.38 478.53 462.87 482.29 0.000241 7.89 50002.89 3468.20 0.26														
Susquehanna Middle Reach 149.327 50-yr 268800.00 446.38 478.53 461.80 479.46 0.000226 7.86 41400.75 2732.69 0.27 Susquehanna Middle Reach 149.327 100-yr 303400.00 446.38 481.37 462.87 482.29 0.000241 7.89 50002.89 3468.20 0.26														
Susquehanna Middle Reach 149.327 100-yr 303400.00 446.38 481.37 462.87 482.29 0.000241 7.89 50002.89 3468.20 0.26														0.27
	Susquehanna													0.26
	Susquehanna													0.25

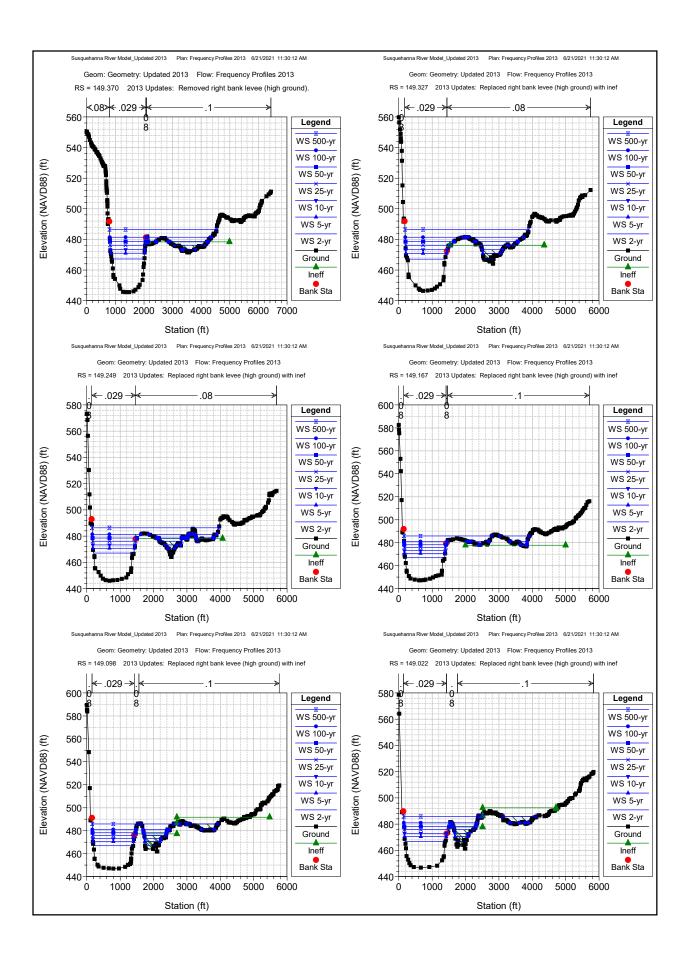
HEC-RAS Plan: F River	requency 2013 Lo Reach	cations: User Defined (Continu	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
				(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
0	MELLIN BOOK	440.040	-	447000.00	445.04	407.07	455.07	107.50	0.000400	5.70	00500.00	1070.00	201
Susquehanna Susquehanna	Middle Reach Middle Reach	149.249 149.249	2-yr 5-yr	117600.00 162000.00	445.94 445.94	467.07 470.79	455.67 457.37	467.58 471.43	0.000192 0.000197	5.73 6.45	20526.36 25102.71	1276.39 1456.48	0.24
Susquehanna	Middle Reach	149.249	10-уг	193500.00	445.94	473.26	458.49	473.99	0.000208	6.86	28211.63	1636.40	0.26
Susquehanna	Middle Reach	149.249	25-уг	239600.00	445.94	476.11	460.00	476.99	0.000227	7.52	31849.70	1940.15	0.27
Susquehanna	Middle Reach	149.249	50-yr	268800.00	445.94	478.48	460.95	479.35	0.000206	7.56	40017.76	2615.23	0.26
Susquehanna Susquehanna	Middle Reach Middle Reach	149.249 149.249	100-yr 500-yr	303400.00 390900.00	445.94 445.94	481.30 486.28	461.99 464.46	482.18 487.24	0.000223 0.000221	7.64 8.11	48425.35 66751.58	3320.09 3799.42	0.25
Ousquerianna	Wildule (Celeti)	140.240	300-yi	030300.00	440.04	400.20	404.40	407.24	0.000221	0.11	00731.00	3733.42	0.24
Susquehanna	Middle Reach	149.167	2-уг	117600.00	447.27	466.90	456.51	467.48	0.000233	6.11	19242.32	1183.54	0.27
Susquehanna	Middle Reach	149.167	5-уг	162000.00	447.27	470.61	458.26	471.34	0.000230	6.83	23705.05	1217.45	0.27
Susquehanna	Middle Reach	149.167	10-yr	193500.00	447.27	473.07	459.41	473.88	0.000239	7.24	26710.56	1228.73	0.27
Susquehanna Susquehanna	Middle Reach Middle Reach	149.167 149.167	25-yr 50-yr	239600.00 268800.00	447.27 447.27	475.89 478.22	460.96 461.87	476.87 479.24	0.000259 0.000244	7.93 8.12	30202.63 33262.41	1241.47 1444.46	0.28
Susquehanna	Middle Reach	149.167	100-уг	303400.00	447.27	481.00	462.93	482.06	0.000269	8.27	38563.93	2449.49	0.27
Susquehanna	Middle Reach	149.167	500-уг	390900.00	447.27	485.88	465.59	487.11	0.000278	8.97	53467.63	3539.34	0.27
			-										
Susquehanna Susquehanna	Middle Reach Middle Reach	149.098 149.098	2-yr 5-yr	117600.00 162000.00	446.96 446.96	466.87 470.58	455.54 457.24	467.38 471.24	0.000190 0.000194	5.74 6.49	20494.65 24962.76	1521.96 1680.05	0.24 0.25
Susquehanna	Middle Reach	149.098	10-yr	193500.00	446.96	473.04	458.38	473.78	0.000206	6.92	27972.50	1746.60	0.26
Susquehanna	Middle Reach	149.098	25-уг	239600.00	446.96	475.86	459.91	476.76	0.000227	7.61	31474.50	1905.54	0.27
Susquehanna	Middle Reach	149.098	50-уг	268800.00	446.96	478.25	460.82	479.11	0.000201	7.57	41414.48	1981.96	0.25
Susquehanna	Middle Reach	149.098	100-yr	303400.00	446.96	481.03	461.86	481.92	0.000222	7.71	47037.44	2504.23	0.25
Susquehanna	Middle Reach	149.098	500-yr	390900.00	446.96	485.90	464.35	486.96	0.000237	8.47	57777.21	3294.18	0.25
Susquehanna	Middle Reach	149.022	2-уг	117600.00	446.89	466.80	455.61	467.30	0.000187	5.68	20702.58	1485.92	0.24
Susquehanna	Middle Reach	149.022	5-yr	162000.00	446.89	470.52	457.31	471.15	0.000191	6.41	25283.60	1629.36	0.25
Susquehanna	Middle Reach	149.022	10-yr	193500.00	446.89	472.97	458.41	473.69	0.000203	6.82	28358.69	1704.27	0.25
Susquehanna	Middle Reach	149.022 149.022	25-yr	239600.00 268800.00	446.89 446.89	475.79 478.18	459.91 460.81	476.66 479.03	0.000221	7.50	32058.67 41149.89	1921.43 2023.19	0.26
Susquehanna Susquehanna	Middle Reach Middle Reach	149.022	50-yr 100-yr	268800.00 303400.00	446.89	478.18 480.94	460.81 461.85	479.03 481.83	0.000197	7.51 7.64	41149.89 46891.29	2023.19	0.25 0.25
Susquehanna	Middle Reach	149.022	500-yr	390900.00	446.89	485.83	464.28	486.86	0.000218	8.34	57736.74	3334.75	0.25
Susquehanna	Middle Reach	148.947	2-уг	117600.00	446.62	466.78	455.05	467.21	0.000156	5.27	22299.75	1261.53	0.22
Susquehanna Susquehanna	Middle Reach Middle Reach	148.947 148.947	5-yr 10-yr	162000.00 193500.00	446.62 446.62	470.50 472.96	456.66 457.71	471.06 473.59	0.000161 0.000171	5.99 6.40	27053.47 30286.12	1373.91 1680.67	0.23
Susquehanna	Middle Reach	148.947	25-yr	239600.00	446.62	472.96	457.71	476.55	0.000171	7.02	36089.05	1885.29	0.23
Susquehanna	Middle Reach	148.947	50-уг	268800.00	446.62	478.15	460.01	478.94	0.000174	7.18	40831.55	2276.35	0.24
Susquehanna	Middle Reach	148.947	100-уг	303400.00	446.62	480.91	460.97	481.72	0.000194	7.32	46684.89	2732.65	0.23
Susquehanna	Middle Reach	148.947	500-уг	390900.00	446.62	485.79	463.30	486.75	0.000208	8.01	57774.51	3326.12	0.24
Susquehanna	Middle Reach	148.863	2 15	117600.00	447.12	466.66	456.00	467.13	0.000186	5.52	21316.58	1288.24	0.24
Susquehanna	Middle Reach	148.863	2-yr 5-yr	162000.00	447.12	470.39	457.59	470.98	0.000183	6.19	26155.35	1520.30	0.24
Susquehanna	Middle Reach	148.863	10-yr	193500.00	447.12	472.84	458.63	473.51	0.000191	6.57	30520.21	1849.23	0.25
Susquehanna	Middle Reach	148.863	25-уг	239600.00	447.12	475.67	460.07	476.46	0.000204	7.16	35851.86	1953.47	0.25
Susquehanna	Middle Reach	148.863	50-yr	268800.00	447.12	478.04	460.93	478.86	0.000188	7.29	40748.94	2090.92	0.25
Susquehanna Susquehanna	Middle Reach Middle Reach	148.863 148.863	100-yr 500-yr	303400.00 390900.00	447.12 447.12	480.80 485.68	461.92 464.23	481.63 486.66	0.000208 0.000218	7.41 8.07	46667.40 58701.57	2209.59 3735.74	0.24
Ousquerianna	Wilduic (Caci)	140.000	300-yi	330300.00	447.12	403.00	404.20	400.00	0.000210	0.07	30701.37	3733.74	0.24
Susquehanna	Middle Reach	148.795	2-уг	117600.00	446.36	466.61	455.60	467.06	0.000179	5.38	21844.02	1333.29	0.23
Susquehanna	Middle Reach	148.795	5-уг	162000.00	446.36	470.34	457.29	470.91	0.000176	6.03	26872.55	1363.05	0.24
Susquehanna	Middle Reach	148.795	10-yr	193500.00	446.36	472.80	458.41	473.43	0.000185	6.39	30594.79	1891.39	0.24 0.25
Susquehanna Susquehanna	Middle Reach Middle Reach	148.795 148.795	25-yr 50-yr	239600.00 268800.00	446.36 446.36	475.63 478.02	459.84 460.69	476.37 478.77	0.000195 0.000177	6.95 7.02	36827.47 42351.32	2300.76 2399.01	0.25
Susquehanna	Middle Reach	148.795	100-уг	303400.00	446.36	480.79	461.68	481.54	0.000192	7.09	48793.39	2658.82	0.23
Susquehanna	Middle Reach	148.795	500-уг	390900.00	446.36	485.69	463.99	486.55	0.000197	7.65	60381.77	3378.06	0.23
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Susquehanna Susquehanna	Middle Reach Middle Reach	148.718 148.718	2-уг 5-уг	117600.00 162000.00	446.43 446.43	466.57 470.30	454.62 456.26	466.98 470.83	0.000154 0.000159	5.18 5.85	22691.39 27673.33	1308.73 1363.17	0.22
Susquehanna	Middle Reach	148.718	10-yr	193500.00	446.43	472.75	457.32	473.35	0.000168	6.23	31222.67	2303.24	0.23
Susquehanna	Middle Reach	148.718	25-уг	239600.00	446.43	475.59	458.76	476.28	0.000177	6.74	38712.57	2425.55	0.24
Susquehanna	Middle Reach	148.718	50-уг	268800.00	446.43	477.99	459.64	478.69	0.000161	6.81	44384.89	2663.93	0.23
Susquehanna Susquehanna	Middle Reach Middle Reach	148.718 148.718	100-yr	303400.00 390900.00	446.43 446.43	480.75 485.67	460.65 463.03	481.45 486.45	0.000174 0.000176	6.87 7.34	50952.57 69070.72	2936.51 3741.20	0.22
Susquenanna	Wildule Reacti	140.710	500-уг	390900.00	440.43	403.07	403.03	400.43	0.000170	7.54	09070.72	3741.20	0.22
Susquehanna	Middle Reach	148.639	2-уг	117600.00	446.64	466.49	454.67	466.92	0.000154	5.24	22426.79	1270.53	0.22
Susquehanna	Middle Reach	148.639	5-уг	162000.00	446.64	470.21	456.32	470.76	0.000157	5.96	27186.01	1295.99	0.23
Susquehanna	Middle Reach	148.639	10-yr	193500.00 239600.00	446.64 446.64	472.65 475.47	457.37	473.28	0.000167 0.000180	6.36	31484.54	2136.71 2430.14	0.23
Susquehanna Susquehanna	Middle Reach Middle Reach	148.639 148.639	25-yr 50-yr	239600.00	446.64	4/5.4/ 477.87	458.77 459.67	476.21 478.62	0.000180	6.94 7.02	37945.15 43576.18	2430.14 2885.34	0.24
Susquehanna	Middle Reach	148.639	100-yr	303400.00	446.64	480.62	460.64	481.37	0.000181	7.11	50089.52	3059.57	0.23
Susquehanna	Middle Reach	148.639	500-yr	390900.00	446.64	485.55	463.03	486.37	0.000183	7.58	69428.42	3743.85	0.22
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Susquehanna Susquehanna	Middle Reach Middle Reach	148.561 148.561	2-уг	117600.00 162000.00	446.44 446.44	466.41 470.12	454.44 456.09	466.85 470.69	0.000155 0.000162	5.32 6.07	22085.66 26819.10	1223.77 1530.79	0.22
Susquenanna Susquehanna	Middle Reach	148.561	5-yr 10-yr	193500.00	446.44	470.12	456.09	470.69	0.000162	6.48	30806.19	1708.57	0.23
Susquehanna	Middle Reach	148.561	25-yr	239600.00	446.44	475.35	458.64	476.13	0.000188	7.10	35792.30	1927.25	0.24
Susquehanna	Middle Reach	148.561	50-yr	268800.00	446.44	477.75	459.51	478.54	0.000174	7.22	40521.33	2008.42	0.24
Susquehanna	Middle Reach	148.561	100-yr	303400.00	446.44	480.48	460.51	481.29	0.000194	7.35	46256.35	2188.92	0.23
Susquehanna	Middle Reach	148.561	500-yr	390900.00	446.44	485.33	462.90	486.28	0.000205	8.01	58847.77	4679.01	0.24
Susquehanna	Middle Reach	148.486	2-уг	117600.00	446.44	466.31	454.69	466.79	0.000171	5.57	21119.16	1947.19	0.23
Susquehanna	Middle Reach	148.486	5-yr	162000.00	446.44	470.00	456.41	470.62	0.000178	6.35	25523.39	2351.27	0.24
Susquehanna	Middle Reach	148.486	10-yr	193500.00	446.44	472.42	457.51	473.13	0.000188	6.76	30489.93	3875.74	0.25
Susquehanna	Middle Reach Middle Reach	148.486 148.486	25-yr	239600.00 268800.00	446.44 446.44	475.24 477.68	459.02 459.92	476.05 478.47	0.000200 0.000179	7.30 7.33	37649.77 44072.35	4041.82 4670.67	0.25 0.24
Susquehanna Susquehanna	Middle Reach Middle Reach	148.486	50-yr 100-yr	268800.00 303400.00	446.44	477.68	459.92 460.93	4/8.4/	0.000179	7.33	51638.53	4670.67 6541.69	0.24
Susquehanna	Middle Reach	148.486	500-yr	390900.00	446.44	485.32	463.37	486.17	0.000196	7.84	66291.58	7970.82	0.23
Susquehanna	Middle Reach	148.413	2-уг	117600.00	446.24	466.24	454.53	466.72	0.000175	5.57	21103.54	1421.39	0.23
Susquehanna Susquehanna	Middle Reach Middle Reach	148.413 148.413	5-yr	162000.00 193500.00	446.24 446.24	469.93 472.36	456.23 457.35	470.55 473.05	0.000181	6.33	25573.73 31453.10	2298.54 3466.70	0.24
Susquenanna	Middle Reach	148.413	10-yr 25-yr	239600.00	446.24	472.36	457.35 458.86	473.05 475.96	0.000190	7.17	40057.91	4872.50	0.25
Susquehanna	Middle Reach	148.413	50-yr	268800.00	446.24	477.65	459.72	478.39	0.000172	7.11	47984.29	6223.76	0.24
Susquehanna	Middle Reach	148.413	100-yr	303400.00	446.24	480.41	460.79	481.10	0.000181	7.05	56855.33	7072.77	0.22
Susquehanna	Middle Reach	148.413	500-yr	390900.00	446.24	485.33	463.24	486.06	0.000177	7.38	72766.41	8191.24	0.22
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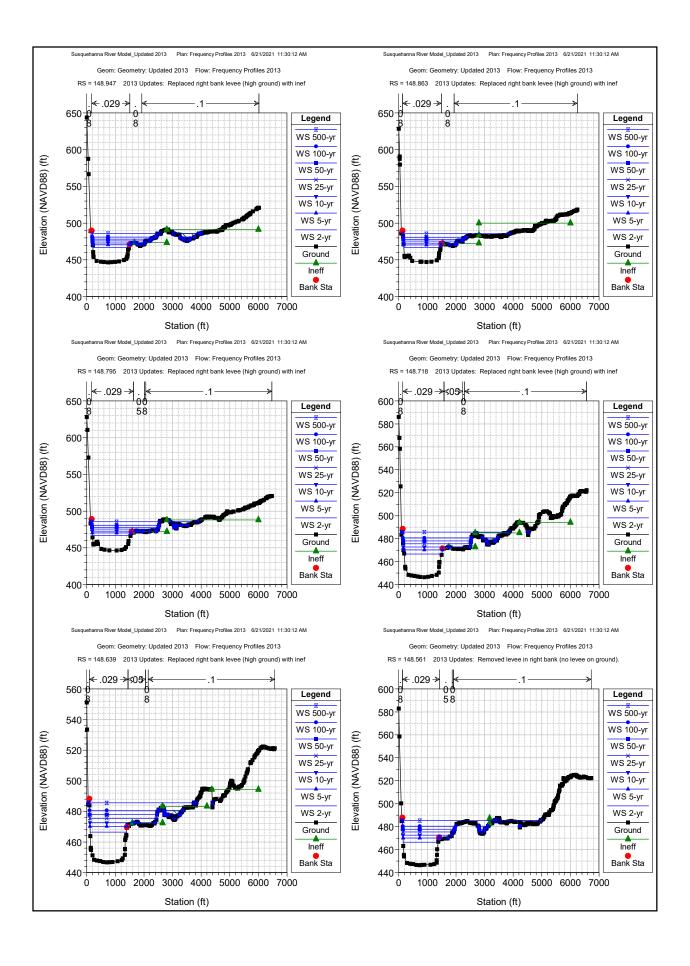
HEC-RAS Plan: Frequency 2013 Locations: User Defined (Continued)

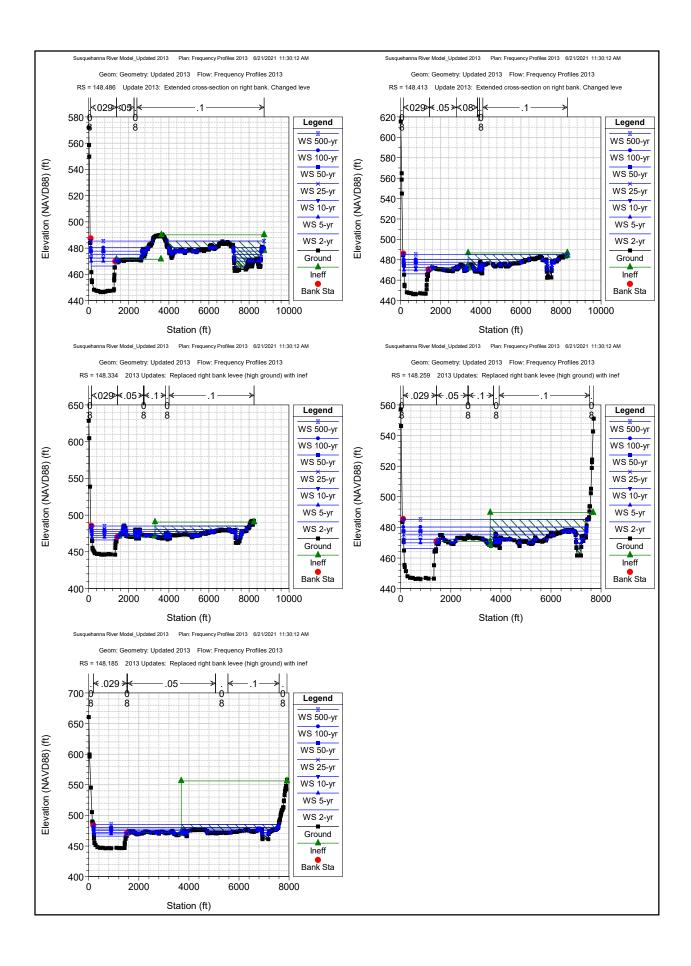
River	Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
				(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Susquehanna	Middle Reach	148.334	2-уг	117600.00	446.14	466.19	454.12	466.64	0.000159	5.35	21964.93	1436.99	0.22
Susquehanna	Middle Reach	148.334	5-уг	162000.00	446.14	469.89	455.79	470.47	0.000166	6.10	26555.00	2087.89	0.23
Susquehanna	Middle Reach	148.334	10-уг	193500.00	446.14	472.31	456.88	472.96	0.000177	6.48	31237.13	3413.69	0.24
Susquehanna	Middle Reach	148.334	25-уг	239600.00	446.14	475.12	458.36	475.87	0.000188	7.04	38828.77	5591.51	0.24
Susquehanna	Middle Reach	148.334	50-уг	268800.00	446.14	477.57	459.24	478.31	0.000169	7.06	45996.72	6275.68	0.23
Susquehanna	Middle Reach	148.334	100-уг	303400.00	446.14	480.29	460.25	481.02	0.000183	7.10	54104.03	7588.98	0.22
Susquehanna	Middle Reach	148.334	500-уг	390900.00	446.14	485.18	462.68	485.98	0.000184	7.55	69130.52	7876.50	0.22
Susquehanna	Middle Reach	148.259	2-уг	117600.00	446.15	466.15	453.89	466.57	0.000150	5.16	22774.39	1474.32	0.22
Susquehanna	Middle Reach	148.259	5-уг	162000.00	446.15	469.85	455.54	470.39	0.000153	5.87	27575.92	2341.10	0.23
Susquehanna	Middle Reach	148.259	10-уг	193500.00	446.15	472.28	456.60	472.88	0.000163	6.26	32453.59	4354.76	0.23
Susquehanna	Middle Reach	148.259	25-уг	239600.00	446.15	475.08	458.06	475.79	0.000175	6.80	41022.80	6339.75	0.23
Susquehanna	Middle Reach	148.259	50-уг	268800.00	446.15	477.55	458.93	478.23	0.000155	6.79	49571.74	6994.65	0.22
Susquehanna	Middle Reach	148.259	100-уг	303400.00	446.15	480.27	459.92	480.93	0.000165	6.78	59022.78	7317.40	0.21
Susquehanna	Middle Reach	148.259	500-уг	390900.00	446.15	485.18	462.25	485.88	0.000164	7.16	76087.17	7401.43	0.21
Susquehanna	Middle Reach	148.185	2-уг	117600.00	446.16	466.11	453.70	466.51	0.000138	5.02	23428.94	1558.07	0.21
Susquehanna	Middle Reach	148.185	5-уг	162000.00	446.16	469.81	455.33	470.32	0.000143	5.73	28285.25	1922.10	0.22
Susquehanna	Middle Reach	148.185	10-уг	193500.00	446.16	472.24	456.39	472.81	0.000152	6.09	33680.32	4032.35	0.22
Susquehanna	Middle Reach	148.185	25-уг	239600.00	446.16	475.05	457.82	475.70	0.000160	6.58	42920.78	6001.03	0.23
Susquehanna	Middle Reach	148.185	50-уг	268800.00	446.16	477.53	458.66	478.15	0.000140	6.52	51613.42	7208.79	0.21
Susquehanna	Middle Reach	148.185	100-уг	303400.00	446.16	480.26	459.65	480.85	0.000148	6.47	61167.34	7381.12	0.20
Susquehanna	Middle Reach	148.185	500-vr	390900.00	446.16	485.18	461.95	485.79	0.000144	6.76	78435.28	7408.89	0.20











WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY, PENNSYLVANIA

Appendix B - Geotechnical Engineering

WEST END FLOOD MITIGATION STUDY ,COLUMBIA COUNTY, PENNSYLVANIA

Appendix B - Geotechnical Engineering

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WEST END FLOOD MITIGATION STUDY

COLUMBIA COUNTY, PENNSYLVANIA

Appendix B - Geotechnical Engineering

1. Proposed Levee/Floodwall System: The project area is located in the Town of Bloomsburg in Columbia County, Pennsylvania, at the confluence of Fishing Creek with the Susquehanna River.

The recommended project will consist of a system of earthen levees, mechanically stabilized earth (MSE) levee, concrete floodwalls, sheet pile floodwalls, road closure structures, and a storm water pumping station. Earthen and MSE levees are proposed for the majority of the flood protection alignment. Riprap will be utilized to protect the waterside slopes of the system along Fishing Creek.

The system begins immediately to the East of Railroad Street where the earthen levee ties into high ground. Elevation 491.00 is the top of the system. The alignment proceeds westward across Railroad Street which is at Elev. 490.0 +/- where the roadway would be raised approximately one foot.

On the west side of Railroad Street, an earthen levee with a landside toe drain extends downstream to Station 11+50. Through this reach, the levee crest is 10' wide with a land side slope of 2.5 Horizontal to 1 Vertical (2.5H:1V) and a riverside side slope of 2H:1V. This reach of the system is through a residential area. The riverside toe will extend into the bed of the creek due to severe erosion since the 2011 Lee Flood has caused loss of the bank along this reach of the creek. The riverside levee slope will be protected by 18 to 24" riprap.

An MSE levee then extends westward adjacent to Fishing Creek from Sta. 11+50 to 14+50. The MSE levee has a 12' wide crest with vertical wall faces, fall protection railings and a landside toe drain. The MSE levee will have a riverside slope of 2H:1V. This reach of the system is also through a residential area. The riverside toe will extend into the bed of the creek

The top of protection descends from Elev. 491.00 at the high ground tie-out at Railroad Street Elev. 490.94 at Sta. 20+00.

A sheet pile wall is proposed 4 feet from the top of bank from Sta. 14+50 to Sta. 22+50. If required, a concrete cap will be added to the sheet piling for additional strength and aesthetics.

This reach of the line of protection is on an alignment with minimal lateral clearance through the residential area. The riverside levee slope will be protected by 18 to 24" riprap.

Beginning at Sta. 22+50, (TOS=Elev.485.00±), an earth levee will extend to the Route 11 road closure structure abutment at Sta. 25+70+. The stop log closure across route 11 is

approximately 6 feet in height if the roadway is pot raised. Being a state highway and also being in the floodplain, it was determined that the road elvation should remain at its' present elevation. On the south side of the closure, an earth levee extends from Sta. 26+50 to the Fairgrounds access road closure structures 2 and 2A. The top of levee is at Elevatioon 485.00, about 6 to 7 feet in height. Riprap is required on the creek side of the levee. Flow velocities from the creek out of bank flows during higher level flood events requires 24" riprap on the levee slope.

Closures 2 and 2A are proposed to be automatic Floodbreak type of closures since the creek flows in this area are fast rising compared to the river backwater which is also a source of flooding in the west end of Bloomsburg. To minimize the activation frequency, the ground level would be raised to elevation 478.00 as indicated on the concept plans.

An MSE levee of varying heights is proposed from the abutment of closure 2A at Sta. 31+30 to the tie-in to a concrete floodwall at Sta. 59+95. The tie-in location is near Closure 5 of the Columbia County levee System #1. This location is also the lowest existing ground elevation, approximately Elev. 470.5. With a top of system elevation of 485.00, the MSE levee would be about 14 feet in height. Extensive investigation of the embankment stability and underseepage potential will be required to determine the final width of the crest of the levee and the riverside earth slope which is assumed to be 3:1. Underseepage may require a deeper base trench (See MSE levee cross section in concept plans). Other options would be a slurry cutoff trench or sheeting.

The above stretch of MSE levee has three access road closure structures located at Sta, 40+35, Sta. 46+10, and sta. 47+25. The closures are proposed stop log systems 10 feet in height.

To minimize the erection time for each flood event, it is assumed most of the approximately 10 foot segments of stop logs between the steel column supports can remain in place until a major Fairgrounds event which would require removal to fully open the access points.

A stormwater pumping station is proposed at approximately Sta. 51+25 to collect and discharge interior stormwater draining towards the levee from the Fairgrounds and the residential and commercial areas of the west end behind the levee system. Detailed drainage calculations will be required to develop a conveyance system which will collect the drainage which now exits to Fishing Creek via several storm sewers along the creek. These sewers extend along town streets from the edge of the fairgrounds to Fishing Creek. Connections to the beginning of the systems would convey the excess flows during high rainfall periods to the combined overland and subsurface system directing the flows to the pumping station at Sta. 51=25. The pumping station is estimated to be a 20,000 gallons per minute (GPM) capacity assuming the very low area of the main promenade of the fairgrounds is utilized for storage to a 2 foot depth.

Other features of the levee system consist of stormwater control structures at each storm sewer penetration of the system along Fishing Creek and at the Route 11 closure structure. The fairgrounds

2. Regional Geology. The study area is in the Appalachian Mountain Section of the Ridge and Valley physiographic province. The long, parallel ridges and valleys in this physiographic region were produced by differential erosion of folded strata. Bloomsburg is located beyond the southern terminus of the late Wisconsinan glacier. That glacial episode produced most of the prominent glacial landforms found in northeast Pennsylvania. Meltwater from the Wisconsinan glacier carried significant quantities of materials through the Fishing Creek and Susquehanna River valleys.

Much of Bloomsburg consists .of a low terrace, where glacial meltwaters and more recent floodwaters deposited material up to boulder-size. Published geologic reports indicate that this material is stratified and moderately to poorly graded. The thickness of these deposits is 3 to 50 feet near Bloomsburg.

The soil unit mapped by the U.S. Department of Agriculture in the study area is the Chenango silt loam. It formed in sand & gravel outwash and is well-drained. The surface layer of this soil consists of silt loam and gravelly sand loam. Below that is gravelly sandy loam to a depth of 20 to 50 inches, followed by stratified gravel and sand. Bedrock is reportedly at a depth greater than 30 feet; however, borings drilled for this project encountered bedrock at shallower depths.

Bedrock underlying most of the study area is part of the Wills Creek Formation. Part of the study area, near the northeast end, is underlain by Bloomsburg Formation rocks. The strike of bedrock bedding at the Railroad Street Bridge is north 65° east; dip is 28° to the south. That bedding dip is within the range measured in test boring cores. Bedrock strike at the test boring locations should be similar to that measured at the outcrop. A bedrock geologic map of the area is included as Figure 1.

The Wills Creek Formation is mostly calcareous claystone or shale, but also consists of calcareous limestone and dolostone. Laminated to thin bedding predominates in Wills Creek rocks. Wills Creek rocks are usually highly weathered to a moderate depth, due to lithology, bedding characteristics, joints, and calcareous content.

The Bloomsburg Formation is mostly claystone and shale, with abundant siltstone and sandstone interbeds. The claystones and shales are medium to thick-bedded. Sandstones and siltstones are thin to medium-bedded. Bloomsburg Formation rocks are also highly susceptible to weathering, but not to the extent that Wills Creek rocks are.

3. Exploration Program - The subsurface conditions were investigated by the Corps of Engineers in November of 2000 along the alignment. Drilling was performed by contractors to Pennsylvania Department of Environmental Protection (DEP). DEP provided the drilling services as in-kind services to the study at that time. No investigations were performed in Fernville. A total of 9 borings were performed to investigate the foundation conditions in the area of the flood protection alignment along Fishing Creek. An overall boring location plan is attached as Figure 2. See the study concept drawings in Appendix C for more detailed boring location information. Field boring logs are included as Attachment 1 to this Appendix. Additional borings should be drilled in the preliminary design phase, which will include additional testing.

The borings were advanced by means of the Standard Penetration Test (SPT) method with continuous sampling. The SPT consists of driving a 1 3/8-inch ID by 2-ft 8-inch long split spoon sampler a total of 18 inches with a 140-pound hammer falling 30 inches. The SPT provides a disturbed sample for defining soil consistency and relative density. Rock coring was performed with NWD4 (2 1/8 inch diameter) bit and double tube barrel.

- a. **Laboratory Testing.** All jar samples were visually inspected and assigned a Unified Soil Classification System (USCS) classification by an experienced laboratory technician. Additionally grain size distributions and Atterberg Limits tests were performed on selected samples. Results of all laboratory tests are included as Attachment 2 to this Appendix.
- b. **Description of Subsurface Conditions** The average soil thickness for the area is approximately 20 feet. Bedrock depths are highly variable over the entire project area. Bedrock was encountered between 12-25 feet in several borings, while it was not encountered at depths greater than 30 feet in several borings towards 6th Street.

Along Fishing Creek from approximately Station 1+00 to 25+80, foundation soils are moderately pervious to very pervious with little to no impervious blanket above. A layer of dense gravel was encountered in most borings at a depth of approximately 10 feet. The soils had varying amounts of fines (material passing No. 200 sieve), but most of the soils were classified as sands and gravels. Also along Fishing Creek, bedrock was encountered between depths of 12 feet to 25 feet along the project alignment.

Borings along the Bloomsburg Fairgrounds portion of the alignment (approximately Station 31+00 to Station 60+00) show a silt/clay blanket (average thickness of 4 feet) overlying a sand/gravel layer. Beneath this sand/gravel layer, highly weathered bedrock was encountered at depths of 10 feet to 20 feet.

4. Seepage and Slope Stability Analysis. Seepage and slope stability analyses were performed during the 2005 study. This consisted of analyzing the earth levee, MSE wall, and floodwall sections of varying heights with varying foundation conditions. The foundation conditions were based upon the foundation drilling described earlier.

With the pervious soils located in the foundation for the levee, an underseepage analysis to estimate seepage quantities and the effect on the stability of the levee and MSE wall sections will be required in the design stage. Due to the proximity of the levee on the bank of Fishing Creek, it is assumed that the foundation zones are directly connected hydraulically to the Creek. In the other project reaches, the levee is located much farther from the Creek and the Susquehanna River. In that case, the conservative assumption of direct hydraulic connection can also be made; however, additional investigations in the project design will be required to confirm this assumption.

Underseepage raises pore pressures in the blanket material, decreases the effective weight of the material, decreases effective stress, and reduces stability on the landside portion of the levee. The increased pore pressures can also lead to piping of the foundation material and undermining of the levee foundation. Many of the foundation soils are silty sands and silty gravels which could be susceptible to piping. Appropriate underseepage control measures should be implemented if the stability of the levee or foundation material is not adequate during high water events. Typical underseepage control measures are seepage cutoffs

(slurry trenches, sheetpile, overexcavation and replacement with impervious material), seepage collection measures (toe drains, relief wells) or weighted landside filters (seepage blankets).

The seepage analysis by the Corps in 2005 utilized the finite element program *SEEP2D*, along with the pre- and post-processor *GMS 4.0. SEEP2D* was developed by the United States Army Engineer Waterways Experiment Station to model a variety of problems involving seepage. *GMS* was developed by the Brigham Young University Environmental Modeling Research Laboratory in cooperation with the Waterways Experiment Station (now Engineering Research and Development Center). The slope stability analysis was performed using the computer program *UTEXAS4*, which was developed for the US Army Corps of Engineers by Dr. Stephen Wright. Pore pressures computed in the seepage analysis were used in the slope stability analysis.

Permeabilities were estimated based on the Unified Classification System for soils (Powers, 1981, pg 45), pump test results, and material gradations. The following table contains the various soil types encountered and the respective horizontal permeabilities used in the analysis. Vertical permeabilities were assumed to be 1/10 of the horizontal permeabilities, due to the layering effect in alluvial soil deposits.

	Horizontal Permeability (ft/min)												
Levee (CL)	CL	CL- ML	ML	MSE Fill	SC	SM	SC- SM	SP	GP- GM				
2.0 x 10-6	2.0 x 10-6	2.0 x 10-5	2.0 x 10-5	5.0 x 10-5	2.0 x 10-4	2.0 x 10-3	2.0 x 10-3	1.0 x 10-2	1.0 x 10-l				
		GP	GP- GC	GW- GM	GC- GM	Toe Drain	Sand Drain						
		2.0 x 10-3	5.0 x 10-2	2.0 x 10-2	4.0 x 10-3	1.0 x 10-l	5.0 x 10-2						

Shear strengths used in the stability analysis were determined by using correlations for the Standard Penetration Test, based on soil type. The chart found in NAVFAC Manual 7.1, page 149, was used to determine the effective shear strength parameters. Since pore pressures were included in the stability analysis, effective shear strength parameters were the only parameters necessary for use.

A seepage analysis for the case with water to the top of the levee/MSE wall/floodwall was performed by the Corps in 2005. Stability analyses were performed using the information from the seepage analysis. The levee foundation may quickly experience saturation and seepage due to higher permeabilities. Thus, a steady seepage conditions should be investigated. Sections were analyzed at each boring location from the drilling using the foundation profile encountered. The sudden drawdown case was not analyzed. Sudden drawdown analysis is highly dependent upon the material used for the levee section. With a typical 2.5H:1V slope, most levee sections are stable against sudden drawdown. In the next design phase, once a levee material is specified, a sudden drawdown analysis should be performed. From previous experience, the material type most susceptible to sudden

drawdown failure is highly plastic clay (CH). Most other material types are typically stable against sudden drawdown when compacted in a controlled manner.

From the analysis for the case with steady seepage conditions developed and water to the top of the levee, underseepage could be a major concern. With no foundation improvements, the levee section may be unstable due to the excess pore water pressures in the landside portion of the foundation. Reasonable variations in permeability and material strength do not affect the factors of safety tremendously. From the seepage and slope stability analyses, in addition to engineering judgment and experience, underseepage must be reduced and/or controlled in order to provide a stable levee section during high water events.

As mentioned previously, typical options for reducing or controlling underseepage are aquifer cutoffs, toe drains, seepage berms, and relief wells. The aquifer cutoffs can consist of slurry trenches backfilled with impervious material, sheetpile, concrete cutoffs, or standard excavate and replace procedures. Cutoffs reduce seepage amounts and seepage pressures, with the magnitude of reduction depending upon the materials used.

Toe drains or relief wells reduce seepage pressures at the landside toe of the levee by providing an efficient outlet for the underseepage water. The toe drains or relief wells are designed to allow water to enter, but to not allow piping of the foundation soils into the drains or wells. Stability and protection against foundation piping is then provided by allowing the pore pressures to dissipate safely and quickly.

The seepage and slope stability analyses modeled cutoffs of the upper aquifer layer, a toe drain, and combinations of the two where appropriate. The normal groundwater level is well below the bottom of the cutoff. Thus, the cutoff should not interfere greatly with groundwater discharge/recharge with Fishing Creek and groundwater should not impact construction of the cutoff. The toe drain sections analyzed all penetrated into a pervious layer, allowing seepage pressures to be relieved safely.

A toe drain is the preferred method of handling the underseepage. This is due to the fact stated above that a cutoff can alter groundwater movement by blocking the groundwater from the river. Therefore, where cutoffs are used, it is considered best not to use long stretches of cutoffs. A toe drain is proposed for the extent of the levee/floodwall alignment along Fishing Creek. In this reach, a slurry trench cutoff was proposed in the Corps report but that was without the addition of a creek side slope embankment down to the creek bed. Additional geotechnical investigations with a modified crrekside slope will be required to verify the need for a seepage cutoff system versus a seepage control system. Any seepage control or sutoff system will be constructed in addition to the toe drain. The toe drain will control underseepage not cut-off as well as any seepage through the levee.

A toe drain is also proposed for the portion of levee that crosses the Fairgrounds. The sand and gravel aquifers in this portion have the potential to destabilize the landside toe of the levee, thus a toe drain will safe!y relieve the high seepage pressures.

The toe drain will most likely consist of open-graded gravel wrapped in a geotextile. The geotextile will prevent the finer foundation materials from moving into and clogging the gravel drain. The geotextile must also be permeable enough to allow water to freely enter the gravel drain without clogging.

The typical levee section will consist of a random material zone (for drawdown protection) on the riverside 1/3, adjacent to a select fill zone, which will in effect be an impervious material. In sections without toe drains, a landside blanket drain will be used. In areas where riprap is determined to be necessary, a layer of riprap on 6 inches of bedding soil will be provided. Exterior levee slopes will be 2.5H or 3: 1V for areas receiving topsoil. Areas requiring riprap can be steepened to 2H:1V. A rock toe keyed into the streambed is recommended for slope stability.

Overexcavation will be required to an approximate depth of 6 feet along all MSE levees. The overexcavation would extend under the entire reinforced earth zone.

Included as Sub-Attachments 3 and 4 to the Geotechnical Attachment to the Engineering Appenidix in the Corps report are selected seepage and slope stability trials. These are not included here but referenced for future use. They are intended to give an illustration of the conditions in the various reaches. Details and typical proposed levee sections are shown in the study drawings.

- **5. Settlement Analysis.** No extensive areas of soft, fine-grained materials were encountered. Due to the granular foundation materials encountered in much of the project area, a long-term settlement analysis was not performed. The settlement caused by the levee/floodwall construction will occur during construction, thus an overbuild due to long-term settlement concerns is not deemed necessary at this time.
- **6. MSE Wall Design.** MSE walls are planned as part of the project. Detailed design calculations are required for these levee systems. MSE walls consist of three main components: 1) Facing, 2) Reinforcement, and 3) engineered backfill. The reinforcement for this project, and most projects near water bodies, should be geogrid. Geogrid is a polymeric material generally consisting of polypropylene, polyethylene, or polyester. Metallic reinforcement (the other predominant type of reinforcement for MSE walls) is very prone to deterioration when exposed to water. Since these walls will be used along a creek as flood walls, they will be subjected to water relatively often.

In MSE wall construction, a leveling pad of lean concrete or compacted aggregate is placed along the wall face alignment. The concrete panels or concrete modular blocks are then placed on the leveling pad one row at a time. Once a row of block is placed, soil is placed and compacted in the reinforced soil zone behind the block or panels. Reinforcement is then placed at specified elevations. Additional soil is placed and compacted above the reinforcement layer. By placing the tensile reinforcements in the soil, the strength of the soil is improved significantly. With the geogrid (or metallic) reinforcement, the reinforced soil mass is essentially self-supporting. The facing for the MSE walls is provided mainly to keep the soil from eroding and for aesthetic reasons. The entire wall is built in lifts in this fashion.

Both an internal and external stability analysis are required for MSE wall design. The MSE wall is considered to act as a mass to resist external forces, much like a concrete gravity wall. External design consists of determining what external loads will be acting on the wall, and what size of wall is required to resist those forces. Internally, the reinforcing must be designed to have the required length and strength to hold the reinforced soil together. Vertical spacing of geogrid is generally kept at a maximum of 2 feet. At spacings larger than 2.5-3 feet, the reinforced soil begins not to act as a reinforced mass.

The MSE walls proposed for this project are currently designed as single-sided walls. This means that the wall facing is on the landside of the levee. Most MSE walls are built with one face, retaining soil behind the reinforced soil zone.

<u>Subsurface Information</u>: Soil parameters utilized by the Corps in the analysis were based on those observed in DH-3 through DH-7 of the November 2000 exploration. The limited exploration performed to date will be supplemented with a more detailed exploration prior to the preliminary and final design. The analyses included in the Corps report of 2005 is therefore preliminary and must be re-visited after completion of a full subsurface investigation program. Additionally, as no borings were performed on the Femville side of the river, any channel work on that side of the creek will require additional borings..

It should be noted that DH-101 performed in April 2002 also falls within the general area of the planned wall and was reviewed as part of the study. The conditions observed in DH-101 were significantly less dense (i.e. lower SPT blow counts) than those observed in the other nearby borings. It is currently assumed that the conditions observed in DH-101 are isolated and possibly associated with previous fills in the area (indications of previous filling activities also seen in other borings). The extent of such "soft" soil areas should be further investigated during the future exploration. Specific wall heights, etc in those areas can then be more closely reviewed and the design adjusted as necessary. The final design may determine that specific "foundation improvement" measures are required in such areas in order to meet the design assumptions or the wall design may require revision. Refer to the "Insitu Soil Parameters for MSE Wall" paragraph included with the design for further discussion.

It should be noted that the current design criteria for MSE levees requires the ground surface at the base of the MSE wall to extend a minimum distance of 10' from the wall before sloping downwards. It also requires that any slopes beyond this minimum distance be no steeper than 2H:1V.

Insitu Soil Parameters for MSE Wall Design:

Insitu soils are primarily silty sands and silty gravels. Standard Penetration Test blow counts in the upper 10 feet of soils at the site are generally in the range of N=7 to 20 and govern the design. Typical SPT blows in the dense sands and gravels below this depth are N>50. When corrected for overburden pressure, the lowest N values increase to approximately N = 10.

Based on conservative correlations, a friction angle of $<!>= 30^{\circ}$ and a unit weight of y = 115 pcf will be used for the insitu soils below the planned MSE wall for the sliding analysis. For the bearing capacity analysis, values of $<!>= 32^{\circ}$ and a unit weight of y = 120 pcf will be used. This is appropriate as the shear failure is affected by soils to a significant depth as compared to the sliding.

7. Material Source. Suitable levee material sources for previous projects must be verified for the project. For cost estimating purposes, borrow material for levee construction was assumed to be available from a commercial source located within ten miles of the project area. Material source investigations will be undertaken in the next phase of design.

8. Closure Structures.

a. **Route 11 Stop Log Closure.** This structure crosses Route 11 at Station 26+10.. The stop log structure will be about 50 feet wide, 6 feet high and consist of 4 bays of closure panels. On both ends of the closure, a concrete abutment will be constructed to support the end spans of the stop log panels and to retain the earth levee embankment. A foundation key parallel to the wall below the foundation will be built to increase the abutment factor of safety against sliding failure.

The subsurface condition at this closure is currently represented by drill hole DH-5. The upper 3 feet of overburden consist of silty sand materials. The second strata consists mainly of sand and gravel (GP, SP, and combinations thereof) to a depth of 6 feet with some silty and clayey zones and to top of rock at a 23 foot depth.

- b. Other closures are of similar abutment construction with concrete sills and footings. Additional test borings will be required at each structure to further refine geotechnical parameters for analysis and design recommendations for the structural engineers.
- c. **Geotechnical Design Parameters.** The following geotechnical design parameters were provided to the Structural Engineer on the 2005 Corps study to analyze the closure structures for stability (i.e. determine forces, moments, and FS against sliding and overturning).

Angle of Internal Friction = 30° Moist Unit Weight of Soil= 125 pounds/ft ³ Active Lateral Earth Pressure Coefficient= Ka= .33 Passive Lateral Earth Pressure Coefficient= Kp = 3.0

- 9. Next Phase of Design. The next phase of design will be the preliminary engineering phase. Final design for the levee, MSE walls, floodwall, and closure structures will be performed based on the additional subsurface explorations and the information recovered to date. Plans and specifications will be prepared based upon the final designs.
- **10. Future Investigations -** During the preliminary engineering design phase, additional subsurface investigations should be undertaken to refine the design features and to identify any unknown foundation conditions. Seepage along the MSE levee has to be confirmed.

Previously identified pervious subsurface soil strata along to bank of Fishing Creek will require testing and geotechnical recommendations. Also, subsurface conditions along the reach of the proposed sheet pile wall require additional investigation and analysis for

acceptable driving conditions for PZ piling to the depths required for stability and seepage control.

The future investigations will consist of additional soil borings, rock coring, test pits, and permeability tests. Samples recovered will be tested as required. Design of the recommended plan will be refined during design, based on the additional information from the investigations and data that will be recovered or developed at that time.

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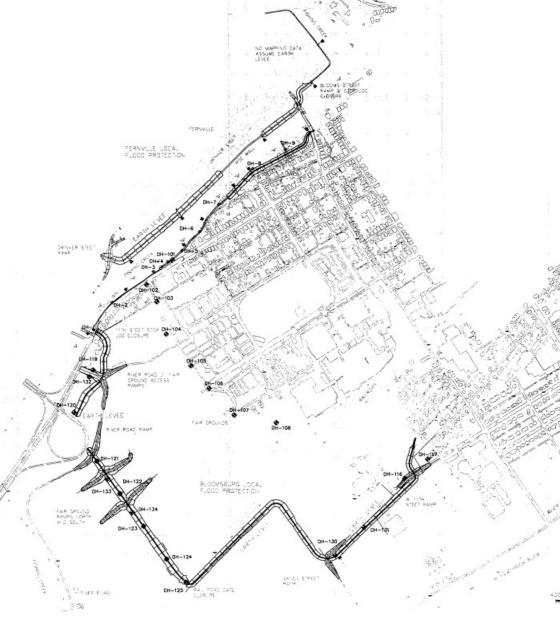
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ATTACHMENTS 1 THRU 3

- 1 Drilling Location Plan
- 2 Field Boring Logs Phase I
- 2A Field Boring Logs Phase II
- 3 Phase I Geologic Profile

Attachment 1 Drilling Location Plan



Attachment 2 Field Boring Logs Phase I

Test Boring Log Page No 1 DH-1 for of 2 Project Name Bloomsburg Phase I | Date Started 10-30-00/9:30 AM Notes No. C 19:3 Completed 10-30-00/2:15 PM Depth to firm rock estimated from other borings to be within Drilling Contractor Pocono Test Borings Inspector S. Cox 5 ft of bottom of hole. Driller Frank Sipple Encountered during drilling
Measured after completion Offset Ground Elevation 477.26 Ground Water Level Location Boring Methods/Diameter SS/2" Date/Time | Depth | Elevation | Notes

	of Rock Not encountered	10-30/2:20	5.5 ▼ 471.76	
A Soft Soft Soft Soft Soft Soft Soft Soft	Lithologic Log and Description		A COUNTS	Pagonery (%)
4762	SILTY SAND: redbrown, moist, loose to med. compact, Artificial Fill (SM) SANDY GRAVEL: red-brown, moist, med. compact, Artificial Fill (GW-GP	0 s-1 s-2	6-4-6	18 60 20 27 13
474 -	SILTY SAND: trace gravel, brown, moist, med. compact, Artificial Fill (SM) SAND: red-brown, moist, loose to med.	-4 - s-3	4-6-7	40 9 10
4708	compact (SW-SP) SILTY SAND: red- brown, moist, med. compact (SM) NO RECOVERY	-6 - s-4 s-5	7-4-18 9-10-5	53 9 15 33 4
468 -	SAND WITH SILT:	s-6	5-3-5	0 9
466 –	brown, wet, med. compact (SM)	-10 - s-7	9-6-6	13 9 9
12	SAND: brown, wet, loose (SW-SP)	-12 - s-8	3-5-2	40 6
46414	SANDY, SILTY CLAY: red-brown, moist, med. stiff (CL-	-14 - s-9	3-4-4	53 7

Page No 2 of 2

Project Name B No. Cox Inspector S. Cox	C19:3 Completed 10-3 Drilling Contractor	0-00/2:15 PM	Notes Depth to firm rock estimated from other borings to be within to f bottom of hole.
Total Depth 27.0 f	Offset Ground Elevation 477.20 ameter SS/2" Casing Depth 26.0 ft Top of Rock Not encountered	6 Ground Water Level	
Elevation Control of C	Lithologic Log and Description	Poten	Parts
462		s-10 2-3-3	100 8
16	SAND WITH SILT: gray-brown, wet, loose? (see note)	-16 -	4 16.0-17.5' blow counts for 2nd
460 -	(SM)	s-11 2-28-26	and 3rd 6" intervals may be result of
18		-18 -	pushing rock fragment
458 -	SAND: trace silt, gray- brown, wet, compact, shale frags. in spoon tip (SM)	-20 - s-12 10-20-21	53 28
456	Decomposed SHALE: lt. olive, very highly		17
456 -	weathered, moist, friable, clay seams, bedding dip 20 deg.	-22 - s-13 18-30-30	53 43
454 —			28
24		-24 -	66 lab grain size
452 –		s-14 39-46-78	87 100 analysis for 23.5-27.0' indicates highly weathered rock
26		-26 -	100 is gravelly silt with sand
		s-15 22-100	100

Project Name Bloomsburg Phase I Date Started 10-31-00/7:30 AM Completed 10-31-00/11:20AM

Inspector S. Cox Drilling Contractor Pocono Test Borings Driller Frank Sipple

			-FF			
Location	Offset	Ground Elevation 476.06	Ground Wat	er Level		Encountered during drilling Measured after completion
Boring Methods	/Diameter SS/2'	" & NWD (2.125") Core	Date/Time	Depth	Elevation	Notes
Casing Size 4 is	nch Casing Dept	h 13.0 ft				
Total Depth 21.	.0 ft Top of Rock	16.0 ft				
	ATE AND NAMED SHOW THE ADDRESS	State - 100 reported a 🕶 100			20	

Casing Size 4 inch Cas Total Depth 21.0 ft Top	of Rock 16.0 ft			·			
Eletation Soft Perm Cones Water Cones Water Cones Letter	Lithologic Log and Description	D. Parts		A SA COMES	*Recor	Casin (%)	100 to 10
4742	LEAN CLAY: drk brown, moist, v. stiff, (topsoil) (CL) SAND & GRAVEL: trace silt, drk graybrown, med. compact,	0	s-1	4-15-4	53	26	· ·
-	Artificial Fill (GM-SM	-	s-2	4-7-7	20	23	
4724		-4	s-3	13-16-18	20	7	ž
470 6	SANDY CLAY: brown, damp, v. stiff (CL)	-6 -	s-4	9-8-8	13	7	
468 8	CLAYEY SAND: brown, damp, med. compact (SC)	-8 -	s-5	7-11-19	53		
	SAND: trace silt, brown, moist, compact (SM)	21	s-6	50-94-100	20	15	
466	GRAVEL: brown, wet, v. compact (GW-GP) SAND & GRAVEL:	-10 -	s-7	29-52-100/0.3	23	35	
46412	trace clay, brown, moist, v. compact (GC-SC) Decomposed SHALE:	-12 -	s-8	25-37-43	53	65	lab grain size analysis for
46214	clay seams, lt. olive, very highly weathered, moist, 45 deg. dip	-14 -	s-9 s-10	50-105 39-50/0.1	83	125	12.0-13.0' indicates highly weathered rock is clayey sand with gravel

Page No 2 of 2

Project Name Bloomsburg Phase I | Date Started 10-31-00/7:30 AM Notes No. C 19:3 Completed 10-31-00/11:20AM Inspector S. Cox Drilling Contractor Pocono Test Borings Driller Frank Sipple Encountered during drilling
Measured after completion Ground Water Level Offset Ground Elevation 476.06 Location Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 13.0 ft Total Depth 21.0 ft Top of Rock 16.0 ft Lithologic Log and Description 50/0 -16 460 SHALE: olive, med. hard, weathered, 45 deg dip, breaks easily along bedding -18 458 -20 -20 456 92 R-1 0%

Project Name Bloomsburg Phase I | Date Started 10-31-00/1:20 PM

Page No 1 of 3

Notes

No. C 19:3 Completed 11-1-00/1:45 PM Drilling Contractor Pocono Test Borings Inspector S. Cox Frank Sipple Driller Encountered during drilling Ground Water Level Offset Ground Elevation 477.76 Location Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 26.0 ft Total Depth 39.0 ft Top of Rock 29.0 Lithologic Log and Description SANDY SILT: drk. brown, moist, stiff (ML) 17 s-1 5-12-7 53 SAND WITH SILT: 476 drk. brown, moist, 14 -2 med. compact (SM) SILT WITH SAND: dk s-2 3-3-10 60 14 gray-brown, moist, med stiff (ML) 474 6 SILTY SAND: red--4 brown, moist, loose to s-3 4-6-12 60 med compact (SM) 13 SANDY CLAY: redbrown, moist, med. 472 stiff (CL) s-4 67 8-6-9 13 -6 SILTY SAND: redbrown, moist, med. 13 compact (SM) s-5 6-8-28 20 --:X 470 SANDY SILT: red-28 -8 -8 brown, wet, stiff to v. stiff (ML) 32-30-31 47 29 s-6 **GRAVEL WITH** CLAY & SAND: red-brown, moist, very 468 34 compact (GP-GC) -10 -10 9:09 40 s-7 32-37-43 0.00 62 0:00 0.00 <u>-:0</u> 466 18-28-50 53 65 s-8 -12 -12 42 s-9 13-43-33 40 464 48 -14

Page No 2 of 3

Project Name Bloomsburg Phase I | Date Started 10-31-00/1:20 PM Notes No. C 19:3 Completed 11-1-00/1:45 PM Drilling Contractor Pocono Test Borings Inspector S. Cox Driller Frank Sipple ✓ Encountered during drilling✓ Measured after completion Offset Ground Water Level Location Ground Elevation 477.76 Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 26.0 ft Total Depth 39.0 ft Top of Rock 29.0 Lithologic Log and Description s-10 | 32-24-30 53 38 0.50 462 40 -16 -16 65 12-28-31 27 s-11 460 77 -18 -18 81 458 s-12 27-40-65 67 58 -20 -20 lab grain size analysis of 21.0 to 29.0' 75 indicates highly Decomposed SHALE: weathered lt. olive, very highly shale is sandy 456 weathered, moist, clay 50 -22 -22 silt, trace gravel seams, friable 40 s-13 18-27-40 65 23.5-25.0' clay CLAY: gray, moist, 454 58 is completely -24 hard -24 weathered shale s-14 12-38-72 80 65 Decomposed SHALE: 452 78 -26 -26 lt. olive, very highly weathered, moist, clay 75-50/0.1 s-15 83 seams, friable 450 -28 -28 s-16 100 100

SHALE: olive, highly

Page No 3 of 3

Project Name Bloomsburg Phase I | Date Started 10-31-00/1:20 PM Notes No. C 19:3 11-1-00/1:45 PM Completed **Drilling Contractor** Inspector S. Cox Pocono Test Borings Driller Frank Sipple Encountered during drilling
Measured after completion Ground Water Level Ground Elevation 477.76 Offset Location Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 26.0 ft Total Depth 39.0 ft Top of Rock 29.0 Lithologic Log and Description weathered, soft to med. hard, 25 deg. dip -30 446 -32 -32 444 0% 66 R-1 -34 -34 all discontinuities SHALE: olive, in shale are 442 -36 moderately weathered, -36 along bedding hard except for one sub-vertical SILTSTONE: gray, fracture slightly weathered, hard to v. hard, no 440 visible bedding -38 -38 SHALE: olive, mod. to R-2 10% 100 highly weathered, soft to hard

Page No 1 of 3

Notes Project Name Bloomsburg Phase I | Date Started 11-2-00/7:30 AM No. C 19:3 11-2-00/2:45 PM Completed Drilling Contractor Pocono Test Borings Inspector S. Cox Frank Sipple Driller Encountered during drilling Offset Ground Water Level Location Ground Elevation 478.16 Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 25.0 ft Total Depth 32.6 ft Top of Rock 27.6 Lithologic Log and Description 478 SILT: red-brown, dry, v. stiff, (topsoil) (ML) 27 s-1 9-12-16 27 SAND & GRAVEL: 56 -2 brown, dry, compact, -2 476 Artificial Fill (GP-SP) s-2 17-24-18 20 46 SILTY SAND: trace gravel, moist, .0 compact, Artificial Fill 35 -4 474 (SM) :O_:::_ 22-20-17 33 s-3 0.50 SANDY GRAVEL 20 0:00 WITH SILT: brown, X---X moist, compact, Artificial Fill (GM) s-4 15-25-19 40 38 -6 -6 472 SILTY SAND: brown, dry, v. compact (SM) 35 s-5 25-35-35 27 70 -8 470 200-100/0.4 s-6 20 <u>-:0-</u> SANDY GRAVEL 45 WITH SILT: brown, moist, v. compact (GM) 25 -10 -10 468 s-7 25-47-75 67 \(\alpha\) \(\frac{1}{2}\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \ s-8 50/0.1 100 **GRAVEL WITH** 47 0.0.02 SAND: trace silt/clay, red-brown, wet, v. compact (GM-GC) 80 -12 -12 466 36 s-9 27-48-68 20 SANDY GRAVEL s-10 100/0.4 50 48 WITH SILT: brown, -14 464

0.53

0.70

moist to 10.6 ft, wet to

Page No 2 of 3

11-2-00/7:30 AM Notes Project Name Bloomsburg Phase I | Date Started 11-2-00/2:45 PM No. C 19:3 Completed Drilling Contractor Pocono Test Borings Inspector S. Cox Driller Frank Sipple Encountered during drilling
Measured after completion Ground Water Level Ground Elevation 478.16 Offset Location Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 25.0 ft Total Depth 32.6 ft Top of Rock 27.6 Lithologic Log and Description 22.5 ft (GM) 62 0.60 34 -16 s-11 16-18-18 20 48 52 -18 -18 460 민 : ' □ 20 37 28-47-58 s-12 0:00 0.60 0:00 80 -20 -20 458 38 0:00 47-68-100/0.2 67 s-13 Ø = Z 48 -22 -22 456 lab grain size Decomposed SHALE: 68 analysis It olive, clay seams, indicates friable, moist to 24 ft, decomposed wet to 27.6 ft shale is clayey s-14 20-40-45 67 70 -24 sand with 454 gravel 115 -26 -26 s-15 70-39-100/02 50 452 s-16 50/0.1 0 SHALE: mod to highly -28 -28 weathered, olive, med 450 hard, 20 deg dip

Page No 3 of 3

Notes Project Name Bloomsburg Phase I | Date Started 11-2-00/7:30 AM 11-2-00/2:45 PM No. C 19:3 Completed Drilling Contractor Pocono Test Borings Inspector S. Cox Driller Frank Sipple Encountered during drilling
Measured after completion Ground Water Level Location Offset Ground Elevation 478.16 Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 25.0 ft Total Depth 32.6 ft Top of Rock 27.6 Lithologic Log and Description SILTSTONE: mod weathered, olive-gray, hard, shale laminae SHALE: mod to highly weathered, olive med hard, 20 deg dip -32 0% R-1 66

Project Name Bloomsburg Phase I | Date Started 11-3-00/8:00 AM Notes No. C 19:3 Completed 11-6-00/1:00 PM Inspector S. Cox Drilling Contractor Pocono Test Borings Driller Frank Sipple Encountered during drilling Offset Ground Elevation 478.56 Ground Water Level Location Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time | Depth | Elevation | Notes Casing Size 4 inch Casing Depth 24.0 ft Total Depth 31.1 ft Top of Rock 26.1 ft Lithologic Log and Description 0 SILT WITH SAND: brown & red-brown, 478 dry, stiff to v. stiff 16 (ML) s-1 60 3-6-7 56 -2 -2 476 s-2 15-30-31 33 20 SAND & GRAVEL: 0000 gray, dry, med compact, Artificial Fill (GP-SP) 10 -4 0 s-3 8-8-8 474 11 0.00 0000 s-4 6-8-15 0 14 -6 -6 SILTY SAND: red-472 brown, moist, med 11 compact (SM) s-5 80 7-6-7 14 -8 -8 470 SANDY CLAY: red-13-12-12 19 s-6 20 brown, moist stiff to v. stiff (CL) 27 -10 -10 SILTY SAND: reds-7 2-5-15 67 brown, moist, med 468 7.0 compact (SM) 0:00 30 O. -- C SILTY GRAVEL □:`○□ WITH SAND: yellow-\(\frac{1}{2}\) \(\frac{1}{2}\) \(\frac{1}2\) \(\frac{1}{2}\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(\frac\ s-8 62-65-75 33 56 -12 brown & red-brown -12 mottled, moist, v. 466 compact (GM) 32 □:♡□ s-9 35-46-43 40 33 -14 -14

· O =

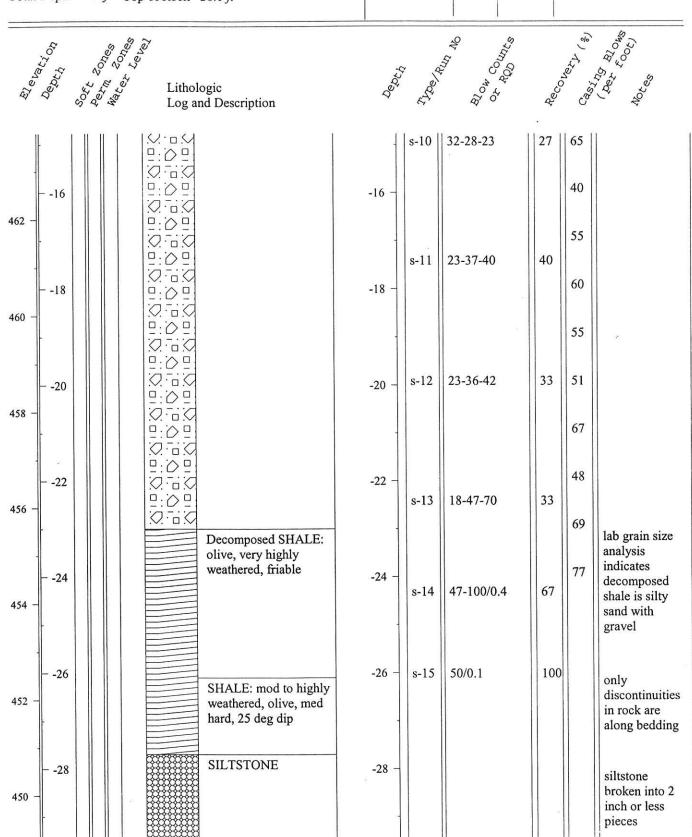
464

Project Name Bloomsburg Phase I Date Started 11-3-00/8:00 AM
No. C 19:3 Completed 11-6-00/1:00 PM

Inspector S. Cox Drilling Contractor Pocono Test Borings
Driller Frank Sipple

Location Offset Ground Elevation 478.56
Boring Methods/Diameter SS/2" & NWD (2.125") Core
Casing Size 4 inch Casing Depth 24.0 ft
Total Depth 31.1 ft Top of Rock 26.1 ft

Ground Water Level Encountered during drilling Measured after completion
Date/Time Depth Elevation Notes



Page No 3 of 3

Project Name Bloomsburg Phase I | Date Started 11-3-00/8:00 AM Notes No. C 19:3 Completed 11-6-00/1:00 PM Drilling Contractor Inspector S. Cox Pocono Test Borings Driller Frank Sipple Encountered during drilling
Measured after completion Offset Ground Water Level Location Ground Elevation 478.56 Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time | Depth | Elevation | Notes Casing Size 4 inch Casing Depth 24.0 ft Total Depth 31.1 ft Top of Rock 26.1 ft Lithologic Log and Description SHALE: mod to highly R-1 weathered, olive, med. hard

Project Name Bloomsburg Phase I | Date Started 11-13-00/7:45 AM Notes No. C 19:3 Completed 11-13-00/2:45 PM Inspector S. Cox Drilling Contractor Pocono Test Borings Driller Frank Sipple Encountered during drilling Offset Ground Water Level Ground Elevation 478.36 Location ▼ Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 24.0 ft Total Depth 38.7 ft Top of Rock 28.7 ft Lithologic Log and Description SANDY CLAY: dk. 478 gray-brown, moist, med. stiff to stiff (CL) 9 2-5-5 27 s-1 SILTY, CLAYEY 14 -2 -2 SAND: red-brown, damp, loose to med 476 compact (SM-SC) s-2 4-5-4 27 9 -4 474 s-3 3-2-5 100 10 s-4 80 3 5-6-5 -6 SANDY CLAY: red-472 brown, moist, med stiff (CL) 6 s-5 3-3-4 87 SILTY, CLAYEY SAND: red-brown, 8 -8 moist, loose to med 470 compact (SM-SC) s-6 9 7-12-19 100 0000 **GRAVEL WITH** SAND: trace silt, red & yellow-brown, 0.00 0 -10 -10 mottled, moist, v. 468 s-7 14-30-47 20 compact (GM) 0:00 38 0.50 SANDY GRAVEL WITH SILT: redbrown, wet, v. s-8 40-34-75 20 45 -12 -12 compact (GM) 日:0日 466 \(\alpha\) --- \(\alpha\) 35 s-9 35-33-40 47 **GRAVELLY SAND** 52 -14 -14 WITH CLAY: redbrown, wet, v. 464

V. 0.V

Page No 2 of 3

of 3 11-13-00/7:45 AM Project Name Bloomsburg Phase I | Date Started Notes No. C 19:3 Completed 11-13-00/2:45 PM Inspector S. Cox **Drilling Contractor** Pocono Test Borings Driller Frank Sipple Encountered during drilling
Measured after completion Ground Water Level Offset Location Ground Elevation 478.36 Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 24.0 ft Total Depth 38.7 ft Top of Rock 28.7 ft Lithologic Log and Description Compact (SC)
SANDY GRA 49-50-45 s-10 67 SANDY GRAVEL WITH SILT: red-88 brown, wet, v. -16 -16 · 'O'. compact (GM) 462 **GRAVELL SAND** 15 WITH CLAY: red-s-11 22-30-58 53 brown, wet, v. 0.50 compact (SC) 44 -18 -18 460 SANDY GRAVEL WITH SILT: red-9:09 58 brown, wet, v. 10.7°C compact (GM) s-12 33-40-35 47 25 **GRAVELLY SAND** -20 -20 WITH CLAY,: red-458 Q:-Q:-Q brown, wet, v. 68 compact (SC) SANDY GRAVEL WITH CLAY: red-27 :O:-:::C -22 -22 brown & yellow-456 53 s-13 22-35-28 brown mottle, moist, v. compact (GC) 47 lab grain size Decomposed SHALE: analysis lt. olive, very highly indicates 100 68--50/0.1 83 weathered, friable, wet -24 s-14 decomposed 454 shale is silty sand, trace grave -26 -26 452 24-60-91 67 s-15 -28 -28

50/0.2

s-16

SHALE: red, mod to highly weathered, soft

100

450

Page No 3 of 3

Project Name Bloomsburg Phase I | Date Started Notes 11-13-00/7:45 AM No. C 19:3 11-13-00/2:45 PM Completed Drilling Contractor Inspector S. Cox Pocono Test Borings Driller Frank Sipple Encountered during drilling Offset Ground Elevation 478.36 Ground Water Level Location Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 24.0 ft Total Depth 38.7 ft Top of Rock 28.7 ft Lithologic Log and Description to med hard, 35 deg -30 dip, a few sub-vertical fractures 448 -32 -32 446 R-1 0% 74 -34 444 -36 -38 -38 15% 72 R-2 440

11-8-00/2:40 PM

Project Name Bloomsburg Phase I | Date Started

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Notes

See report text for discussion of apparentl No. C 19:3 Completed 11-9-00/2:30 PM very 'soft' materials from 3' to 7', and Drilling Contractor Inspector S. Cox Pocono Test Borings 29' to 31.5'. No SPT for these intervals Frank Sipple Driller Ground Elevation 477.16 Ground Water Level Offset Location Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 31.0 ft Total Depth 37.0 ft Top of Rock 32.0 ft Lithologic Log and Description 0 SILTY SAND: graybrown, damp, med compact (SM) 7 476 s-1 5-10-9 20 NO RECOVERY 12 -2 s-2 7-4-3 0 8 While cleaning 474 NO SAMPLE: casing to 3' Apparently loose, casing rotated coarse Artificial Fill, 14 and moved see note vertically, due to loose and 6 probably 472 coarse fill. Cleaning casing 2 to 6' caused -6 casing to drop to 7'. 0 470 SILTY GRAVEL 0:00 WITH SAND: redbrown & yellow-20 -8 brown mottled, moist, 8-35-38 s-3 40 v. compact (GM) 30 250 468 0:00 0.737 40 44 40-33-61 s-4 -10 -10 □:♡□ 0.50 20:0 38 0.50 466 10-26-35 33 s-5 0:00 58 0.50 -12 -12 38-40-68 100 60 s-6 0.00 464 : O = 36 -14 -14 20 37-33-38

Page No 2 of 3

almost

Project Name Bloomsburg Phase I | Date Started Notes 11-8-00/2:40 PM See report text for discussion of apparentl No. C 19:3 Completed 11-9-00/2:30 PM very 'soft' materials from 3' to 7', and Drilling Contractor Pocono Test Borings Inspector S. Cox 29' to 31.5'. No SPT for these intervals Frank Sipple Driller Ground Water Level Offset Ground Elevation 477.16 Location Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 31.0 ft Total Depth 37.0 ft Top of Rock 32.0 ft Lithologic Log and Description 2:09 2:09 2:00 2:00 462 47 s-8 23-33-30 50 -16 0.60 **GRAVELLY SAND** 48 WITH SILT: red-0 460 brown, moist, v. compact (SM) 38 -18 -18 0 s-9 21-30-48 0 55 458 Decomposed SHALE: red to 26.5', lt. olive 26.5-29.0', moist to 20 -20 -20 21.0', wet 21.0-29.0', friable, clayey 45 s-10 13-25-37 67 456 45 -22 -22 58 454 23-24-25 27 s-11 100 -24 -24 18 452 s-12 40-42-37 40 11 -26 -26 8 450 20 -28 -28 18-20-13 67 s-13 28.5 to 31.5' SILTY SAND: orange, 10 silty sand is saturated, v. loose,

see note (SM)

448

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Project Name Bloomsburg Phase I | Date Started 11-8-00/2:40 PM Notes See report text for discussion of apparentl No. C 19:3 Completed 11-9-00/2:30 PM very 'soft' materials from 3' to 7', and Drilling Contractor Pocono Test Borings Inspector S. Cox 29' to 31.5'. No SPT for these intervals Driller Frank Sipple Encountered during drilling
Measured after completion Ground Water Level Location Offset Ground Elevation 477.16 Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time | Depth | Elevation | Notes Casing Size 4 inch Casing Depth 31.0 ft Total Depth 37.0 ft Top of Rock 32.0 ft Lithologic Log and Description completely -30 decomposed shale. After cleaning hole to 8 29.5' casing 446 dropped to 31.0'. s-14 1-50/0.2 100 Decomposed SHALE: -32 lt. olive, wet SHALE: olive, mod. to highly weathered, soft 444 to hard, 35 deg. dip -34 442 -36 -36 14% 84 R-1

Notes Project Name Bloomsburg Phase I | Date Started 11-8-00/8:15 AM Poor recovery from 6.0-9.0'; gravel No. C 19:3 11-8-00/1:30 PM Completed at bottom of samples suggests that Inspector S. Cox **Drilling Contractor** Pocono Test Borings unrecovered intervals are gravel/ Driller Frank Sipple sand soils Encountered during drilling
Measured after completion Ground Water Level Offset Ground Elevation 478.16 Location Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 18.5 ft Total Depth 23.6 ft Top of Rock 18.6 ft Lithologic Log and Description 0 478 **ASPHALT** 30 7:07 SANDY GRAVEL: \(\alpha \) = \(\alpha \) 9-24-16 20 s-1 trace silt, brown, damp, med compact to 25 -2 -2 compact, Artificial Fill 476 (GP-GM) Ø:-i:< s-2 10-9-10 20 31 NO RECOVERY: probably a noncohesive soil 6 -4 similar to 0.9 to 3.0' 474 0 s-3 8-7-6 10 SILTY SAND WITH s-4 10-9-14 20 11 -6 GRAVEL: red-brown, 0 moist, med compact (SM) 7 0 s-5 6-11-10 33 -8 \Diamond 470 10 1-20-31 40 s-6 SANDY GRAVEL --: WITH SILT: red-민 (): 민 brown, moist to 10.5', 14 -10 -10 O. 13 C wet 10.5 to 14.7', med 468 47 s-7 12-18-25 0.00 compact to compact (GM) 0.50 20 0:00 0.50 D:00 s-8 24-22-13 13 24 -12 -12 466 0.50 :00 20 0.50 0:00 4-10-14 13 s-9 --:X 23 -14 0:00

464

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		V8:15 AM	Ĭ	Notes		
w		V1:30 PM		Poor recove at bottom of	ry from 6.0-9.0'; gravel samples suggests that	
Inspector S. Cox Drillin	Drilling Contractor Pocono Test Borings Driller Frank Sipple			unrecovered intervals are gravel/ sand soils		
Boring Methods/Diameter SS/2" & NWD (2.12) Casing Size 4 inch Casing Depth 18.5 ft Total Depth 23.6 ft Top of Rock 18.6 ft	Elevation 478.16 25") Core	Ground Ward Date/Time	Encountered during drilling Measured after completion Notes			
Lithologic Log and Descripti	on	The Court	ON THE TO SEE THE TO S	to the contract of the contrac	(25) (3) (3) (3) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	
46216 CLAYEY S gray, wet, of (SC) SANDY G WITH SILL yellow-bow moist, v. co	RAVEL T: red & vn mottled,	-16 - s-10	17-19-22	370 2	195 51	
46018 (GM)		-18 - s-11 s-12	36-46-68	100	70	
	& soft 20.6- eg dip, only ties are	-20 -				
456		-22 -	0%	76		

Page No 1 of 2

Project Name Bloomsburg Phase I | Date Started 11-7-00/8:30 AM Notes No. C 19:3 11-7-00/2:00 PM Completed Drilling Contractor Pocono Test Borings Inspector S. Cox Driller Frank Sipple Encountered during drilling Offset Ground Elevation 481.16 Ground Water Level Location Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 22.0 ft caved at 5.0 ft 11-8/7:30 AM Total Depth 28.5 ft Top of Rock 23.5 ft Lithologic Log and Description 0 SANDY GRAVEL: dk gray & blue-gray, moist, loose to 18 compact, Artificial Fill 480 5-21-20 27 s-1 (GP) 00.02 37 -2 -2 0.0.02 s-2 14-21-12 20 20 00.00 478 00.00 8 -4 0000 10-8-4 27 s-3 00.00 14 476 0000 s-4 5-4-4 20 5.8 to 6.0' sandy 0.00 -6 gravel with silt, red-brown, moist. loose, 6 474 Artificial Fill s-5 5-3-1 0 7 -8 7 3-4-11 13 s-6 8.8 to 9.0' sandy 472 NO RECOVERY gravel with silt, red-brown, moist, loose, 0 -10 -10 Artificial F s-7 7-3-2 0 SANDY GRAVEL 6 WITH SILT: red-470 □:``>□ brown, moist, :O. ---:C compact, Artificial Fill 19-20-17 20 s-8 (GM) -12 -12 NO RECOVERY 13 468 s-9 6-12-7 0 SANDY, SILTY 20 CLAY: red-brown, -14

wet, soft to med stiff

Page No 2 of 2

Project Name Bloomsburg Phase I | Date Started 11-7-00/8:30 AM Notes No. C 19:3 Completed 11-7-00/2:00 PM Inspector S. Cox Drilling Contractor Pocono Test Borings Driller Frank Sipple Encountered during drilling Offset Location Ground Elevation 481.16 Ground Water Level Measured after completion Boring Methods/Diameter SS/2" & NWD (2.125") Core Date/Time Depth | Elevation | Notes Casing Size 4 inch Casing Depth 22.0 ft 11-8/7:30 AM caved at 5.0 ft Total Depth 28.5 ft Top of Rock 23.5 ft Lithologic Log and Description (CL-ML) s-10 | 3-2-2 466 **GRAVEL WITH** □:`○□ 9 -16 CLAY & SAND: red--16 0.50 brown, wet, compact 9:09 to v. compact (GP-GC) 0.5.0 32 464 9:00 s-11 22-25-28 27 0.7.0 84 -18 -18 --: **CLAYEY GRAVEL** □:``>□ WITH SAND: red-Z:-:Z brown, wet, compact 28 to v. compact (GC) 462 0:00 0.50 29-28-39 s-12 33 58 -20 민 (상:민 -20 0.50 0:00 60 0.50 460 21.0 to 22.1' red P:0 P shale fragments 0.50 140 55 -22 -22 24-58-50/0.1 s-13 <u>-:></u> 22.1 to 23.5' 0.50 advanced with 민상: rotary bit, 458 0.50 probably highly 50/0.0 weathered SANDSTONE: fineshale or -24 grained, red, slightly -24 sandstone, weathered, hard, 30 (clayey gravel deg. dip, several highwith sand?) angle fractures; other 456 discontinuities are along bedding -26 -26 454 -28 -28 0% R-1 96

Attachment 2A Field Boring Logs Phase II



Field Borehole Log

Borehole ID: DH-101

Page 1 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >/= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/25-26/02

DRILLING TIME:

10:19-2:00 (4/25) - 07:15-10:38 (4/26)

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

TUOD

Hollow Stem Auger Continuous Split Spoon

SAMPLING METHOD:

TOTAL DEPTH:

30.5 feet

LOCATION: WEATHER:

Main St., by Magee Center

Cold and wet.

DEP ⁻ (Fee	USC	BLOW S COUNT	RECOVER' (Feet)	Y SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
0 -1	ML	2,2,4	0.5	S-1	SILT: Brown, medium stiff silt. Moist.	Silty
-2 -3	ML	1,1,1	1.0	S-2	SILT AND CLAY: Brown silt and trace clay. Organics (roots). Moist.	Sand (SM)
-4	SM	1/12,1	1.3	S-3	SILTY SAND: Brown silt and fine grain sand. Soft. Loose. Moist.	
-5 -6	SM- SC	1,1,1	1.3	S-4	SILT AND CLAY: Brown fine grain sand and fines (silt and clay). Moist. Soft. S//ty Sand	
-7	ML	1,2,3	1.3	S-5	SILT AND SAND: Brown silt with fine grain sand. Moist. Soft.	
-8 -9	SM	3,1,2	1.2	s-6	SAND AND SILT: Brown fine to medium grain sand and silt. Trace rounded pebbles. Moist Soft.	Permeability test conducted at 7.5 feet.
-10	SM	2,3,3	-	s-7	SAND AND SILT: Brown fine grain sand and silt. Trace gravel, rounded. Moist. Soft.	Sand, tr.
-11	GM-	8.16,16	_	S-8	GRAVEL AND SAND: Mixed gravel, weathered shale, sand and fines. Gray to brown with red. Medium dense.	Permeability test conducted
-13		8,8,10	0.0	S-9	BLANK: No recovery - no description BLANK: Augering only. No sample.	at 12 feet.



Field Borehole Log

Borehole ID: DH-101

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >/= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/25-26/02

DRILLING TIME:

10:19-2:00 (4/25) - 07:15-10:38 (4/26)

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH:

LOCATION: WEATHER:

Continuous Split Spoon

Geo-Environmental

Hollow Stem Auger

30.5 feet

Main St., by Magee Center

Cold and wet.

DEPTH (Feet)		USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-14		SM	22,22,16	1.0	S-10	SILT AND SAND: Brown, red and yellow mottled silt and sand with trace gravel. Gravel medium grain in size and rounded. Moist to dry. Dense. BLANK: Augering only. No sample.	
		GP	16,21,28	1.3	S-11	GRAVEL AND SAND: Sand and gravel. Brown, moist. Rounded grains, poorly sorted, poorly graded. Dense Layey Sandw. gravel BLANK: Augering only. No sample.	
-20		GM-	8,13,13	1.3	S-12	GRAVEL AND SAND: Sand and gravel with fines. Poorly sorted, poorly graded. Rounded to sub-rounded grains. Wet. Medium dense. 5//6/Sand W. gravel BLANK: Augering only. No sample.	Water level at 19.0 feet.
=		GM-	9,20,26	0.7	S-13	GRAVEL AND SAND: Sand and gravel. Sub-rounded, poorly sorted with fines. Wet. Dense. BLANK: Augering only. No sample.	
-24 -25 -26		GM- GC	19,13,31	0.2	S-14	GRAVEL AND SAND: Gravel and sand with fines. Some weathered shale. Brown to gray. Poorly sorted, poorly graded. Wet. BLANK: Augering only. No sample.	
1	0.101.01.0 0.001.01.0 0.001.01.0					GRAVEL AND SAND: Gravel and sand with shale fragments. Poorly sorted	



Field Borehole Log

Borehole ID: DH-101

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >/= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE: DRILLING TIME:

04/25-26/02 10:19-2:00 (4/25) - 07:15-10:38 (4/26) DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

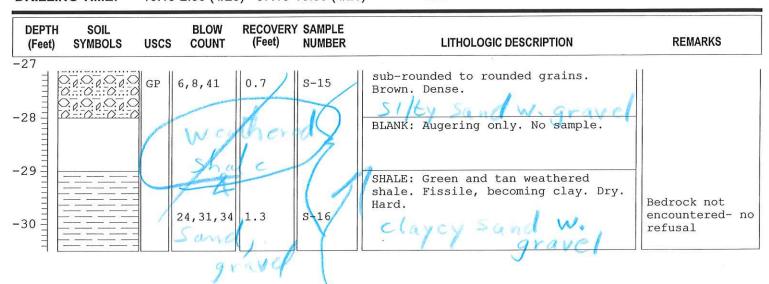
TOTAL DEPTH:

30.5 feet

LOCATION:

Main St., by Magee Center

WEATHER: Cold and wet.



Decomposed shale



Borehole ID: DH -102

Page 1 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 31.7 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/24/02 - 04/25/02

DRILLING TIME:

14:12-16:30 (4/24) - 07:08-9:30 (4/25)

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH:

LOCATION: WEATHER:

Geo-Environmental

Hollow Stem Auger

Continuous Split Spoon

37.2 feet

By Gate 2 of Fairgrounds

Cold and wet.

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
0		GM- GC	4,3,3	1.1	S-1	GRAVEL AND FINES: Rounded gravel and pebbles with fines. Red-brown dry. Medium grained. Very loose.	Augered through 6" asphalt
-2		GM- GC	6,12,9	1.0	S-2	GRAVEL AND FINES: Brown to tan gravel with fines. Rounded gravel and pebbles. Loose. Dry.	(21)
-4		ML	5,2,2	1.0	s-3	SILT: Red-brown silt and trace clay Dry. Very loose. fine Sandy lean	Sandy
-5 -6		ML	2,3,9	1.0	S-4	SILT: Red-brown silt with clay. Dry. Very loose.	(CL-ML)
-7		GM	6,7,13	1.0	S-5	GRAVEL AND FINES: Red-brown gravel and fines. Dry. Rounded gravel and rock. Loose.	DTW = 6.26 feet. Water level taken after coring completed.
-8 -9		GM- GC	19,20,21	0.5	S-6	GRAVEL AND FINES: Brown to tan gravel and fines. Medium grain. Dry. Loose.	Paurly-grad
-10		GM-	9,11,15	0.9	S-7	GRAVEL AND SAND: Brown to gray gravel with sand and fines. Rounded gravel, fine sand. Dry. Loose.	silt, clay
-11						Blank: Augering only. No sample.	
-12 -		CC	11,13,16	0.8	S-8	GRAVEL AND SAND: Brown-red and tan gravel with sand and fines. Rounded stones, fine grained sand. Dry. Loose.	
-13	TO 3.50 3.50 3.50				Tarkinsterior	BLANK: Augering only. No sample,	A CAMPAGE AND A STATE OF THE ST



Borehole ID: DH -102

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 31.7 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/24/02 - 04/25/02

DRILLING TIME:

14:12-16:30 (4/24) - 07:08-9:30 (4/25)

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH:

LOCATION: **WEATHER:**

Geo-Environmental

Hollow Stem Auger

Continuous Split Spoon 37.2 feet

By Gate 2 of Fairgrounds

Cold and wet.

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-15 K		GM-	29,30, 50/5	1.0	S-9	GRAVEL AND SAND: Brown to gray gravel with sand and fines. Rounded stones. Moist. BLANK: Augering only. No sample.	gravel with silt sand
-17		GM-	12,20,20	0.95	S-10	GRAVEL AND SAND: Brown gravel with sand and fines. Rounded gravel and fine grained sand. Moist. BLANK: Augering only. No sample.	clayey
-20		GM-	9,20,16	1.1	s-11	GRAVEL AND SAND: Brown to red gravel with sand and fines and some weathered shale. Dense, medium grained. Wet. BLANK: Augering only. No sample.	Sand (GC)
-21 - 22 - 23 - 23 -			11,14,16	1.3	S-12	SHALE: Green and yellow weathered shale. Fissile. Medium dense. Moist to dry. BLANK: Augering only. No sample.	
-24			16,23,32	2.0	s-13	SHALE: Green and yellow weathered shale. Fissile. Medium dense. Moist to dry. BLANK: Augering only. No sample. SHALE: Green, yellow and tan, mottled, weathered shale becoming	



Borehole ID: DH -102

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 31.7 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY: DRILLING DATE: E. Pacinda

DRILLING DATE:

04/24/02 - 04/25/02

DRILLING TIME:

14:12-16:30 (4/24) - 07:08-9:30 (4/25)

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH:

LOCATION:

WEATHER:

Geo-Environmental

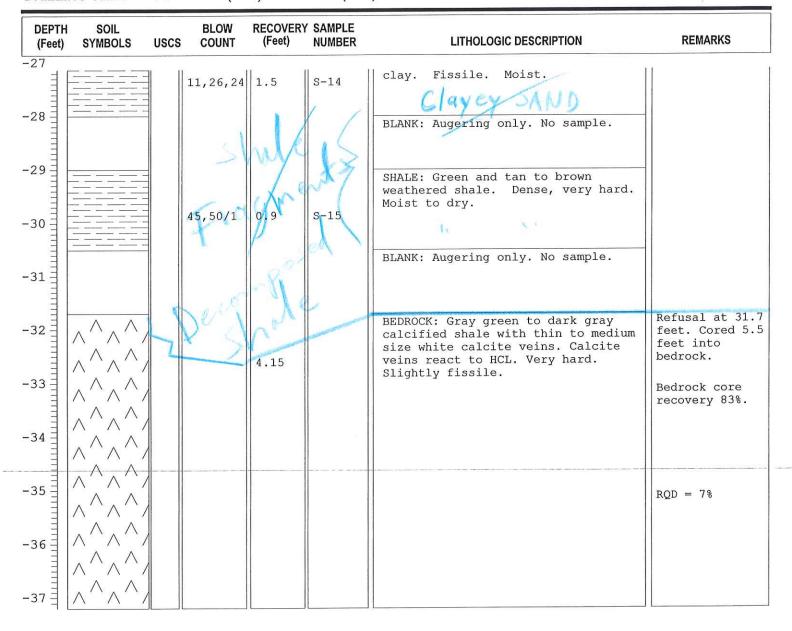
Hollow Stem Auger

Continuous Split Spoon

37.2 feet

By Gate 2 of Fairgrounds

Cold and wet.





Borehole ID: DH - 103

Page 1 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 27.0 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

J. O'Connor

DRILLING DATE:

04/18/02

DRILLING TIME:

15:30 - 18:45

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH:

LOCATION: WEATHER:

Geo-Environmental

Hollow Stem Auger

Continuous Split Spoon

32.0 feet

Fairgrounds

Sunny, warm. 70's

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-1		CL	4,7,8	0.7	S-1	CLAY: Clay- stiff, medium brown. Top few inches gravel fill. Dry.	
-2		СГ	6,3,4	1.0	S-2	CLAY: Clay- medium stiff, medium brown. Dry.	Sandy
-3		CL	6,5,6	0.8	s-3	CLAY: Clay- medium stiff, medium brown. Dry.	CLAY
-5		CL	3,3,3	0.4	S-4	CLAY AND SAND: Medium brown clay. Medium stiff. Dry.	(CL)
-6 -7	7-1-1-1-1-1-1 7-1-1-1-1-1-1-1 7-1-1-1-1-	SW	2,4,5	1.3	s-5	CLAY AND SAND: Medium brown, medium stiff clay changing to sand- fine, medium brown then to fine gravel. Dry.	
-8	7-1-1-1-1-1-1 1-1-1-1-1-1-1-1 1-1-1-1-1-	CL- SM	16,25,28	1.1	s-6	CLAY AND SAND: 0.5 feet- medium stiff, medium brown clay. 0.6 feet- fine to coarse grained sand. Some silt and fines. Dry.	SAND
-10			18,50/4	1.0	S-7	SAND: Sand- medium dense, medium brown, fine to coarse. Some fine to coarse gravel. Trace silt and clay. Last two inches moist.	gravel (SE)
-11						Blank: Augering only. No sample.	DTW= 10.90 feet. Water level taken
-12		SM- SC	16,21,28	1.6	S-8	SAND: Sand- dense to medium brown, fine to coarse. Some fine to coarse gravel. Some silt and clay. Moist	before coring.
-13						BLANK: Augering only. No sample.	



Borehole ID: DH - 103

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 27.0 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

J. O'Connor

DRILLING DATE:

04/18/02

DRILLING TIME:

15:30 - 18:45

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

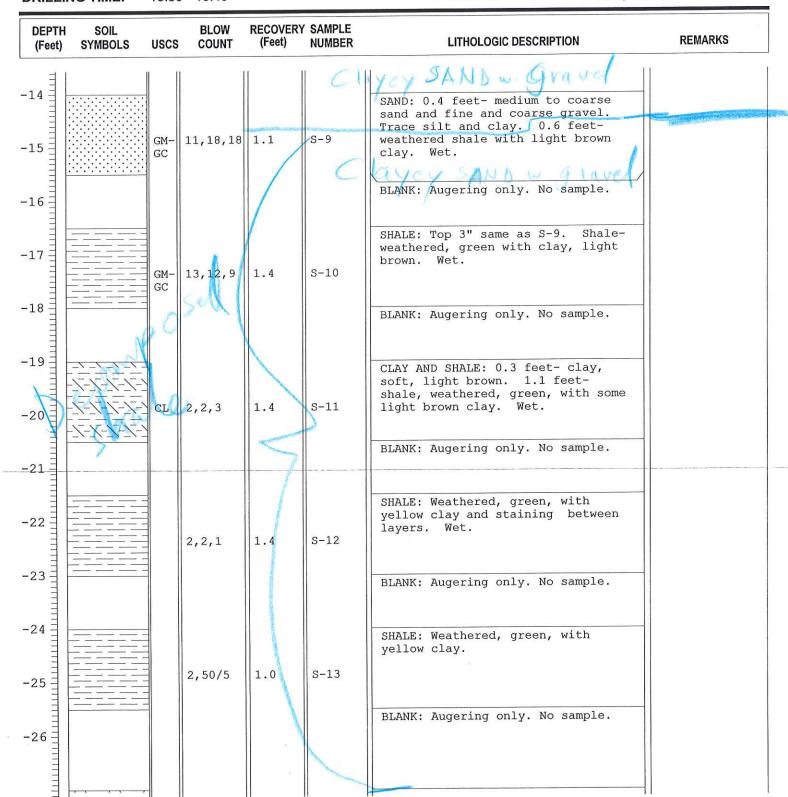
32.0 feet

LOCATION:

Fairgrounds

WEATHER:

Sunny, warm. 70's





Borehole ID: DH - 103

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 27.0 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

J. O'Connor

DRILLING DATE: DRILLING TIME:

04/18/02

15:30 - 18:45

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH:

LOCATION:

WEATHER:

Geo-Environmental

Hollow Stem Auger

Continuous Split Spoon

32.0 feet

Fairgrounds

Sunny, warm. 70's

DEPTH SO (Feet) SYMB		BLOW S COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-28	^ /		4.0		BEDROCK: Calcareous, green-brown shale interbedded with limestone, light brown, with interbedded clay traces.	Refusal at 27.0 feet. Cored 5.0 feet into bedrock
-29 A						Bedrock core recovery 80%
-30 =						RQD = 0%
-31 \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \						



Borehole ID: DH-104

Page 1 of 3

Geo-Environmental

Hollow Stem Auger

32.0 feet

Continuous Split Spoon

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 27.0 feet

SITE LOCATION: Bloomsburg, PA

LOGGED BY: E. Pacinda
DRILLING DATE: 04/22/02

SAMPLING METHOD: TOTAL DEPTH:

DRILLING CO.: RIG TYPE/ METHOD:

LOCATION: Fairgrounds
WEATHER: Cloudy, cold, wet

DRILLING TIME: 13:00 - 17:20

WEATHER: Cloudy, cold, wet

DEPTH SOIL BLOW RECOVERY SAMPLE
(Feet) SYMBOLS USCS COUNT (Feet) NUMBER LITHOLOGIC DESCRIPTION REMARKS

DEPTH (Feet)	SOIL SYMBOLS	uscs	BLOW	(Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
0 -1		ML- CL	4,4,4	0.8	S-1	CLAY: Silty clay, dry, medium stiffness. Brown to medium brown with trace organics.	
-2		ML- CL	2,3,54	0.8	S-2	CLAY: Brown to medium brown, silty clay with trace organics. Dry. Stiff.	
-4		SP	4,4,5	1.3	s-3	CLAY AND SAND: Silty clay, dry, medium stiffness. Brown to medium brown with trace organics. Grades to red-brown, fine grain sand. Homogeneous. Stiff. Dry.	clayey sandw. gravel
-5 -6	<i>ا</i> ل	GM- GC	12,12,14	1.1	S-4	SAND: Red-brown, fine grain sand. Homogeneous. Stiff. Dry. Grades to fine grained sand with gravel and fines. Poorly sorted. Dry. Very stiff.	DTW = 5.3 feet. Water level taken after coring.
 		SP	15,23,24	1.1	S-5	SAND AND GRAVEL: Fine grained sand with gravel. Poorly sorted, rounded to well-rounded, Very stiff. Dry. Some silt.)
~ = I		SM	8,19,16	1.1	S-6	SAND AND GRAVEL: Fine grained sand with gravel. Poorly sorted, rounded to well-rounded, Very stiff. Dry. Little silt.	
			15,23,24	-	s-7	SAND AND GRAVEL: Fine grained sand with gravel. Poorly sorted, rounded to well-rounded. Dense. Dry. Little silt.	Recovery not measured.
-11 🗒					Anne process of the last of th	Blank: Augering only. No sample.	
-12		SM	17,21,22	0.9	S-8	SAND AND GRAVEL: Fine grained sand with gravel. Poorly sorted, rounded to well-rounded, Hard. Dry. Little silt. Last 5 inches wet. BLANK: Augering only. No sample.	clayer, grabelw, sand



Borehole ID: DH-104

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 27.0 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/22/02

DRILLING TIME:

13:00 - 17:20

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH:

LOCATION:

WEATHER:

Geo-Environmental

Hollow Stem Auger

Continuous Split Spoon

32.0 feet

Fairgrounds

Cloudy, cold, wet

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-15		SM	17,14,18	1.0	S-9	GRAVEL AND SAND: Fine grained sand with gravel. Poorly sorted, rounded to well-rounded. Dense. Wet. BLANK: Augering only. No sample.	(clayey) gravel Sound
-17		24	22,27,29	1.2	S-10	SHALE: Brown to red weathered shale with clay. Hard. Moist. BLANK: Augering only. No sample.	
-19 -20 -21		1	6,5,5	1.0	S-11	SHALE: Yellow weathered silt becoming clay. Stiff. Moist. BLANK: Augering only. No sample.	
-22			1,5,17	1.0	S-12	SHALE: Yellow weathered silt becoming clay. Stiff. Moist. Last 2" gray in color with less clay. Very stiff. Wet. BLANK: Augering only. No sample.	DTW = 22.5 feet. Water level taken before coring.
-24 -25 -26			50/5	0.3	S-13	SHALE: Gray weathered shale. Very stiff. Wet. CANAL	
207	===		50/3	0.0	S-14	SHALE: Gray, weathered shale. Very stiff. Wet. Wet.	State



Borehole ID: DH-104

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 27.0 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda 04/22/02

DRILLING DATE:
DRILLING TIME:

13:00 - 17:20

DRILLING CO.:

__

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

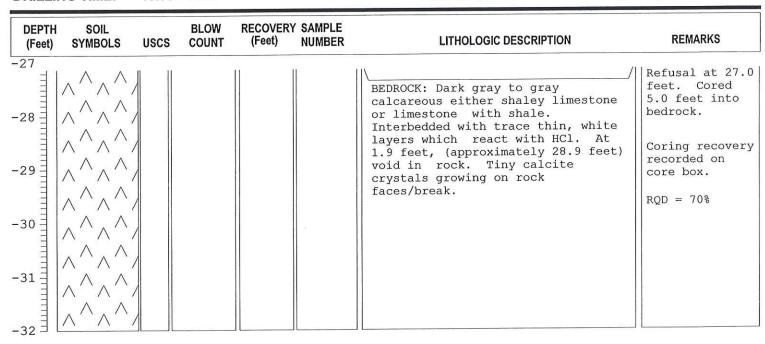
32.0 feet

LOCATION:

Fairgrounds

WEATHER:

Cloudy, cold, wet





Borehole ID: DH - 105

Page 1 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY: **DRILLING DATE:** E. Pacinda

04/23/02

DRILLING TIME:

7:00-10:30

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

30.5 feet

LOCATION:

Fairgrounds

WEATHER:

Cloudy, cool.

DEPTH (Feet)	SOIL SYMBOLS	uscs	BLOW COUNT	RECOVER\ (Feet)	/ SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
0		ML	5,10,10	0.6	S-1	SILT AND GRAVEL: Red-brown clay- like silt with angular gravel. First 1-2 inches with organics (soil). Dry.	V. Sand &
-2			12,5,5	0.0			No recovery due to broken basket.
-3		ML- CL	2,2,10	0.9	S-2	SILT AND CLAY: Red-brown silt and clay. Very fine and homogeneous. Dry. Stiff. Low plasticity.	W. sand
-5		ML- CL	2,3,5	1.1	S-3	SILT AND CLAY: Red-brown silt and clay. Homogeneous. Medium stiffness. Dry. Low plasticity.	to grand
-7		ML- CL	3,4,8	1.0	S-4	SILT AND CLAY: Brown and gray mottled silt and clay - high silt. Dry. Stiff. Low plasticity.	(t) Ct
-8		ML- CL, GP	11,15,17	1.4	S-5	SAND AND SILT: First 4" mottled clay and silt. Remaining is fine grained sand and rounded gravel. Poorly sorted. Brown to gray in color. Dry to moist.	
		GP	6,18,25	1.2	S-6	GRAVEL AND SAND: Poorly sorted, brown to gray sand and gravel. Dry to moist. Blank: Augering only. No sample.	DTW= 10.4 feet. Water level
-11	- a. V a. V a. V					The second secon	taken after
31		ML-	11,17,23	1.3	s-7	GRAVEL AND SAND: 4" of silt and clay. 4" of fine-grained sand and gravel. Rest is fine-grained, homogeneous sand. Brown to gray. Wet to saturated. BLANK: Augering only. No sample.	Szek Newk



Borehole ID: DH - 105

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE: DRILLING TIME:

04/23/02

7:00-10:30

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

30.5 feet

LOCATION: **WEATHER:**

Fairgrounds Cloudy, cool.

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-15 = 10		GM-	18,17	0.7	S-8	GRAVEL AND SAND: Red-brown gravel, sand, and fines. Poorly sorted, rounded with fine sand. Wet. BLANK: Augering only. No sample.	gradel W. Silt &
-17		SM	10,30,32	1.1	S-9	SAND: 2" of brown, fine-grained homogeneous sand. Remaining is brown sand with gravel and fines. Poorly sorted, rounded. Wet. BLANK: Augering only. No sample.	
-1920 - : : : : : : : : : : : : : : : : : :		GM- GC	17,36,45	1.1	s-10	SAND: 3" of fine-grained sand. Remaining is gravel, sand, and fines. Shale interbedded. Poorly sorted, rounded stones. Brown in color. Wet. BLANK: Augering only. No sample.	
-22 - C		GM-	16,20,27	1.0	S-11	GRAVEL AND SAND: Poorly sorted gravel, sand, and fines. Rounded. Brown in color. Wet. Shale interbedded. BLANK: Augering only. No sample.	
-24 -25 -26		SP	5,3,3	0.3	s-12	SAND: Fine-grained, homogeneous brown and gray sand. Wet. BLANK: Augering only. No sample.	
						SHALE: 3" of fine-grained homogeneous sand. Brown. Remaining	



Borehole ID: DH - 105

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/23/02

DRILLING TIME:

7:00-10:30

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

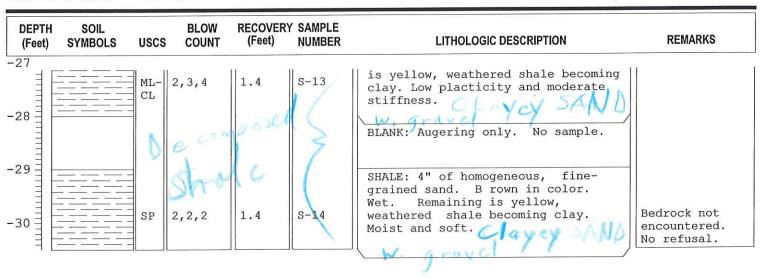
30.5 feet

LOCATION:

Fairgrounds

WEATHER:

Cloudy, cool.





Borehole ID: DH-106

Page 1 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 23 feet SITE LOCATION: Bloomsburg, PA LOGGED BY: J. O'Connor

DRILLING DATE: 04/19/02 **DRILLING TIME:** 07:25 - 11:15

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD: SAMPLING METHOD:

Hollow Stem Auger Continuous Split Spoon

TOTAL DEPTH:

28.0 feet

LOCATION:

Fairgrounds Sunny, hot

WEATHER:

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	/ SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-1		CL	11,5,3	0.9	s-1	FILL AND CLAY: 0.6 feet- Fill beneath roadway.0.3 feet- Claymedium stiff, light brown. Dry.	
-2		CL	3,3,3	1.1	s-2	CLAY: Medium stiffness. Light brown to red in color. Dry.	
-3		CL	5,5,7	1.1	s-3	CLAY: Stiff, light brown to red in color. Trace sand grading to fine sand. Some silt and clay. Dry.	SAVB W.
-5		sc	9,13,14	1.3	S-4	SAND: Dense, medium brown, fine to coarse-grained sand and gravel. Some clay. Dry. Last 2 inches wet.	gravor
-6 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1		GC	10,15,18	0.8	S-5	SAND: Medium dense, light brown, medium to coarse grained. With fine to coarse-grained gravel. Some clay. Wet.	
-8		GC	9,15,22	1.0	S-6	SAND: Medium dense, medium brown, fine to coarse-grained sand and fine to coarse-grained gravel. Some clay. Wet.	GRAVIS U w. silt&
-10		GC	9,16,18	0.7	s-7	SAND: Medium dense, medium brown, fine to coarse-grained sand and fine to coarse-grained gravel. Some clay. Wet.	sand
-11	*,*,*,*,*,*,*,*,*					Blank: Augering only. No sample.	DTW= 11.29 feet. Water
-12		sc	16,18,28	1.0	S-8	SAND: Dense, medium brown, fine to coarse-grained with some clay. 0.3 foot lense-no clay, some fine t coarse grained gravel. Wet.	level taken before coring.
-13						BLANK: Augering only. No sample.	



Borehole ID: DH-106

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 23 feet SITE LOCATION: Bloomsburg, PA J. O'Connor LOGGED BY:

DRILLING DATE: **DRILLING TIME:**

04/19/02 07:25 - 11:15 **DRILLING CO.:**

Geo-Environmental **RIG TYPE/ METHOD:**

Hollow Stem Auger Continuous Split Spoon

SAMPLING METHOD: TOTAL DEPTH:

28.0 feet

LOCATION: WEATHER:

Fairgrounds Sunny, hot

DRILLIN	G TIME:	07.20	o - 11:15		- 8	WEATHER: Sunny, no	
DEPTH (Feet)	SOIL SYMBOLS	uscs	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-14		SC	16,28,32	0.7	S-9	SHALE: Weathered, green with fine to coarse-grained sand. Trace gravel. Wet. BLANK: Augering only. No sample.	۲,
-17		GC	19,22,16	1.1	S-10	SAND: Coarse, medium brown with fine gravel. Some coarse gravel. Some weathered shale. Trace clay. Wet. BLANK: Augering only. No sample.	11
-20		SC	19,21,36	0.7	S-11	SAND: Medium brown, fine to coarse grained with some gravel, some shale, and limestone fragments. Some clay. Wet. BLANK: Augering only. No sample.	
-22			5,6,50/5	11	S-12	SHALE: Green-brown, very weathered with yellow clay. Some limestone fragments. Wet. BEDROCK: Black, shaley, hard	Refusal at 23.0
-24				1.2	RW-1	limestone with interbedded yellow clay BEDROCK: Gray, shaley, hard limestone with rocks and interbedded clay traces.	feet. Cored 5.0 feet into bedrock. Bedrock core recovery = 61%
-26							



Borehole ID: DH-106

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 23 feet SITE LOCATION: Bloomsburg, PA

LOGGED BY: DRILLING DATE: J. O'Connor 04/19/02

DRILLING TIME:

07:25 - 11:15

DRILLING CO.:

RIG TYPE/ METHOD:

SAMPLING METHOD:

TOTAL DEPTH: LOCATION:

WEATHER:

Geo-Environmental

Hollow Stem Auger

Continuous Split Spoon 28.0 feet

Fairgrounds
Sunny, hot

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
27	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			1.9	RW-2		



Borehole ID: DH - 107

Page 1 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/23/02

DRILLING TIME:

09:36 - 11:35

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

.__

Hollow Stem Auger

SAMPLING METHOD: TOTAL DEPTH: Continuous Split Spoon

TOTAL DEF III.

30.5 feet

LOCATION:

By Landfill, Behind Fairgrounds.

WEATHER: Cloudy, cool.

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	/ SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
0 = [4,8,10	1.2	S-1	SHALE: Top 3" soil and gravel with organics. Remaining weathered shale, mottled in color. Stiff. Dry.	Clayey 5AND a. gravel
-2			7,13,10	1.1	S-2	SHALE: 1" of soil with organics. Remaining is weathered shale, mottled. Dry.	- 11 18
-3		ML	2,2,2	0.3	s-3	SHALE: Weathered, mottled shale. Dry.	lean CLAY
-5		ML-	1,2,1	0.8	S-4	SILT AND CLAY: Mottled silt and clay. Grades to dark gray. Soft and sticky with low plasticity. Moist.	(SI JEAND)
-6 = -7 =		ML-	2,3,3	1.3	s-5	SILT AND CLAY: Mottled silt and clay wiith trace organincs. Black in color. Moderate stiffness with low plasticity. Dry.	to sugar on a great of
-8		ML-	2,3,4	1.4	S-6	CLAY: Mottled gray and brown soft clay with organics. Low plasticity. Dry.	X-1
-9 -10		CL	1,2,1	0.9	S-7	CLAY: Dark gray and brown clay with some organics. Low plasticity. Dry. Soft.	÷ 1
-11						Blank: Augering only. No sample.	
-12		ML-	1,1,1	1.3	S-8	CLAY AND SILT: Dark gray, very soft, silt and clay. Trace organics. Low plasticity. Moist.	पत्
-13	工:工:工:					BLANK: Augering only. No sample.	



Borehole ID: DH - 107

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION: Bloomsburg, PA

LOGGED BY: E. Pacinda
DRILLING DATE: 04/23/02
DRILLING TIME: 09:36 - 11:3

acinda TOTAL DEPT

09:36 - 11:35 **WEATHE**

DRILLING CO.: Geo-Environmental
RIG TYPE/ METHOD: Hollow Stem Auger
SAMPLING METHOD: Continuous Split Spoon

TOTAL DEPTH: 30.5 feet

LOCATION: By Landfill, Behind Fairgrounds.

WEATHER: Cloudy, cool.

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-15		GM- GC	17,21,25	1.3	S-9	GRAVEL AND SAND: Wet sand, gravel, and fines. Gray-brown. Last 3" dry, mottled (orange, yellow, brown) silt and clay with interbedded shale. Low plasticity. BLANK: Augering only. No sample.	d
-17		GM- GC	50/5	0.5	S-10	SAND: 1" brown gravel, sand, and fines. Wet. Remaining white quartz sand. Well rounded, poorly sorted, with small to medium grain. Wet.	DTW = 17.25
-19 -20 -21	12-12-12-12-12-12-12-12-12-12-12-12-12-1	SW	8,11,11	1.0	S-11	CLAY AND SAND: 4" fine to medium-grained, gray to brown sand. Rounded. Wet. Remaining is mottled (yellow, green, rusty red) weathered shale becoming clay with medium-size rounded pebbles. BLANK: Augering only. No sample.	
	7-7-7-7-7-7 72-7-7-7-7-7-7 72-7-7-7-7-7-		27,50/5	0.4	S-12	CLAY AND SAND: 1.5" fine-grained, subrounded sand. Brown to gray in color. Remaining is mottled, weathered shale becoming clay. BLANK: Augering only. No sample.	
-24 -25 -26			7,11,15	0.9	s-13	SHALE: 3" of fine-grained, gray sand. Wet. Remaining is yellow and orange mottled, weathered shale with rounded, medium-sized pebbles. Wet. BLANK: Augering only. No sample.	
-27						SAND: Rusty, red to brown graded sand. Rounded to subrounded.	



Borehole ID: DH - 107

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/23/02

DRILLING TIME:

09:36 - 11:35

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

30.5 feet

LOCATION: WEATHER:

By Landfill, Behind Fairgrounds.

Cloudy, cool.

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVER (Feet)	Y SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS	
			7,1,21	1.1	S-14	Medium to large size grains. Wet.		
-30			5,7,10	1.8	S-15	SAND AND SILT: 10" of rounded to subrounded, fine-grained sand with silt. Brown to gray. Wet. Remaining is mottled, sticky, weathered shale becoming clay. Low plasticity. Stiff.	Bedrock not encountered. refusal.	No

29.8 decomposed

1 can CLAY



Borehole ID: DH - 108

Page 1 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/23/02

DRILLING TIME:

13:14 - 15:30

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

30.5 feet LOCATION:

By Landfill, Behind Fairground

WEATHER:

Cloudy, cool.

DEPTH (Feet)	SOIL SYMBOLS	uscs	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION REMARKS
0			5,6,6	1.3	S-1	SILT: 4" of soil with organics and fill material (glass and coal ash) Remaining is dry, fine silt. Brown and moderatly stiff.
-2		ML- CL	3,4,4	1.1	S-2	CLAY AND SILT: Dry, brown silt and clay with trace organics. Becoming mottled. Low plasticity and medium stiffness.
-3		CL- ML	3,4,5	1.2	s-3	CLAY AND SILT: Mottled clay with silt and trace organics. Brown and gray in color. Low plasticity stiff. Dry.
-5		ML- CL	4,5,5	6.9	S-4	CLAY AND SILT: Dry, mottled brown and gray clay and silt. Last 3" are very fine-grained, homogeneous sand and silt. Brown. Moist.
-7		GM	8,13,16	1.1	s-5	GRAVEL AND SAND: 2" of brown, silt and fine-grained sand. Remaining is gravel with sand and silt. Angular to rounded and brown in color. Moist.
-8		GM	10,12,7	0.7	S-6	SHALE: Weathered gray shale. Wet. Last 2" are poorly sorted, rounded gravel. Small to medium in size with sand and silt.
-10		ML, SP- SM	13,26,20	1.0	S-7	SILT: Brown to gray, weathered silt Fine-grained sand with rounded pebbles and silt. Wet.
-11					- Change	Blank: Augering only. No sample.
-12		CC	10,26,11	1.1	S-8	GRAVEL AND SAND: 2" of fine to medium grain, brown sand. 6" of mixed gravel, sand, and fines. Brown, well-rounded to rounded with some weathered shale. Remaining is very-fine sand.



Borehole ID: DH - 108

Page 2 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/23/02

DRILLING TIME:

13:14 - 15:30

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

LOCATION:

30.5 feet

By Landfill, Behind Fairground

Cloudy, cool. WEATHER:

DEPTH (Feet)	uscs	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-14	GM- GC	28,42, 50/2	0.9	S-9	BLANK: Augering only. No sample. SAND AND SILT: 3" of brown, fine grain sand with silt. Remaining is mix of weathered shale, rounded gravel, sand, and fines. Wet. BLANK: Augering only. No sample.	17
-16 = -17 = -18 = -18	SM- SC	9,10,10	0.5	S-10	SAND: Fine to medium-grained sand with fines. Homogeneous. Wet. BLANK: Augering only. No sample.	
-19	SM	2,3,3	1.4	s-11	SAND AND SILT: Gray to dark gray in color. Moist. BLANK: Augering only. No sample.	
-21	ML- CL	5,8,8	1.7	S-12	CLAY AND SILT: Dark gray. Homogeneous. Moist. BLANK: Augering only. No sample.	
-24 -25 -26	ML- CL	6,6,6	0.9	s-13	CLAY AND SILT: Dark gray. Homogeneous. Moist. BLANK: Augering only. No sample.	
					CLAY AND SILT: Dark gray. Homogeneous.Trace sand grains.	DTW = 26.5 feet



Borehole ID: DH - 108

Page 3 of 3

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: >= 30.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

E. Pacinda

DRILLING DATE:

04/23/02

DRILLING TIME:

13:14 - 15:30

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

30.5 feet

LOCATION: WEATHER:

By Landfill, Behind Fairground

Cloudy, cool.

DEPTH (Feet)	SOIL SYMBOLS	uscs	BLOW COUNT	RECOVER' (Feet)	Y SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
-27 -28		ML- CL	5,5,6	0.9	S-14	Moist. Company BLANK: Augering only. No sample.	-
-30		ML- CL	8,20,22	1.3	s-15	CLAY AND SILT: Dark gray with some organics. Limestone fragment found at bottom of boring.	Bedrock not encountered. No Refusal.



Borehole ID: DH - 116

Page 1 of 2

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 20.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

B. Hallam

DRILLING DATE:

04/29/02

DRILLING TIME:

12:30 - 15:11

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

TOTAL DEPTH:

25.5 feet

LOCATION: WEATHER:

By Landfill, Behind Fairgrounds.

Cloudy, cold.

DEPTH (Feet)	SOIL SYMBOLS	USCS	BLOW COUNT	RECOVERY (Feet)	SAMPLE NUMBER	LITHOLOGIC DESCRIPTION	REMARKS
0		ML	2,7,8	1.0	S-1	SILT AND GRAVEL: Brown silt and gravel with organics. Soft to medium. Coal and red shale fragments. Dry.	
-2		ML	3,3,4	0.5	S-2	SILT: Brown silt and medium, rounded to well- rounded gravel. Poorly sorted. Dry.	DTW = 1.51 feet. Water level taken after coring.
-4		ML	4,3,3	0.8	s-3	SILT: Light brown to tan, mottled silt. Dry.	
-5		ML	3,4,3	0.7	S-4	SILT: Dark gray silt with medium stiffness. Dry.	
-6 ·		ML	2,5,9	1.1	S-5	SILT: Light gray silt with organics Medium stiff to stiff. Dry.	
-8		ML	5,9,11	1.3	s-6	SILT: Light gray silt with organics Stiff. Dry.	SILLAY
-9 -10		ML	3,6,6	1.3	S-7	SILT: Light gray silt with organics Mottled, with medium stiffness. Dry.	to. Sand
-11						Blank: Augering only. No sample.	
-12		CL-	2,1,2	1.4	S-8	CLAY AND SILT: Gray silt and clay with low placticity. Moist and soft.	Tean
-13	: + : + : + : : : : : : : = : =	ML			and the situation of the situation of the	BLANK: Augering only. No sample.	CLAYTY



Borehole ID: DH - 116

Page 2 of 2

PROJECT NAME/ NUMBER: PA DEP Bloomsburg / 601-0100

THICKNESS OF OVERBURDEN: 20.5 feet

SITE LOCATION:

Bloomsburg, PA

LOGGED BY:

B. Hallam

DRILLING DATE:

04/29/02

DRILLING TIME: 1

12:30 - 15:11

DRILLING CO.:

Geo-Environmental

RIG TYPE/ METHOD:

Hollow Stem Auger

SAMPLING METHOD:

Continuous Split Spoon

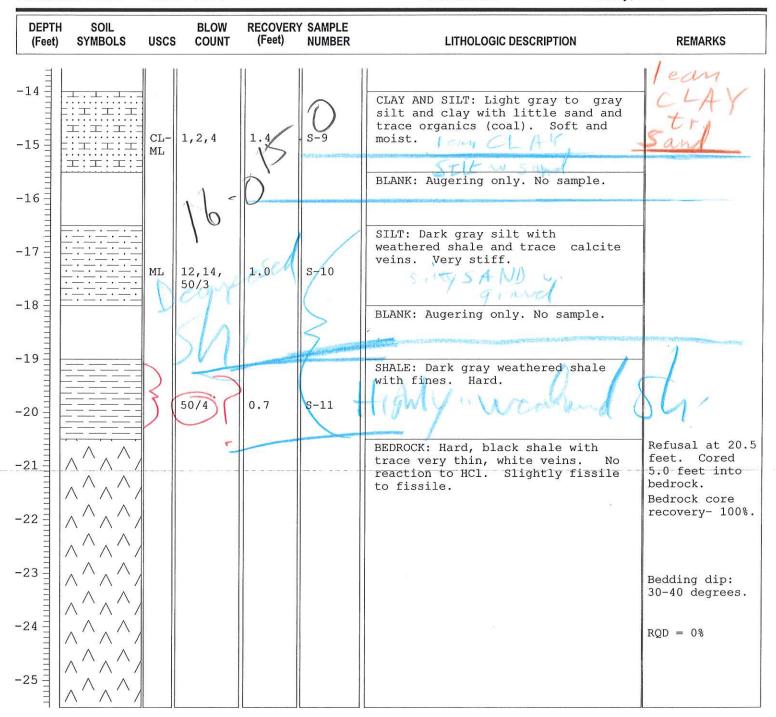
TOTAL DEPTH:

25.5 feet

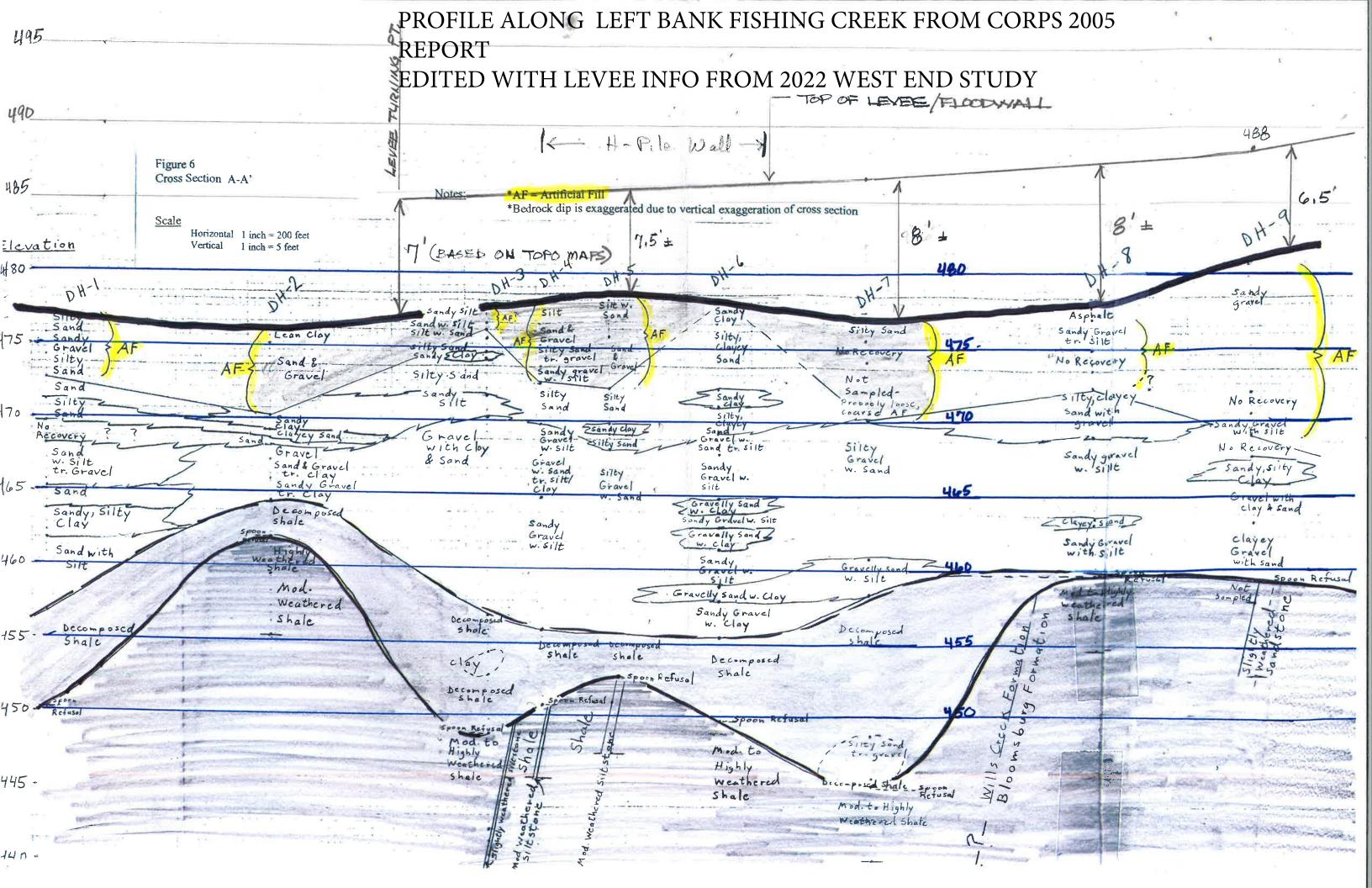
LOCATION:

By Landfill, Behind Fairgrounds.

WEATHER: Cloudy, cold.



Attachment 3 Phase I Geologic Profile



WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY, PENNSYLVANIA

Appendix C Environmental and Regulatory Compliance

WEST END FLOOD MITIGATION STUDY

Appendix C

Environmental and Regulatory Compliance

TABLE OF CONTENTS:

1.	LOCATION / DESCRIPTION OF THE STUDY AREA
2.	LOCATION / DESCRIPTION OF THE STUDY AREA
3.	PHYSICAL SETTING
4.	CLIMATE AND WEATHER
5.	WATER RESOURCES
6.	BIOLOGICAL RESOURCES. 6A. VEGETATION. 6B. WETLANDS. 6C. WILDLIFE. 6D. FISH. 6E. THREATENED AND ENDANGERED SPECIES.
7.	AIR QUALITY
8.	CULTURAL RESOURCES 8A. ARCHAEOLOGICAL INVESTIGATIONS 8B. ARCHITECTURAL INVESTIGATIONS 8C. OTHER KNOWN HISTORIC SITES
9.	HAZARDOUS, TOXIC AND RADIOACTIVE WASTE
10.	SOCIOECONOMICS
11.	ENVIRONMETNAL JUSTICE
12.	NOISE
13.	TRAFFIC
14.	AESTHETICS
15.	LAND USE
16.	PARKS AND RECREATION

LIST OF ATTACHMENTS

- 1. THE BLOOMSBURG, PENNSYLVANI, FLOOD DAMAGE REDUCTION FEASIBILITY STUDY (2005 CORPS REPORT)
- 2. PNDI RECEIPT PROJECT SEARCH ID: PNDI-742254
- **3.** PHMC SUMMARY LETTER ER PROJECT #2021PR06578

WEST END FLOOD MITIGATION STUDY

Attachment C

Environmental and Regulatory Compliance

1. LOCATION / DESCRIPTION OF THE STUDY AREA

Bloomsburg is located in the north central portion of the Commonwealth of Pennsylvania approximately 40 miles west of Scranton and 90 miles northwest of Harrisburg, Pennsylvania. The study area is in the Upper Susquehanna Basin along the North Branch of the Susquehanna River, approximately 8 miles above its confluence with the West Branch at Sunbury.

The primary focus of the study was the communities located along both banks of Fishing Creek from the Railroad Street Bridge to Fishing Creek's confluence with the Susquehanna River. The Townships of Hemlock and Montour are situated along the north bank of Fishing Creek whereas the West End of the Town of Bloomsburg and the Fairgrounds are located on the south bank of the creek. The remainder of the study area south of the creek is primarily comprised of open fields which serve as parking for Fairground events as shown below.

Study Area

West End - Floodplains of:

- · Town of Bloomsburg
- · Hemlock Township
- Montour Township

Approximately 500 Parcels

- Bloomsburg 286
- · Hemlock 131
- · Montour 80

349 Parcels with Structures

- · Bloomsburg 271
- Hemlock 42
- Montour 36



Fishing Creek flows into the Susquehanna River and is generally aligned north to south downstream (south) of SR 0011 (Main Street). Upstream (north) of SR 0011 Fishing Creek bends to the east,

flowing parallel to SR 0011, north of the roadway. Upstream of the Railroad Street Bridge, Fishing Creek turns back to the north. Given the proximity of the site to the Susquehanna River and Fishing Creek, the west end is subject to extensive flooding from the river and the creek.

2. BASELINE CONDITIONS / AFFECTED ENVIRONMENT

In April 2005, "The Bloomsburg, Pennsylvania, Flood Damage Reduction Feasibility Study" (Corps Report) was issued by the U.S. Army Corps of Engineers. The study area for that study included generally the same area as this West End study. Data presented in the 2005 Corps study was utilized for this study, updated when necessary. The areal extent of lands that experienced flooding in 2011 is considered the study area. This section describes existing conditions and possible constraints on mitigation proposals.

The 2005 Corps Report is referenced and will not be re-written in this section if environmental conditions have not changed or if particular studies were not suitable at this phase of the project. However, nearly two decades have elapsed since that study was conducted and some environmental findings have changed since that time and will be discussed in this section. The description provides a baseline for measuring expected changes in the physical, environmental, cultural, social, and economic settings that would result from implementation of a flood damage reduction project in the study area.

3. PHYSICAL SETTING (See 2005 Corps Report for Physiography, Geomorphology, and Soils)

4. CLIMATE AND WEATHER

Climate and weather patterns have changed over the last 20 years and so have some of the statistics for Bloomsburg since the 2005 Corps Report. In Bloomsburg. The summers remain warm and wet, while winters are cold and snowy, and it is partly cloudy year-round. Variations in temperatures and precipitation trends have changed over this period. Over the course of the year, the temperature typically varies from 21°F to 84°F and is rarely below 6°F or above 92°F. The warm season lasts for 3.7 months, from May 25 to September 15, with an average daily high temperature above 74°F. The hottest month of the year in Bloomsburg is July, with an average high of 83°F and low of 63°F. The cold season lasts for 3.2 months, from December 1 to March 6, with an average daily high temperature below 44°F. The coldest month of the year in Bloomsburg is January, with an average low of 22°F and high of 35°F.

A wet day in Bloomsburg is one with at least 0.04 inches of liquid or liquid-equivalent precipitation. The chance of wet days in Bloomsburg varies throughout the year. The wetter season lasts 4.8 months, from April 2 to August 29, with a greater than 30% chance of a given day being a wet day. The month with the most wet days in Bloomsburg is June, with an average of 11.5 days with at least 0.04 inches of precipitation. The drier season lasts 7.1 months, from August 29 to April 2. The month with the fewest wet days in Bloomsburg is January, with an average of 6.5 days with at least 0.04 inches of precipitation. The month with the most days of rain alone in Bloomsburg is June, with an average of 11.5 days.

Bloomsburg experiences *significant* seasonal variation in monthly rainfall. Rain falls throughout the year in Bloomsburg. The month with the most rain in Bloomsburg is *September*, with an average rainfall of 3.7 *inches*. The month with the least rain in Bloomsburg is *February*, with an average rainfall of 1.6 *inches*. Bloomsburg experiences significant seasonal variation in monthly snowfall as well. The snowy period of the year lasts for 5 months, from November to April, with a sliding 31-day

snowfall of at least 1.0 inches. The month with the most snow in Bloomsburg is February, with an average snowfall of 7.1 inches. The snowless period of the year lasts for the other 7 months (weatherspark.com).

5. WATER RESOURCES

Below is a description of the existing water resources in the study area. State and federal surface water listings have changed some since the 2005 Corps Report and are discussed below. However, hydrogeology and groundwater studies were not part of this updated assessment and can be referenced in the 2005 Army Corps Report.

5A. Surface Waters

Bloomsburg is within the Middle Susquehanna River subbasin. In the upper part of the subbasin, the Susquehanna River flows southeast through high, flat-topped plateaus separated by steep-sided valleys. Midway down the basin, the Lackawanna River joins the Susquehanna River before turning and flowing southwest towards Bloomsburg.

The Susquehanna River forms Bloomsburg's southern boundary and is the most prominent drainage feature, draining an area of approximately 10,576 square miles. Fishing Creek forms the northern and western boundary of the Town of Bloomsburg and drains an area of approximately 385 square miles at its confluence with the Susquehanna River. Fishing Creek and its tributaries - Huntington, Greene, Little Fishing, Spruce, and Hemlock Creeks - drain the northern nine townships of Columbia County southward to the bend of the Susquehanna River between Bloomsburg and Catawissa.

The middle Susquehanna River sub-basin is a mixture of urban and rural lands that include forest, agriculture, abandoned mines, and urban development. A section of this subbasin was heavily mined and remnants of mining activities (e.g., coal slag piles, abandoned mines, and acid mine drainage) still impact the water quality of many miles of streams and rivers throughout the Wyoming Valley (SRBC, 2002).

According to PA DEP's eMAP website, Susquehanna River in this stretch of Bloomsburg also has an attaining use of "impaired" with the source cause being unknown with polychlorinated biphenyls (PCBs) and also having an unknown source of Mercury.

Impairment status of Fishing Creek has changed for the better since the 2005 Corps Report. In the previous study, various reaches of Fishing Creek were listed on the PA-DEP 303(d) Impaired Streams and Rivers List (PADEP, 2002). Several reaches were listed for violations of Aquatic Life Use based on siltation from agriculture, road runoff, and removal of vegetation. Additionally, one reach of Fishing Creek (#20020111-1226-FIT) was listed for violations of Human Health Uses due to mercury. Little Fishing Creek, which flows into Fishing Creek at Bloomsburg, was also listed for violations related to Recreational Use due to pathogens. According to PA DEP's eMAP website, Fishing Creek in the stretch of Bloomsburg has an attained use of supporting aquatic life, potable water use, and fish consumption; and it is not listed as impaired.

6. BIOLOGICAL RESOURCES

- **6A.** Vegetation (previously addressed in the 2005 Corps Report)
- **6b.** Wetlands (previously addressed in the 2005 Corps Report)

Wetlands were noted in the 2005 Corps Report in the study area. An updated wetland delineation will need to be completed for any projects identified for advancement to preliminary design. Permitting involving anticipated wetland and stream impacts by any proposed structural components of a levee within Fishing Creek and its floodway, as well as any channel modifications to Fishing Creek. Early coordination with agencies such as the Army Corps of Engineers, PA Department of Environmental Protection and PA Fish and Boat Commission will be key to the success of this project in order to ensure all regulatory compliance requirements are met.

Field investigations were conducted along the project area in June 2003 by others to assess and determine the presence/absence of wetlands. The specific area investigated included the footprints and vicinities of two levee alignment corridors under consideration. The wetlands investigation was conducted in accordance with the "Corps of Engineers Wetland Delineation Manual," Technical Report Y-87-1, and specific regulatory guidance modifications subsequently issued.

Within the expected areas of disturbance, wetlands were identified only along the southeastern side of the Bloomsburg Fairgrounds property and delineated using a global positioning system unit. The 11 mapped wetlands (labeled A through K) are shown in Figure 2-3 of the 2005 Corps Report. The wetlands were further characterized as palustrine emergent wetland (PEM), palustrine shrub-scrub wetland (PSS), and palustrine forested wetland (PFO) characterized according to their cover type (Cowardin, 1979). The hydrologic source for these wetlands appears to be from local surface runoff (from parking lots and landfills) and a surface and groundwater connection to Snyder's Run.

In November 2004, a forested wetland system was identified along Fishing Creek's floodplain across the creek from the water treatment plant. This is a typical forested floodplain wetland (PFO) several acres in size with hydrology from both groundwater and overbank flooding from the Creek.

6C. Wildlife (previously addressed in the 2005 Corps Report)

6D. Fish

The previous 2005 Corps Report discussed the fish collected during a survey of Fishing Creek in 1998. The species list indicated that a cool/coldwater fishery existed at that time, and that the coldwater fish, (e.g., trout) were stocked (unknown if natural reproduction was occurring). According to the current PADEP eMapPA, Fishing Creek is listed as a Warm Water Fishery with no special trout listings in the project area by the PA Fish and Boat Commission. However, Fishing Creek is known for its great flyfishing and many public access areas north of Interstate 80 along Fishing Creek, where the stream inhabits both wild trout and stocked trout.

The proposed earthen/MSE/sheet pile levee would have a slight negative effect on Fishing Creek within the building footprint as it would eliminate the riparian corridor on the left bank of the stream, in turn affecting fish and other wildlife inhabiting this stretch. Mitigation assessment protocols regulated by the governing agencies will allow for compensation in the watershed to make up for this alteration.

6E. Threatened and Endangered Species

Except for the occasional transient species, no Federally listed endangered, threatened, or candidate species under U.S. Fish and Wildlife Service (USFWS) jurisdiction are known to exist in the project

area (USFWS, 2000). Therefore, no Biological Assessment or further Section 7 consultation under the Endangered Species Act is required with the USFWS.

However, the Pennsylvania Natural Diversity Inventory (PNDI) indicated that there are potential impacts to state regulated species of special concern within the project area (PNDI, 2022). According to the Pennsylvania Department of Conservation and Natural Resources (PA DCNR), further review of the project is necessary to resolve the potential impact to a "sensitive species" resource with a current status of Special Concern Resource and to the Fassett Jeweled Shooting Star (*Primula fassettii*), a flowering plant with a current status of Threatened.

It is anticipated that a botanical survey will be required for this species, which is time sensitive and would need to occur during its flowering period in late April to May. Further inquiry into the unidentified species is required to determine if a habitat survey will be required.

Pennsylvania Fish and Boat Commission (PFBC) requires further review of the project to resolve the potential impact to the Triangle Floater (Alasmidonta undulata). If in-stream work is to occur as a result of this project, a mussel study may be required. The study period is not time of year sensitive, however, safety concerns for the malacologist would deter the study from being performed in the winter months.

7. AIR QUALITY (See 2005 Corps Report for Air Quality)

8. CULTURAL RESOURCES

BL submitted a project review to the PA Historical and Museum Commission for the Columbia County - West End Flood Mitigation Study (ER Project # 2021PR06578.001) and received a summary letter on November 8, 2021requesting more information for their environmental review due the high probability for archaeological resources.

It was PHMC's opinion that "a Phase IA archaeological study should be undertaken to assess this property's potential for National Register significant archaeological resources. This study should consist of a thorough review of all available historic through recent maps and other documentary sources which may provide information on past land use within the project area. A geomorphological assessment of the project area is recommended at this stage as it will provide useful information on the total depth and overall integrity of potential archaeological deposits. If this research suggests that potentially significant archaeological resources may be present, it will be our opinion that a Phase I archaeological testing plan should be developed to identify such resources."

The 2005 Corps Report has well documented findings from previous studies that will be utilized in the next phase of the project, as to not duplicate moneys and efforts. Historical and archaeological data does not expire and can be used for overlapping project areas. Additional studies outside of the initial APE are anticipated and will need to be addressed with similar studies. The next two sections below were taken from the 2005 Corps Report, addressing the actions that have been taken to date.

8A. Archeological Investigations

Phase IA archaeological investigations were conducted by KAR in 1999 along the project area. The investigated portion runs from the Route 11 / Route 42 interchange, southeast across the Bloomsburg Fairgrounds parking area, and then generally northeast to the area adjacent to the now vacated Windsor Plant. KAR concluded that there was a high potential for significant

archaeological resources in the tested area. The findings were reported to the PA-DEP and the State Historic Preservation Officer (SHPO) in a letter report, dated 16 July 1999 (KAR, 1999). The report recommended Phase IB testing of all undisturbed portions of the tested area.

The Phase IB investigation of the undisturbed portion of the Phase IA-tested area included a series of excavation units dug along two parallel transects within the project area in the vicinity of the Fairgrounds. Tests along each transect were spaced at 60-meter intervals and were staggered so that there was a test every 30 meters along the corridor. Additional test units were dug whenever suspected archaeological materials were identified.

Forty (40) units of the systematic sample were completed, plus five additional units to examine suspected archaeological materials. None of the latter has been found to meet minimum criteria for an archaeological site, as defined by the Bureau for Historic Preservation. The recovered materials include two chert flakes and one apparently worked piece of chert, found in the plow zones of three separate units in the systematic sample. None of the supplemental tests recovered any additional cultural material.

Further Phase I investigations of the remaining portions of the project area were proposed for spring 2005. The remaining portions to be tested include an area northeast of Windsor, and an area adjacent to the left descending bank of Fishing Creek.

8B. Architectural Investigations

During the initial planning stages for this study, the Corps, PADEP and the Pennsylvania State Historic Preservation Office agreed that due to the uncertainty of the Area of Potential Effect (APE) for the project, it would be necessary to document, at least through a Phase I Level survey, all of the potentially affected historic properties up to a level of flooding equal to the 500-year event.

The following resources were identified within the original APE for this project:

The identification and documentation of National Register districts for the West Main Street portion of Bloomsburg, the Village of Femville, and thirty individual structures located throughout the APE. Additionally, other new potential historic districts were identified, which consisted of the North Branch Canal workers housing district, a potential district of post-World War I housing, a potential district encompassing the village of Rupert, and individual forms to document the bridges, rail, and canal resources, Bloomsburg Airport, the Irondale water treatment plant, and Bloomsburg Fairgrounds.

While most of the identified buildings and sites are not located within the project area, the Irondale water treatment plant (currently owned and operated by Suez Water Pennsylvania) is located immediately upstream of the project area.

8C. Other Known Historic Sites

In addition to Bloomsburg's rich background in Native American history, as well as the industrial boom that lasted three-quarters of a century in the 1800's, all of which is discussed in the 2005 Army Corps Report, other very notable historic structures lie within or close to the project area.

Rupert's Covered Bridge, a historically significant bridge spanning Fishing Creek and located downstream of the project area on TR409, was added to the National Register of Historic Places in 1979 and is the oldest existing bridge in Columbia County. Leonard Rupert settled on Fishing Creek

in 1788 and established a village and a ferry where the covered bridge was later built. At just over 185 feet in length, it is Columbia County's longest covered bridge. The bridge has Burr arches with multiple king-post trusses and vertical board siding. After 150 years of continuous use, the bridge was reinforced with steel I-beams and two concrete piers and is open to traffic with no restrictions.

One of the non-structural mitigation options involves Fishing Creek channel modifications. A recent development is the proposed removal of Boone's Dam along Fishing Creek by its' current owner, Suez Water. Boone's Dam is not listed on PHMC's website as a landmark of historic significance. The dam was built in the 1850's to generate power to the mill that Samuel Boone constructed along Fishing Creek. The dam has been associated with the tranquil setting of the property and Boone's Dam Barn, which has been home to many families over the years, the most famous being artist David Armstrong. The current owners of The Barn at Boone's Dam own and operate a wedding venue. The removal of the dam would not impact the flood flows on Fishing Creek.

The study area is near the Delaware, Lackawanna & Western Railroad (also known as the DL&W or Lackawanna Railroad). This was a U.S. <u>Class 1 railroad</u> that connected <u>Buffalo</u>, <u>New York</u>, and <u>Hoboken</u>, <u>New Jersey</u> (and by ferry with <u>New York City</u>), a distance of about 400 miles (640 km). Incorporated in <u>Pennsylvania</u> in 1853 primarily for the purpose of providing a connection between the <u>anthracite coal</u> fields of Pennsylvania's <u>Coal Region</u> and the large markets for coal in New York City, the railroad gradually expanded both East and West, eventually linking Buffalo with New York City.

The Great Warrior Path is also a known historic resource within the project area, with its eligibility noted as undetermined. The Great Warrior Path travels from present day Athens (then known as Tioga) to Sunbury (then known as Shamokin). This path was used in both times of war and in times of peace. It was often frequented by Iroquois ambassadors who were traveling south.

17. HAZARDOUS, TOXIC AND RADIOACTIVE WASTE (see 2005 Corps Report for Hazardous Sites)

In previous studies within the project area, sites of potential concern were identified. In the URS 2003 report, sampling results revealed elevated concentrations of heavy metals in excess of applicable cleanup levels throughout the project area and volatile organics contamination within an area that passes through an inactive landfill (URS, 2003). Since the heavy metals that were detected are likely a local background condition and since much of the contaminated soil along the project area is considered historic fill, it is likely suitable for reuse during the construction of the flood protection elements from a regulatory perspective (URS, 2003).

Contaminated soil in the landfill area is unlike the material found elsewhere within the project area due to the presence of large amounts of debris and is unsuitable for reuse during construction.

The potential impact of underground storage tanks adjacent to the project area along Fishing Creek must be further defined to determine whether relocation or removal is necessary. There is little concern about potential human exposure to contaminants from drinking groundwater because nearly all residences near the proposed alignment are believed to utilize drinking water delivered by Suez Water Pennsylvania (USACE, 2003).

A Phase II Environmental Site Assessment (ESA) is recommended in the next phase of the project within the project limits in order to complete proper site characterization. The Phase II ESA would consist of a subsurface investigation to identify potential contamination sources that may affect the

environmental integrity of the project. The results of the Phase II ESA may be used to ascertain the need for and extent of potential site remediation activities (i.e., Phase III ESA).

10. SOCIOECONOMICS

The Town of Bloomsburg is a rural and moderate density community characterized by attractive single-family residential neighborhoods, tree-lined streets and limited agricultural and industrial land use on the outskirts of town. Bloomsburg is the Columbia County seat and is the only incorporated town in Pennsylvania. The Town has a land area of 4.4 square miles and approximately 4,400 housing units. The Town of Bloomsburg had a population of 14,197 as of July 1, 2021. Bloomsburg ranks in the upper quartile for Population Density and Diversity Index when compared to the other cities, towns and Census Designated Places (CDPs) in Pennsylvania (HomeTownLocator.com).

The age distribution of Bloomsburg has a high proportion of persons in the 18- to 24-year-old category, which would be expected in a town with a moderately sized university. The median household income for Bloomsburg is \$32,217. The economy of Bloomsburg employs about 5,300 people. The largest industries in Bloomsburg are Health Care & Social Assistance, Accommodation & Food Services, and Educational Services, and the highest paying industries are Transportation & Warehousing, & Utilities, Public Administration, and Manufacturing.

11. ENVIRONMENTAL JUSTICE

As stated in the 2005 Corps Report, "Executive Order 12898, Federal Actions to Address Environmental Justice in Minority Population and Low-Income Populations (Executive Order, 1994), directs Federal agencies to identify and address, as appropriate, disproportionately high and adverse human health or environmental effects of their programs, policies, and activities on minority population and low- income populations." According to PADEP eMapPA, the project area is located within an Environmental Justice Area, Census Block Group 2015, Tract 512, Block Group 5 (eMapPA, 2022).

- **12. NOISE** (see 2005 Corps Report for Noise)
- **13. TRAFFIC** (see 2005 Corps Report for Traffic)
- **14. AESTHETICS** (see 2005 Corps Report for Aesthetics)

The proposed West End Flood Mitigation structures of earth levee, MSE levee with retaining wall, sheet pile levee, pump station, and gate closures, all can fit into the surrounding landscape of the Town of Bloomsburg with the proper design.

15. LAND USE (see 2005 Corps Report for Land Use)

16. PARKS AND RECREATION

Several state, local, and private park facilities are located near the study area and have been discussed in the 2005 Corps Report. But the most immediate park that the project will affect in a positive way is the Bloomsburg Fairgrounds. The fairgrounds is a 248-acre facility located within Bloomsburg's town limits and includes a grandstand with an 8,000-person seating capacity,

78,000 square feet of exhibition buildings, an indoor arena, a covered band shell, a half-mile racetrack, and other large outdoor event amenities. The Bloomsburg Fair begins the third Saturday after Labor Day and draws over 650,000 people (2003 estimate) from all along the Eastern Seaboard. The Fairgrounds also attracts many trade shows and conventions throughout the year. This project would mitigate the flood risk to the fairgrounds each year in September.

1. PROJECT INFORMATION

Project Name: West End Columbia County Flood Mitigation Alternative

Date of Review: 3/3/2022 12:39:37 PM

Project Category: In-stream / Riverine Activities and Projects, Levees and similar flood control structures

(construction, modification, maintenance)

Project Area: **124.23 acres** County(s): **Columbia**

Township/Municipality(s): BLOOMSBURG

ZIP Code:

Quadrangle Name(s): **BLOOMSBURG**; **CATAWISSA**Watersheds HUC 8: **Upper Susquehanna-Lackawanna**Watersheds HUC 12: **Fishing Creek-Susquehanna River**

Decimal Degrees: 40.991320, -76.470171

Degrees Minutes Seconds: 40° 59' 28.7519" N, 76° 28' 12.6157" W

This is a draft receipt for information only. It has not been submitted to jurisdictional agencies for review.

2. SEARCH RESULTS

Agency	Results	Response	
PA Game Commission	No Known Impact	No Furth <mark>er Review R</mark> equired	
PA Department of Conservation and Potential Impact Natural Resources		FURTHER REVIEW IS REQUIRED, See Agency Response	
PA Fish and Boat Commission	Potential Impact	FURTHER REVIEW IS REQUIRED, See Agency Response	
U.S. Fish and Wildlife Service	No Known Impact	No Further Review Required	

As summarized above, Pennsylvania Natural Diversity Inventory (PNDI) records indicate there may be potential impacts to threatened and endangered and/or special concern species and resources within the project area. If the response above indicates "No Further Review Required" no additional communication with the respective agency is required. If the response is "Further Review Required" or "See Agency Response," refer to the appropriate agency comments below. Please see the DEP Information Section of this receipt if a PA Department of Environmental Protection Permit is required.

West End Columbia County Flood Mitigation Alternative

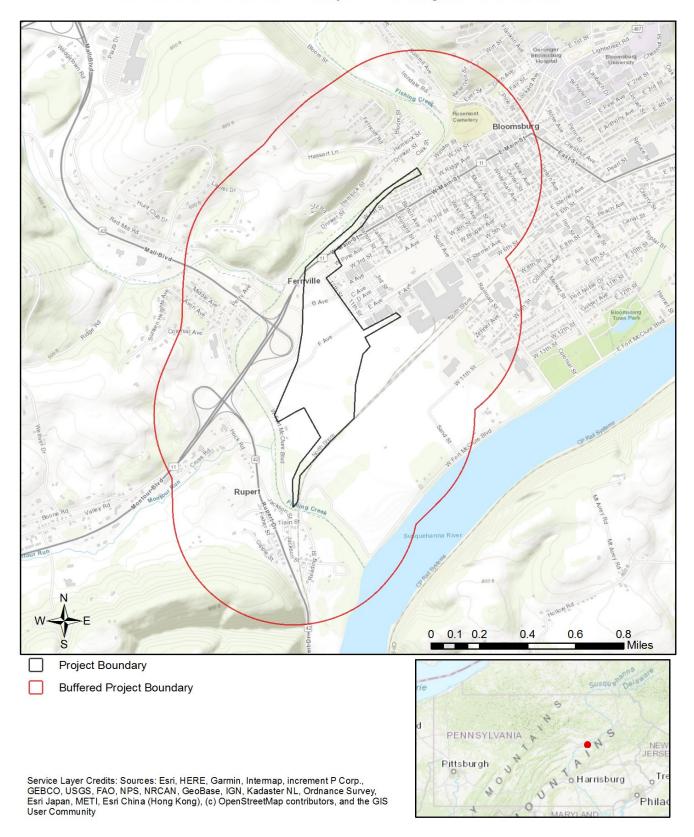


Project Boundary

Buffered Project Boundary

Service Layer Credits: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community Esri, HERE, Garmin, (c) OpenStreetMap contributors, and the GIS user community Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China

West End Columbia County Flood Mitigation Alternative



RESPONSE TO QUESTION(S) ASKED

Q1: Will the project require permanent alteration or removal of natural vegetation, soils, water (streams, ponds, vernal pools, etc.)?

Your answer is: Yes

Q2: Will any and all on-land (non-aquatic) disturbance occur in or on an existing building, parking lot, driveway, road, road shoulder, street, runway, paved area, railroad bed, maintained (periodically mown) lawn, crop agriculture field or maintained orchard?

Your answer is: No

3. AGENCY COMMENTS

Regardless of whether a DEP permit is necessary for this proposed project, any potential impacts to threatened and endangered species and/or special concern species and resources must be resolved with the appropriate jurisdictional agency. In some cases, a permit or authorization from the jurisdictional agency may be needed if adverse impacts to these species and habitats cannot be avoided.

These agency determinations and responses are **valid for two years** (from the date of the review), and are based on the project information that was provided, including the exact project location; the project type, description, and features; and any responses to questions that were generated during this search. If any of the following change: 1) project location, 2) project size or configuration, 3) project type, or 4) responses to the questions that were asked during the online review, the results of this review are not valid, and the review must be searched again via the PNDI Environmental Review Tool and resubmitted to the jurisdictional agencies. The PNDI tool is a primary screening tool, and a desktop review may reveal more or fewer impacts than what is listed on this PNDI receipt. The jurisdictional agencies **strongly advise against** conducting surveys for the species listed on the receipt prior to consultation with the agencies.

PA Game Commission

RESPONSE:

No Impact is anticipated to threatened and endangered species and/or special concern species and resources.

PA Department of Conservation and Natural Resources RESPONSE:

Further review of this project is necessary to resolve the potential impact(s). Please send project information to this agency for review (see WHAT TO SEND).

DCNR Species: (Note: The Pennsylvania Conservation Explorer tool is a primary screening tool, and a desktop review may reveal more or fewer species than what is listed below. After desktop review, if a botanical survey is required by DCNR, we recommend the DCNR Botanical Survey Protocols, available here: https://conservationexplorer.dcnr.pa.gov/content/survey-protocols)

Scientific Name	Common Name	Current Status	Proposed Status	Survey Window
Sensitive Species**		Special Concern Resource*	Special Concern Resource*	
Primula fassettii	Fassett Jeweled Shooting Star	- Threatened	Threatened	Flowers in late April – May

PA Fish and Boat Commission RESPONSE:

Further review of this project is necessary to resolve the potential impact(s). Please send project information to this agency for review (see WHAT TO SEND).

Project Search ID: PNDI-742254

PNDI Receipt: project_receipt_west_end_columbia_county__742254_DRAFT_2.pdf

PFBC Species: (Note: The Pennsylvania Conservation Explorer tool is a primary screening tool, and a desktop review may reveal more or fewer species than what is listed below.)

Scientific Name	Common Name	Current Status
Alasmidonta undulata	Triangle Floater	Special Concern Species*

U.S. Fish and Wildlife Service **RESPONSE:**

No impacts to federally listed or proposed species are anticipated. Therefore, no further consultation/coordination under the Endangered Species Act (87 Stat. 884, as amended; 16 U.S.C. 1531 et seg. is required. Because no take of federally listed species is anticipated, none is authorized. This response does not reflect potential Fish and Wildlife Service concerns under the Fish and Wildlife Coordination Act or other authorities.

- * Special Concern Species or Resource Plant or animal species classified as rare, tentatively undetermined or candidate as well as other taxa of conservation concern, significant natural communities, special concern populations (plants or animals) and unique geologic features.
- ** Sensitive Species Species identified by the jurisdictional agency as collectible, having economic value, or being susceptible to decline as a result of visitation.

WHAT TO SEND TO JURISDICTIONAL AGENCIES

If project information was requested by one or more of the agencies above, upload* or email the following information to the agency(s) (see AGENCY CONTACT INFORMATION). Instructions for uploading project materials can be found here. This option provides the applicant with the convenience of sending project materials to a single location accessible to all three state agencies (but not USFWS).

*If information was requested by USFWS, applicants must email, or mail, project information to IR1_ESPenn@fws.gov to initiate a review. USFWS will not accept uploaded project materials.

Check-list of Minimum Materials to be submitted:

- Project narrative with a description of the overall project, the work to be performed, current physical characteristics of the site and acreage to be impacted.
- A map with the project boundary and/or a basic site plan(particularly showing the relationship of the project to the physical features such as wetlands, streams, ponds, rock outcrops, etc.)

In addition to the materials listed above, USFWS REQUIRES the following

SIGNED copy of a Final Project Environmental Review Receipt

The inclusion of the following information may expedite the review process.

- Color photos keyed to the basic site plan (i.e. showing on the site plan where and in what direction each photo was taken and the date of the photos)
- Information about the presence and location of wetlands in the project area, and how this was determined (e.g., by a qualified wetlands biologist), if wetlands are present in the project area, provide project plans showing the location of all project features, as well as wetlands and streams.

4. DEP INFORMATION

The Pa Department of Environmental Protection (DEP) requires that a signed copy of this receipt, along with any required documentation from jurisdictional agencies concerning resolution of potential impacts, be submitted with applications for permits requiring PNDI review. Two review options are available to permit applicants for handling PNDI coordination in conjunction with DEP's permit review process involving either T&E Species or species of special concern. Under sequential review, the permit applicant performs a PNDI screening and completes all coordination with the appropriate jurisdictional agencies prior to submitting the permit application. The applicant will include with its application, both a PNDI receipt and/or a clearance letter from the jurisdictional agency if the PNDI Receipt shows a Potential Impact to a species or the applicant chooses to obtain letters directly from the jurisdictional agencies. Under concurrent review, DEP, where feasible, will allow technical review of the permit to occur concurrently with the T&E species consultation with the jurisdictional agency. The applicant must still supply a copy of the PNDI Receipt with its permit application. The PNDI Receipt should also be submitted to the appropriate agency according to directions on the PNDI Receipt. The applicant and the jurisdictional agency will work together to resolve the potential impact(s). See the DEP PNDI policy at https://conservationexplorer.dcnr.pa.gov/content/resources.



5. ADDITIONAL INFORMATION

The PNDI environmental review website is a preliminary screening tool. There are often delays in updating species status classifications. Because the proposed status represents the best available information regarding the conservation status of the species, state jurisdictional agency staff give the proposed statuses at least the same consideration as the current legal status. If surveys or further information reveal that a threatened and endangered and/or special concern species and resources exist in your project area, contact the appropriate jurisdictional agency/agencies immediately to identify and resolve any impacts.

For a list of species known to occur in the county where your project is located, please see the species lists by county found on the PA Natural Heritage Program (PNHP) home page (www.naturalheritage.state.pa.us). Also note that the PNDI Environmental Review Tool only contains information about species occurrences that have actually been reported to the PNHP.



November 8, 2021

Lisa Clementoni Borton Lawson 613 Baltimore Drive, Ste. 300 Wilkes-Barre PA 187020000

RE: ER Project # 2021PR06578.002, Columbia County - West End Flood Mitigation Study, Army Corps of Engineers, Hemlock Township, Columbia County

Dear Lisa Clementoni:

Thank you for submitting information concerning the above referenced project. The Pennsylvania State Historic Preservation Office (PA SHPO) reviews projects in accordance with state and federal laws. Section 106 of the National Historic Preservation Act of 1966, and the implementing regulations (36 CFR Part 800) of the Advisory Council on Historic Preservation, is the primary federal legislation. The Environmental Rights amendment, Article 1, Section 27 of the Pennsylvania Constitution and the Pennsylvania History Code, 37 Pa. Cons. Stat. Section 500 et seq. (1988) is the primary state legislation. These laws include consideration of the project's potential effects on both historic and archaeological resources.

Archaeological Resources

More Information Requested - Environmental Review - More Info Archaeological - High Prob

As this project area is located wholly or partially within an urban area, it is our opinion that a Phase IA archaeological study should be undertaken to assess this property s potential for National Register significant archaeological resources. This study should consist of a thorough review of all available historic through recent maps and other documentary sources which may provide information on past land use within the project area. A geomorphological assessment of the project area is recommended at this stage as it will provide useful information on the total depth and overall integrity of potential archaeological deposits. If this research suggests that potentially significant archaeological resources may be present, it will be our opinion that a Phase I archaeological testing plan should be developed to identify such resources. Guidelines and instructions for conducting all phases of archaeological survey in Pennsylvania are available on our website http://www.phmc.pa.gov/Preservation/About/Documents/SHPO-Guidelines-Archaeological-Investigation.pdf

More Information Requested - New Survey

Please use this Request for More Information to enter survey and resource details and upload the survey report. Please submit the requested materials to the PA SHPO through PA-SHARE using the link under SHPO Requests More Information on the Response screen.

For questions concerning archaeological resources, please contact Casey Hanson at chanson@pa.gov.

Sincerely,

Andrea MacDonald

andrea AT law Donald

Director, State Historic Preservation Office

WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY, PENNSYLVANIA

Appendix D

Public and Stakeholder Outreach

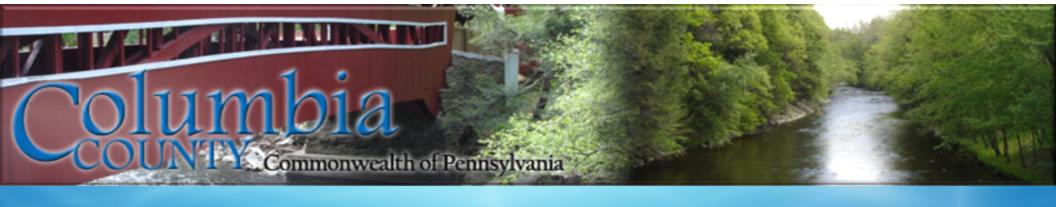
WEST END FLOOD MITIGATION STUDY

Appendix D

Public and Stakeholder Outreach

TABLE OF CONTENTS:

- 1. Public Meeting Presentations
- 2. Municipal Stakeholder Meeting Minutes



WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY

PUBLIC MEETING JULY 29, 2021



Welcome

COLUMBIA COUNTY BOARD OF COMMISSIONERS

CHRIS YOUNG – CHAIRMAN RICHARD RIDGWAY DAVID KOVACH

SEDA-COUNCIL OF GOVERNMENTS

TERI PROVOST

DIRECTOR

HOUSING REHABILITATION & FLOOD RESILIENCY



Study Team



Columbia County – Study Sponsor SEDA-COG – Study Administrator









Brozena Consulting Services, LLC







Columbia County Flood Damage Reduction/Mitigation Efforts 2011 - 2021

- Updated County Hazard Mitigation Plan
- Community Rating System (CRS) Bloomsburg Improved Classification to Class 7
- Inventory of Flood Plain Properties Homeowner Surveys
- Identified Repetitive Loss (RL) and Severe Repetitive Loss (SRL) Properties
 - o Active 166 Mitigated 25
- FEMA Buyouts 11
- CDBG-DR Funded Structure Elevations 2 Completed
- FMA Funded Elevations 2 Underway
- Completed 2 Structural Mitigation Projects (Levee/ flood wall projects)



Phase I Flood Mitigation Project - Completed 2016

Non-Federal Project

Timeline:

- Design/Bidding 18 months
- Construction 18 months
- Total Timeline: 3 years



Phase II Flood Mitigation Project - Completed 2020

Non-Federal Project

Timeline:

• Design/Bidding 18 months

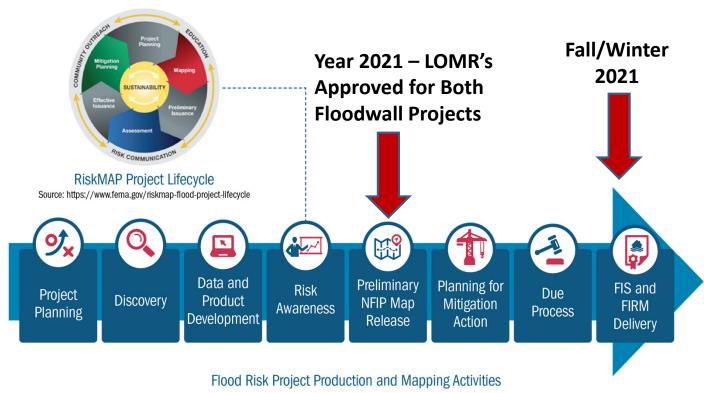
• Construction 20 months

• Total Timeline: 3 + years

Construction Cost: \$14,800,000



Flood Insurance Rate Map Update



Souce: Fema Guidance for Stakeholder Engagement, Project Planning Phase (Nov 2015)

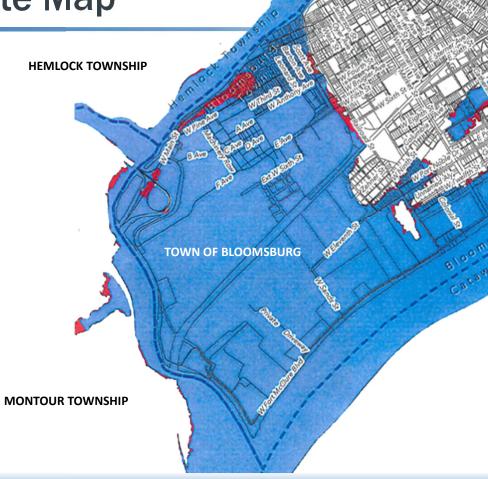


Preliminary Flood Insurance Rate Map

Changes & Impacts

Updated Base Flood (100 Year) = Existing Base Flood + 1.3 Feet

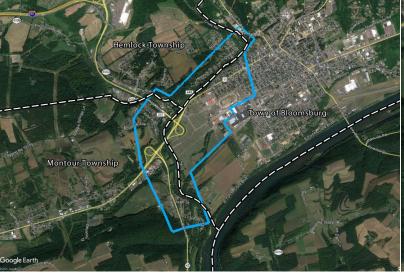
Red is increase in floodplain. Some areas will see a decrease in the floodplain area.

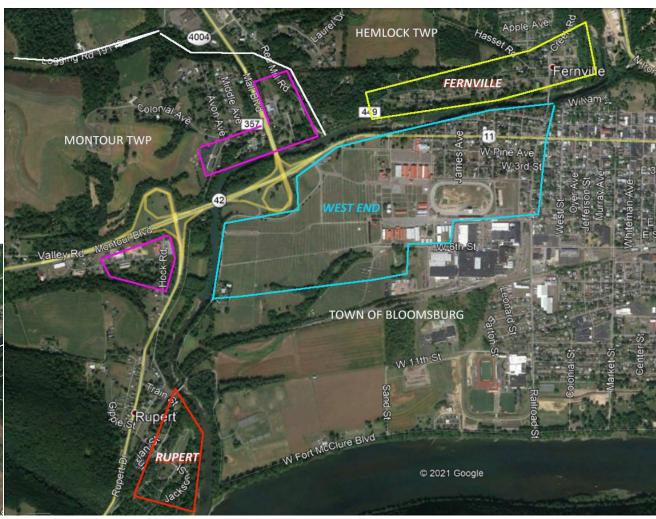




Study Area

- West End Town of Bloomsburg, Hemlock Twp and Montour Twp in area of Floodplain
- Approx. 600 parcels





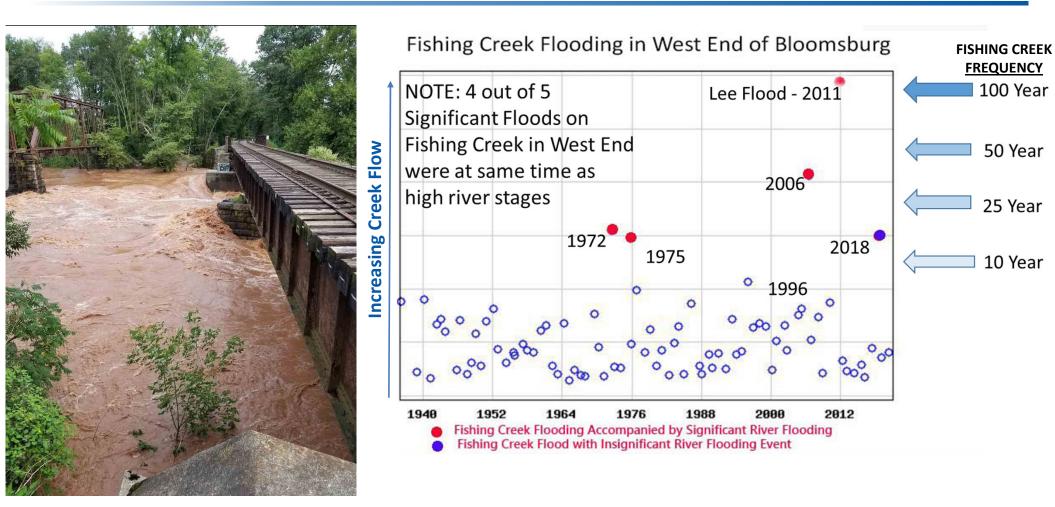
History of Fishing Creek Flooding

100 Year

50 Year

25 Year

10 Year





West End 2011 Flooding



Fairgrounds 2018 Flooding

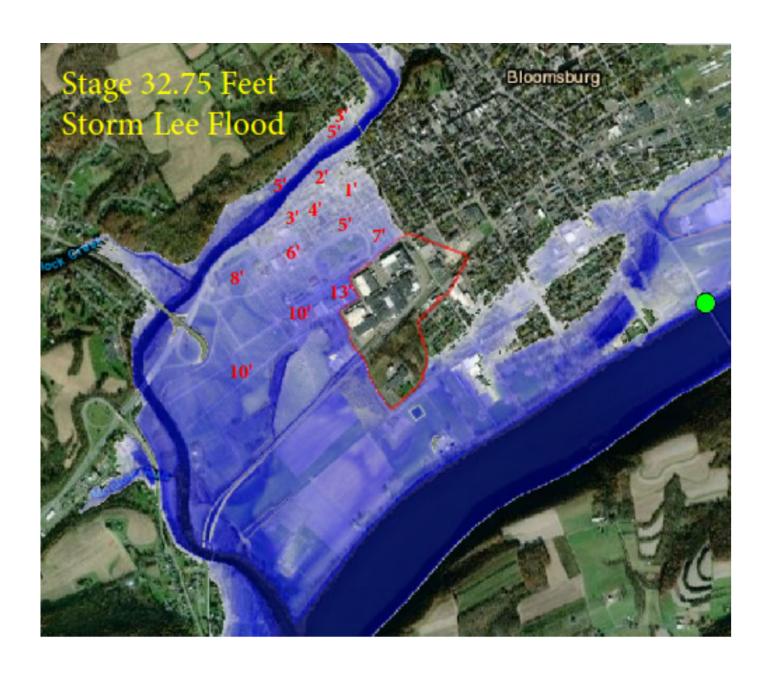


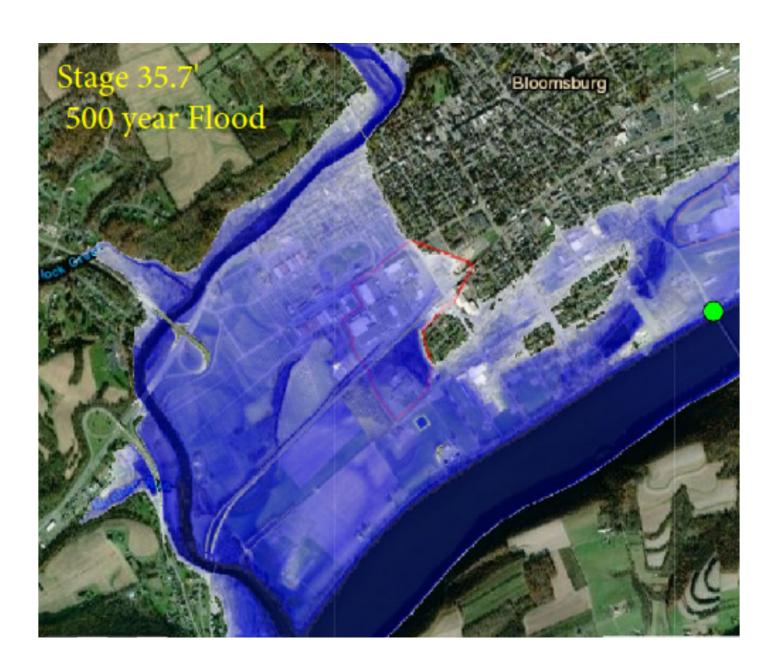












Purpose & Goals of Study

Identify and determine best structural and non-structural project(s) to:

- Provide long-term flood resiliency (reduce long-term risk to loss of life and property damage)
- Reduce flood insurance premiums
- Minimize flood mitigation impacts on community fabric
- Identify possible funding sources



Scope of Study

- Inventory existing conditions
- Perform building elevation surveys
- Gather community input on possible solutions
- Assess flood reduction opportunities from upstream mitigation options identified in the Fishing Creek Watershed Study
- Formulate alternatives for flood mitigation



Scope of Study (continued)

- Perform Benefit/Cost Analysis (BCA) for all Alternatives
- Public Outreach

Public Meetings Study Website Email Questions

- Recommend plan
- Study Timeframe May 2021 through March 2022



Structural Alternatives

Levees/Flood Walls

- Similar to completed projects Walls and earth levees
- Height = Lee Flood + 1.5 feet, generally 10 feet
- Property aquisition
- Channel improvements
- Cost and community impacts will be major factor in feasibility



Non Structural Mitigation Actions

Physical Measures

- Acquisition
- Elevation
- Flood Proofing
- Abandon Basement
- Utility Floodproofing
- Mitigation Relocation

Non-Physical Measures

- Evacuation Plans
- Flood Warning
- Land Use / Zoning
- Flood Insurance



Outreach Overview - Educate & Inform

- Offer multiple avenues and opportunities for participation at various stages in the study
- Develop outreach goals for public education and information
- Engagement and outreach materials throughout the study
- Conduct a survey to
 - ✓ Gather local knowledge
 - ✓ Understand issues
 - ✓ Identify best solutions



Outreach and Engagement Strategy

Target Groups

- General Public
- Stakeholders

Outreach Goals

- Provide multiple opportunities for engagement
- Educate public and stakeholders on the study
- Garner interest and input
- Gather information

Inform

- Web Page
- Educational Briefings
- Press Releases
- Social Media
- Surveys
- Meetings Stakeholder& Public



Study Participants

<u>Public</u>

 Approximately 600 parcels in Study Area

Stakeholders

- Federal, State & Local Officials
- PADEP, USACE, FEMA, PEMA, Conservation District
- Local Businesses, Schools, Healthcare
 Systems, Utilities, affected by flooding



Public Survey - We Want Your Feedback!

We would like to hear your feedback on:

- Risk of flooding
- Frequency/ history of flooding
- Type and amount of damage
- Personal preventative measures
- Need for flood mitigation efforts
- Communication preferences

By completing a survey and providing input, you have the opportunity to:

- Provide study team valuable information
- Support development of best mitigation alternatives and recommendations



Public Survey – Opportunities for Feedback

- Email/ Mailing Lists
- Mailed surveys
- Study Webpage/ SEDA-COG website
- Survey Forms at Municipal Offices
- Survey Forms at upcoming public meetings



Public Information - Project Updates & Meetings

SEDA-COG's Columbia County Flood Mitigation Study webpage:

https://seda-cog.org/departments/floodresiliency/columbia-county-flood-mitigationstudies/

Provides information on

- Upcoming Meetings
- Study Schedule
- Study Deliverables/ Report
- Presentations
- Surveys



Columbia County Flood Mitigation Study

Columbia County has contracted with Herbert, Rowland & Grubic, Inc (HRG) to provide engineering services to undertake a flood mitigation study for the **Fishing Creek Watershed** in the County. This study will include an investigation of the existing conditions, as well as potential flood resiliency and mitigation projects throughout the watershed. This project has been financed by grants from the Commonwealth of Pennsylvania, Commonwealth Financing Authority and the Department of Community and Economic Development.

The County of Columbia has contracted with Borton Lawson (B-L) to provide engineering services to undertake a flood mitigation study near, in and surrounding the known as the "West End" of the Town of Bloomsburg, Columbia County. This study will include an investigation of potential flood resiliency and mitigation projects in the floodplain of Fishing Creek and the Susquehanna River. This project has been financed by grants from the Commonwealth of Pennsylvania, Commonwealth Financing Authority and the Department of Community and Economic Development.



BACK TO FLOOD RESILIENCY

Study Participant Meetings

Public & Stakeholder Meetings

- Three (3) separate meetings to be held with each group
 - Kickoff
 - Project midpoint, survey results, preliminary data, project direction
 - Study Findings/Final Report

Columbia County SEDA-COG Town of Bloomsburg Hemlock Township Montour Township Columbia County Housing and Redevelopment Authority Bloomsburg Municipal Authority Bloomsburg Area School District County Conservation District Geisinger Health System Federal & State Representatives Local Business/Industry Officials Residential Leaders



Other Ways to Stay Informed and Engaged

Press Releases

- Distributed via traditional newspaper outlets (Press Enterprise)
- Developed at key milestones throughout the project
- Provide information on
 - Public Meetings
 - Opportunity for Involvement
 - How to review published study report, mapping





Website/ Social Media

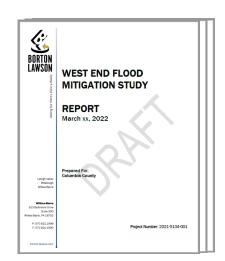
- Provide information on
 - Upcoming meetings/events
 - Surveys/Questionnaires open to the public
 - Major milestone accomplishment
 - Flood risk mitigation analyses findings
 - Presentations
- Share with us your
 - Personal experiences with flooding
 - Photos of local flood events / damaged infrastructure
 - Personal mitigation projects undertaken
 - Ideas for flood mitigation or resiliency projects



Deliverables

Study Report

- Mitigation Alternatives- Identify & Analyze
- Recommended Plan
 - Project Features / Renderings
 - Induced Flooding If Any / Mitigation
 - Permitting Requirements
 - Benefit/Cost Analysis All alternatives
 - Community Benefits / Impacts / Environmental Justice
- Planning Opportunities for Complimentary Projects
- Funding Options
- Schedule for Implementation





Next Study Update Public Meeting - Fall 2021

FOR MORE PROJECT INFO...



Study Webpage

https://seda-cog.org/departments/flood-resiliency/columbia-county-flood-mitigation-studies

Study YouTube Channel

https://www.youtube.com/channel/UCgayzkKnERaUJpeVQfKmKkg

Email Questions/ Comments

Geralee Zeigler, SEDA-COG: gslotterback@seda-cog.org







THANK YOU!

Questions?





WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY

PUBLIC MEETING
DECEMBER 1, 2021



Welcome

COLUMBIA COUNTY BOARD OF COMMISSIONERS

CHRIS YOUNG – CHAIRMAN RICHARD RIDGWAY DAVID KOVACH

SEDA-COUNCIL OF GOVERNMENTS

TERI PROVOST

DIRECTOR

HOUSING REHABILITATION & FLOOD RESILIENCY



Study Team



Columbia County – Study Sponsor SEDA-COG – Study Administrator









Brozena Consulting Services, LLC





Study Area

West End - Floodplains of:

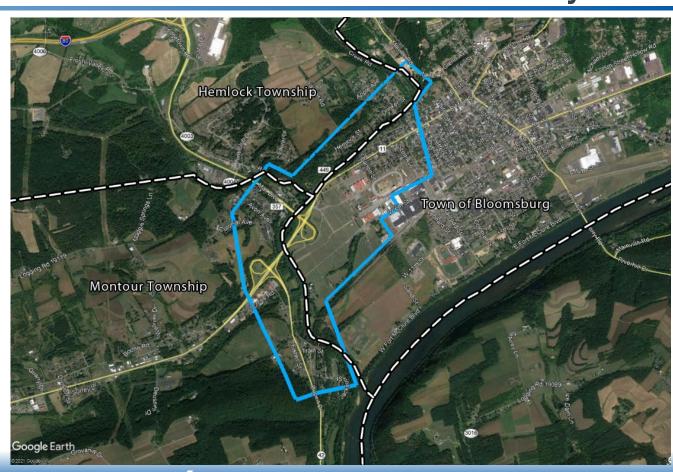
- Town of Bloomsburg
- Hemlock Township
- Montour Township

~500 Parcels

- Bloomsburg 286
- Hemlock 131
- Montour 80

~350 Parcels Surveyed

- Bloomsburg 271
- Hemlock 42
- Montour 36





Purpose & Goals of Study

Identify and determine best structural and non-structural project(s) to:

- Provide flood resiliency (reduce long-term risk to loss of life and property damage)
- Reduce impacts of increasing insurance premiums
- Minimize flooding impacts on community
- Identify possible funding sources for flood mitigation projects



What's Been Accomplished To Date

- Property Owner Surveys/ Questionnaires
- Field Structure Surveys
- Mapping Floodway, Floodplain & Zone X Properties
- Stakeholder Outreach
- Assessment of Non-Structural Mitigation Alternatives
- Detailed Hydrologic & Hydraulic Analysis River and Fishing Creek
- Assessment of Structural Mitigation Alternatives



Property Surveys / Questionnaires:

Survey Distribution

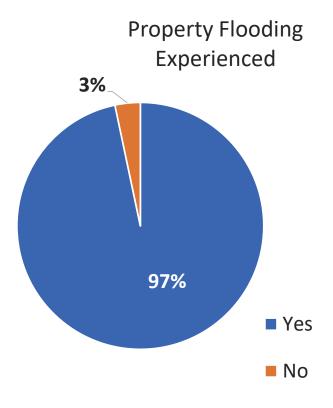
- Surveys were mailed on September 21, 2021, to the property owners of all 350 parcels in the Study Area. A letter outlining the purpose of the survey and directions for its completion accompanied the survey.
- Respondents could return their completed survey via mail or complete the survey online using the provided link and QR code.

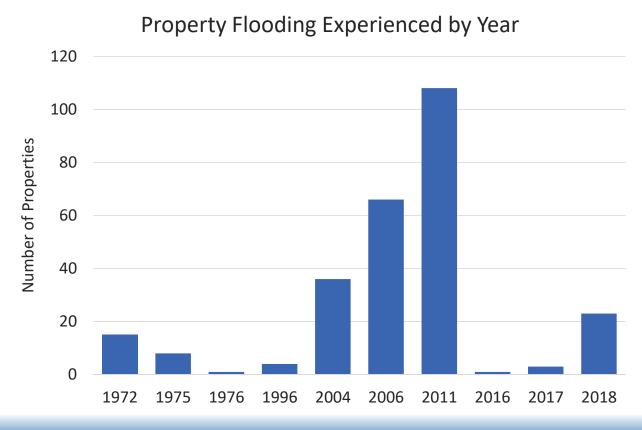
Survey Response Rate

• 123 survey responses - Response Rate: ~35%



Property Flooding – Past Experiences

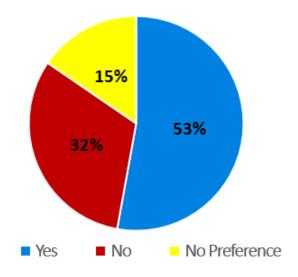






Relocation Preferences

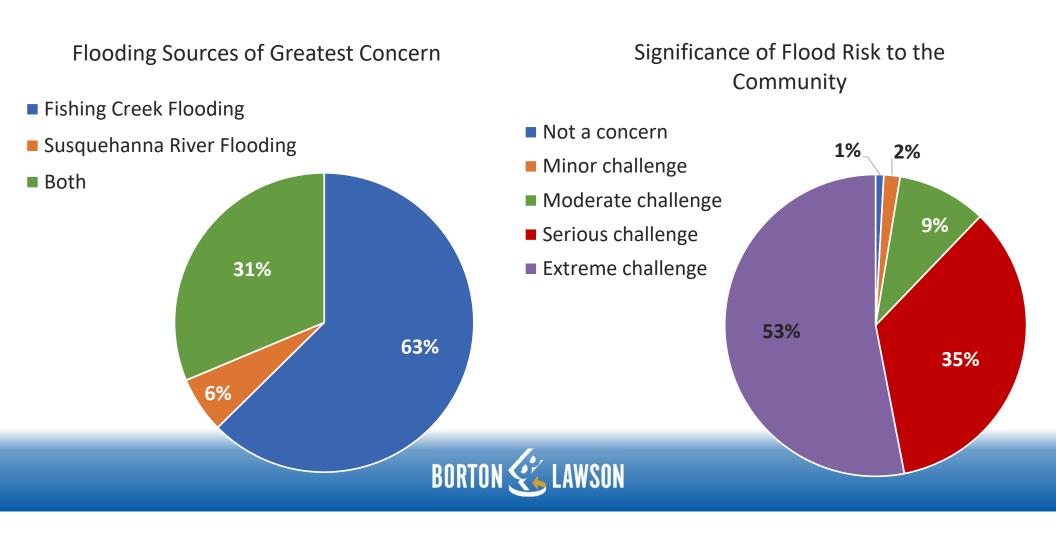




- Yes I am looking at buying/renting at a new location in the near future because of flooding.
- Yes I am considering buying/renting at a new location in the future if flood events become more frequent
- Yes I considered buying/renting at a new location, but I have nowhere else to go or conditions preventing me.
- Yes But buyout would be financial loss, would sell but flood insurance too high no one will buy, would sell but property value assessed too low.
- No I do not want to leave my current location.
- No My property never floods, so it is not a factor in my decision to stay or leave.
- No Preference Rentals/Vacant/Property Floods but not Structure



Perception of Flooding Risks

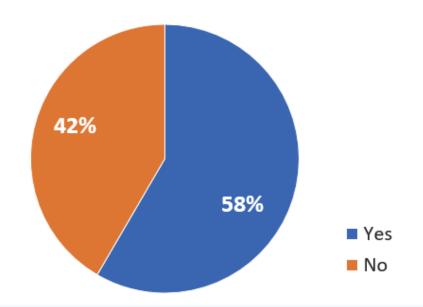


Properties with Flood Insurance:

Property Owner Survey Responses:

~350 Properties with Structures in Floodway & Floodplain

Properties with Flood Insurance





Field Structure Surveys

~350 Parcels Surveyed in Study Area

- First Floor Elevations
 (accuracy to within +/- 2 inches)
- Location and elevation in front of structure (accuracy to within +/- 3/8 of an inch)
- General Structure Information
 - ✓ Structure type
 - ✓ Basement
 - ✓ Number of stories
 - ✓ Detached Structures
 - ✓ Inhabited
 - ✓ Photos

Flood study responses needed

Official: Bloomsburg-area surveys to help determine mitigation options



Press Enterprise/Jimmy Ma

WADE WEBER, surveying crew chief, left, and **Catrian Coppola**, surveying assistant, document the property at the intersection of West Third and Leonard streets this week. They were working in the west end of Bloomsburg. Resident surveys need to be returned by Oct. 30.

By PETER KENDRON

BLOOMSBURG
— Survey crews are
on the streets of west
Bloomsburg and the
flood-prone areas of
Hemlock and Montour
townships. They're taking measurements for a
flood mitigation study,
officials say.

Meanwhile, the company doing the study, Borton Lawson, sent about 350 surveys to area residents weeks ago. They're asking for measurements on their homes, the flood history of their property and their feelings on flood protection.

But so far, only about 25% — fewer than 100 — have come back. Those in charge of the study hope to boost that number by the end of the survey period Oct. 30.

Those responses are important, said Jim Brozena. He's a consultant assisting Borton-Lawson on flood miti-



Changes Coming with Preliminary Flood Insurance Rate Map

Changes & Impacts

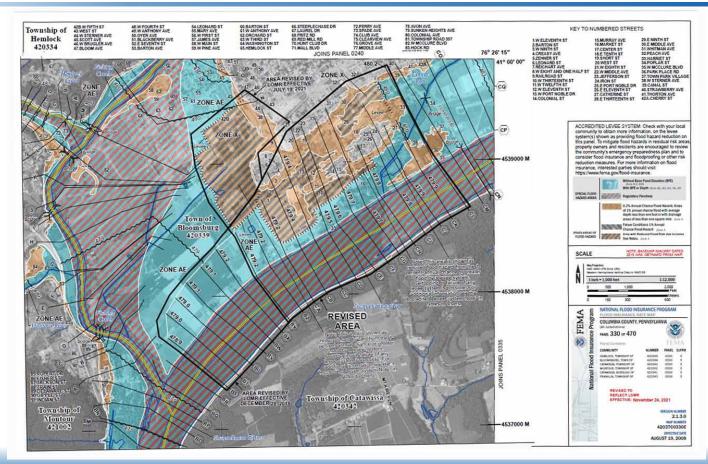
Updated Base Flood (100 Year) (Existing Base Flood + 1.2 Feet)

PURPLE is <u>in</u>crease in floodplain area. TAN is <u>de</u>crease in floodplain area.





Preliminary Flood Insurance Rate Map





Montour Twp: Floodway, Floodplain, Lee Flood Limit



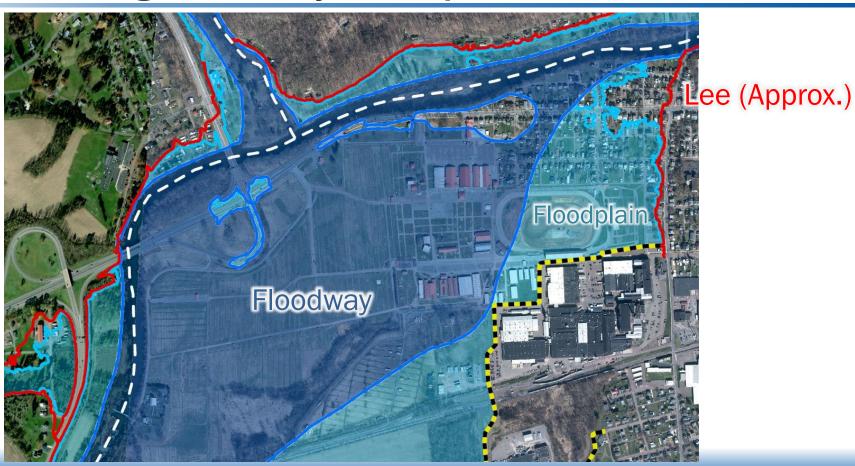


Hemlock Twp: Floodway, Floodplain, Lee Flood Limit





Bloomsburg: Floodway, Floodplain, Lee Flood Limit





Stakeholder Outreach

Columbia County
SEDA-COG
Town of Bloomsburg
Hemlock Township
Montour Township
Columbia County Housing & Redevelopment Authority
Bloomsburg Municipal Authority
Bloomsburg Area School District
Bloomsburg University
Geisinger Health System
Bloomsburg Fairgrounds



Stakeholder Outreach

Common Concerns:

- Access
 - Route 11 toGeisinger/Danville
 - Staff
 - Supplies
- Loss of Utilities
 - Electric
 - Drinking Water
- BASD & University Impact to students
- Municipalities, BASD Loss of tax base
- Fairgrounds Loss of revenue, loss of services to community

Mitigation Actions Since 2011

- Drinking Water Treatment Plant Rebuilt
- PPL Substation/Distribution System Upgraded
- 2 Levee Systems constructed



Flood Mitigation - Non Structural Mitigation Actions

Township Makeup

- 915 Structures (80 in Floodplain, 9%)
- 7% of Population in Floodplain
- 15 Flood Insurance Policies

Study Area - 80 Parcels

- Floodway: 16 (9 vacant)
- Floodplain: 34 (11 vacant)
- Zone X: 17
- Buyouts: 10 (vacant)

Proposed Actions

- HMGP Buyouts
- Evaluate County Bldg for Floodproofing
- RV Park EAP required
- Sanitary Pump Stations
- Ordinance Revisions

MONTOUR TOWNSHIP

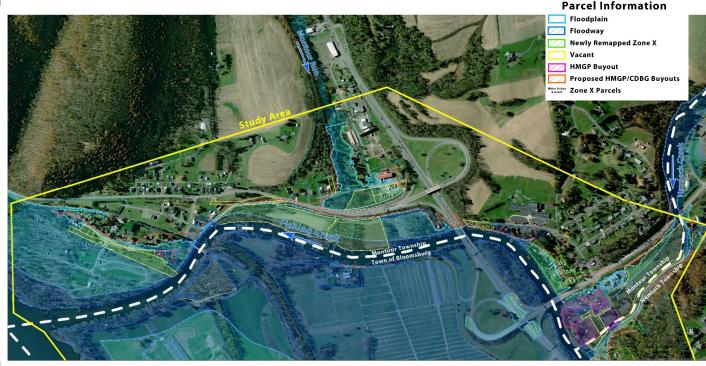
Legend

Floodway

1% Annual Chance of Flooding

- Approx Extent of 2011 Lee Flood

Previous Mitigation Project
Study Area





Flood Mitigation - Non Structural Mitigation Actions

Township Makeup

- 1,910 Structures (135 in Floodplain, 7%)

10% of Population in Floodplain

37 Flood Insurance Policies

Study Area - 131 Parcels

Floodway: 25 (16 vacant)

Floodplain: 45 (17 vacant)

Zone X: 13

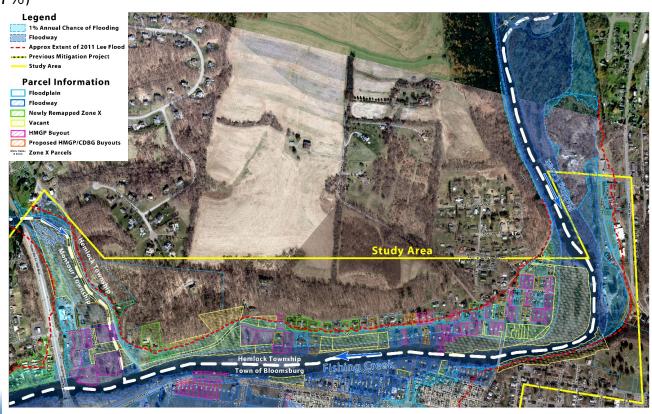
Buyouts: 37 (vacant)

- Future Buyouts: 11

Proposed Actions

- HMGP Buyouts
- Emergency Road Access
- Ordinance Revisions
- Creek Road Elevation

HEMLOCK TOWNSHIP





Flood Mitigation – Non Structural Mitigation Actions

TOWN OF BLOOMSBURG

Town Makeup

- 3,160 Structures (560 in Floodplain, 21%)
- 8% of Population in Floodplain
- 291 Flood Insurance Policies
- 168 Repetitive Loss Properties

Study Area - 286 Parcels

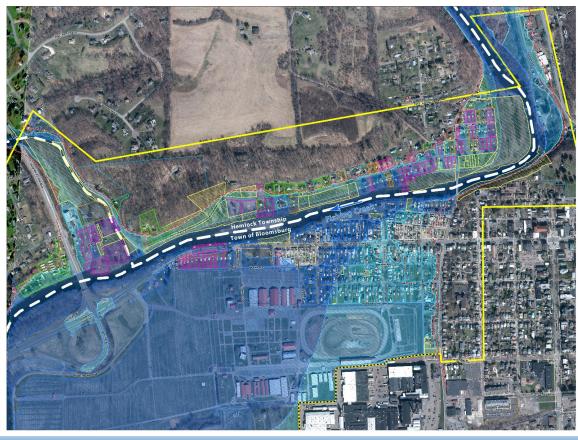
Floodway: 107 (15 vacant)

- Floodplain: 128 (16 vacant)

Zone X: 40

Buyouts: 11 (vacant)







Flood Risk Mitigation - Non Structural Mitigation Actions

TOWN OF BLOOMSBURG

Past Actions

- Buyouts
- Elevations
- CRS CommunityClass 8

Proposed Actions

- Buyouts
- Elevations
- Utility Relocations
- Floodproofing (commercial)
- Mitigation Reconstruction
- Ordinance Review
- Evacuation Plan
- Fishing Creek Gauge (early notification)

FAIRGROUNDS

Past Actions

Utility Relocations

Proposed Actions

- Floodproofing
- Emergency Action Plan



Flood Risk Mitigation - Non Structural Mitigation Actions

Other Non-Physical Measures

- Evacuation Plans
- Flood Warning
- Land Use / Zoning
- Flood Insurance



River and Fishing Creek Flooding

- History of Flooding
- Analysis of Flooding
- Impacts of Flooding
- Structural Mitigation Alternatives



Major Floods Ranked							
Fishing Creek @ West End of Town					Susquehanna River		
Return Period	COE Modelling Updated with Lee Event 2011	Rank	Date		Recurrenc e Interval	Rank (Floods after 1920)	Date
500 yr	89,600				500 yr		
350	78,700	1	2011		250 yr		
250 yr	75,300					1	2011
100 yr	58,900					2	1972
95	57,900	2	2006		100 yr		
50 yr	48,200					3	2006
45	43,400	3	1972		50 yr		
35	42,000	4	2018			4	1936
30	41,300	5	1975			5	1975
25 yr	38,800					6	2004
14	29,900	6	1996			7	1996
10 yr	28,000					8	1940
		7	1976		25 yr		

History of Flooding

Stream flow data covers past 85 years

Three of top 5 major floods on Fishing Creek have occurred over last 15 years (2006, 2011, 2018)
Others were 1972 and 1975

River flooding generally same timeframe as creek flooding except 2018

Creek flooding can precede river flooding (2011)



2011. **Base Flood** 1972 2006 <u>1975</u> <u>1936</u> 2004 10 Feet 2005 16 Other Events

History of Flooding

Bloomsburg Fairgrounds

Lligh water marks on born bobi

High water marks on barn behind grandstand

35 floods impacted Fairgrounds over last 120 years

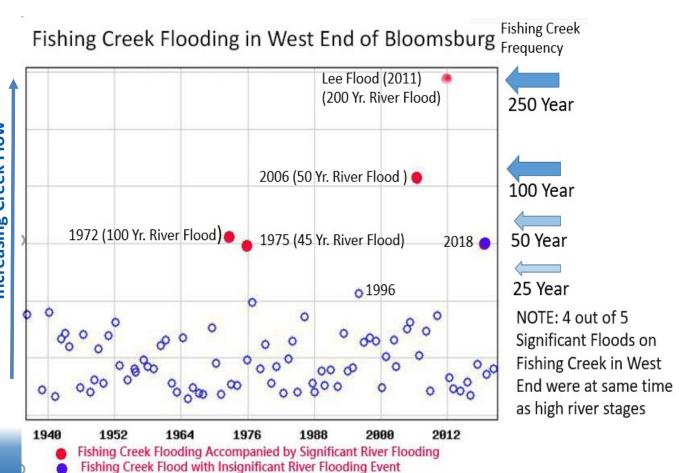
1972 (Agnes Flood) 6" higher than Base Flood.



2/3 of survey respondents said creek is bigger concern than river, although river flooding is 80% of higher flood events.

Creek Flow Increasing

History of Fishing Creek Flooding



NOUNTON CONTROL

History of Fishing Creek Flooding

Fishing Creek Flooding of 2011 was devastating to lower West End. Creek Flooding preceded river flooding. Essentially two flooding events.

The 2018 Creek Flooding in West End reinforced residents' fears of creek flooding as their biggest concern. Water moves with a destructive velocity.





History of Fishing Creek Flooding

1950 2021





Analysis of Flooding

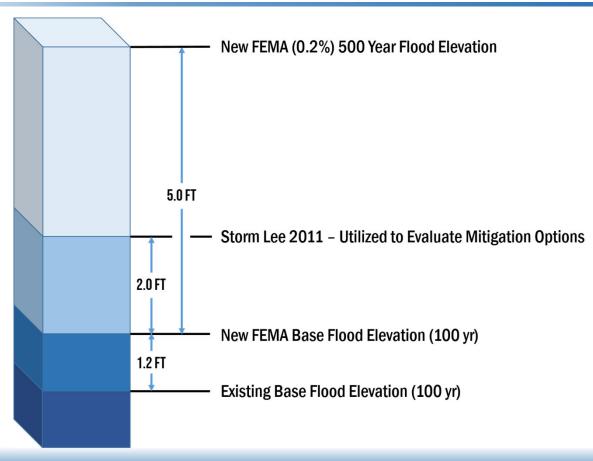
Analyzed Fishing Creek and Susquehanna River flooding to address all flooding scenarios.

- ✓ All singular or combination of events.
- ✓ Study team updated FEMA flood model for Fishing Creek to include all flood events including 2018.

 Last update by FEMA was in 1979.
- ✓ Utilized Susquehanna River FEMA model updated in 2013 Includes 2011 Lee Flooding



Analysis of Flooding – Flood Levels







Montour Twp: Depth of Flooding (Lee Flood - 2011) Base Flood = Lee Flood - 2 Feet

Township Efforts focused on Buyouts.

Lack of density of impacted homes along creek and river does not justify levee system from a funding standpoint.

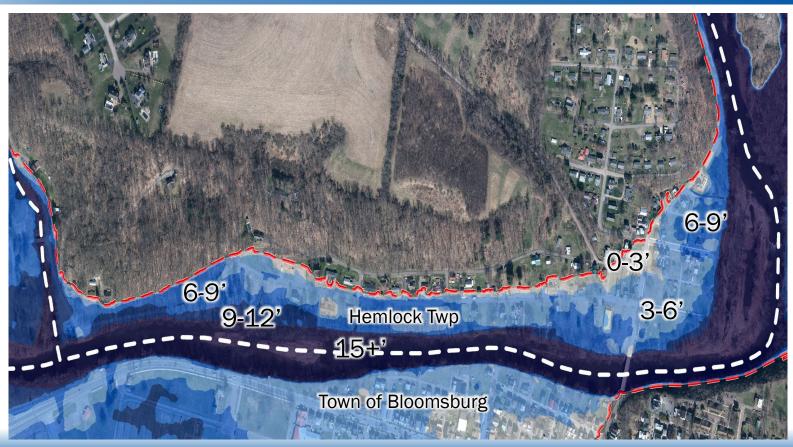


Hemlock Twp: Depth of Flooding (Lee Flood - 2011) Base Flood = Lee Flood - 2 Feet

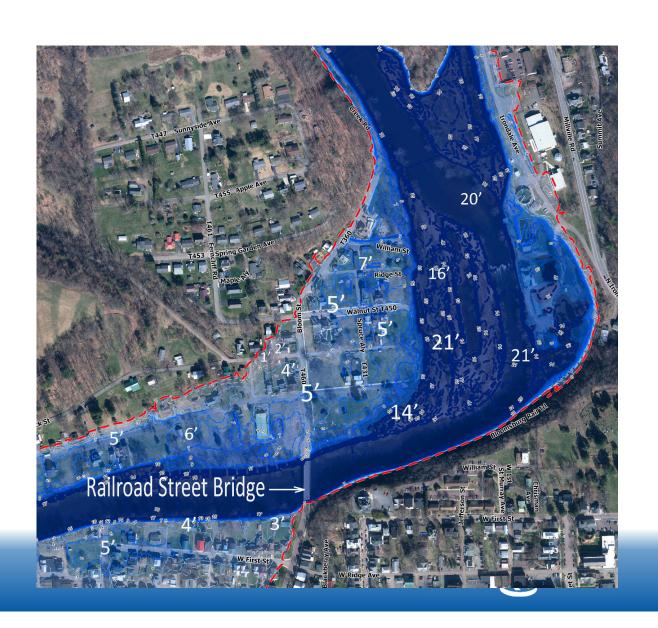
Buyouts completed Additional planned

Levees or Floodwalls not cost effective

Town planning for growth outside floodplain.







Hemlock Twp:

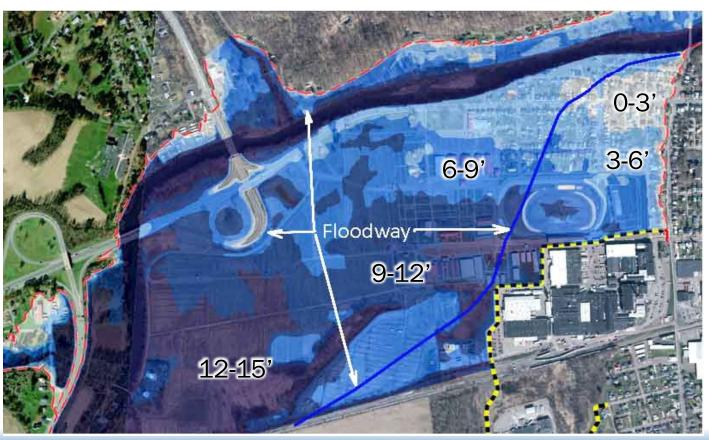
Depth of Flooding (2011)

Fishing Creek at bend upstream of Railroad Street bridge.

Flow channel wide and deep but loss of energy due to turbulence.

Raising Railroad Street Bridge being considered to reduce flood levels upstream – especially for flooding similar to 2011 (Storm Lee Flood)

Bloomsburg: Depth of River Flooding (2011)



Fairgrounds impacted by deep water flooding.

Town residential area experiences significant first floor flooding.

Majority of deeper flooding in Fishing Creek floodway



Structural Mitigation Alternatives

- Bridge Removal / Raising
 - Covered bridge, railroad bridge, and old truss bridge Reduction of Fishing Creek Flooding of 3 feet - tapers to zero at upstream Route 11
 - Railroad Street Bridge Raising could decrease 2011
 flooding levels about 2 feet upstream of the bridge.







Structural Mitigation Alternatives

- Channel Improvements Widening, island removal Ongoing Review
- Upstream Stormwater Management Facilities (Fishing Creek Watershed Study)
- Levees / Floodwalls



Conceptual Floodwall/Levee System - Bloomsburg



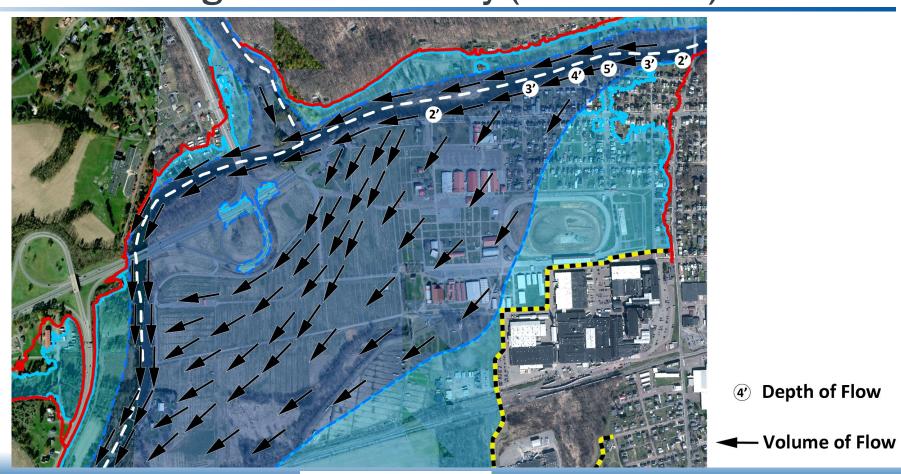


Conceptual Floodwall/Levee System - Bloomsburg

- River backwater and creek flooding eliminated behind system
- Length of Floodwall System 6,200 Feet (1.2 Miles)
- Stormwater Pumping Stations 2
- Roadway Closure Structures 4
- System Height
 - Railroad Street to Route 11 crossing 6 to 8 feet
 - Route 11 across Fairgrounds 10 to 13 feet
- Property Aquisitions Approximately 5 Full / 9 Partial
- Induced flooding (base flood levels):
 - Upstream of Railroad Street Negligible
 - Downstream of Railroad Street along levee length 12 to 15 inches
 - Mitigation of induced flooding to be investigated by altering system length along creek and minimizing levee encroachment in stream.



Fishing Creek Floodway (Base Flood)



Proposed Creek Floodway Revision System - Bloomsburg

Floodway Revision Levee

Purpose: Redirect Creek overbank flows downstream to minimize severe damage risk to homes/businesses.

Levee could be Phase I of eventual full levee / floodwall system.

Floodway designation can be removed. Reconstruction with elevated homes would be possible.

River and creek flooding still possible but with negligible velocity.

Induced flooding: Less than 2"





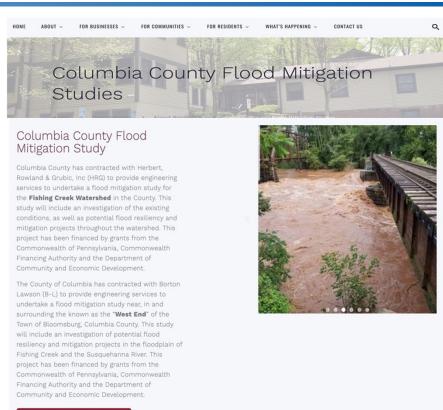
Public Information - Project Updates & Meetings

SEDA-COG's Columbia County Flood Mitigation Study webpage:

https://seda-cog.org/departments/floodresiliency/columbia-county-flood-mitigationstudies/

Provides information on

- Public Meetings
- Study Schedule
- Study Deliverables/ Report
- Surveys
- Contacts for Questions/Comments





BACK TO FLOOD RESILIENCY

Ways to Stay Informed and Engaged

Press Releases

 Distributed via traditional newspaper outlets (Press Enterprise)

Public Meetings

Final Public Meeting – February/March 2022

Email

- Share with us your
 - Personal experiences with flooding
 - Photos of local flood events / damaged infrastructure
 - Personal mitigation projects undertaken
 - Ideas for flood mitigation or resiliency projects







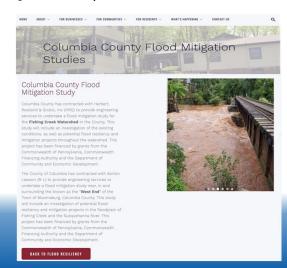


Website/ Social Media

 SEDA-COG's Columbia County Flood Mitigation Study webpage

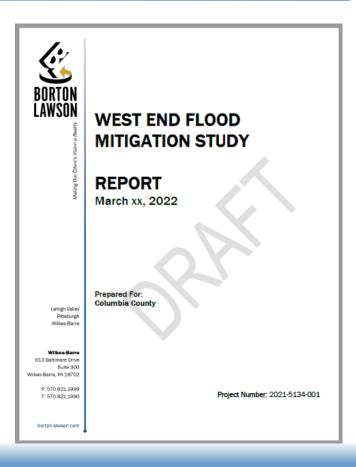
Provides information on

- Public Meetings
- Study Deliverables/ Report
- Property Owner Survey
- Contacts for Questions/Comments



Final Public Meeting

- ✓ Flood Mitigation Alternatives Identify, Summarize Evaluation
- ✓ Recommendations
 - Concept Level Drawings for Alternatives
 - Induced Flooding / Mitigation
 - Environmental Impacts/ Permitting Requirements
 - Benefit/Cost Analysis All alternatives
 - Community Benefits / Impacts / Environmental Justice
- √ Funding Options
- √ Schedule for Implementation





Next Study Update.... Final Public Meeting – February/ March 2022

FOR MORE PROJECT INFO...



Study Webpage

https://seda-cog.org/departments/flood-resiliency/columbia-county-flood-mitigation-studies

Send Questions/ Comments

floodstudy@borton-lawson.com







THANK YOU!

Questions?





WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY

FINAL PUBLIC MEETING MARCH 10, 2022



This study has been financed by grants from the Commonwealth of Pennsylvania, Commonwealth Financing Authority and the Department of Community and Economic Development.

Welcome

COLUMBIA COUNTY BOARD OF COMMISSIONERS

Chris Young, Chairman Richard Ridgway David Kovach

COLUMBIA COUNTY RESILIENCY OFFICE

Eric Stahley
Columbia County Resiliency Officer

SEDA-COUNCIL OF GOVERNMENTS

Teri Provost

Director, Housing Rehabilitation and Flood Resiliency
Geralee Zeigler
Program Analyst, Flood Resiliency



Study Team



Columbia County – Study Sponsor SEDA-COG – Study Administrator





Brozena Consulting Services, LLC







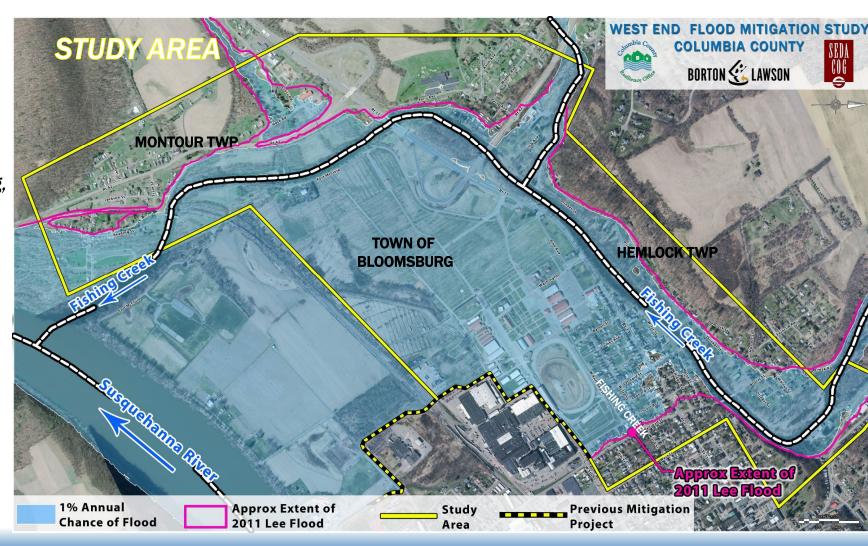


West End Flood Study Area

Floodplains of Fishing Creek in Town of Bloomsburg, Hemlock Twp & Montour Twp

~500 parcels

~350 structures





Purpose & Goals of Study

Identify and Determine Best Structural and Non-Structural Flood Mitigation Alternatives:

- Provide flood resiliency reduce long-term risk to loss of life and property damage
- Minimize future flooding impacts on Community
- Identify possible funding sources
- Reduce impacts of increasing flood insurance premiums



Overview of Study - Major Tasks

- Inventory of Parcels & Structures Mailed Surveys, Field Survey, First Floor Elevations, Parcel Data
- Stakeholder Meetings to Obtain Input
- Hydrologic & Hydraulic Modeling of Fishing Creek
- Identified Flood Mitigation Alternatives
- Evaluated Flood Mitigation Alternatives Impact, Cost-Benefit Analysis, Funding



Flood Mitigation Projects Considered

Non-Structural Mitigation Projects

- Residential Structures in Floodway Acquisition/Demolition
- Residential Structures in Floodplain Acquisition/ Demolition, Elevations or Mitigation Reconstruction
- Commercial Buildings Wet Floodproofing
- Other Emergency Access Roads, Floodproofing Wastewater/Utility
 Systems, Emergency Action Plans, Additional Stream Gauges, Ordinances

Structural Mitigation Projects

- Levee/ Floodwall Systems
- Channel/ Floodplain Modifications

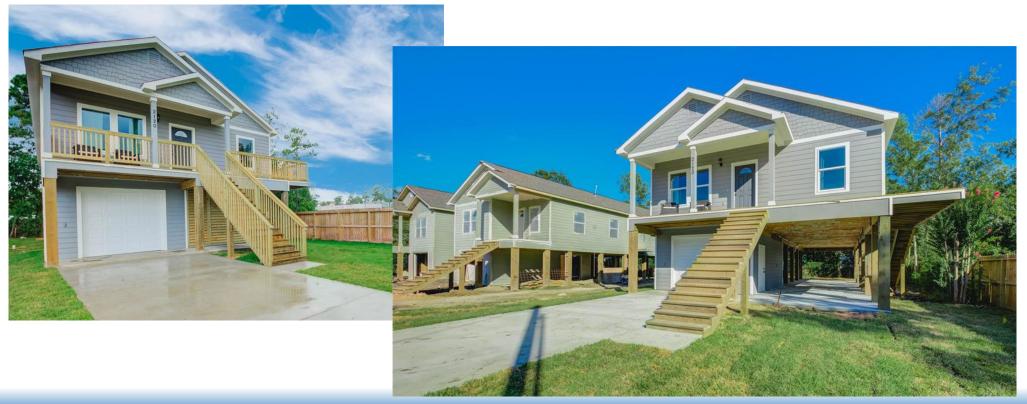


Typical Non-Structural Mitigation – Elevations



Non Structural Mitigation – Mitigation Reconstruction

Example Rebuild with An Elevated Home at Same Location





Analysis of Flooding Impacts

Structure Flooding Analysis - Flood Lee

- Historical Accounts High Water Marks
- H&H Modeling, First Floor Elevations, GIS Mapping
- Structure Flood Depths utilized for evaluation of Mitigation Alternatives, Benefit-Cost Analysis, and FEMA Criteria for Funding projects



Analysis of Lee Flooding Depths-above 1st Floor Elevation





6' - 8' Above First Floor (1) 8' - 10' Above First Floor (0) 10' - 14' Above First Floor (0)

Analysis of Lee Flooding Depths-above 1st Floor Elevation





- Above First Floor (5)
- Above First Floor (2)
- Above First Floor (0)
- 8' 10' Above First Floor (0)
- 10' 14' Above First Floor (0)

Analysis of Lee Flooding Depths-from 1st Floor Elevation





Legend

- 1% Annual Chance of Flooding
 Floodway
- Approx Extent of 2011 Lee Flood
- Study Area

Depth of Flooding

- No Flooding (17)
- Basment Only (16)
- 0' 2' Above First Floor (83)
- 2'-4' Above First Floor (91)
- 4' 6' Above First Floor (34)
- 6' 8' Above First Floor (20)
- 8' 10' Above First Floor (7)
- 10' 14' Above First Floor (29)

Analysis of Lee Flooding Impacts from 1st Floor

TOTALS

Bloom		Hemlock	[Montour	•	Project Wi	de
Basement Only:	16	Basement Only:	3	Basement Only:	1	Basement Only:	20
0' - 2'	83	0' - 2'	12	0' - 2'	2	0' - 2'	97
2' - 4'	91	2' - 4'	5	2' - 4'	2	2' - 4'	98
4' - 6'	34	4' - 6'	2	4' - 6'	3	4' - 6'	39
6' - 8'	20	6' - 8'	0	6' - 8'	1	6' - 8'	21
8' - 10'	7	8' - 10'	0	8' - 10'	0	8' - 10'	7
10' - 14'	29	10' - 14'	0	10' - 14'	0	10' - 14'	29
Total:	280	Total:	22	Total:	9	Total:	311
No Flooding:	17	No Flooding:	13	No Flooding:	15	No Flooding:	45
Total		Total		Total		Total	
Evaluated:	297	Evaluated:	35	Evaluated:	24	Evaluated:	356



FEMA Funding Criteria Non-Structural Mitigation

FEMA Pre-Calculated Benefit Acquisitions: \$323,000 per structure Voluntary Program

- Project deemed eligible when project cost is less than \$323,000
- If project costs is greater than \$323,000, need to show Benefit-Cost Ratio (BCR) > 1

~90% Residential Properties in Floodplain will qualify under FEMA Pre-Calculated Benefits

25% Local Share required with FEMA FMA and BRIC programs; HMGP no local share



FEMA Funding Criteria Non-Structural Mitigation

FEMA Pre-Calculated Benefit Elevations & Mitigation Reconstruction: \$205,000 per structure Voluntary Program

- Project deemed eligible when project cost is less than \$205,000
- If project costs is greater than \$205,000 need to show BCR > 1

Other funding required when:

- The homeowner desires a higher elevated home resulting in a greater costs than covered by FEMA (BFE + 2' or Flood of Record Elev.)
- If BCR is less than 1 (using FEMA Benefit-Cost Analysis) not eligible
- 25% Local Share required with FEMA FMA and BRIC programs; HMGP no local share



Benefit-Cost Analysis (BCA)

BCA used to determine Cost Effectiveness

- FEMA Methodology
- Calculated Benefit-Cost Ratio (BCR) for each property and for total Aggregate
- Inputs included Building Replacement Value, Square Footage, Modeled Depth of First Floor Flooding
- Considered Site Conditions (structure type, basement, USACE Generic Depth Damage Curves determined expected damages and costs based on range and frequency of flood events)
- Mitigation Costs (Levee, Acquisitions, Elevation or Mitigation Reconstruction)
- Incorporated Environmental and Social Benefits



Flood Mitigation Alternatives

Non-Structural Flood Mitigation Alternatives Evaluated For Each Municipality

Montour Township

Hemlock Township

Town of Bloomsburg



Montour Township

- FEMA Buyouts Voluntary
- FEMA Elevations Voluntary
- RV Park Emergency Action Plan
- 3 Sanitary Pump Stations Dry Floodproof
- Construct Emergency Access Route from Reading St to Jackson St across RR Montour Twp
- Ordinance Revisions Floodplain Management
- Evaluate County Building for Floodproofing



MONTOUR TOWNSHIP EMERGENCY EVACUATION ROUTE VIA JACKSON STREET



ESTIMATED COST = \$125,000

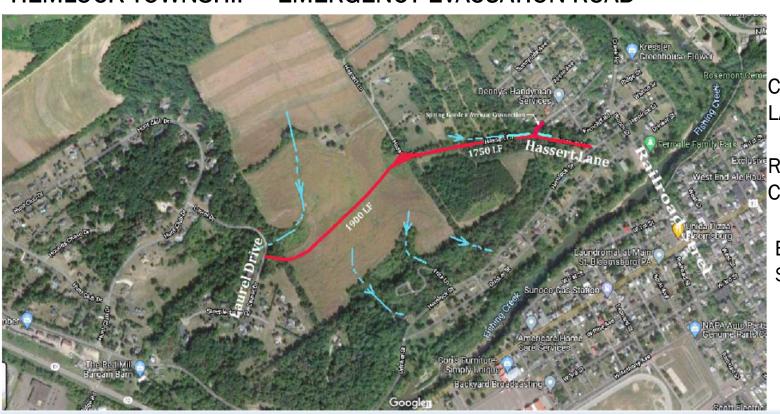


Hemlock Township

- FEMA Buyouts Voluntary
- FEMA Elevations Voluntary
- Emergency Access Road Hassert to Laurel Street
- Ordinance Revisions



HEMLOCK TOWNSHIP - EMERGENCY EVACUATION ROAD



CONNECTS HASSERT
LANE TO LAUREL DRIVE

REQUIRES LAND OWNER COOPERATION

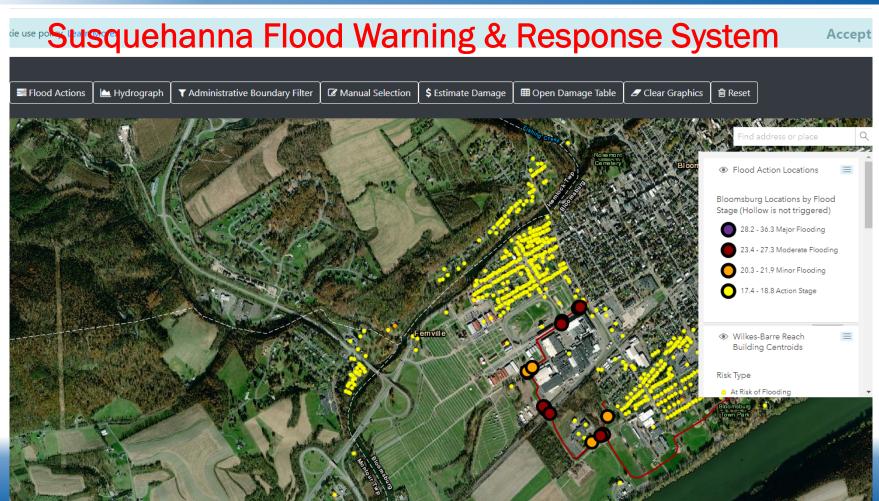
ESTIMATED COST = \$600,000



Town of Bloomsburg

- FEMA Buyouts Voluntary
- FEMA Elevations Voluntary
- Wet Floodproofing Commercial Buildings
- Emergency Evacuation Notification Siren (by W. First Street)
- Fishing Creek Radar Gauge at Railroad Street
- Fairgrounds Additional Floodproofing
- Ordinance Review Floodplain Management





Is There a Better Way?

- RetroFIT Charlotte-Mecklenburg, North Carolina (2016)
 - Full range of flood mitigation options
 - Funded by County Stormwater Services Flood Mitigation Capital Budget
 - Property owner provides financial contribution, sliding scale
- Valmeyer Acquisition Monroe County, Illinois (1993)
 - Acquired 242 Properties and relocated to high ground
 - Completed in 2 years
 - FEMA HMGP, State, EDA Funding
- Isle De Jean Charles Resettlement, Louisiana (2016)
 - Acquired 515 acres for 120 residential properties, commercial, retail, public spaces on higher ground
 - State CDBG Funding



National Flood Insurance Program

NFIP Risk Rating 2.0

Changes

- Changes from Zone to Individual Rating
- Zone changes smaller difference in costs
- Replacement cost is part of premium calculation
- No elevation certificates needed
- Premiums reflect unique flood risk

Staying the Same

- Statutory rate caps on annual premium increases
- Availability of premium discounts
- Transfer of policy discounts to new owners
- FIRM's used for mandatory purchase and Floodplain Management
- FEMA Community Rating System discounts



National Flood Insurance Program

Existing Rating Methodology

FEMA-sourced data

Rating Variables

- · Flood Insurance Rate Map Zone
- Base Flood Elevation
- Foundation Type
- Structural Elevation (Special Flood Hazard Area Only)

1% Annual Chance of Flooding (Frequency)

Fees and Surcharges





Risk Rating 2.0: Equity in Action Methodology*

FEMA-sourced data

Additional data sources: Federal governmentsourced data, commercially available third-party

Cost to Rebuild

Rating Variables

- Distance to Coast/Ocean/River
- River Class
- Flood type Fluvial/Pluvial
- Ground Elevation
- First Floor Height
- Construction Type/Foundation Type

Broader Range of Flood Frequencies

Fees and Surcharges

*Additional variables are not shown here



H&H Evaluation of Fishing Creek – Channel Modifications to Reduce Flooding

- Lee Flood is considered 300-Year Flood on Creek and 200-Year Flood on River.
- Evaluated existing creek channel to reduce Base Flood and Storm Lee Flood Elevations. Doesn't mitigate flooding to degree necessary for Bloomsburg or Hemlock Twp.
- Railroad Street Bridge and Stream Floodplain modifications provide significant reduction for Fernville flooding in vicinity of Railroad St Bridge and can mitigate some induced flooding from levee on Bloomsburg side.
- Dredging not feasible. Rock in stream bed prevents adequate excavation.



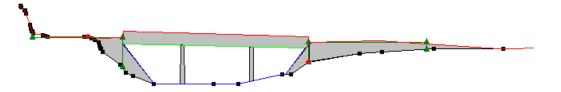
Fishing Creek 2011 Record Flood

2011 FERNVILLE FLOODING AT RAILROAD STREET BRIDGE

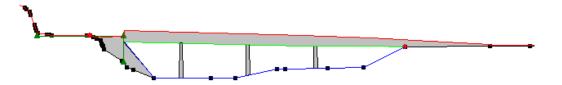
Fishing Creek 2011 Record Flood







EXISTING RAILROAD STREET BRIDGE - FACING DOWNSTREAM



LENGTHENED RAILROAD STREET BRIDGE WITH BENCHED FLOODPLAIN - FACING DOWNSTREAM



BENCHED FLOODPLAIN BENEFITS:

- Compensates for lost conveyance in Bloomsburg Floodplain with levee option
- Allows more flow through RR St Bridge rather than through Fernville
- Environmental benefits of creek to Floodplain during lower flood flows.

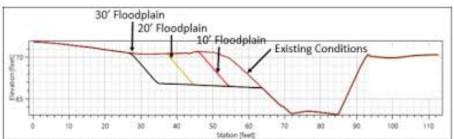


Figure 24. Typical cross section showing the three different floodplain bench alternatives.





FISHING CREEK HYDRAULICS

100-YR EVENT

REDUCTION OF **EXISTING** FLOOD LEVELS

Modification Alternatives	Near Hock Road	@ Route 42 Bridge	@ Barton Street	Above RR ST Bridge
Remove Covered Bridge & Railroad Bridges	2.1 FT	0.0 FT	0.0 FT	0.0 FT
Remove Route 11 & 42 Interchange Ramp Fill	0.0 FT	0.3 FT	0.2 FT	0.0 FT
Remove Existing Island	0.0 FT	0.0 FT	0.0 FT	0.1 FT
Excavate Benched Floodplain and Modify RR St Bridge	0.0 FT	0.0 FT	0.2 FT	3.0 FT
Remove Railroad Street Bridge	0.0 FT	0.0 FT	0.0 FT	2.6 FT



Full Floodwall/ Levee System Bloomsburg 6,200 LF

Total Estimated
Cost
\$29 million



Structural Flood Mitigation (Levees)

Full Levee System - West End of Bloomsburg

- Length of Floodwall System 6,200 Feet (1.2 Miles)
- Induced flooding
 - Upstream of Railroad Street Negligible
 - ➤ Downstream of Railroad Street along levee length 1.8 Feet

Must be Mitigated to Zero



H&H Evaluation – Mitigate Fishing Creek Impacts

MITIGATION OF INDUCED FLOODING

100-YR EVENT

REDUCTION OF **INDUCED** FLOOD LEVELS FROM LEVEE

Location	Indused Flooding	Mitigation Alternatives			
Location	Induced Flooding	Excavate Flood Bench & Modify RR Street Bridge	Replace all Bridges		
Barton St	2.5 FT	-1.1 FT	-0.6 FT		
Leonard St	2.4 FT	-1.5 FT	-1.0 FT		
Scott Ave	1.9 FT	-2.0 FT	-1.7 FT		
Hemlock St	0.0 FT	-1.0 FT	-1.0 FT		



Flood Mitigation - Structural Mitigation (Levee)

Benefits:

- Protect 294 Structures (including Fairgrounds Bldgs) in Floodway, Floodplain,
 Zone x
- Total Property value = \$42.9 Million
- Total Taxes Generated = \$657,000

Challenges:

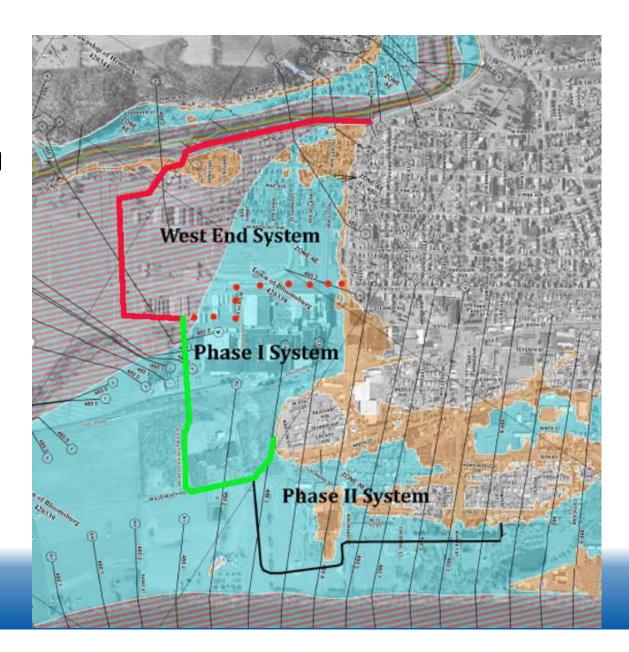
- Permitting Levee in Floodway / Eliminate Induced Flooding
- Property Acquisitions

Schedule:

- Engineering, Permitting, Property Acquisition 18 to 20 months
- Construction 20 months



OVERALL LEVEE/ FLOODWALL SYSTEM CONFIGURATION



FEMA BENEFIT-COST ANALYSIS FLOOD MITIGATION ALTERNATIVES

Municipality	Flood Mitigation Alternative	Estimated Cost (w/ Maintenance Costs) Over Life of System**	Benefit-Cost Ratio (BCR) BCR > 1 indicates "Cost Effective"
Bloomsburg	Levee System	\$30 Million	3.65
	Residential Acquisition – Floodway & Floodplain*	\$45 Million	2.07
	Residential Floodplain Elevation & Floodway Buyout*	\$42.6 Million	1.84
	Residential Floodplain Mitigation Reconstruction & Floodway Buyout*	\$52.9 Million	1.47
Hemlock	Residential Acquisition*	\$6.3 Million	2.39
	Residential Elevation*	\$4.3 Million	2.08
Montour	Residential Acquisition*	\$4.3 Million	2.65
	Residential Elevation*	\$3.3 Million	0.63

^{*}Calculated with 100% participation.

^{**}Life of System for BCR calculations - Levee = 50 yrs, Acquisition = 100 yrs

BORTON LAWSON

Funding - Non Structural Mitigation

FEMA Grant Programs

Hazard Mitigation Grant Program - HMGP

Flood Mitigation Assistance - FMA

Building Resilient Infrastructure and Communities – BRIC

- US Department of Housing and Urban Development HUD CDBG-DR
- American Flood Coalition

Flood Funding Finder, resource for flood mitigation funding information

https://floodcoalition.org/resources/floodfundingfinder/



Helping small communities fund resilience

Across the country, small communities are on the front lines of protecting residents from flooding and sea level rise. The challenges of flooding can be especially daunting for smaller and rural communities, but these are the very places that are critical to the country's overall resilience to flooding. From assessing risk to implementing projects, small communities can face enormous costs that they often cannot cover alone. Several federal agencies have programs that fund flood mitigation, flood risk reduction, and disaster recovery, but navigating these funding opportunities can be time-consuming and difficult.

The American Flood Coalition's Flood Funding Finder is the first tool of its kind that uses a robust filtering system to prioritize the needs of small communities and help them identify the right federal funding programs to fund flood resilience. While the Flood Funding Finder makes it easier to access federal funding, funding for resilience remains insufficient and does not work for many communities across the country. The American Flood Coalition exists to push for more accessible and robust funding that meets the reality of higher seas, stronger storms, and more frequent flooding.

Launch the Flood Funding Finder tool



Funding - Structural Mitigation Systems (Levee)

- FEMA Building Resilient Infrastructure and Communities BRIC
- FEMA Flood Mitigation Assistance FMA
- The <u>Federal Infrastructure Bill</u> contains billions for flood mitigation and coastal restoration from storms. The Senate version of the bill contains \$3.5 billion for FEMA's Flood Mitigation Assistance program, and \$1 billion for FEMA BRIC
- State



Study Summary

Study Summary

- Flood Insurance April 2022, All existing policies renewing under Risk Rating
 2.0, Contact Your Insurance Carrier
- Flood Mitigation Alternatives Non Structural & Structural (Levee) Alternatives are Cost Effective (Benefit-Cost Ratios > 1), some Non Structural require individual analysis
- County and Municipalities Determine Mitigation Alternatives to Implement
- Challenges
 - Acquisitions/ Elevations/ Mitigation Reconstruction Voluntary Program
 Commercial Properties Funding Options
 - ☐ Levee Further Analysis of Impacts/ Mitigation of Induced Flooding
 - Levee Permitting in Floodway



Next Steps - Final Study Report to be Published

WILL BE AVAILABLE FOR PUBLIC



Study Webpage

https://seda-cog.org/departments/flood-resiliency/columbia-county-flood-mitigation-studies

Send Questions/ Comments

floodstudy@borton-lawson.com







THANK YOU!

Questions?





Making Our Client's Vision a Reality

MEETING MINUTES

RE: Flood Study Team Meeting with Town of Bloomsburg

Columbia County West End Flood Mitigation Study

DATE & TIME OF

September 30, 2021

MEETING:

10:00AM - 11:30AM

LOCATION:

Town Hall - Council Chambers

MEETING ORGANIZER:

Borton-Lawson

ITEMS FOR DISCUSSION:

I. Introduction/Overview of Meeting

The meeting was lead by Borton-Lawson (BL) and BL's sub-consultant Jim Brozena of Brozena Consulting. Teri Provost from SEDA-COG was also present at the meeting, as well as numerous representatives from the Town of Bloomsburg including the mayor, Town Manager, Director of Public Works, Director of Governmental Services and lead for management of Floodplain Ordinance, and Police Sergeant responsible for emergency services.

The purpose of the meeting was to introduce Bloomsburg representatives to the West End Flood Mitigation Study as well as obtain feedback from the Town as related to parcels located within the floodway and floodplains in the study area located in Bloomsburg, obtain feedback on properties that have been or are in the process of acquisition, and obtain feedback on preferences for flood mitigation alternatives.

II. Attendees

Town of Bloomsburg

Justin Hummel - Mayor

Lisa Dooley - Town Manager

Charles Fritz - Director of Governmental Services

John Fritz - Director of Public Works

Emergency Services/ Police Sergeant

SEDA- Council of Government

Teri Provost - Director of Flood Resiliency and Housing

Borton Lawson Engineering

Samantha Albert – Project Manager, Water Services Leader Tom Lawson –,Technical Lead, Senior Engineer

Jim Brozena - Brozena Consulting, Inc. - Nonstructural Mitigation Lead

III. Study Objectives and Timeline

The primary purpose of the West End Flood Mitigation Study is to identify potential flood mitigation alternatives for the West End section of the Town of Bloomsburg. Mitigation alternatives are classified into either structural (earthen levee/flood wall) or non-structural (home acquisitions, elevation raisings, flood proofing, etc). The

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Study will evaluate induced flooding as a result of structural alternatives and also financial impacts to the Town and community as a result of non-structural alternatives.

The first public meeting was held on July 29th. A second Public meeting is tentatively scheduled for late November 2021. The final public meeting will take place at the conclusion of the study in March 2022.

IV. Data/Map Review

An overview of various maps prepared by BL was completed. This included a map showing the study area, a color-coded parcel map showing modeled depths of flooding from 2011 Lee Flood in structures, and a map showing structures in the Floodway and Floodplains. The maps also identified the approximate extents of Tropical Storm Lee flooding. The color coded parcel map identified vacant parcels, buyout parcels, and parcels located within the FEMA designated floodway and floodplain. Town officials were asked to provide feedback on the accuracy of the maps and noted that the Tropical Storm Lee flood extents appears reasonably correct.

V. Public Survey

BL briefly discussed the property owner survey that was mailed out to owners of all properties within the floodway/floodplain. The mailed survey is the same survey that is also available online in electronic format. Field topographic survey and property surveys are scheduled to take place in October by BL's surveyors and engineers. Discussion with the Town on notifying property owners of this field work in the newspaper and in the survey letters. The purpose of the field survey is to obtain structure information and first floor elevations.

VI. Discussion Points

- An abbreviated PowerPoint presentation was provided by BL to the attendees reviewing the goals and purpose of the study and what types of flood mitigation alternatives are to be evaluated as part of the study.
- 2. Group discussion on the make-up of the study area within Bloomsburg West End number of renters versus owners, number of residential versus commercial properties. BL requested the current list of renters from the Town if that was available. BL also requested current list of RL and SRL properties.
- 3. BL/ Jim Brozena requested updated list of properties within the Town that will participate in any buyout programs.
- 4. BL indicated that the Fairgrounds property is listed as a commercial property on the County GIS tax database.
- 5. The Town handles acquisitions/buyouts themselves and does not go through SEDA-COG. They are a direct entitlement community for CDBG.
- 6. Discussion on impacts to tax base with acquisition of structures within the floodway and floodplain. The Town expressed concern with loss of property taxes with this option. Town does not prefer the option of acquisition/demolition of all the properties in the floodway and floodplain. The Town indicated that they receive about \$200,000 per year in amusement tax from the Fair.



- 7. Town expressed concerned with low property values within the floodway and floodplain areas. Concerned with fair buy out values to property owners so they are not hurt financially. The Mayor specifically expressed concern for disabled veterans who may own property in the floodway/floodplain areas, whose properties are tax exempt, and being compensated fairly for buy outs.
- 8. Discussion on benefits to the Town of not having structures in the floodway and floodplains.
- 9. Town suggested study area may include low to moderate income area. BL to verify as part of study.
- 10. Discussion on the ability to bring in fill in the floodplain to raise grade of properties. This would not be allowed in the floodway, and if it were done on a large scale in the floodplain modeling would need to be completed to evaluate impact. Also need to consider if this is in conflict with Town's Floodplain Management Ordinance.
- 11. Discussion on the use of eminent domain to require homeowners to rebuild in Zone X or outside of Floodway and Floodplain. All generally agreed it would be difficult process to implement, would not be received well by residents, overall not preferred.
- 12. Discussion on the concept of Mitigation Reconstruction for homes in the floodplain demolish home and potentially subdivide parcel if footprint allows, and rebuild new home at higher/floodproof elevation the Mayor liked this option.
- 13. The Town indicated that it was extremely difficult to get the current Floodplain Ordinance adopted, and did not think it would be possible by the Town to amend this ordinance to regulate structures within Zone X. BL requested a copy of the Town's current floodplain ordinance.
- 14. Town discussed their desire to have a stream gage added to Fishing Creek to monitor stream levels, possibly at Railroad Street.
- 15.BL reviewed proposed levee alignment concepts and associated preliminary cost estimates. Also review a low height levee concept along Fishing Creek that could effectively change a portion of the floodway to a floodplain, which allows more funding for elevations and mitigation reconstruction projects.
- 16.BL reviewed the concept to rebuild homes on higher ground within the Town limits. Three parcels of vacant land on high ground, brought to BL's attention by the County, were discussed with the Town as an option for rebuilding homes.
- 17. Teri Provost suggested looking at the American Rescue Plan Act and use for under QCTs (Qualified Census Tracts).
- 18. The Town will provide BL the list of parcels they own.



- 19.BL discussed that the Bloomsburg Municipal Authority reached out to them to inquire as to why they were not included in this study, and then requested BL provide a proposal to complete a flood mitigation study for their WWTP facility.
- 20. The Town indicated that they currently have a Code Red system but they may not be keeping it.
- 21. Discussion on the Town's Evacuation Plan. There is good communication in place, biggest concern is Fishing Creek flash flooding. The Town has an Emergency Action Plan from the County and they use the same plan.
- 22. BL will inform the Town when the BL surveyors and engineers will be in the Town performing topographic and physical structure surveys. The Town mentioned that posters regarding the mailed homeowner surveys and the upcoming field survey could be posted on Leonard & West Main St for public viewing.





Making Our Client's Vision a Reality

MEETING MINUTES

RE: Flood Study Team Meeting with Montour Township

Columbia County West End Flood Mitigation Study

DATE & TIME OF

MEETING:

September 16, 2021 1:00PM - 2:30PM

LOCATION: Montour Township Municipal Building

195 Rupert Drive

MEETING ORGANIZER:

Borton-Lawson

ITEMS FOR DISCUSSION:

I. Introduction/Overview of Meeting

The meeting was lead by Borton-Lawson (BL) and BL's sub-consultant Jim Brozena of Brozena Consulting. The purpose of the meeting was to introduce Montour Township (Township) representatives to the West End Flood Mitigation Study as well as obtain feedback from the Township related to parcels located within the floodway and floodplains in Montour Township section of the study area.

II. Attendees

A sign-in sheet was provided at the meeting and is attached to these minutes.

III. Study Objectives and Timeline

The primary purpose of the West End Flood Mitigation Study is to identify potential flood mitigation alternatives for the West End section of the Town of Bloomsburg. Mitigation alternatives are classified into either structural (earthen levee/flood wall) or non-structural (home acquisitions, elevation raisings, flood proofing, etc). The Study will evaluate induced flooding as a result of structural alternatives and also financial impacts to the township and community as a result of non-structural alternatives.

The first public meeting was conducted on July 29th.

A second Public meeting is tentatively scheduled for late November.

The final public meeting will take place at the conclusion of the study in March.

IV. Data/Map Review

Jim Brozena of Brozena Consulting Services provided township officials an overview of a color-coded parcel map prepared by Borton-Lawson. The map identified approximate extents of Tropical Storm Lee flooding as well as vacant parcels, buyout parcels, and parcels located within the FEMA designated floodway and floodplain. Township officials were asked to provide feedback on the accuracy of the maps and noted that the Tropical Storm Lee flood extents appears reasonably correct.

V. Public Survey

Samantha Albert briefly discussed the property owner survey that was mailed out to owners of all properties within the floodway/floodplain. The mailed survey is the same survey that is also available online in electronic format. Physical property

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surveys will take place at a later date to collect structure information and determine first floor elevations.

VI. Discussion Points

- 1. 9 Perry Avenue was identified for acquisition. Residents moved in without permission and Township lawyers are currently involved.
- 2. The county building located on Perry Avenue has experience frequent flooding damage and is currently not used except for the rear of the building which is still utilized by the maintenance department.
- 3. Most of the trailers located within the trailer park on Perry Avenue were flooded as a result of Tropical Storm Lee. The preliminary FEMA mapping shows the special flood hazard area increasing on this property.
- 4. The Montour Township ordinance regulates the 500-year floodplain by requiring permits for any development within this zone.
- 5. An evacuation plan is required from the RV park by the township ordinance. Regulations are not followed and an evacuation plan has not been provided as of this time.
- 6. The township is interested in buying out a property along Hemlock Creek where inoperable vehicles are stored on the property and near the creek.
- 7. An error was noted on the parcel map at 238 Jackson Street. The property where the police station and maintenance buildings are located is identified as vacant.
- 8. There are three (3) sanitary pump stations located within the study area that are impacted by flooding.
 - a. Pump Station on Hock Road becomes inundated and needs to be raised.
 - b. Pump Station on Perry Avenue has had electrical components raised.
 - c. Design has been completed to raise the electrical components of the pump station located near the campground.
- The Township expressed frustration with previous experience participating in property buyout programs. Montour Township was forced to take out a loan for several hundred thousand dollars to complete the acquisitions and was not made whole for several years.
- 10. A discussion on Legion Road, although outside of the project study limits, revealed that Legion Road was not flooded in Tropical Storm Lee; however, the bend of the creek flooded as was Thunder Chicken Auto Sales. One home has been acquired in this area and the Township continues to pursue action using code enforcement and buyouts.



Click Here and Type Date - Page 3

11. Borton-Lawson will inform Montour Township when the survey mailings have been sent and when crews will be in the township performing physical structure surveys.





Making Our Client's Vision a Reality

SIGN IN SHEET

RE:

Meeting - Flood Study Team with Montour Township

Columbia County West End Flood Mitigation Study

DATE & TIME OF MEETING:

September 16, 2021

1;00PM -2:30PM

LOCATION:

Montour Township Municipal

195 Rupert Drive

Building

MEETING ORGANIZER:

Borton-Lawson

4	NAME	ODCANIZATION	- FNANU
	NAME	ORGANIZATION	EMAIL
	SAMANTHA ALBEM	BONDOW LAWYON	I salbert @ borrow laws
	Clint Sorber	Borton-Lawson	Csorber@borton-lawson.com
	Lori Ebright	Montour Twp	lorie Montour township
	Mex Stoner		maxaglaceeng.com
	Fishley Ebnaht	Montour Tup	acbrighte montourtourshp.
	Perny tellart	Muniour Twp	teckar+Cpta.net
	MIKE HINKLE	Monitare Tel	MIKE HINKLE 251@G MAIL. G.
	Jim Brozena	BROZANA GUSULTAL SER	Trosano prosend course Hud.
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MEETING MINUTES

RE: Flood Study Team Meeting with Hemlock Township

Columbia County West End Flood Mitigation Study

DATE & TIME OF

September 23, 2021

MEETING:

9:00AM - 10:30AM

LOCATION:

Hemlock Township Municipal Building 26 Firehall Road

MEETING ORGANIZER:

Borton-Lawson

ITEMS FOR DISCUSSION:

I. Introduction/Overview of Meeting

The meeting was conducted by Borton-Lawson Engineering and Brozena Consulting Services. The purpose of the meeting was to introduce Hemlock Township representatives to the West End Flood Mitigation Study which includes the Town of Bloomsburg, Montour Township, and Hemlock Township as key stakeholders.

II. Attendees

A sign-in sheet was provided at the meeting and is attached to these minutes.

III. Study Objectives and Timeline

The primary purpose of the West End Flood Mitigation Study is to identify potential flood mitigation alternatives for the West End section of the Town of Bloomsburg. Mitigation alternatives are classified into either structural (earthen levee/flood wall) or non-structural (home acquisitions, elevation raisings, flood proofing, etc). The Study will evaluate induced flooding as a result of structural alternatives and also financial impacts to the township and community as a result of non-structural alternatives.

- -The first public meeting was conducted on July 29th.
- -A second Public meeting is tentatively scheduled for late November.
- -The final public meeting will take place at the conclusion of the study in March.

IV. Data/Map Review

Jim Brozena of Brozena Consulting Services provided township officials an overview of a color-coded parcel map prepared by Borton-Lawson. The map identified approximate extents of Tropical Storm Lee flooding as well as vacant parcels, buyout parcels, and parcels located within the FEMA designated floodway and floodplain. Township officials were asked to provide feedback on the accuracy of the maps and noted that the Tropical Storm Lee flood extents appear reasonably correct.

There are approximately 126 parcels within the study area in Hemlock Township. Approximately 37 parcels are impacted by either the floodway or floodplain.

V. Public Survey

Samantha Albert briefly discussed the property owner survey that was mailed to owners of all properties within the floodway/floodplain. The mailed survey is the

September, 24, 2021

same survey that is also available online in electronic format. Physical property surveys will take place at a later date to collect structure information and determine first floor elevations.

VI. Discussion Points

- 1. Borton-Lawson informed Hemlock Township that residents should soon be receiving surveys that were sent via US mail. Borton-Lawson will also inform the township when crews will be performing physical structure surveys.
- 2. A large number of buyouts occurred as part of an HMGP Project (~2013) after Tropical Storm Lee in 2011. Properties that withdrew or were administratively withdrawn include:
 - a. 24 William Street
 - b. 270 William Street
- 3. Eric Stahley asked if the properties within the study area are renters or owners. Michele Bella replied that properties are primarily owner occupied.
- 4. It is noted that many of the homes located along the upper side of Drinker Street, though situated on higher ground, still experience significant basement flooding. 399 Drinker Street was highlighted as experiencing basement flooding to the floor joists during Tropical Storm Lee.
- 5. Evacuation Routes and Planning are a priority for the Township as many properties become isolated when Fishing Creek flooding occurs.
 - Red Mill Road floods blocking evacuation to the west.
 - Bloom Street/Creek Road floods blocking evacuation to the east.
 - Jim Brozena mention the potential of constructing a gated stone road connecting Hassert Lane to Laurel Drive to serve as an emergency evacuation route. Hemlock Township officials replied that there is an existing field road from Red Mill Road that has been used by emergency services to reach otherwise inaccessible areas.
 - A deep gully between Hassert Lane and the Ferncliff Road community would prevent these residents from utilizing this potential evacuation route if Bloom Street is flooded unless a bridge or culvert was constructed across the gully.
 - A solution providing an alternative exit route does not solve the issue of flooding along Creek Road. Township officials are interested in a plan to raise the profile of Creek Road above the floodplain.
- 6. The implementation of a structural flood mitigation solution in the West End of Bloomsburg would result in induced flooding on the opposite bank in the community of Fernville. Induced flooding could impacts homes which are not currently impacted or homes which have already been elevated. A structural option such as a floodwall or earthen levee would include a mitigation component for impacted communities upstream and downstream of the project.
- 7. Hemlock Township has a sewer co-op. A sanitary pump station located at Red Mill Road and Drinker Street has been elevated.
- 8. Hemlock Township is located in the Bloomsburg School District.





Making Our Client's Vision a Reality

SIGN IN SHEET

RE: Flood Study Team Meeting with Hemlock Township

Columbia County West End Flood Mitigation Study

DATE & TIME OF September 23, 2021 **MEETING:** 9:00AM - 10:30AM

LOCATION: Hemlock Township Municipal 195 Rupert Drive

Building

MEETING Borton-Lawson

ORGANIZER:

NAME	ORGANIZATION	EMAIL
Samantha Albert	Borton-Lawson	salbert@borton-lawson.com
Clint Sorber	Borton-Lawson	csorber@borton-lawson.com
Jim Brozena	Brozena Consulting	jbrozena@brozenaconsulting.com
Eric Stahley	Columbia County	estahley@columbiapa.org
Michelle Bella	Hemlock Township	bella@hemlocktownship.org
Jeff Sutton	Hemlock Township	sutton@hemlocktownship.org
Dan Carr	Hemlock Township	dancarr1@verizon.net
Scott Traugh	Hemlock Township	traugh@hemlocktownship.org
Andy Keister	MKA	akeister@mctish.com
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WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY, PENNSYLVANIA

Appendix E

Mitigation Alternatives and Concept Plans

WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY, PENNSYLVANIA

Appendix E – Mitigation Alternatives and Concept Plans

TABLE OF CONTENTS:

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- **E.2** Prioritization Process
- E.3 Proposed System Rendering
- E.4 Levee/ Floodwall System Description
- E.5 Concepts Plans, Sections, and Typical Details

WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY, PENNSYLVANIA

Appendix E

Mitigation Alternatives and Concept Plans

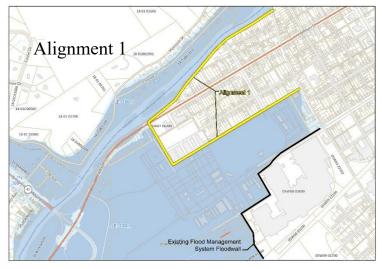
E.1 Mitigation Alternatives

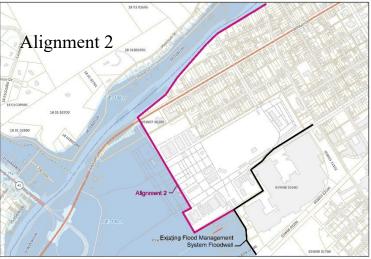
The floodwall or levee system alternative for the west end of Bloomsburg considered impacts to the Town tax base and the community fabric, present and future. Two alignments were considered as shown and outlined below:

Alignment 1 would be a levee or floodwall system extending along the left bank of the creek from the Railroad Street Bridge westward, then south to a point where it would turn east resulting in a U-shaped system tying out to high ground near Scott Avenue and W. Anthony Street. This alignment would avoid the Fairgrounds to minimize disruption to access points and the general operation of the facility. It was also thought to be more economical.

Right-of Way constraints limited the type of system options to an H-pile or sheetpile floodwall.

Alignment 2 (*pictured right*) would extend through the Fairgrounds to tie into the first floodwall system in the vicinity of 6th Street. The Fairgrounds expressed interest in participating in this alignment due to the repeated flooding on their large parcel with 54 structures.





This alignment was not as limited as Alignment 1 with regard to right-of-way thus permitting the use of more economical earth and MSE levees.

E.2 Prioritization Process

Prioritizing structural system alignments usually depends on the number and type of structures behind the system, available real estate, community support, permitting issues, and the total project cost. Alignment #1 is actually higher in cost as #2 with 54 fewer buildings behind the system.

The fairgrounds also overwhelmingly supports alignment 2 even though it will require a sizeable area for the system footprint and access easements.

Alignment #2 was carried forward for final consideration as a structural system.

E.3 Proposed System Rendering

The proposed alignment is shown below as a schematic level concept without the benefit of detailed design documentation and analysis. The Fishing Creek floodway will be encroached upon in a significant way. The flow depths through the floodway area are shallow however, an H&H analysis performed to verify the induced flooding impacts resulted in about two (2) feet of increase in the base flood levels. This



must be decreased through mitigation efforts to zero feet.

The alignment minimizes property takes, however, several properties will need to be acquired and as many as nine other properties will require partial takes for removal of garages and sheds along the levee alignment. Arriving at the proposed alignment considered the construction cost and the impact of reducing the tax base with property takes.

The system features represent the proper mix of context sensitive floodwall and levees on the most cost effective alignment for flood mitigation. A cost estimate for the proposed alignment was developed for the economic analysis. A summary of the estimate is included at the end of this section.

Hydraulic analysis of the system was performed to determine induced flooding impacts up and down stream and the impact on obtaining FEMA approval for a structural system in the creek floodway.

E.4 Levee/ Floodwall System Description

The recommended project (Alternate 2) will consist of a system of earthen levees, mechanically stabilized earth (MSE) floodwalls, concrete floodwalls, sheet pile floodwalls, road closure structures, and a storm water pumping station. Earthen and MSE levees are proposed for the majority of the flood protection alignment. Riprap will be utilized to protect the waterside slopes of the system along Fishing Creek.

The system begins immediately to the East of Railroad Street where the earthen levee ties into high ground. The top of the system at this location is Elevation 491.00. The alignment proceeds westward across Railroad Street which is at Elev. 490.0 +/- . The roadway would be raised approximately one foot. The top of protection elevation descends from Elev. 491.00 at Railroad Street to Elev. 485.00 at the Route 11 closure structure.

On the west side of Railroad Street, an earthen levee with a landside toe drain extends downstream to Station 11+50. Through this reach the levee crest is 10' wide with a land side slope of 2.5 Horizontal to 1 Vertical (2.5H:1V) and a riverside side slope of 2H:1V. This reach of the system is through a residential area. The riverside toe will extend into the bed of the creek since severe erosion since the 2011 Lee Flood has caused loss of the bank along this reach of the creek. The riverside levee slope will be protected by 18 to 24" riprap.

A MSE levee then extends westward adjacent to Fishing Creek from Sta. 11+50 to 14+50. The MSE levee has a 12' wide crest with vertical wall faces, fall protection railings and a landside toe drain. The MSE levee will have a riverside slope of 2H:1V. This reach of the system is also through a residential area. The riverside toe will extend into the bed of the creek

Starting at Sta. 14+50 a sheet pile wall is proposed 4 feet from the top of bank to Sta. 22+50. A concrete cap can be added to the sheet piling for additional strength and aesthetics.



This reach of the line of protection is on an alignment with minimal lateral clearance through the residential area. The riverside levee slope will be protected by 18 to 24" riprap.



Beginning at Sta. 22+50, an earth levee will extend to the Route 11 road closure structure abutment at Sta. 25+70+_. The stop log closure across route 11 is approximately 6 feet in height if the roadway is not raised. Being a state highway and also being in the floodplain, it was determined that the road should not be raised to lower the activation frequency.

On the south side of the closure, an earth levee begins at Sta. 26+50 extending to the Fairgrounds road closure structures 2 and 2A. The top of levee is at Elevation 485.00, about 6 to 7 feet in height. Flow velocities from the creek overbank flows during higher level flood events requires 24" riprap on the levee slope.

Closures 2 and 2A are proposed to be automatic Floodbreak type of closures since the creek flows in this area are fast rising compared to the river backwater which is also a source of flooding in the west end of Bloomsburg. To minimize the activation frequency, the ground level would be raised to elevation 478.00 as indicated on the concept plans.



An MSE levee of varying heights is proposed from the abutment of closure 2A at Sta. 31+30 to the tie-in to a concrete floodwall at Sta. 59+95. The tie-in location is near Closure 5 of the Columbia County levee System #1. This location is also the lowest existing elevation, approximately Elev. 470.5. With a top of system elevation of 485.00, the MSE levee would be about 14 feet in height. Extensive investigation of the embankment stability and underseepage potential will be required to determine the final width of the crest of the levee and the riverside earth slope which is assumed to be 3:1. Underseepage may require a deeper base trench (See MSE levee cross section in concept plans). Other options would be a slurry cutoff trench or sheeting.

The above stretch of MSE levee has three access road closure structures located at Sta, 40+35, Sta. 46+10, and sta. 47+25. They are proposed stop log closures 10 feet in height.

To minimize the erection time for each flood event, it is assumed most of the approximately 10 foot segments of stop logs between the steel column supports can remain in place until a major Fairgrounds event which would require removal to fully open the access points.



E.5 Concept Plans and Typical Sections and Details

Wilkes-Barre 613 Baltimore Dr. Suite 300 Wilkes-Barre, PA 18702 570-821-1999

CONCEPTUAL DESIGN

REVISIONS

DRAWING TITLE & PROJECT NAME

14+00 PROFILE STATION 0+00 TO

COLUMBIA COUNTY
END FLOOD MITIGATION STUDY
COLUMBIA COUNTY, PENNSYLVANIA

DRAWN BY CHECKED BY DATE
PROJECT NO.
PROJECT STATUS FEBRUARY 2022 2021-5134-001 CONCEPTUAL DESIGN

ROUTE 11 CLOSURE **PLAN** 500 495 490 TOP OF PROTECTION 485 _EXISTING GROUND 480 475 470 | 19+50 15**+**00 | 14+50 25**+00** 21**+00** 20+00 19**+00** 16**+**00 22+00 21+50 15+50 **PROFILE**

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SEALS

CONCEPTUAL DESIGN

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PLAN AND PROFILE STATION 14+00 TO 26+00

COLUMBIA COUNTY
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COLUMBIA COUNTY, PENNSYLVANIA

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PROJECT STATUS FEBRUARY 2022 2021-5134-001

CONCEPTUAL DESIGN

DH-103 SEALS DH-104 ROUTE 11 CLOSURE CLOSURE 2A & 2B **PLAN** 500 PLAN AND PROFILE STATION 26+00 TO 36+00 495 490 TOP OF PROTECTION EXISTING GROUND 480 **`**----475 **— 470** 470 ∣ 35+50 29**+**50 35+00 34+50 33+50 33+00 32+50 31+00 30+00 29+00 28+50 28+00 27+50 27+00 26+50 DRAWN BY **PROFILE**

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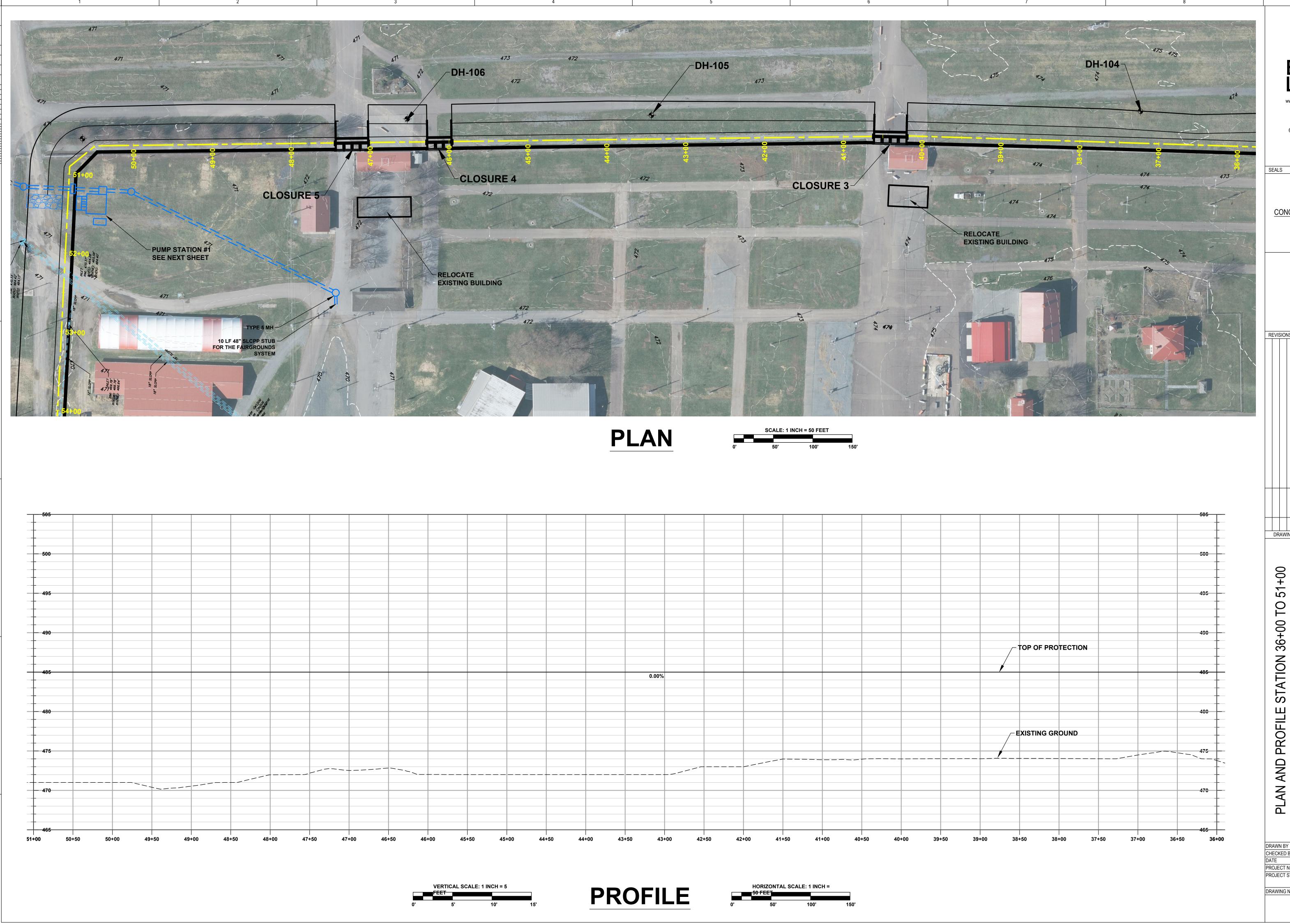
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ATION 36+00 TO 51+00

COUNTY

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COLUMBIA COUNTY, PENNSYLVANIA

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CONCEPTUAL DESIGN

RAWING NO.

C104

- EXISTING SURFACE DRAINAGE PUMP DISCHARGE RISER CHAMBER -INTAKE CHAMBER -**PLAN** SCALE: 1 INCH = 50 FEET

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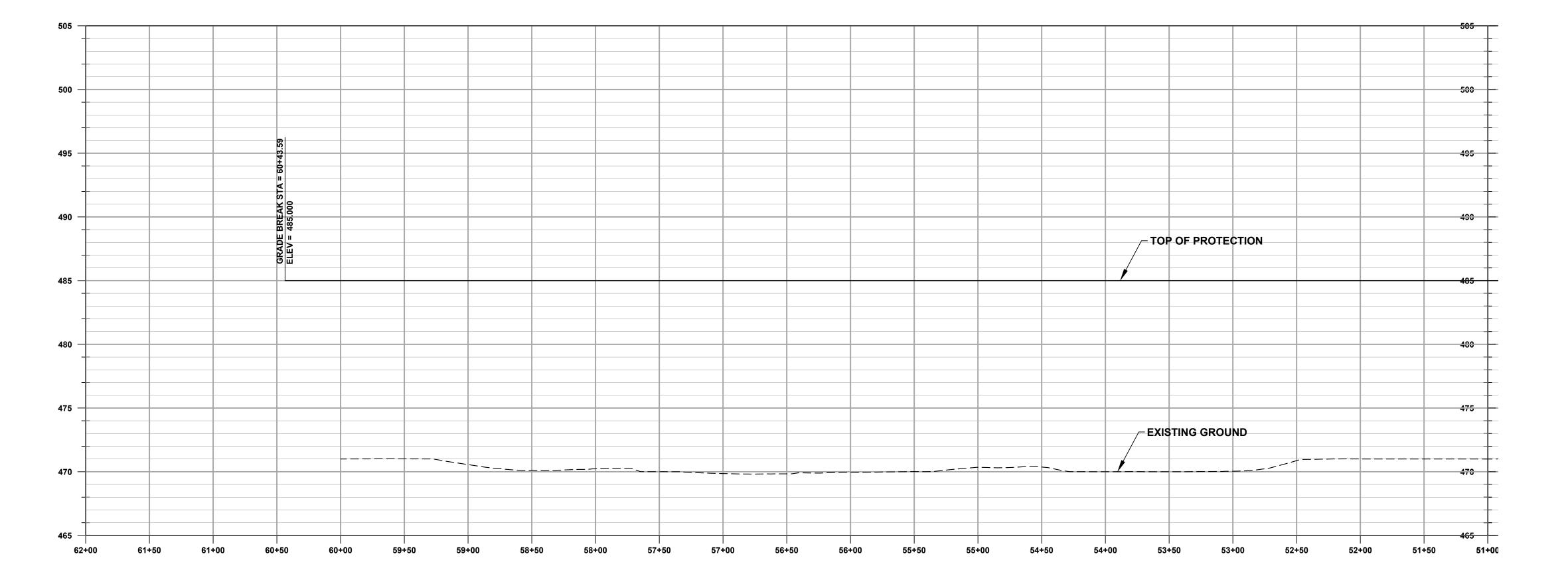
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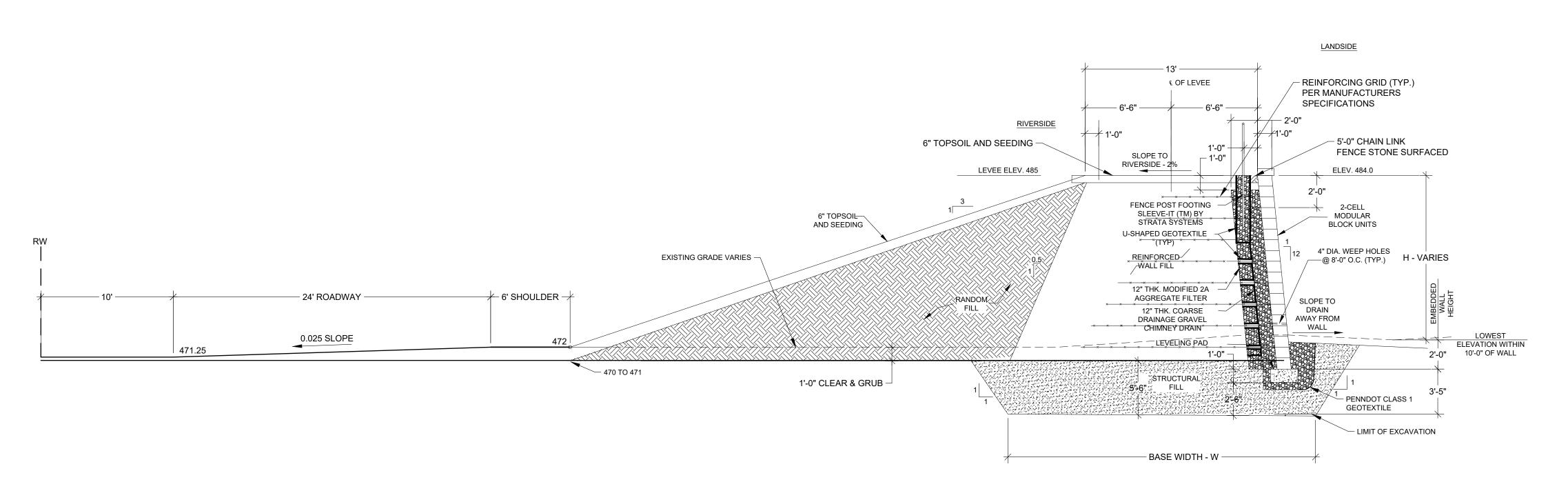
PLAN AND PROFILE STATION 51+00 TO 62+00

COLUMBIA COUNTY
END FLOOD MITIGATION STUDY
COLUMBIA COUNTY, PENNSYLVANIA

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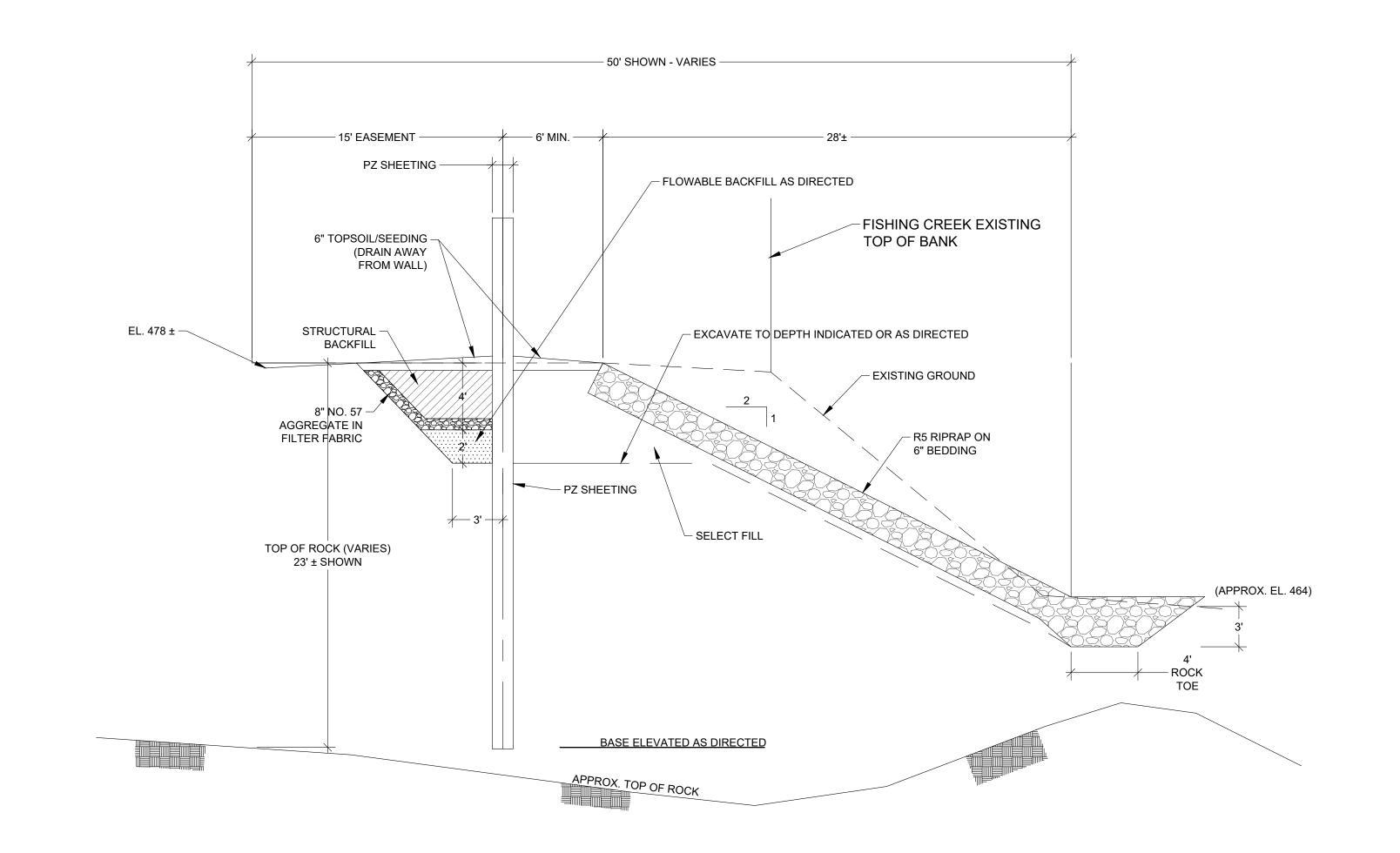
PROFILE





6TH STREET MSE LEVEE SECTION

SCALE: NTS



SECTION AT SHEETPILE WALL - STATION 23+00 SHOWN

SCALE: 1"=5'-0"

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- END FLOOD MITIGATION STUDY

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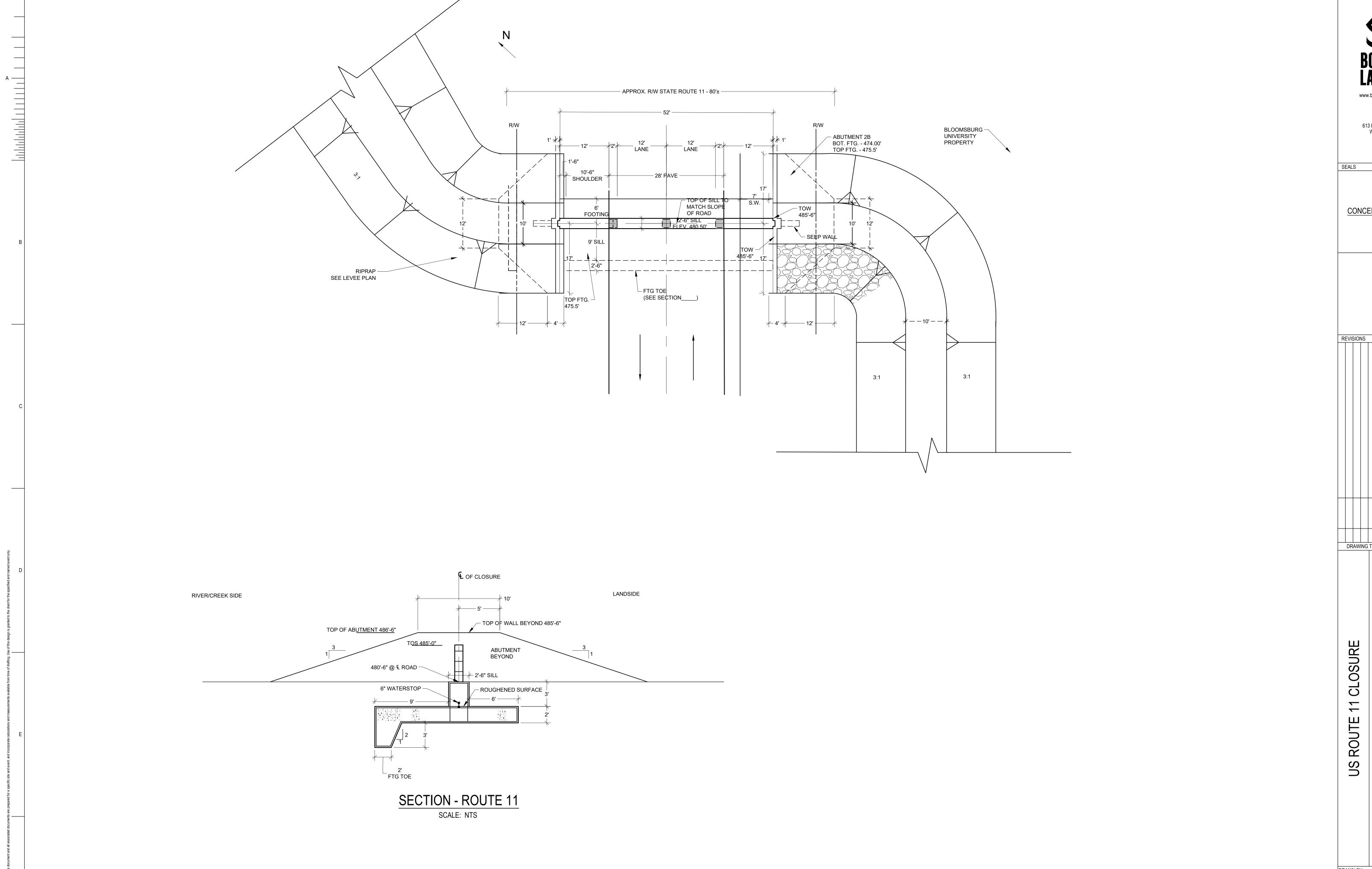
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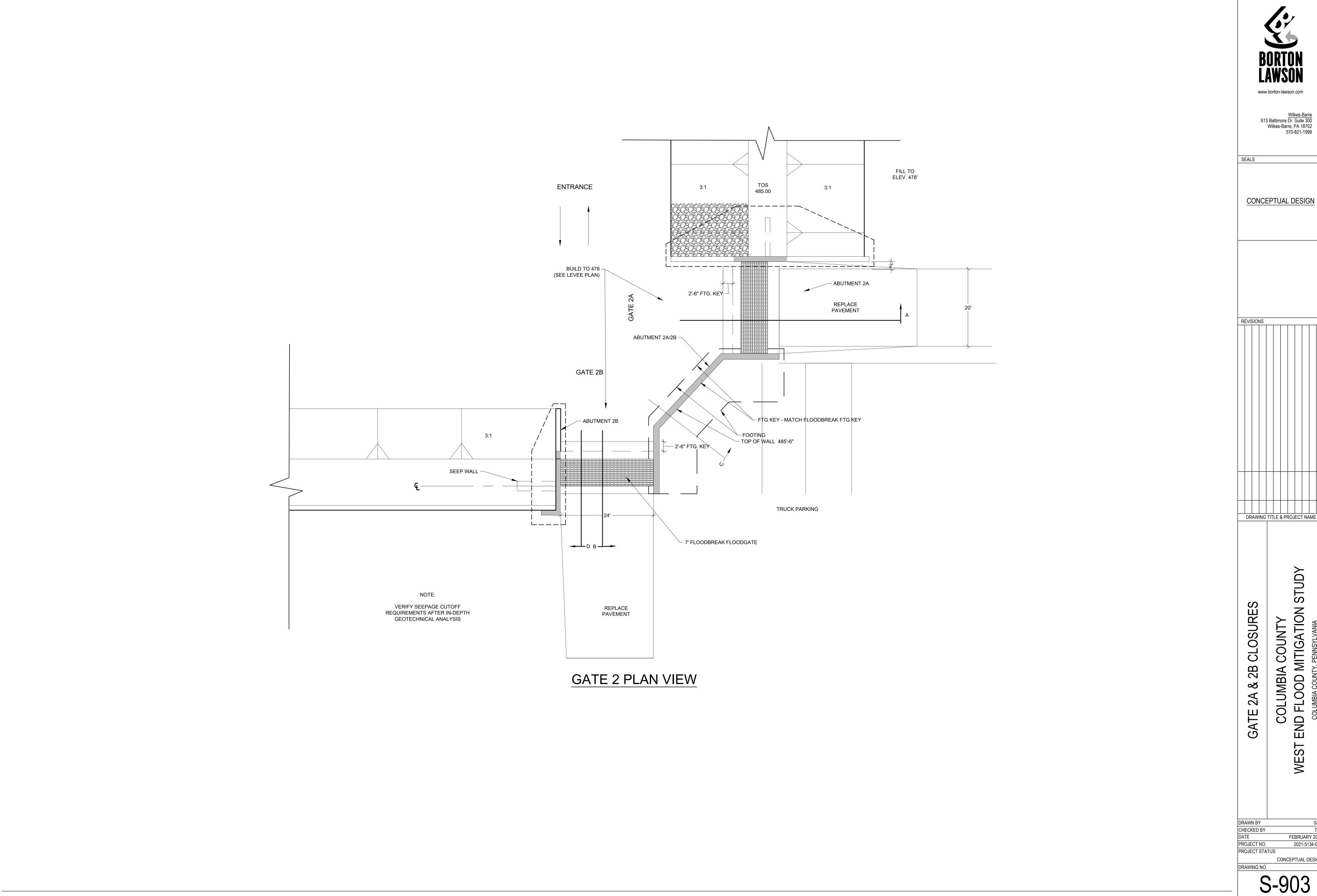
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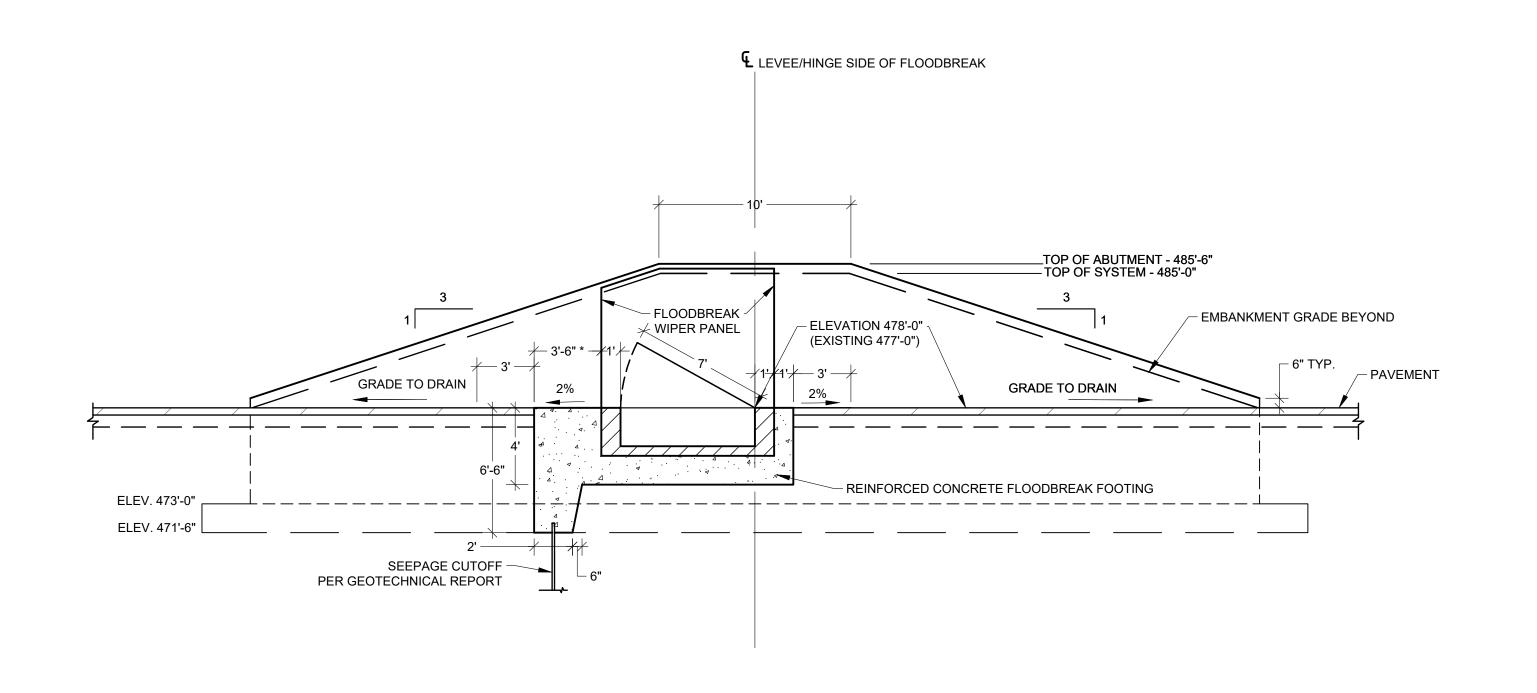
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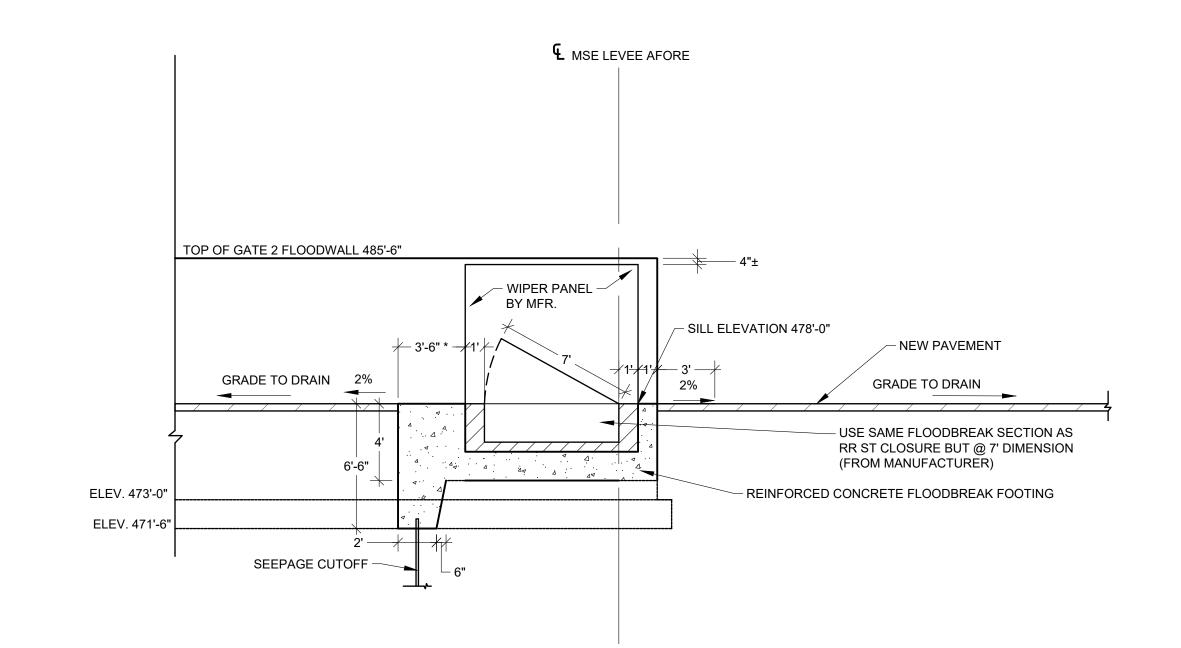
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COLUMBIA COUNTY, PENNSYLVANIA

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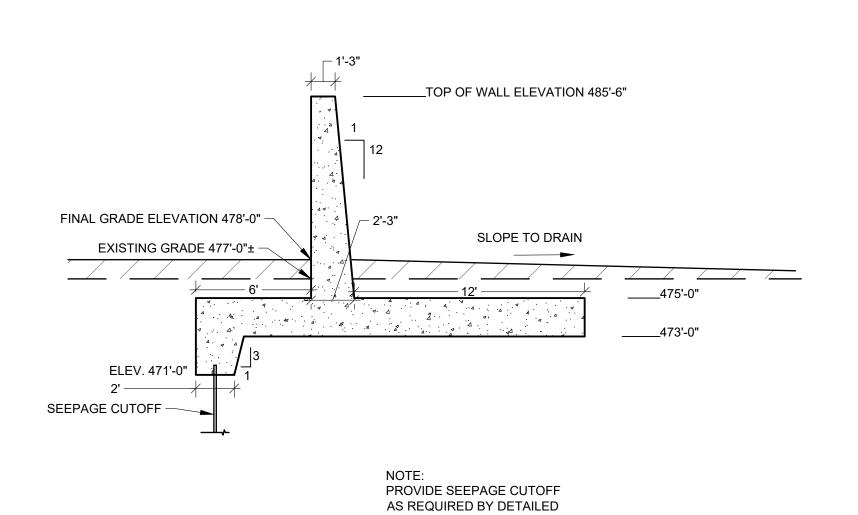


GATE 2 - CLOSURE 2B SECTION B

GATE 2A - CLOSURE SECTION A

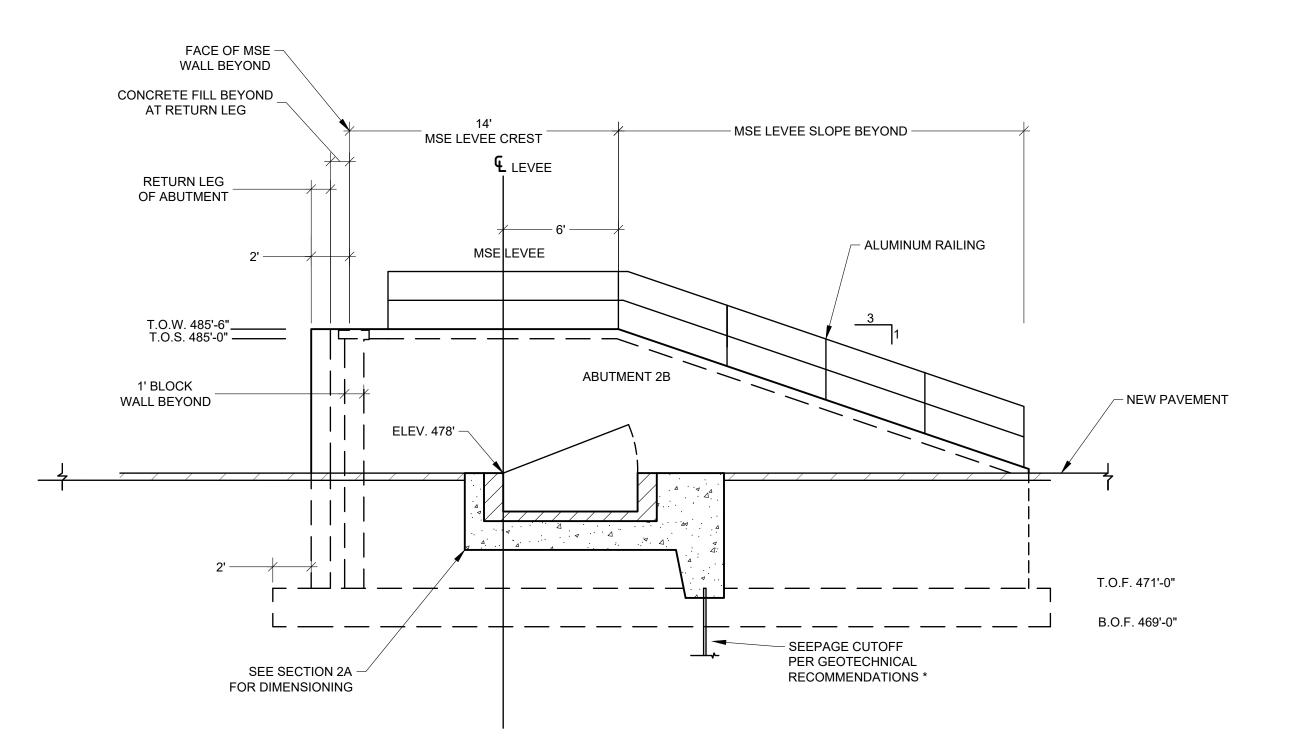
ALL DIMENSIONS TO BE
VERIFIED BY STRUCTURAL ENGINEER DURING DESIGN PHASE

* - TO BE VERIFIED



GEOTECHNICAL ANALYSIS. *

GATE 2A/2B - FLOODWALL SECTION C



GATE 2 - CLOSURE 2B
SECTION D

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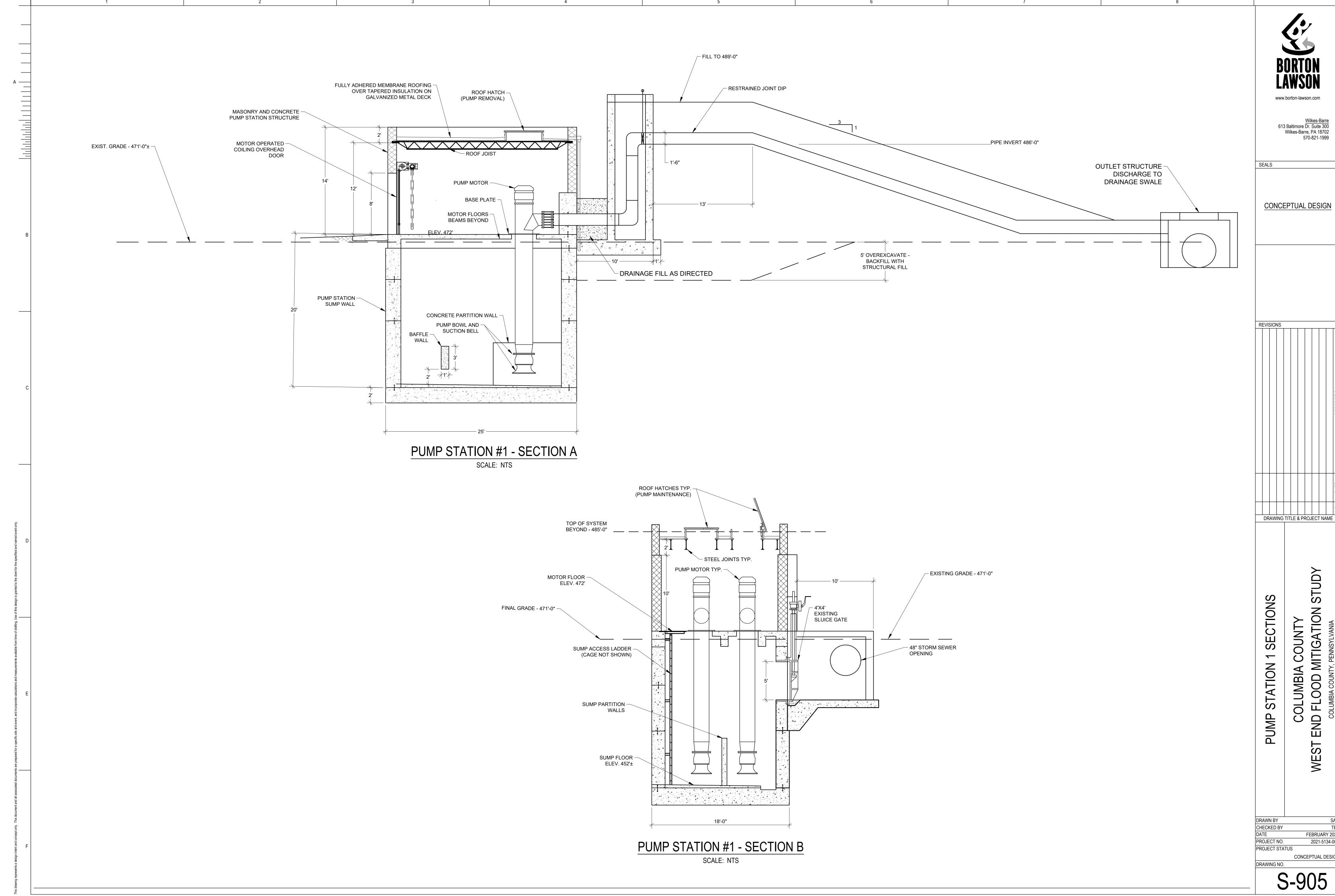
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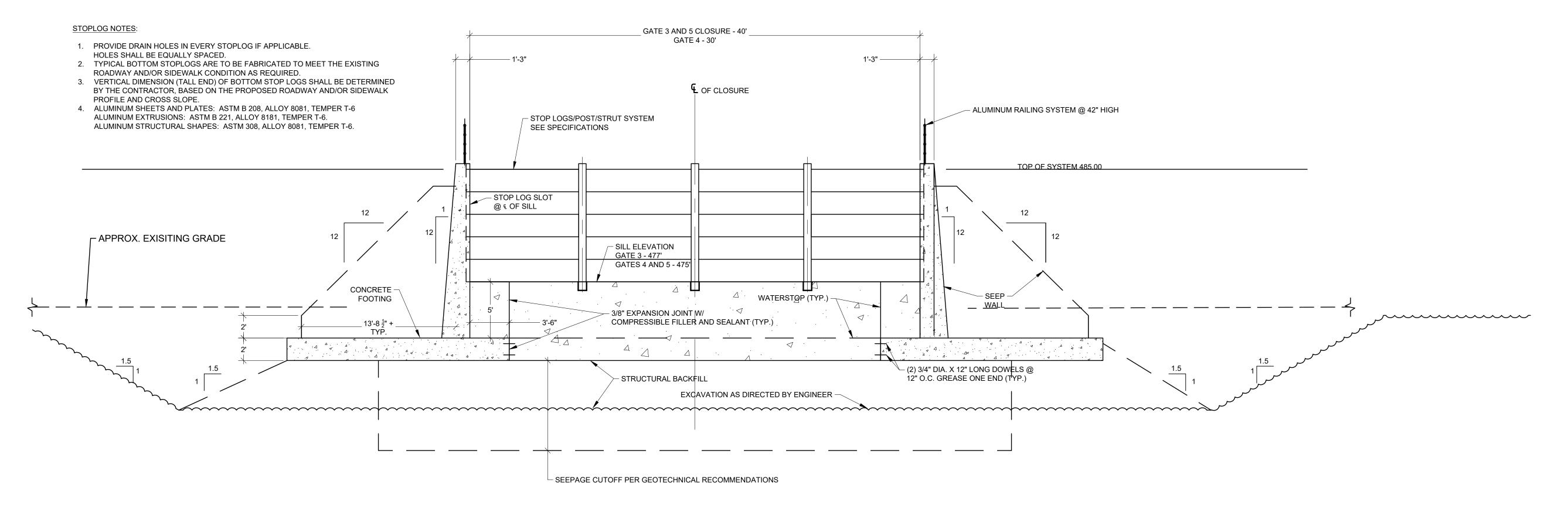
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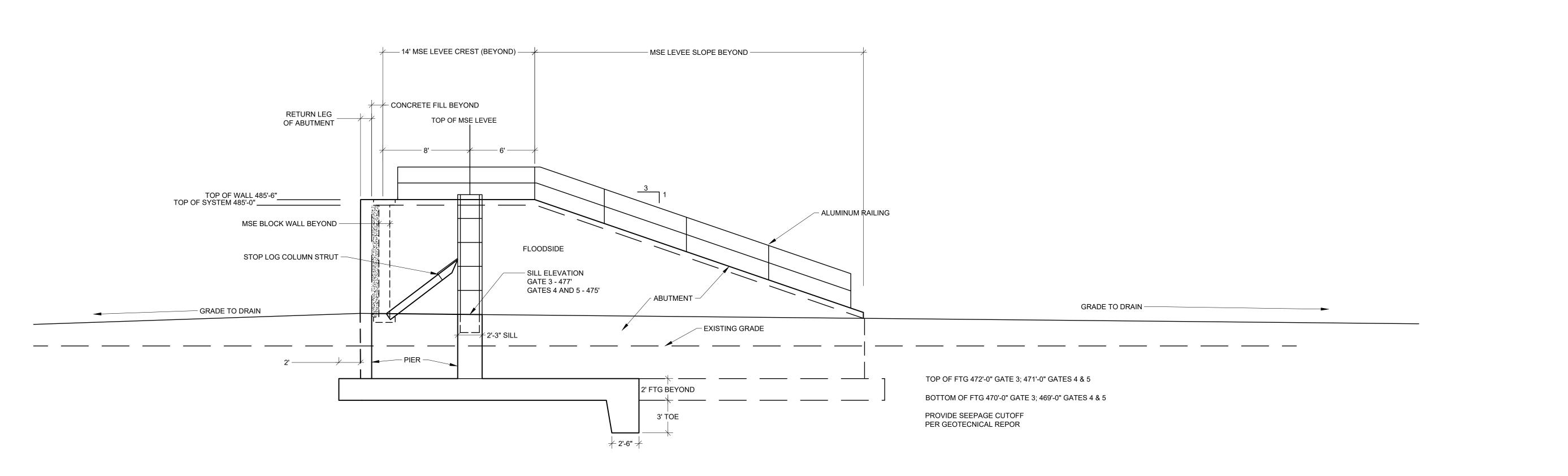
FEBRUARY 2022

2021-5134-001 CONCEPTUAL DESIGN



ELEVATION - TYPICAL GATES 3, 4, AND 5 CLOSURE STRUCTURE

SCALE: NTS



GATES 3, 4, AND 5 CLOSURES

TYPICAL SECTION AT & OF CLOSURE STRUCTURE

SCALE: NTS



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613 Baltimore Dr. Suite 300
Wilkes-Barre, PA 18702
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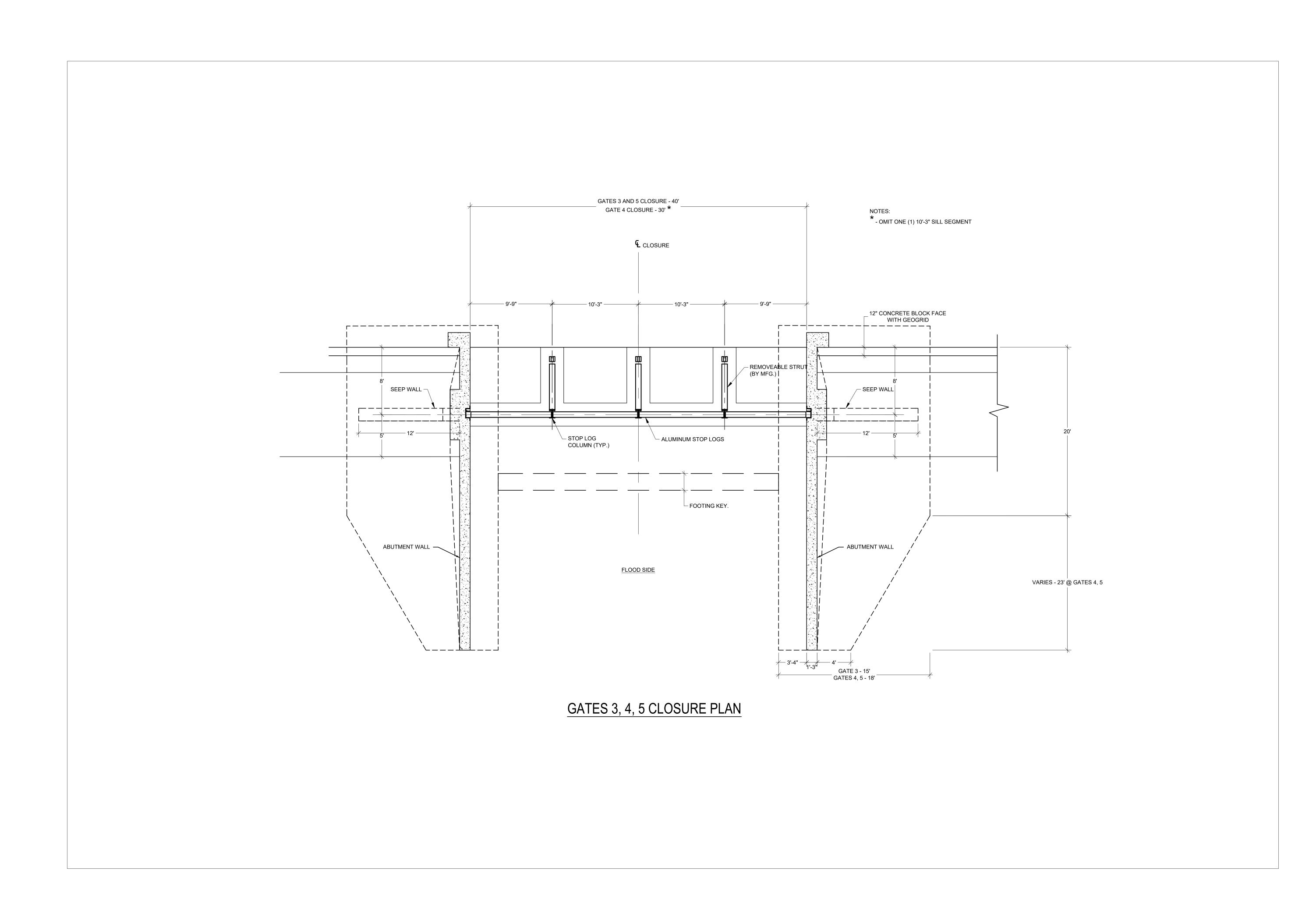
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PROJECT STATUS

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CONCEPTUAL DESIGN DRAWING NO.

S-907

WEST END FLOOD MITIGATION STUDY

COLUMBIA COUNTY, PENNSYLVANIA

Appendix F

Floodplain / Floodway, Depth of Flooding, and Depth of Flooding in Structures Maps

WEST END FLOOD MITIGATION STUDY

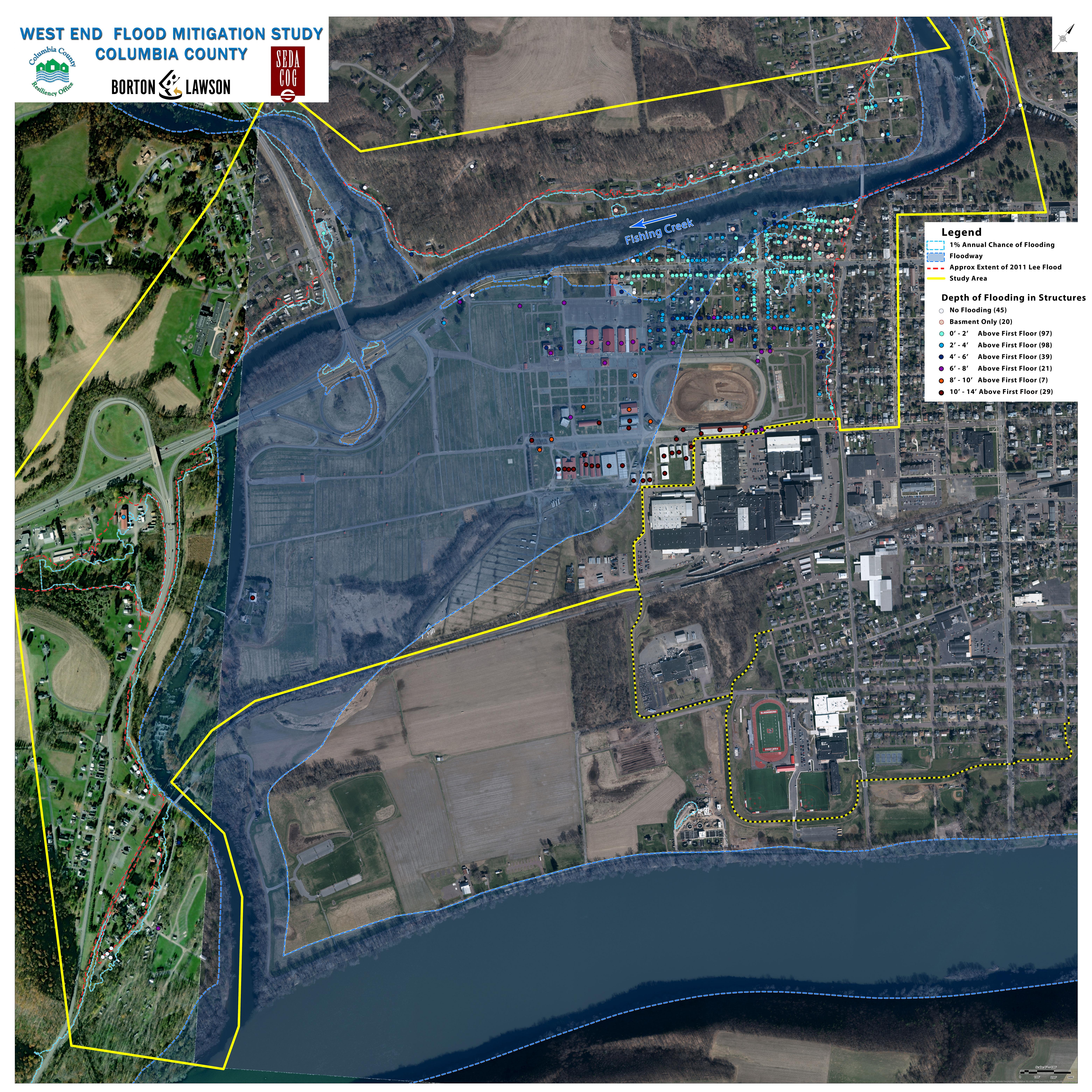
COLUMBIA COUNTY, PENNSYLVANIA

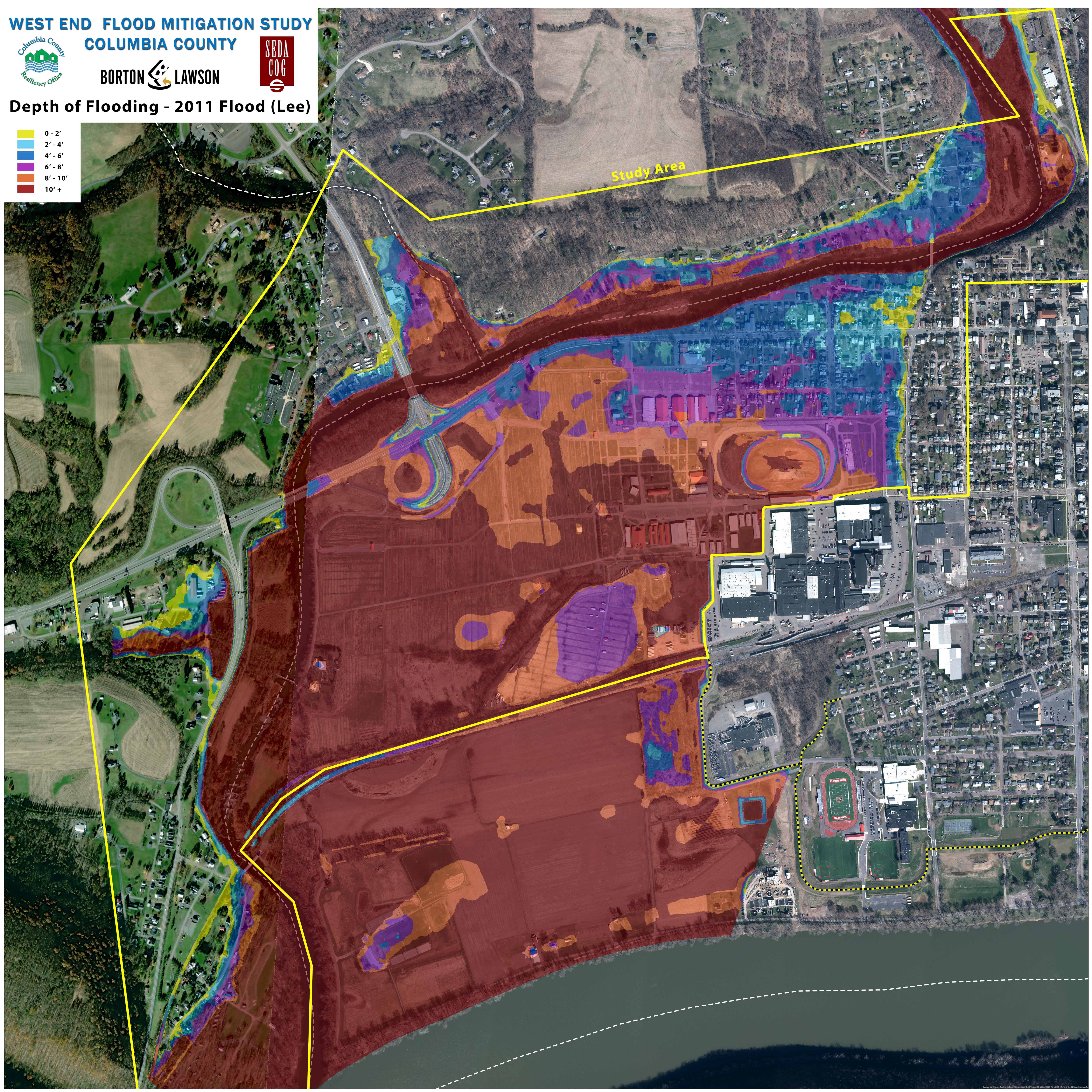
Appendix F

Floodplain, Depth of Flooding, and Depth of First Floor Flooding Maps

TABLE OF CONTENTS:

- 1. Depth of Flooding in Structures 2011 Flood
- 2. Depth of Flooding from Grade 2011 Flood
- 3. Floodway/ Floodplain in Study Area by Municipality
- 4. Proposed Levee West End Bloomsburg in Floodway/ Floodplain





Montour Twp: Floodway, Floodplain, Lee Flood Limit



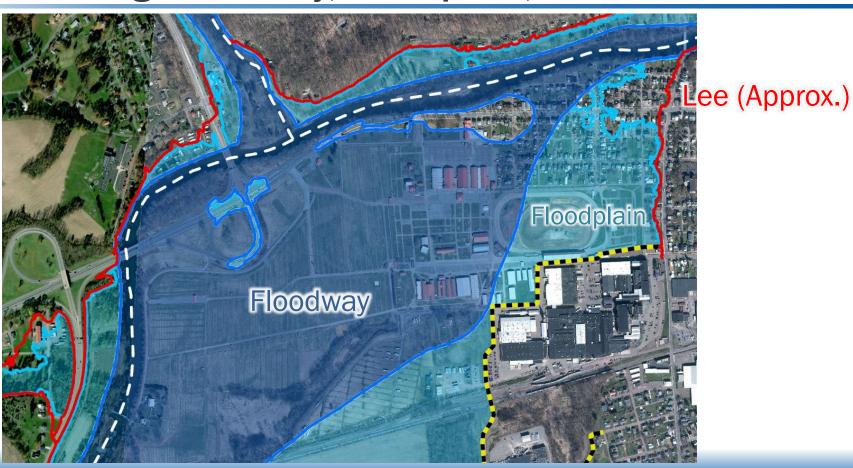


Hemlock Twp: Floodway, Floodplain, Lee Flood Limit

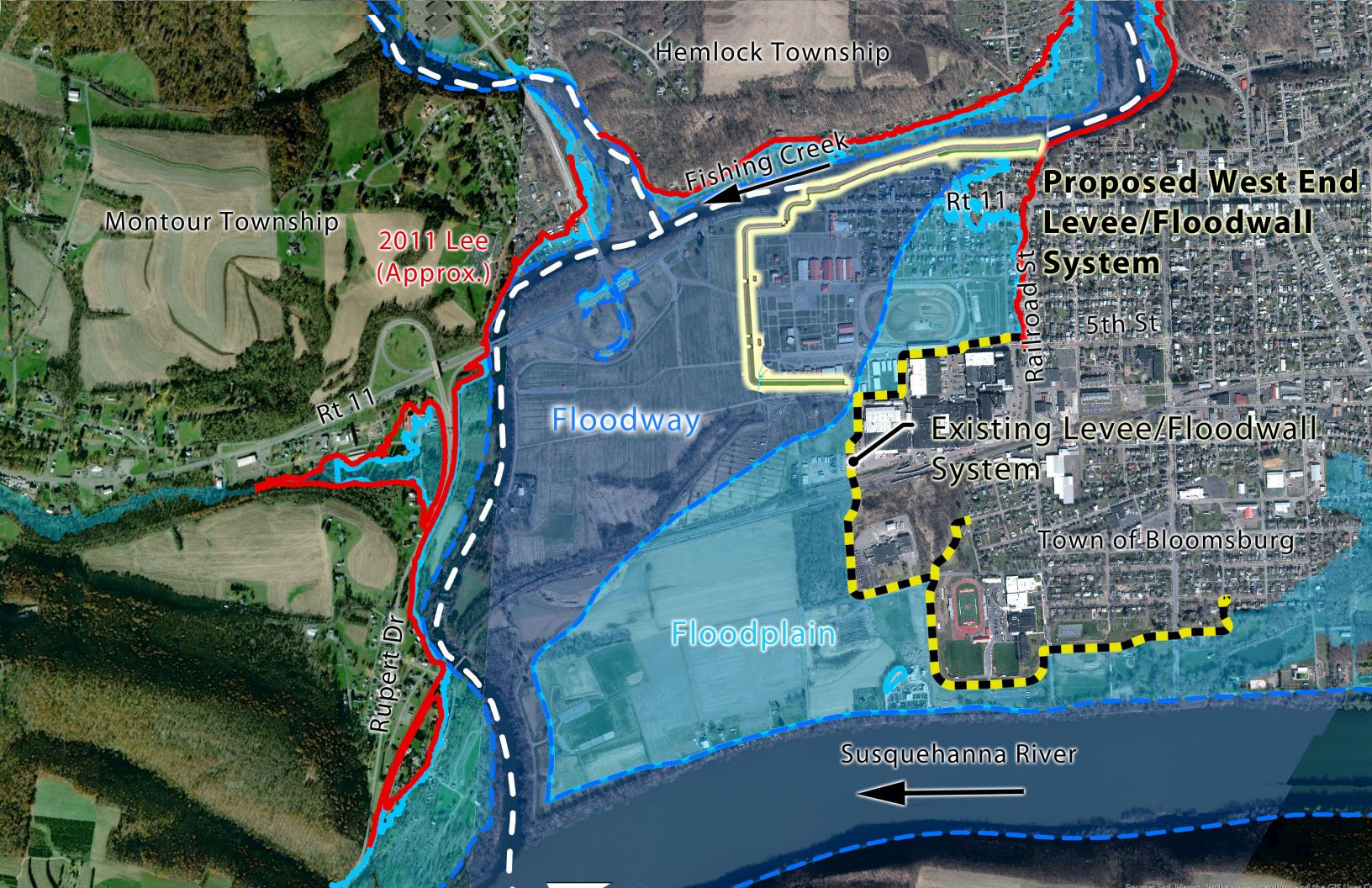




Bloomsburg: Floodway, Floodplain, Lee Flood Limit







WEST END FLOOD MITIGATION STUDY

COLUMBIA COUNTY, PENNSYLVANIA

Appendix G

Benefit Cost Analysis

WEST END FLOOD MITIGATION STUDY

COLUMBIA COUNTY, PENNSYLVANIA

Appendix G

Benefit Cost Analysis

TABLE OF CONTENTS:

- 1. Summary of Inputs for FEMA BCA Tool
- 2. FEMA BCA Tool Output \$29 Million Project Cost
- 3. FEMA BCA Tool Output \$26 Million Project Cost
- 4. FEMA FAST Tool Output 2011 Flood Lee

Summary of FEMA BCA Tool Inputs

For Levee System

June 1, 2022

Column	Data source
Identifier*	Assigned by Borton Lawson (B-XXX)
Street Address*	From Columbia County GIS parcel data
City*	Bloomsburg
State*	Pennsylvania
Zip Code*	17815
County*	Columbia
Latitude	Center of Structure, From ESRI ArcPro
Longitude	Center of Structure, From ESRI ArcPro
Longitude	Just used Non-Residential & Residential. Identified in the Columbia County obtained GIS
Structure Type*	parcel data
Structure Type	Residential was entered for houses apartment buildings with less than 4 units
Mitigation Action Type*	Floodproofing Measures - FEMA help desk directed us to use this for a "Levee"
Project Useful Life*	75 years
Mitigation Project Cost (\$)*	Total estimated project cost of levee system diviided by the number of structures
Use Default Number of Years of Maintenance?	Yes - makes maintenance years equivalent to project useful life (This is the default setting)
Number of Years of Maintenance	75 years (default input)
	Estimated annual O&M cost of levee divided of number of structures (used \$75,000 per
Annual Maintenance Cost (\$)	year)
	Used first floor elevations from BL survey (did <u>NOT</u> use basement elevations). If structure
Lowest Floor Elevation of the Property (ft)	was elevated, used the elevated FF elevation which was an estimated elevation.
Streambed Elevation at Property Location (ft)	Fishing Creek Cross sections per Preliminary Flood Insurance Study, dated August 2021
Feet Lowest Floor Is Being Raised	Zero (0) feet, not required with a levee system
	Entered proposed Levee heights, broken out into different sections based on location of
	structure relative to proposed levee
Elevation for the Top of Barrier or	Railroad Street to Scott Street - 489.9'
Floodproofing (ft)	Scott Street to Barton Ave - 488.2'
	Barton Street to Leonard Street - 487.2'
	Leonard Street to Barton Ave - 486' Barton Ave to End - 485'
Building Type (Residential)	One story or two story - identified by BL from field survey
building Type (Residential)	BL identifed structure type. 73 total Non-residential structures (51- Fairgrounds, 16 other
	commercial properties, 6 garages/sheds). FEMA defined categories used in this analysis-
Building Use (Non-Residential)	COM1 Retail Trade, Apartments entered as COM3 Personal & Repair Services, Fairgrounds
ballaring ose (Non Residential)	structures were entered as COM8 Entertainment & Recreation, Large garages and sheds
	entered as IND2 Industrial Light
	BL identified the specific type of use. More specific categories (apartment, offices,
Building Type (Non-Residential)	convience stores, etc.)
Is Building is located outside of hundred-year	
flood area (applies only to Non-	3 Non-Residential structures are located outside of 1% SFHA. Structures in 500-yr "tadpole"
Residential/Critical Facility)?	area shown on FIRM, we assume is 100-yr area
·	Data taken from homeowner survey & BL field survey to determine if home has a
Building has Basement (Residential question	basement. For the houses that have basements, BL assumed all are unfinished basements.
only)	YES for 213 out 294 structures in Bloomsburg
Building is Engineered (Non-Residential or	
Critical Facility)	Assume none - no other information to indicate otherwise
Building has Active NFIP Policy	Used answers from Homeowner Surveys. Entered 51 properties with flood insurance
	USACE Generic was utilized - This curve is not specific to geographic location (this curve
Damaga Curus	only applies to residential structures - commercial damage curve is selected based on
Damage Curve	building type)
First Floor Area (applies only to Non-Residential	Not provided in County parcel data. BL estimated commercial building SF using May 2021
or Critical Facility - sq.ft)	BL aerial imagery to determine bldg perimeter
	This is total finished SF of structure. Residential - used SF from County parcel data; Commercial - BL estimated SF multiplied by # of stories of structure. BL has photos of all
Size of Building (sq.ft)	structures.
Size of building (sq.it)	NO for Residential; NO for garages/ sheds; YES for fairgrounds; NO for all other Non-
Use Default Building Replacement Value?	Residential Structures
ose Delaare banding Replacement value:	Used \$150/ SF for Residnential and Non-Residential structures- BL received quote from ;
Building Replacement Value (\$/sq.ft)	used \$25/ SF for Garages/ sheds
Use Default Demolition Threshold?	Yes
Demolition Threshold (%)	blank
Use Default Building Contents Value?	Yes, Farigrounds is No
ose betaut bahaning contents value:	. 50, . 5110, 541145 15 115

Summary of FEMA BCA Tool Inputs For Levee System

June 1, 2022

	54.10 _, _ 5
	Used default value for residential structures; entered value for Fairgrounds building from
Contents Value (\$)	Schedule of Property from insurance company (contents value provided for 7 buildings); used \$500 for garages and sheds
Utilities are Elevated (Residential)	Assumed none
Annual Street Maintenance Budget (\$)	Not an option for Floodproofing Model
Number of Street Miles Maintained	Not an option for Floodproofing Model
Street Miles that will not require future	Not all option for Floodproofing Wodel
maintenance	Not an option for Floodproofing Model
Annual Operating Budget (\$) - for Non-	Not all option for Floodprooting Wodel
	Entered \$0
residential properties	Entered 50
Use Default Monthly Cost of Temporary Space?	Yes
Monthly Cost of Temporary Space	
(\$/sq.ft/month)	N/A using default
Use Default One Time Displacement Cost?	Yes for residential; No for garages & sheds & Fairgrounds; default for commercial
One Time Displacement Cost (\$/sq.ft)	\$0 for garages & sheds & Fairgrounds
Use Default Lodging Per Diem?	Yes
Current Federal Lodging Per Diem (\$/night)	blank
Use Default Meals Per Diem?	Yes
Current Federal Meals Per Diem (\$/day)	blank
Number of Building Residents	2 per structure, 2 per aparmtnet unit, unless known otherwise (from flood survey)
Number of Volunteers Required	Did not enter anything
Enter the Number of Days Lodging for	
Volunteers	Did not enter anything
Use Default Per-Person Cost of Lodging?	Yes
Enter the Per-Person Cost of Lodging for a	
Volunteer (\$)	Did not enter anything
Number of Workers	Assumed 2 per structure
Use Acres?	Yes
Total Project Area (acres or sq.ft)	Did not enter anything
Green Open Space (%)	Did not enter anything
Riparian (%)	Did not enter anything
Wetlands (%)	Did not enter anything
Forests (%)	Did not enter anything
Marine & Estuary (%)	Did not enter anything



Benefit-Cost Calculator

V.6.0 (Build 20220513.1658 | Release Notes)

Benefit-Cost Analysis

Project Name: Levee \$29 Million

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	1		44	Riverine Flood	\$ 919	\$ 102,261	0.01	D
<u> </u>	2			Riverine Flood	\$ 171,051	\$ 102,280	1.67	Ъ
<u> </u>	3		☆	Riverine Flood	\$ 0	\$ 102,261	0.00	Ф
<u> </u>	4		☆	Riverine Flood	\$ 23,779	\$ 102,261	0.23	Ф
<u> </u>	5		☆	Riverine Flood	\$ 35,016	\$ 102,261	0.34	Ъ
✓	6		☆	Riverine Flood	\$ 22,159	\$ 102,261	0.22	Ф
<u> </u>	7		44	Riverine Flood	\$ 8,857	\$ 102,261	0.09	Ф
<u> </u>	8			Riverine Flood	\$ 44,262	\$ 102,261	0.43	Ф
<u> </u>	9		☆	Riverine Flood	\$ 42,834	\$ 102,261	0.42	D
<u> </u>	10			Riverine Flood	\$ 51,485	\$ 102,261	0.50	D
<u> </u>	11		☆	Riverine Flood	\$ 43,027	\$ 102,261	0.42	Ď
<u> </u>	12		☆	Riverine Flood	\$ 129,322	\$ 102,261	1.26	Ď
<u> </u>	13		☆	Riverine Flood	\$ 121,410	\$ 102,261	1.19	Ď
<u> </u>	14		☆	Riverine Flood	\$ 50,724	\$ 102,261	0.50	Ď
<u> </u>	15		☆	Riverine Flood	\$ 34,589	\$ 102,261	0.34	Ф



Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	16		☆	Riverine Flood	\$ 30,290	\$ 102,261	0.30	Ф
<u>~</u>	17		☆	Riverine Flood	\$ 22,165	\$ 102,261	0.22	Ф
<u>~</u>	18		☆	Riverine Flood	\$ 52,117	\$ 102,261	0.51	Ď
<u>~</u>	19		☆	Riverine Flood	\$ 26,741	\$ 102,261	0.26	D
~	20		<u>k</u>	Riverine Flood	\$ 25,830	\$ 102,261	0.25	D
~	21		☆	Riverine Flood	\$ 26,172	\$ 102,261	0.26	D
~	22		☆	Riverine Flood	\$ 1,129	\$ 102,261	0.01	D
<u>~</u>	23		☆	Riverine Flood	\$ 107,149	\$ 102,280	1.05	D
<u>~</u>	24		M	Riverine Flood	\$ 730,452	\$ 102,261	7.14	Ф
<u>~</u>	25		☆	Riverine Flood	\$ 14,106	\$ 102,261	0.14	Ō
<u>~</u>	26		☆	Riverine Flood	\$ 17,224	\$ 102,261	0.17	D
<u>~</u>	27		☆	Riverine Flood	\$ 28,364	\$ 102,261	0.28	D
~	28			Riverine Flood	\$ 26,134	\$ 102,261	0.26	Ò
~	29		☆	Riverine Flood	\$ 53,141	\$ 102,261	0.52	D
~	30			Riverine Flood	\$ 35,616	\$ 102,261	0.35	Ò
~	31			Riverine Flood	\$ 186	\$ 102,261	0.00	Ō
~	32			Riverine Flood	\$ 73,503	\$ 102,261	0.72	Ò
<u> </u>	33			Riverine Flood	\$ 56,801	\$ 102,261	0.56	D
~	34		^	Riverine Flood	\$ 24,068	\$ 102,261	0.24	D
~	35		☆	Riverine Flood	\$ 22,576	\$ 102,261	0.22	D
~	36		â	Riverine Flood	\$ 23,720	\$ 102,261	0.23	Ď
<u> </u>	37			Riverine Flood	\$ 70,917	\$ 102,261	0.69	Ò

Select ✓	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	38		☆	Riverine Flood	\$ 33,026	\$ 102,261	0.32	D
<u> </u>	39		☆	Riverine Flood	\$ 30,608	\$ 102,261	0.30	Ō
~	40			Riverine Flood	\$ 37,870	\$ 102,261	0.37	D
~	41		☆	Riverine Flood	\$ 47,057	\$ 102,261	0.46	D
<u> </u>	42		<u></u>	Riverine Flood	\$ 30,212	\$ 102,261	0.30	D
<u> </u>	43		<u></u>	Riverine Flood	\$ 55,910	\$ 102,261	0.55	D
<u> </u>	44		<u></u>	Riverine Flood	\$ 41,873	\$ 102,261	0.41	D
~	45		☆	Riverine Flood	\$ 25,796	\$ 102,261	0.25	D
~	46			Riverine Flood	\$ 65,947	\$ 102,261	0.64	Ò
~	47			Riverine Flood	\$ 118,953	\$ 102,261	1.16	Ō
~	48		^	Riverine Flood	\$ 31,709	\$ 102,261	0.31	Ф
<u> </u>	49		☆	Riverine Flood	\$ 66,375	\$ 102,261	0.65	Ō
~	50		☆	Riverine Flood	\$ 7,894	\$ 102,261	0.08	Ò
~	51			Riverine Flood	\$ 12,040	\$ 102,261	0.12	Ð
<u> </u>	52		☆	Riverine Flood	\$ 13,379	\$ 102,261	0.13	Ō
~	53			Riverine Flood	\$ 11,663	\$ 102,261	0.11	Ò
<u> </u>	54			Riverine Flood	\$ 29,092	\$ 102,261	0.28	Ō
<u> </u>	55		☆	Riverine Flood	\$ 14,293	\$ 102,261	0.14	D
<u> </u>	56		☆	Riverine Flood	\$ 28,507	\$ 102,261	0.28	D
<u> </u>	57		â	Riverine Flood	\$ 33,299	\$ 102,261	0.33	D
✓	58		☆	Riverine Flood	\$ 5,339	\$ 102,261	0.05	D
✓	59		☆	Riverine Flood	\$ 26,665	\$ 102,261	0.26	D

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	60		☆	Riverine Flood	\$ 59,020	\$ 102,261	0.58	Ф
<u>~</u>	61		☆	Riverine Flood	\$ 21,051	\$ 102,261	0.21	Ō
<u>~</u>	62		☆	Riverine Flood	\$ 16,552	\$ 102,261	0.16	Ō
✓	63		M	Riverine Flood	\$ 22,840	\$ 102,261	0.22	D
~	64			Riverine Flood	\$ 507	\$ 102,261	0.00	D
~	65			Riverine Flood	\$ 24,286	\$ 102,261	0.24	D
<u> </u>	66		☆	Riverine Flood	\$ 30,128	\$ 102,261	0.29	D
<u>~</u>	67		☆	Riverine Flood	\$ 13,127	\$ 102,261	0.13	D
<u>~</u>	68		☆	Riverine Flood	\$ 11,124	\$ 102,261	0.11	D
<u>~</u>	69		☆	Riverine Flood	\$ 15,876	\$ 102,261	0.16	Ō
<u>~</u>	70		☆	Riverine Flood	\$ 17,957	\$ 102,261	0.18	D
<u>~</u>	71		☆	Riverine Flood	\$ 17,111	\$ 102,261	0.17	D
~	72		☆	Riverine Flood	\$ 31,328	\$ 102,261	0.31	D
~	73		<u>k</u>	Riverine Flood	\$ 0	\$ 102,261	0.00	Ō
~	74		☆	Riverine Flood	\$ 13,669	\$ 102,261	0.13	D
~	75			Riverine Flood	\$ 16,648	\$ 102,261	0.16	D
~	76		<u>k</u>	Riverine Flood	\$ 13,249	\$ 102,261	0.13	D
~	77			Riverine Flood	\$ 27,993	\$ 102,261	0.27	D
~	78		☆	Riverine Flood	\$ 32,762	\$ 102,261	0.32	D
<u> </u>	79		☆	Riverine Flood	\$ 13,819	\$ 102,261	0.14	D
✓	80		☆	Riverine Flood	\$ 9,066	\$ 102,261	0.09	Ò
<u> </u>	81		☆	Riverine Flood	\$ 27,440	\$ 102,261	0.27	Ď

Select	Map Marker▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	82			Riverine Flood	\$ 29,473	\$ 102,261	0.29	
<u> </u>	83		☆	Riverine Flood	\$ 39,511	\$ 102,261	0.39	Ď
~	84			Riverine Flood	\$ 27,321	\$ 102,261	0.27	Ò
✓	85			Riverine Flood	\$ 18,757	\$ 102,261	0.18	Ò
~	86			Riverine Flood	\$ 22,945	\$ 102,261	0.22	Ò
~	87			Riverine Flood	\$ 34,015	\$ 102,261	0.33	Ò
~	88			Riverine Flood	\$ 23,575	\$ 102,261	0.23	Ò
✓	89			Riverine Flood	\$ 53,880	\$ 102,261	0.53	D
✓	90			Riverine Flood	\$ 131,793	\$ 102,261	1.29	D
<u> </u>	91			Riverine Flood	\$ 21,570	\$ 102,261	0.21	Ō
~	92			Riverine Flood	\$ 21,928	\$ 102,261	0.21	Ò
~	93			Riverine Flood	\$ 14,371	\$ 102,261	0.14	Ò
~	94		☆	Riverine Flood	\$ 12,853	\$ 102,261	0.13	Ò
~	95		☆	Riverine Flood	\$ 4,159	\$ 102,261	0.04	Ò
<u> </u>	96		☆	Riverine Flood	\$ 1,100	\$ 102,261	0.01	Ò
<u> </u>	97		☆	Riverine Flood	\$ 5,108	\$ 102,261	0.05	Ò
<u> </u>	98		☆	Riverine Flood	\$ 15,194	\$ 102,261	0.15	Ò
~	99		<u>k</u>	Riverine Flood	\$ 201,120	\$ 102,261	1.97	Ò
~	100			Riverine Flood	\$ 23,563	\$ 102,261	0.23	Ò
~	101			Riverine Flood	\$ 46,249	\$ 102,261	0.45	Ò
~	102			Riverine Flood	\$ 32,224	\$ 102,261	0.32	Ò
✓	103			Riverine Flood	\$ 70,503	\$ 102,261	0.69	Ō

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	104		☆	Riverine Flood	\$ 24,595	\$ 102,261	0.24	
<u>~</u>	105		☆	Riverine Flood	\$ 34,192	\$ 102,261	0.33	D
✓	106		M	Riverine Flood	\$ 21,264	\$ 102,261	0.21	D
~	107		☆	Riverine Flood	\$ 32,593	\$ 102,261	0.32	D
~	108			Riverine Flood	\$ 32,750	\$ 102,261	0.32	D
~	109			Riverine Flood	\$ 136,748	\$ 102,261	1.34	D
~	110			Riverine Flood	\$ 36,247	\$ 102,261	0.35	D
✓	111		M	Riverine Flood	\$ 14,915	\$ 102,261	0.15	D
✓	112		☆	Riverine Flood	\$ 42,477	\$ 102,261	0.42	D
✓	113		M	Riverine Flood	\$ 151,338	\$ 102,261	1.48	D
✓	114		4 4	Riverine Flood	\$ 197,258	\$ 102,261	1.93	D
<u> </u>	115		☆	Riverine Flood	\$ 23,686	\$ 102,261	0.23	D
✓	116		☆	Riverine Flood	\$ 54,369	\$ 102,261	0.53	D
✓	117		☆	Riverine Flood	\$ 46,785	\$ 102,261	0.46	D
✓	118		☆	Riverine Flood	\$ 19,610	\$ 102,261	0.19	D
✓	119			Riverine Flood	\$ 4,852	\$ 102,261	0.05	D
✓	120		☆	Riverine Flood	\$ 9,446	\$ 102,261	0.09	D
~	121		k	Riverine Flood	\$ 6,214	\$ 102,261	0.06	Ď
~	122		☆	Riverine Flood	\$ 12,908	\$ 102,261	0.13	Ò
<u> </u>	123		☆	Riverine Flood	\$ 19,561	\$ 102,261	0.19	Ò
<u> </u>	124		☆	Riverine Flood	\$ 63,068	\$ 102,261	0.62	Ò
<u> </u>	125			Riverine Flood	\$ 118,322	\$ 102,261	1.16	Ď

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	126		☆	Riverine Flood	\$ 34,424	\$ 102,261	0.34	
<u>~</u>	127		4 4	Riverine Flood	\$ 5,049	\$ 102,261	0.05	D
<u> </u>	128		☆	Riverine Flood	\$ 12,014	\$ 102,261	0.12	D
<u>~</u>	129			Riverine Flood	\$ 7,077	\$ 102,261	0.07	D
<u> </u>	130			Riverine Flood	\$ 21,051	\$ 102,261	0.21	Ō
~	131			Riverine Flood	\$ 19,062	\$ 102,261	0.19	D
<u> </u>	132			Riverine Flood	\$ 26,886	\$ 102,261	0.26	D
<u>~</u>	133			Riverine Flood	\$ 38,605	\$ 102,261	0.38	D
<u>~</u>	134			Riverine Flood	\$ 33,262	\$ 102,261	0.33	D
<u>~</u>	135			Riverine Flood	\$ 40,655	\$ 102,261	0.40	Ō
<u>~</u>	136			Riverine Flood	\$ 24,373	\$ 102,261	0.24	D
<u>~</u>	137			Riverine Flood	\$ 44,564	\$ 102,261	0.44	D
~	138			Riverine Flood	\$ 15,919	\$ 102,261	0.16	Ò
~	139			Riverine Flood	\$ 25,931	\$ 102,261	0.25	Ō
~	140			Riverine Flood	\$ 29,763	\$ 102,261	0.29	Ò
~	141			Riverine Flood	\$ 22,245	\$ 102,261	0.22	Ò
~	142			Riverine Flood	\$ 54,529	\$ 102,261	0.53	D
~	143			Riverine Flood	\$ 40,279	\$ 102,261	0.39	D
~	144		M	Riverine Flood	\$ 1,541	\$ 102,261	0.02	D
<u> </u>	145		☆	Riverine Flood	\$ 58,188	\$ 102,261	0.57	Ď
✓	146		☆	Riverine Flood	\$ 65,925	\$ 102,261	0.64	Ď
<u> </u>	147		☆	Riverine Flood	\$ 34,290	\$ 102,261	0.34	Ò

Select	Map Marker▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	148		k	Riverine Flood	\$ 58,388	\$ 102,261	0.57	Ф
~	149			Riverine Flood	\$ 39,002	\$ 102,261	0.38	
<u>~</u>	150		☆	Riverine Flood	\$ 65,571	\$ 102,261	0.64	Ō
✓	151			Riverine Flood	\$ 26,703	\$ 102,261	0.26	D
~	152			Riverine Flood	\$ 30,426	\$ 102,261	0.30	D
~	153			Riverine Flood	\$ 58,646	\$ 102,261	0.57	D
<u> </u>	154		M	Riverine Flood	\$ 1,680	\$ 102,261	0.02	D
<u>~</u>	155			Riverine Flood	\$ 49,471	\$ 102,261	0.48	D
<u>~</u>	156			Riverine Flood	\$ 56,171	\$ 102,261	0.55	D
<u>~</u>	157			Riverine Flood	\$ 65,368	\$ 102,261	0.64	Ō
<u>~</u>	158			Riverine Flood	\$ 57,647	\$ 102,261	0.56	D
<u>~</u>	159			Riverine Flood	\$ 55,937	\$ 102,261	0.55	Ō
~	160			Riverine Flood	\$ 64,182	\$ 102,261	0.63	D
~	161			Riverine Flood	\$ 55,376	\$ 102,261	0.54	D
~	162			Riverine Flood	\$ 51,353	\$ 102,280	0.50	D
~	163			Riverine Flood	\$ 4,516	\$ 102,280	0.04	D
~	164			Riverine Flood	\$ 110,290	\$ 102,280	1.08	D
~	165			Riverine Flood	\$ 17,830	\$ 102,261	0.17	D
~	166		☆	Riverine Flood	\$ 11,789	\$ 102,261	0.12	D
<u> </u>	167		☆	Riverine Flood	\$ 17,582	\$ 102,261	0.17	Ď
~	168		☆	Riverine Flood	\$ 12,586	\$ 102,261	0.12	Ò
<u> </u>	169		☆	Riverine Flood	\$ 16,283	\$ 102,261	0.16	Ď

Select ✓	Map Marker▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	170		☆	Riverine Flood	\$ 7,517	\$ 102,261	0.07	Ф
<u>~</u>	171		☆	Riverine Flood	\$ 2,023	\$ 102,261	0.02	D
~	172			Riverine Flood	\$ 2,284	\$ 102,261	0.02	D
<u> </u>	173		☆	Riverine Flood	\$ 262	\$ 102,261	0.00	D
<u> </u>	174		☆	Riverine Flood	\$ 293	\$ 102,261	0.00	D
<u> </u>	175		☆	Riverine Flood	\$ 1,914	\$ 102,261	0.02	Ò
✓	176		<u> </u>	Riverine Flood	\$ 69,087	\$ 102,261	0.68	Ф
~	177		<u></u>	Riverine Flood	\$ 118,391	\$ 102,261	1.16	Ф
<u> </u>	178		<u></u>	Riverine Flood	\$ 46,019	\$ 102,261	0.45	D
<u> </u>	179		<u> </u>	Riverine Flood	\$ 19,895	\$ 102,261	0.19	D
~	180		<u> </u>	Riverine Flood	\$ 27,863	\$ 102,261	0.27	D
~	181		<u> </u>	Riverine Flood	\$ 19,115	\$ 102,261	0.19	D
~	182		<u> </u>	Riverine Flood	\$ 50,080	\$ 102,261	0.49	D
~	183		<u> </u>	Riverine Flood	\$ 59,877	\$ 102,261	0.59	D
~	184		<u> </u>	Riverine Flood	\$ 31,308	\$ 102,261	0.31	D
<u> </u>	185		<u> </u>	Riverine Flood	\$ 0	\$ 102,261	0.00	D
~	186		<u> </u>	Riverine Flood	\$ 131	\$ 102,261	0.00	D
<u>~</u>	187		<u></u>	Riverine Flood	\$ 11,739	\$ 102,261	0.11	Ď
<u> </u>	188		<u></u>	Riverine Flood	\$ 11,067	\$ 102,261	0.11	Ъ
<u> </u>	189		<u></u>	Riverine Flood	\$ 13,422	\$ 102,261	0.13	Ò
<u> </u>	190		<u> </u>	Riverine Flood	\$ 12,068	\$ 102,261	0.12	Ф
<u> </u>	191			Riverine Flood	\$ 16,365	\$ 102,261	0.16	

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	192		☆	Riverine Flood	\$ 25,497	\$ 102,261	0.25	
~	193			Riverine Flood	\$ 41,877	\$ 102,261	0.41	Ď
<u>~</u>	194		☆	Riverine Flood	\$ 101,632	\$ 102,261	0.99	D
<u> </u>	195			Riverine Flood	\$ 36,455	\$ 102,261	0.36	D
~	196			Riverine Flood	\$ 99,942	\$ 102,261	0.98	Ō
~	197			Riverine Flood	\$ 1,227	\$ 102,261	0.01	D
<u> </u>	198			Riverine Flood	\$ 2,526	\$ 102,261	0.02	D
<u>~</u>	199			Riverine Flood	\$ 2,395	\$ 102,261	0.02	D
<u>~</u>	200			Riverine Flood	\$ 7,732	\$ 102,261	0.08	D
<u>~</u>	201			Riverine Flood	\$ 8,651	\$ 102,261	0.08	D
<u>~</u>	202			Riverine Flood	\$ 2,417	\$ 102,261	0.02	D
<u>~</u>	203			Riverine Flood	\$ 30,074	\$ 102,261	0.29	Ō
~	204			Riverine Flood	\$ 3,812	\$ 102,261	0.04	Ō
~	205			Riverine Flood	\$ 4,418	\$ 102,261	0.04	Ō
~	206			Riverine Flood	\$ 18,959	\$ 102,261	0.19	Ò
~	207			Riverine Flood	\$ 18,641	\$ 102,261	0.18	Ō
<u> </u>	208			Riverine Flood	\$ 3,233	\$ 102,261	0.03	D
~	209			Riverine Flood	\$ 9,376	\$ 102,261	0.09	D
~	210			Riverine Flood	\$ 10,556	\$ 102,261	0.10	D
~	211		☆	Riverine Flood	\$ 2,359	\$ 102,261	0.02	D
~	212		☆	Riverine Flood	\$ 18,888	\$ 102,261	0.18	Ď
<u> </u>	213		☆	Riverine Flood	\$ 1,000	\$ 102,261	0.01	Ò

Riverine Flood \$10,356 \$102,261 0.10 218	Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
Pload St.913 St02.261 0.13	✓	214				\$ 15,682	\$ 102,261	0.15	
Flood \$4,709 \$102,261 0.05	<u> </u>	215				\$ 12,913	\$ 102,261	0.13	D
Flood \$10,356 \$102,261 \$0.00	~	216		☆		\$ 4,709	\$ 102,261	0.05	Ò
218	~	217				\$ 10,356	\$ 102,261	0.10	D
Plood \$1,052 \$102,261 \$0.05	<u> </u>	218		^		\$ 9,447	\$ 102,261	0.09	D
Plood Flood Floo	<u> </u>	219		^		\$ 5,411	\$ 102,261	0.05	D
Flood \$11,052 \$102,261 0.11 222	<u> </u>	220		44		\$ 0	\$ 102,261	0.00	D
Flood \$7,155 \$102,261 0.07 Flood \$7,125 \$102,261 0.07 Riverine Flood \$7,125 \$102,261 0.07 Flood \$7,125 \$102,261 0.07 Flood \$2,397 \$102,261 0.02 Flood \$7,44 \$102,261 0.01 Flood \$7,44 \$102,261 0.01 Flood \$7,44 \$102,261 0.05 Flood \$1,004 \$1,004 \$102,261 0.05 Flood \$1,004 \$1,004 \$102,261 0.05 Flood \$1,004 \$102,261 0.05 Flood \$1,004 \$102,261 0.15 Flood \$1,004 \$102,261 0.15 Flood \$1,004 \$102,261 0.15 Flood \$1,004 \$100,261 0.16	<u>~</u>	221		^		\$ 11,052	\$ 102,261	0.11	Ф
Flood \$ \(\), \(\), \(\) 224 \\ \(\) \	<u> </u>	222		^		\$ 7,155	\$ 102,261	0.07	D
Flood \$2,397 \$102,261 0.02	<u>~</u>	223		^		\$ 7,125	\$ 102,261	0.07	Ò
Plood \$744 \$102,261 0.01	~	224				\$ 2,397	\$ 102,261	0.02	D
V 227 Riverine \$4,921 \$102,261 0.05 V 228 Riverine \$15,351 \$102,261 0.15 V 229 Riverine \$100d \$15,351 \$102,261 0.24 V 230 Riverine \$15,655 \$102,261 0.15 V 231 Riverine \$10,043 \$102,261 0.16 V 232 Riverine \$10,043 \$102,261 0.16 V 232 Riverine \$10,043 \$102,261 0.18 V 232 Riverine \$18,067 \$102,261 0.18	~	225		4 4		\$ 744	\$ 102,261	0.01	D
V 227 Flood \$ 4,921 \$ 102,261 0.05 V 228 Riverine Flood \$ 15,351 \$ 102,261 0.15 V 229 Riverine Flood \$ 24,532 \$ 102,261 0.24 V 230 Riverine Flood \$ 15,655 \$ 102,261 0.15 V 231 Riverine Flood \$ 10,043 \$ 102,261 0.10 V 232 Riverine \$ 18,067 \$ 102,261 0.18	~	226				\$ 5,611	\$ 102,261	0.05	D
V 228 Flood \$ 15,351 \$ 102,261 0.15 ✓ 229 Riverine Flood \$ 24,532 \$ 102,261 0.24 ✓ 230 Riverine Flood \$ 15,655 \$ 102,261 0.15 ✓ 231 Riverine Flood \$ 10,043 \$ 102,261 0.10 ✓ 232 Riverine Flood \$ 18,067 \$ 102,261 0.18	~	227				\$ 4,921	\$ 102,261	0.05	D
Flood \$24,532 \$102,261 0.24 230 Riverine Flood \$15,655 \$102,261 0.15 231 Riverine Flood \$10,043 \$102,261 0.10 Riverine Flood \$10,043 \$102,261 0.10	~	228				\$ 15,351	\$ 102,261	0.15	D
230 Flood \$15,655 \$102,261 0.15 231 Riverine Flood \$10,043 \$102,261 0.10 Riverine Flood \$10,043 \$102,261 0.10	~	229				\$ 24,532	\$ 102,261	0.24	D
231 \$10,043 \$102,261 0.10 Flood \$222 \$\infty \text{Riverine} \text{\$\frac{1}{8} \text{067}} \	~	230		<u></u>		\$ 15,655	\$ 102,261	0.15	D
232 \$18.0b/ \$102.2b1 0.18	~	231			Flood	\$ 10,043	\$ 102,261	0.10	Ò
	<u> </u>	232			Flood	\$ 18,067	\$ 102,261	0.18	D
233 Riverine \$21,216 \$102,261 0.21 Flood	<u> </u>	233				\$ 21,216	\$ 102,261	0.21	Ò
234 Riverine \$ 31,919 \$ 102,261 0.31 Flood	~	234				\$ 31,919	\$ 102,261	0.31	Ò
235 Riverine \$ 12,239 \$ 102,261 0.12 Flood	✓	235		☆		\$ 12,239	\$ 102,261	0.12	Ò

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	236			Riverine Flood	\$ 11,913	\$ 102,261	0.12	
<u>~</u>	237		☆	Riverine Flood	\$ 22,768	\$ 102,261	0.22	Ф
✓	238		k	Riverine Flood	\$ 120,003	\$ 102,261	1.17	Ф
~	239		<u>ka</u>	Riverine Flood	\$ 578,941	\$ 102,261	5.66	Ф
~	240		<u>k</u>	Riverine Flood	\$ 81,600	\$ 102,261	0.80	Ф
✓	241		M	Riverine Flood	\$ 308,539	\$ 102,261	3.02	Ф
✓	242		k	Riverine Flood	\$ 318,431	\$ 102,261	3.11	Ф
✓	243		M	Riverine Flood	\$ 11,607	\$ 102,261	0.11	Ф
✓	244		M	Riverine Flood	\$ 10,084	\$ 102,261	0.10	Ф
✓	245		M	Riverine Flood	\$ 15,644	\$ 102,261	0.15	Ф
✓	246		M	Riverine Flood	\$ 23,039	\$ 102,261	0.23	Ф
~	247		<u>k</u>	Riverine Flood	\$ 735,627	\$ 102,261	7.19	Ф
✓	248		4 4	Riverine Flood	\$ 4,038	\$ 102,261	0.04	Ф
✓	249		4 4	Riverine Flood	\$ 684,981	\$ 102,261	6.70	Ф
✓	250		4 4	Riverine Flood	\$ 380,143	\$ 102,261	3.72	Ф
~	251		<u>k</u>	Riverine Flood	\$ 238,137	\$ 102,261	2.33	Ф
~	252		<u>k</u>	Riverine Flood	\$ 824,319	\$ 102,261	8.06	Ф
~	253		<u>k</u>	Riverine Flood	\$ 33,606	\$ 102,261	0.33	Ф
<u> </u>	254		<u>ka</u>	Riverine Flood	\$ 103,583	\$ 102,261	1.01	Ф
<u> </u>	255		<u>ka</u>	Riverine Flood	\$ 60,894	\$ 102,261	0.60	Ф
<u> </u>	256		<u>k</u>	Riverine Flood	\$ 7,414	\$ 102,261	0.07	Ф
<u>~</u>	257		<u>k</u>	Riverine Flood	\$ 575,067	\$ 102,261	5.62	Ф

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	258		44	Riverine Flood	\$ 785,078	\$ 102,261	7.68	
<u>~</u>	259		44	Riverine Flood	\$ 3,056	\$ 102,261	0.03	D
<u>~</u>	260		4 4	Riverine Flood	\$ 795,078	\$ 102,261	7.77	D
~	261		<u>k</u>	Riverine Flood	\$ 322,583	\$ 102,261	3.15	D
~	262		<u>ka</u>	Riverine Flood	\$ 287,437	\$ 102,261	2.81	D
~	263		<u>ka</u>	Riverine Flood	\$ 300,454	\$ 102,261	2.94	D
~	264		<u>ka</u>	Riverine Flood	\$ 633,690	\$ 102,261	6.20	D
✓	265		<u>ka</u>	Riverine Flood	\$ 554,814	\$ 102,261	5.43	D
✓	266		<u>ka</u>	Riverine Flood	\$ 1,890,675	\$ 102,261	18.49	D
✓	267		44	Riverine Flood	\$ 1,296,960	\$ 102,261	12.68	D
✓	268		<u>ka</u>	Riverine Flood	\$ 309,610	\$ 102,261	3.03	D
<u> </u>	269		44	Riverine Flood	\$ 297,697	\$ 102,261	2.91	D
✓	270		44	Riverine Flood	\$ 31,195	\$ 102,261	0.31	D
✓	271		44	Riverine Flood	\$ 623,484	\$ 102,261	6.10	D
✓	272		44	Riverine Flood	\$ 622,547	\$ 102,261	6.09	D
✓	273		<u>ka</u>	Riverine Flood	\$ 934,306	\$ 102,261	9.14	D
✓	274		<u>ka</u>	Riverine Flood	\$ 893,853	\$ 102,261	8.74	D
<u> </u>	275		<u>ka</u>	Riverine Flood	\$ 202,907	\$ 102,261	1.98	D
~	276		k	Riverine Flood	\$ 874,669	\$ 102,261	8.55	Ò
~	277		<u>k</u>	Riverine Flood	\$ 868,925	\$ 102,261	8.50	Ò
<u> </u>	278		<u>k</u>	Riverine Flood	\$ 453,022	\$ 102,261	4.43	Ò
<u> </u>	279		<u>k</u> 4	Riverine Flood	\$ 277,102	\$ 102,261	2.71	Ò

Select ✓	Map Marker▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	280		44	Riverine Flood	\$ 3,555,878	\$ 102,261	34.77	Ď
~	281		4 4	Riverine Flood	\$ 8,786	\$ 102,261	0.09	Ď
✓	282		44	Riverine Flood	\$ 55,501	\$ 102,261	0.54	D
<u> </u>	283		<u>k</u>	Riverine Flood	\$ 29,912	\$ 102,261	0.29	D
<u>~</u>	284		<u>k</u>	Riverine Flood	\$ 18,978	\$ 102,261	0.19	D
✓	285		M	Riverine Flood	\$ 29,137	\$ 102,261	0.28	D
<u>~</u>	286		44	Riverine Flood	\$ 36,859	\$ 102,261	0.36	D
✓	287		M	Riverine Flood	\$ 435,153	\$ 102,261	4.26	D
✓	288		44	Riverine Flood	\$ 574,702	\$ 102,261	5.62	
✓	289		☆	Riverine Flood	\$ 161,717	\$ 102,261	1.58	Ō
✓	290		☆	Riverine Flood	\$ 13,813	\$ 102,261	0.14	D
✓	291		☆	Riverine Flood	\$ 114,327	\$ 102,261	1.12	Ō
~	292		☆	Riverine Flood	\$ 12,633	\$ 102,261	0.12	Ď
~	293		<u>k</u>	Riverine Flood	\$ 590	\$ 102,261	0.01	Ď
~	294		<u>k</u>	Riverine Flood	\$ 622	\$ 102,261	0.01	Ď
TOTAL (SELECTED)				\$ 31,664,794	\$ 30,064,829	1.05	
TOTAL					\$ 31,664,794	\$ 30,064,829	1.05	



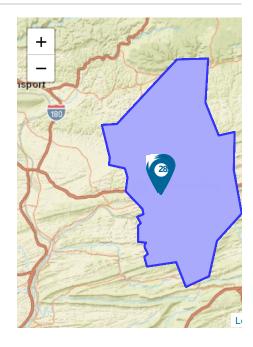
Benefit-Cost Calculator

V.6.0 (Build 20220513.1658 | Release Notes)

Benefit-Cost Analysis

Project Name: Levee \$26 Million

Select	Map Marker▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
~	1		4 4	Riverine Flood	\$ 919	\$ 92,057	0.01	Ъ
✓	2		☆	Riverine Flood	\$ 171,051	\$ 92,075	1.86	Ъ
✓	3		☆	Riverine Flood	\$ 0	\$ 92,057	0.00	Ф
✓	4		☆	Riverine Flood	\$ 23,779	\$ 92,057	0.26	D
✓	5		☆	Riverine Flood	\$ 35,016	\$ 92,057	0.38	D
<u> </u>	6		☆	Riverine Flood	\$ 22,159	\$ 92,057	0.24	Ф
✓	7		44	Riverine Flood	\$ 8,857	\$ 92,057	0.10	Ф
✓	8			Riverine Flood	\$ 44,262	\$ 92,057	0.48	Ф
✓	9			Riverine Flood	\$ 42,834	\$ 92,057	0.47	Ф
✓	10		☆	Riverine Flood	\$ 51,485	\$ 92,057	0.56	Ф
✓	11			Riverine Flood	\$ 43,027	\$ 92,057	0.47	Ф
<u> </u>	12		☆	Riverine Flood	\$ 129,322	\$ 92,057	1.40	Ф
<u> </u>	13		☆	Riverine Flood	\$ 121,410	\$ 92,057	1.32	Ъ
<u> </u>	14		☆	Riverine Flood	\$ 50,724	\$ 92,057	0.55	Ъ
<u> </u>	15		☆	Riverine Flood	\$ 34,589	\$ 92,057	0.38	Ъ



Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	16		☆	Riverine Flood	\$ 30,290	\$ 92,057	0.33	
<u> </u>	17		☆	Riverine Flood	\$ 22,165	\$ 92,057	0.24	D
~	18			Riverine Flood	\$ 52,117	\$ 92,057	0.57	D
~	19			Riverine Flood	\$ 26,741	\$ 92,057	0.29	Ò
~	20		<u>k</u>	Riverine Flood	\$ 25,830	\$ 92,057	0.28	Ò
~	21			Riverine Flood	\$ 26,172	\$ 92,057	0.28	Ò
~	22			Riverine Flood	\$ 1,129	\$ 92,057	0.01	Ò
~	23			Riverine Flood	\$ 107,149	\$ 92,075	1.16	Ò
~	24		<u>k</u>	Riverine Flood	\$ 730,452	\$ 92,057	7.93	D
~	25			Riverine Flood	\$ 14,106	\$ 92,057	0.15	Ō
~	26		☆	Riverine Flood	\$ 17,224	\$ 92,057	0.19	Ò
~	27		☆	Riverine Flood	\$ 28,364	\$ 92,057	0.31	Ò
~	28		☆	Riverine Flood	\$ 26,134	\$ 92,057	0.28	Ò
~	29		☆	Riverine Flood	\$ 53,141	\$ 92,057	0.58	Ò
~	30		☆	Riverine Flood	\$ 35,616	\$ 92,057	0.39	Ò
<u> </u>	31		☆	Riverine Flood	\$ 186	\$ 92,057	0.00	Ò
<u> </u>	32		☆	Riverine Flood	\$ 95,861	\$ 92,057	1.04	Ò
<u> </u>	33		☆	Riverine Flood	\$ 56,801	\$ 92,057	0.62	Ò
~	34			Riverine Flood	\$ 24,068	\$ 92,057	0.26	Ò
~	35			Riverine Flood	\$ 22,576	\$ 92,057	0.25	Ō
~	36			Riverine Flood	\$ 23,720	\$ 92,057	0.26	D
~	37			Riverine Flood	\$ 93,275	\$ 92,057	1.01	D

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	38		☆	Riverine Flood	\$ 33,026	\$ 92,057	0.36	Ф
<u>~</u>	39		☆	Riverine Flood	\$ 30,608	\$ 92,057	0.33	Ф
<u>~</u>	40		☆	Riverine Flood	\$ 37,870	\$ 92,057	0.41	Ф
✓	41		☆	Riverine Flood	\$ 47,057	\$ 92,057	0.51	D
<u> </u>	42		☆	Riverine Flood	\$ 30,212	\$ 92,057	0.33	D
~	43		☆	Riverine Flood	\$ 55,910	\$ 92,057	0.61	D
<u> </u>	44		☆	Riverine Flood	\$ 41,873	\$ 92,057	0.45	Ф
<u>~</u>	45		☆	Riverine Flood	\$ 25,796	\$ 92,057	0.28	D
<u>~</u>	46		☆	Riverine Flood	\$ 65,947	\$ 92,057	0.72	Ф
<u>~</u>	47		☆	Riverine Flood	\$ 118,953	\$ 92,057	1.29	D
<u>~</u>	48		☆	Riverine Flood	\$ 31,709	\$ 92,057	0.34	D
<u>~</u>	49		☆	Riverine Flood	\$ 66,375	\$ 92,057	0.72	Ф
~	50		☆	Riverine Flood	\$ 7,894	\$ 92,057	0.09	Ф
~	51		☆	Riverine Flood	\$ 12,040	\$ 92,057	0.13	Ф
~	52		☆	Riverine Flood	\$ 13,379	\$ 92,057	0.15	Ф
~	53		☆	Riverine Flood	\$ 11,663	\$ 92,057	0.13	D
<u> </u>	54		^	Riverine Flood	\$ 29,092	\$ 92,057	0.32	D
~	55		^	Riverine Flood	\$ 14,293	\$ 92,057	0.16	D
~	56		☆	Riverine Flood	\$ 28,507	\$ 92,057	0.31	D
<u> </u>	57		☆	Riverine Flood	\$ 33,299	\$ 92,057	0.36	Ф
✓	58		☆	Riverine Flood	\$ 5,339	\$ 92,057	0.06	Ò
<u> </u>	59		☆	Riverine Flood	\$ 26,665	\$ 92,057	0.29	Ď

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	60		☆	Riverine Flood	\$ 59,020	\$ 92,057	0.64	
<u> </u>	61		☆	Riverine Flood	\$ 21,051	\$ 92,057	0.23	Ф
~	62		☆	Riverine Flood	\$ 16,552	\$ 92,057	0.18	D
<u> </u>	63		<u>k</u>	Riverine Flood	\$ 22,840	\$ 92,057	0.25	D
~	64			Riverine Flood	\$ 507	\$ 92,057	0.01	Ò
<u> </u>	65		☆	Riverine Flood	\$ 24,286	\$ 92,057	0.26	D
✓	66		☆	Riverine Flood	\$ 30,128	\$ 92,057	0.33	D
✓	67		☆	Riverine Flood	\$ 13,127	\$ 92,057	0.14	D
<u> </u>	68		☆	Riverine Flood	\$ 11,124	\$ 92,057	0.12	Ď
✓	69			Riverine Flood	\$ 15,876	\$ 92,057	0.17	Ō
<u> </u>	70		☆	Riverine Flood	\$ 17,957	\$ 92,057	0.20	D
<u> </u>	71		☆	Riverine Flood	\$ 17,111	\$ 92,057	0.19	D
~	72		☆	Riverine Flood	\$ 31,328	\$ 92,057	0.34	D
✓	73		M	Riverine Flood	\$ 0	\$ 92,057	0.00	
✓	74		☆	Riverine Flood	\$ 13,669	\$ 92,057	0.15	
<u> </u>	75		☆	Riverine Flood	\$ 16,648	\$ 92,057	0.18	Ď
✓	76		44	Riverine Flood	\$ 13,249	\$ 92,057	0.14	
<u> </u>	77		☆	Riverine Flood	\$ 27,993	\$ 92,057	0.30	Ò
<u> </u>	78			Riverine Flood	\$ 32,762	\$ 92,057	0.36	Ò
<u> </u>	79			Riverine Flood	\$ 13,819	\$ 92,057	0.15	Ò
✓	80		☆	Riverine Flood	\$ 9,066	\$ 92,057	0.10	Ò
~	81		☆	Riverine Flood	\$ 27,440	\$ 92,057	0.30	Ò

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	82		☆	Riverine Flood	\$ 29,473	\$ 92,057	0.32	
✓	83		☆	Riverine Flood	\$ 39,511	\$ 92,057	0.43	D
<u>~</u>	84		☆	Riverine Flood	\$ 27,321	\$ 92,057	0.30	D
~	85		☆	Riverine Flood	\$ 18,757	\$ 92,057	0.20	D
~	86		☆	Riverine Flood	\$ 22,945	\$ 92,057	0.25	Ō
~	87		☆	Riverine Flood	\$ 34,015	\$ 92,057	0.37	D
~	88		☆	Riverine Flood	\$ 23,575	\$ 92,057	0.26	D
✓	89		☆	Riverine Flood	\$ 53,880	\$ 92,057	0.59	D
✓	90		☆	Riverine Flood	\$ 131,793	\$ 92,057	1.43	D
~	91		☆	Riverine Flood	\$ 21,570	\$ 92,057	0.23	D
✓	92		☆	Riverine Flood	\$ 21,928	\$ 92,057	0.24	D
~	93		☆	Riverine Flood	\$ 14,371	\$ 92,057	0.16	Ō
~	94			Riverine Flood	\$ 12,853	\$ 92,057	0.14	Ò
~	95			Riverine Flood	\$ 4,159	\$ 92,057	0.05	Ò
~	96			Riverine Flood	\$ 1,100	\$ 92,057	0.01	Ò
<u> </u>	97			Riverine Flood	\$ 5,108	\$ 92,057	0.06	Ō
<u> </u>	98		^	Riverine Flood	\$ 15,194	\$ 92,057	0.17	D
<u> </u>	99		<u>k</u>	Riverine Flood	\$ 201,120	\$ 92,057	2.18	D
<u> </u>	100		☆	Riverine Flood	\$ 23,563	\$ 92,057	0.26	D
~	101		â	Riverine Flood	\$ 46,249	\$ 92,057	0.50	Ď
~	102		☆	Riverine Flood	\$ 32,224	\$ 92,057	0.35	Ò
<u> </u>	103		☆	Riverine Flood	\$ 92,861	\$ 92,057	1.01	Ď

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	104		☆	Riverine Flood	\$ 24,595	\$ 92,057	0.27	
<u> </u>	105		☆	Riverine Flood	\$ 34,192	\$ 92,057	0.37	D
<u>~</u>	106		M	Riverine Flood	\$ 21,264	\$ 92,057	0.23	D
~	107		☆	Riverine Flood	\$ 32,593	\$ 92,057	0.35	D
~	108			Riverine Flood	\$ 32,750	\$ 92,057	0.36	Ō
~	109			Riverine Flood	\$ 136,748	\$ 92,057	1.49	D
~	110			Riverine Flood	\$ 36,247	\$ 92,057	0.39	D
✓	111		M	Riverine Flood	\$ 14,915	\$ 92,057	0.16	D
✓	112		☆	Riverine Flood	\$ 42,477	\$ 92,057	0.46	D
✓	113		M	Riverine Flood	\$ 151,338	\$ 92,057	1.64	D
✓	114		M	Riverine Flood	\$ 197,258	\$ 92,057	2.14	D
<u> </u>	115		☆	Riverine Flood	\$ 23,686	\$ 92,057	0.26	D
✓	116		☆	Riverine Flood	\$ 54,369	\$ 92,057	0.59	D
✓	117		☆	Riverine Flood	\$ 46,785	\$ 92,057	0.51	D
✓	118		☆	Riverine Flood	\$ 19,610	\$ 92,057	0.21	D
✓	119			Riverine Flood	\$ 4,852	\$ 92,057	0.05	D
✓	120		☆	Riverine Flood	\$ 9,446	\$ 92,057	0.10	D
<u> </u>	121		<u>k</u>	Riverine Flood	\$ 6,214	\$ 92,057	0.07	D
~	122		☆	Riverine Flood	\$ 12,908	\$ 92,057	0.14	Ò
<u> </u>	123		☆	Riverine Flood	\$ 19,561	\$ 92,057	0.21	Ò
<u> </u>	124		☆	Riverine Flood	\$ 63,068	\$ 92,057	0.69	Ò
<u> </u>	125			Riverine Flood	\$ 118,322	\$ 92,057	1.29	Ď

	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	126			Riverine Flood	\$ 34,424	\$ 92,057	0.37	
<u>~</u>	127		<u>k</u>	Riverine Flood	\$ 5,049	\$ 92,057	0.05	Ď
✓	128		☆	Riverine Flood	\$ 12,014	\$ 92,057	0.13	D
~	129			Riverine Flood	\$ 7,077	\$ 92,057	0.08	D
<u> </u>	130		^	Riverine Flood	\$ 21,051	\$ 92,057	0.23	D
~	131		^	Riverine Flood	\$ 19,062	\$ 92,057	0.21	D
~	132		^	Riverine Flood	\$ 26,886	\$ 92,057	0.29	Ъ
✓	133		^	Riverine Flood	\$ 38,605	\$ 92,057	0.42	D
✓	134		^	Riverine Flood	\$ 33,262	\$ 92,057	0.36	D
✓	135		^	Riverine Flood	\$ 40,655	\$ 92,057	0.44	Ф
✓	136		^	Riverine Flood	\$ 24,373	\$ 92,057	0.26	Ъ
<u> </u>	137			Riverine Flood	\$ 44,564	\$ 92,057	0.48	D
~	138		^	Riverine Flood	\$ 15,919	\$ 92,057	0.17	Ф
✓	139		^	Riverine Flood	\$ 25,931	\$ 92,057	0.28	Ъ
~	140		^	Riverine Flood	\$ 29,763	\$ 92,057	0.32	Ф
<u> </u>	141		^	Riverine Flood	\$ 22,245	\$ 92,057	0.24	Ф
<u> </u>	142		^	Riverine Flood	\$ 54,529	\$ 92,057	0.59	Ф
~	143			Riverine Flood	\$ 40,279	\$ 92,057	0.44	D
✓	144		k	Riverine Flood	\$ 1,541	\$ 92,057	0.02	D
<u> </u>	145		☆	Riverine Flood	\$ 58,188	\$ 92,057	0.63	D
<u>~</u>	146		☆	Riverine Flood	\$ 65,925	\$ 92,057	0.72	Ď
<u> </u>	147			Riverine Flood	\$ 34,290	\$ 92,057	0.37	Ď

Select ✓	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	148		k	Riverine Flood	\$ 58,388	\$ 92,057	0.63	Ф
✓	149			Riverine Flood	\$ 39,002	\$ 92,057	0.42	Ф
✓	150			Riverine Flood	\$ 65,571	\$ 92,057	0.71	
✓	151			Riverine Flood	\$ 26,703	\$ 92,057	0.29	Ď
✓	152		☆	Riverine Flood	\$ 30,426	\$ 92,057	0.33	Ď
✓	153		☆	Riverine Flood	\$ 58,646	\$ 92,057	0.64	Ō
✓	154		<u>k</u>	Riverine Flood	\$ 1,680	\$ 92,057	0.02	Ď
✓	155			Riverine Flood	\$ 49,471	\$ 92,057	0.54	D
✓	156			Riverine Flood	\$ 56,171	\$ 92,057	0.61	D
✓	157			Riverine Flood	\$ 65,368	\$ 92,057	0.71	Ò
✓	158		☆	Riverine Flood	\$ 57,647	\$ 92,057	0.63	Ō
✓	159			Riverine Flood	\$ 55,937	\$ 92,057	0.61	Ō
✓	160			Riverine Flood	\$ 64,182	\$ 92,057	0.70	Ō
✓	161			Riverine Flood	\$ 55,376	\$ 92,057	0.60	Ō
✓	162			Riverine Flood	\$ 51,353	\$ 92,075	0.56	Ф
✓	163			Riverine Flood	\$ 4,516	\$ 92,075	0.05	Ф
✓	164			Riverine Flood	\$ 110,290	\$ 92,075	1.20	D
✓	165			Riverine Flood	\$ 17,830	\$ 92,057	0.19	Ō
✓	166			Riverine Flood	\$ 11,789	\$ 92,057	0.13	Ф
✓	167			Riverine Flood	\$ 17,582	\$ 92,057	0.19	Ф
✓	168		☆	Riverine Flood	\$ 12,586	\$ 92,057	0.14	Ф
······································	169			Riverine Flood	\$ 16,283	\$ 92,057	0.18	Ф

Select ✓	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	170		☆	Riverine Flood	\$ 7,517	\$ 92,057	0.08	D
✓	171		☆	Riverine Flood	\$ 2,023	\$ 92,057	0.02	Ф
✓	172			Riverine Flood	\$ 2,284	\$ 92,057	0.02	
✓	173			Riverine Flood	\$ 262	\$ 92,057	0.00	Ď
✓	174			Riverine Flood	\$ 293	\$ 92,057	0.00	Ď
✓	175			Riverine Flood	\$ 1,914	\$ 92,057	0.02	Ď
✓	176			Riverine Flood	\$ 91,445	\$ 92,057	0.99	Ď
✓	177			Riverine Flood	\$ 118,391	\$ 92,057	1.29	D
✓	178			Riverine Flood	\$ 46,019	\$ 92,057	0.50	D
✓	179		^	Riverine Flood	\$ 19,895	\$ 92,057	0.22	Ò
✓	180		M	Riverine Flood	\$ 27,863	\$ 92,057	0.30	Ō
✓	181			Riverine Flood	\$ 19,115	\$ 92,057	0.21	Ō
✓	182		☆	Riverine Flood	\$ 50,080	\$ 92,057	0.54	Ō
✓	183		☆	Riverine Flood	\$ 59,877	\$ 92,057	0.65	Ò
✓	184			Riverine Flood	\$ 31,308	\$ 92,057	0.34	Ф
✓	185			Riverine Flood	\$ 0	\$ 92,057	0.00	Ф
✓	186			Riverine Flood	\$ 131	\$ 92,057	0.00	Ď
✓	187		☆	Riverine Flood	\$ 11,739	\$ 92,057	0.13	Ō
✓	188		^	Riverine Flood	\$ 11,067	\$ 92,057	0.12	Ф
✓	189		^	Riverine Flood	\$ 13,422	\$ 92,057	0.15	Ф
✓	190			Riverine Flood	\$ 12,068	\$ 92,057	0.13	Ф
······································	191		^	Riverine Flood	\$ 16,365	\$ 92,057	0.18	Ъ

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	192			Riverine Flood	\$ 25,497	\$ 92,057	0.28	
~	193		â	Riverine Flood	\$ 41,877	\$ 92,057	0.45	Ď
~	194			Riverine Flood	\$ 101,632	\$ 92,057	1.10	Ō
~	195		☆	Riverine Flood	\$ 36,455	\$ 92,057	0.40	Ò
<u> </u>	196		☆	Riverine Flood	\$ 99,942	\$ 92,057	1.09	Ò
<u> </u>	197		☆	Riverine Flood	\$ 1,227	\$ 92,057	0.01	Ò
~	198		☆	Riverine Flood	\$ 2,526	\$ 92,057	0.03	Ò
~	199		☆	Riverine Flood	\$ 2,395	\$ 92,057	0.03	Ò
~	200		☆	Riverine Flood	\$ 7,732	\$ 92,057	0.08	Ò
~	201		<u></u>	Riverine Flood	\$ 8,651	\$ 92,057	0.09	Ò
<u> </u>	202		☆	Riverine Flood	\$ 2,417	\$ 92,057	0.03	Ò
~	203		<u></u>	Riverine Flood	\$ 30,074	\$ 92,057	0.33	Ò
~	204		☆	Riverine Flood	\$ 3,812	\$ 92,057	0.04	Ò
~	205		☆	Riverine Flood	\$ 4,418	\$ 92,057	0.05	Ò
~	206		☆	Riverine Flood	\$ 18,959	\$ 92,057	0.21	Ò
~	207		☆	Riverine Flood	\$ 18,641	\$ 92,057	0.20	Ò
~	208		☆	Riverine Flood	\$ 3,233	\$ 92,057	0.04	Ò
~	209			Riverine Flood	\$ 9,376	\$ 92,057	0.10	Ō
~	210			Riverine Flood	\$ 10,556	\$ 92,057	0.11	D
~	211			Riverine Flood	\$ 2,359	\$ 92,057	0.03	D
<u> </u>	212		â	Riverine Flood	\$ 18,888	\$ 92,057	0.21	D
<u> </u>	213			Riverine Flood	\$ 1,000	\$ 92,057	0.01	Ò

217 Riverine Flood \$10,356 \$92,057 0.11 218 Riverine Flood \$9,447 \$92,057 0.10 219 Riverine Flood \$5,411 \$92,057 0.06 220 Riverine Flood \$11,052 \$92,057 0.00 221 Riverine Flood \$11,052 \$92,057 0.00 221 Riverine Flood \$11,052 \$92,057 0.12 222 Riverine Flood \$7,155 \$92,057 0.08 223 Riverine Flood \$7,125 \$92,057 0.08 224 Riverine Flood \$7,125 \$92,057 0.08 225 Riverine Flood \$7,44 \$92,057 0.01 226 Riverine Flood \$7,44 \$92,057 0.01 227 Riverine Flood \$4,921 \$92,057 0.05 228 Riverine Flood \$15,351 \$92,057 0.05 229 Riverine Flood \$15,351 \$92,057 0.07 229 Riverine Flood \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351 \$15,351	
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Flood \$4,709 \$92,057 0.05	Ò
Plood S 10,356 S 92,057 O.11	D
Flood Flood \$ 9,447 \$ 92,057 0.10 219 Riverine Flood \$ 5,411 \$ 92,057 0.06 220 Riverine Flood \$ 11,052 \$ 92,057 0.00 221 Riverine Flood \$ 11,052 \$ 92,057 0.12 222 Riverine Flood \$ 7,155 \$ 92,057 0.08 223 Riverine Flood \$ 7,125 \$ 92,057 0.08 224 Riverine Flood \$ 7,125 \$ 92,057 0.08 224 Riverine Flood \$ 7,125 \$ 92,057 0.03 225 Riverine Flood \$ 5,611 \$ 92,057 0.01 226 Riverine Flood \$ 5,611 \$ 92,057 0.06 227 Riverine Flood \$ 4,921 \$ 92,057 0.05 228 Riverine Flood \$ 4,921 \$ 92,057 0.05 228 Riverine Flood \$ 15,351 \$ 92,057 0.17	D
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Flood \$0 \$92,057 0.00	D
✓ 221 Flood \$11,052 \$92,057 0.12 ✓ 222 Riverine Flood \$7,155 \$92,057 0.08 ✓ 223 Riverine Flood \$7,125 \$92,057 0.08 ✓ 224 Riverine Flood \$2,397 \$92,057 0.03 ✓ 225 Riverine Flood \$744 \$92,057 0.01 ✓ 226 Riverine Flood \$5,611 \$92,057 0.06 ✓ 227 Riverine Flood \$4,921 \$92,057 0.05 ✓ 228 Riverine Flood \$15,351 \$92,057 0.17 ✓ 229 Riverine Flood \$24,532 \$92,057 0.27	D
Flood Flood \$7,125 \$92,057 0.08 Riverine Flood \$7,125 \$92,057 0.08 Z224 Riverine Flood \$2,397 \$92,057 0.03 Riverine Flood \$744 \$92,057 0.01 Riverine Flood \$5,611 \$92,057 0.06 Riverine Flood \$4,921 \$92,057 0.05 Riverine Flood \$15,351 \$92,057 0.17 Riverine Flood \$15,351 \$92,057 0.17	D
Flood \$7,125 \$92,057 0.08 Z224 Riverine \$2,397 \$92,057 0.03 Z225 Riverine Flood \$744 \$92,057 0.01 Z226 Riverine Flood \$5,611 \$92,057 0.06 Z27 Riverine Flood \$4,921 \$92,057 0.05 Riverine Flood \$15,351 \$92,057 0.17 Riverine Flood \$15,351 \$92,057 0.17 Riverine Flood \$15,351 \$92,057 0.17	D
V 224 Flood \$ 2,397 \$ 92,057 0.03 ✓ 225 Riverine Flood \$ 744 \$ 92,057 0.01 ✓ 226 Riverine Flood \$ 5,611 \$ 92,057 0.06 ✓ 227 Riverine Flood \$ 4,921 \$ 92,057 0.05 ✓ 228 Riverine Flood \$ 15,351 \$ 92,057 0.17 ✓ 229 Riverine Flood \$ 24,532 \$ 92,057 0.27	Ф
V 225 Flood \$744 \$ 92,057 0.01 ✓ 226 Riverine Flood \$ 5,611 \$ 92,057 0.06 ✓ 227 Riverine Flood \$ 4,921 \$ 92,057 0.05 ✓ 228 Riverine Flood \$ 15,351 \$ 92,057 0.17 ✓ 229 Riverine Flood \$ 24,532 \$ 92,057 0.27	D
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✓ 227 Flood \$ 4,921 \$ 92,057 0.05 ✓ 228 Riverine Flood \$ 15,351 \$ 92,057 0.17 ✓ 229 Riverine \$ 24,532 \$ 92,057 0.27	Ф
228 Flood \$15,351 \$92,057 0.17 229 Riverine \$24,532 \$92,057 0.27	Ф
229 \$ 24,532 \$ 92,057 0.27	Ф
	Ф
Riverine \$ 15,655 \$ 92,057 0.17	Ф
Riverine \$10,043 \$92,057 0.11 Flood	Ф
Riverine \$18,067 \$92,057 0.20	D
Riverine \$ 21,216 \$ 92,057 0.23	D
234 Riverine \$ 31,919 \$ 92,057 0.35	D
235 Riverine \$12,239 \$92,057 0.13 Flood	D

Select	Map Marker ▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	236			Riverine Flood	\$ 11,913	\$ 92,057	0.13	
<u> </u>	237			Riverine Flood	\$ 22,768	\$ 92,057	0.25	Ф
✓	238		k	Riverine Flood	\$ 120,003	\$ 92,057	1.30	Ф
~	239		<u>k</u>	Riverine Flood	\$ 578,941	\$ 92,057	6.29	Ф
~	240		<u>k</u>	Riverine Flood	\$ 81,600	\$ 92,057	0.89	D
✓	241		M	Riverine Flood	\$ 308,539	\$ 92,057	3.35	Ф
✓	242		M	Riverine Flood	\$ 318,431	\$ 92,057	3.46	Ф
✓	243		M	Riverine Flood	\$ 11,607	\$ 92,057	0.13	Ф
✓	244		M	Riverine Flood	\$ 10,084	\$ 92,057	0.11	Ф
✓	245		M	Riverine Flood	\$ 15,644	\$ 92,057	0.17	Ф
✓	246		M	Riverine Flood	\$ 23,039	\$ 92,057	0.25	Ф
✓	247		M	Riverine Flood	\$ 735,627	\$ 92,057	7.99	Ф
~	248		4 4	Riverine Flood	\$ 4,038	\$ 92,057	0.04	Ф
~	249		4 4	Riverine Flood	\$ 684,981	\$ 92,057	7.44	Ф
~	250		4 4	Riverine Flood	\$ 380,143	\$ 92,057	4.13	Ф
~	251		<u>k</u>	Riverine Flood	\$ 238,137	\$ 92,057	2.59	Ф
~	252		<u>k</u>	Riverine Flood	\$ 824,319	\$ 92,057	8.95	D
~	253		<u>k</u>	Riverine Flood	\$ 33,606	\$ 92,057	0.37	Ф
~	254		<u>k</u>	Riverine Flood	\$ 103,583	\$ 92,057	1.13	D
<u> </u>	255		k	Riverine Flood	\$ 60,894	\$ 92,057	0.66	Ф
<u> </u>	256		<u>k</u>	Riverine Flood	\$ 7,414	\$ 92,057	0.08	Ф
<u> </u>	257		<u>k</u>	Riverine Flood	\$ 575,067	\$ 92,057	6.25	Ф

Select	Map Marker▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	258		44	Riverine Flood	\$ 785,078	\$ 92,057	8.53	
<u> </u>	259		<u>ka</u>	Riverine Flood	\$ 3,056	\$ 92,057	0.03	Ф
~	260		<u>k</u>	Riverine Flood	\$ 795,078	\$ 92,057	8.64	Ф
~	261		<u>k</u>	Riverine Flood	\$ 322,583	\$ 92,057	3.50	Ъ
~	262		<u>k</u>	Riverine Flood	\$ 287,437	\$ 92,057	3.12	Ф
~	263		<u>k</u>	Riverine Flood	\$ 300,454	\$ 92,057	3.26	Ф
<u> </u>	264		<u>k</u>	Riverine Flood	\$ 633,690	\$ 92,057	6.88	Ф
<u> </u>	265		<u>k</u>	Riverine Flood	\$ 554,814	\$ 92,057	6.03	Ъ
~	266		<u>k</u>	Riverine Flood	\$ 1,890,675	\$ 92,057	20.54	Ъ
<u> </u>	267		<u>k</u>	Riverine Flood	\$ 1,296,960	\$ 92,057	14.09	Ъ
<u> </u>	268		<u>k</u>	Riverine Flood	\$ 309,610	\$ 92,057	3.36	D
<u> </u>	269		<u>k</u>	Riverine Flood	\$ 297,697	\$ 92,057	3.23	D
<u> </u>	270		<u>k</u>	Riverine Flood	\$ 31,195	\$ 92,057	0.34	D
<u> </u>	271		<u>k</u>	Riverine Flood	\$ 623,484	\$ 92,057	6.77	D
~	272		<u>k</u>	Riverine Flood	\$ 622,547	\$ 92,057	6.76	Ъ
<u> </u>	273		<u>k</u>	Riverine Flood	\$ 934,306	\$ 92,057	10.15	Ф
<u> </u>	274		<u>k</u>	Riverine Flood	\$ 893,853	\$ 92,057	9.71	D
<u> </u>	275		<u>k</u>	Riverine Flood	\$ 202,907	\$ 92,057	2.20	D
<u> </u>	276		<u>k</u>	Riverine Flood	\$ 874,669	\$ 92,057	9.50	Ъ
~	277		<u>k</u>	Riverine Flood	\$ 868,925	\$ 92,057	9.44	D
~	278		<u>ka</u>	Riverine Flood	\$ 453,022	\$ 92,057	4.92	Ъ
<u> </u>	279		M	Riverine Flood	\$ 277,102	\$ 92,057	3.01	Ф

Select 🗸	Map Marker▲	Mitigation Title	Property Type	Hazard	Benefits (B)	Costs (C)	BCR (B/C)	Сору
✓	280		44	Riverine Flood	\$ 3,555,878	\$ 92,057	38.63	
<u>~</u>	281		<u>ka</u>	Riverine Flood	\$ 8,786	\$ 92,057	0.10	Ф
<u>~</u>	282		44	Riverine Flood	\$ 55,501	\$ 92,057	0.60	Ф
<u> </u>	283		<u>ka</u>	Riverine Flood	\$ 29,912	\$ 92,057	0.32	Ф
<u>~</u>	284		ka .	Riverine Flood	\$ 18,978	\$ 92,057	0.21	Ф
<u>~</u>	285		<u>ka</u>	Riverine Flood	\$ 29,137	\$ 92,057	0.32	Ф
✓	286		ka .	Riverine Flood	\$ 36,859	\$ 92,057	0.40	Ф
✓	287		44	Riverine Flood	\$ 435,153	\$ 92,057	4.73	Ф
✓	288		44	Riverine Flood	\$ 574,702	\$ 92,057	6.24	Ф
✓	289		☆	Riverine Flood	\$ 161,717	\$ 92,057	1.76	Ф
✓	290		☆	Riverine Flood	\$ 13,813	\$ 92,057	0.15	Ф
✓	291		☆	Riverine Flood	\$ 114,327	\$ 92,057	1.24	Ф
✓	292		☆	Riverine Flood	\$ 12,633	\$ 92,057	0.14	Ф
<u>~</u>	293		<u>k</u>	Riverine Flood	\$ 590	\$ 92,057	0.01	Ф
<u> </u>	294		<u>k</u>	Riverine Flood	\$ 622	\$ 92,057	0.01	Ф
TOTAL (SELECTED)				\$ 31,754,226	\$ 27,064,848	1.17	
TOTAL					\$ 31,754,226	\$ 27,064,848	1.17	

			Tatal	Total									Depth of	Damah af			DI-J-				C				C								Min Dave	May Dave
INPUT	FIELD ID STRUCTURE	Occupancy/	County Fair	County Assessed	# of	Foundatio	n 1st Floor Height above	Total SE	Latituda	Longitudo [Depth of Lee Flo	ood OUPUT	Flood	Depth of Flood in	Floodng	Struc	Depth	% Bldg	Bldg Loss	Contents	Contents Depth	% Contents	Content	Commercial Inventory	Comm Inventory	% Comm Inventory	Comm Inventory [obric ID	Dobric Fin	Debris from	Debris from	Debris	to	Max Days to
FIELDS	FIELD ID STRUCTURE	Zoning	Market	alue x CLR	Stories	Type	Grade (Ft)	TOTAL SF	Latitude	Longitude F	lood Lee Elev	FIELDS	Ground		Expected?	Occup ID		Damage	\$\$	Value \$\$	Damage	Damage	Loss \$\$	Cost (\$)	Depth	Damage	Loss \$\$	ebris iD	Debris_Fin	Struc	Foundation	Total		
			Value (\$)	(\$)									(Ft)	(Ft)			ID				ID				Damage ID								Struc	Struc
	1 B-003 2 B-004	COM1 RES1		1326572.1 102457.81	3	3	-0.012387168 2.933105465			-76.4608 -76.4609	-0.50739 483.23 5 706825	268 483	-0.61954	4 -0.60715 2 2.76677		C1LN R12B	0 108	38 30033		1326572 51228.5		28 06711	0 14378.36	112679.06	0	0	0	ES1BSG0	13.1384	Ó) (13.1384	0 180	
	3 B-005	RES1		110396.16	2	4	1.373709306			-76.4603		483		3 0.811029		R12B	108	20.62206				17.62206		0	0	0		ES1BSG0		0			180	
	4 B-006	RES1		101781.82	3	4	2.229872566				2.736238 484.7			0.49550		R13B	110	12.99101					9398.737	0	0	0		ES1BSG0		O		21.4368	180	
	5 B-007	RES3A	37856	98047.04	2	4	2.456922456				2.881273 484.6		2.833309	0.376387	7 1	R3A1B	205	13.12916	12872.75	49023.5	82		8091.597	0	0	0	0 F	ES3ANBS(0) 0		180	
	6 B-008	RES1		147847.56	2	4	1.782625563				3.495756 484.6			3 1.663543		R12B	108	24.31771					16739.83	0	0	0		ES1BSG0		0) (180	
	7 B-009	RES1		96754.63	2	4	0.911190667				2.648974 484.3			5 1.656369		R12B	108		23493.66			22.59458		0	0	0		ES1BSG0		0) 0	12.1792	180	
	8 B-010 9 B-011	RES1 RES1	43061 : 34720	111527.99 89924.8	2	4	1.627379489 2.581807928				4.468245 484.4 5.635397 484.3			3 2.929918 3 3.08139		R12B R12B	108 108		32108.35 26443.91			28.71967 29.32556	13185.36	0	0	. 0		ES1BSG0 ES1BSG0	12.8128 12.32	0) (12.8128	180 180	
	10 B-012	RES1		55369.02	2	3	1.735531709				3.925266 484.1			2 2.23947		R12N	107	14.95788	8282.03			19.95788		0	0	0		ES1NBFT1		O) 0	3.8253	180	
	11 B-013	RES1	32715	84731.85	3	4	2.276737623	1152	41.00075	-76.4646	5.292456 484.2	677	5.340778	3.064043	1 1	R13B	110	25.38424	21508.32	42365.5	26	28.06404	11889.47	0	0	0	0 F	ES1BSG0	10.1376	0) (10.1376	180	360 Depth
	12 B-014	RES1		143587.01	3	4	2.402549888				5.422522 484.1			4 3.032264		R13B	110		36174.71		26	28.03226		0	0	0		ES1BSG0	21.472	0) (21.472	180	
	13 B-015 14 B-016	RES1		100763.95	2	4	1.908990148				3.334428 483.9 3.873653 483.9			2 1.423552		R12B R13B	108 110		23294.15			20.96486		0	0	0		ES1BSG0	16.7552	0) (16.7552 20.2752	180 180	
	14 B-016 15 B-017	RES1 COM1	143115	133478.24 370667.85	2	3	3.117529605 0.520618778				4.148505 483.8°			9 0.787499 4 3.487225		C1LN	217		18119.64 62918.68		26 90		13689.83 229245.3	4306.25	1	70.35947188		ES1BSG0 OM1NBF1	20.2752	0) (1.125	360	
	16 B-018	RES1		122532.9	3	4	7.498650264				3.078622 483.			3 -4.5022		R13B	110	3	3675.96			0		0	0	0	0			_			0	0 Depti
	17 B-019	RES1	67825	175666.75	3	4	0.457914978	2676	40.99994	-76.4644	2.276919 483.9	035	2.321374	1.863459	9 1	R13B	110	19.18076	33694.07	87833	26	26.3173	23115.27	0	0	0	0 F	ES1BSG0	23.5488	0) (23.5488	180	360 Depth
	18 B-020	COM1		168927.57	2	4	2.025469741				3.629855 483.8			4 1.51004		C1LB	217		19511.44		90		57706.65	8853.65	1	40.18079017				0) (2.313	360	
	19 B-021	RES1		81401.11	3	4	2.240551631				3.761753 483.7			3 1.51933		R13B	110		13932.59			24.59666		0	0	0		ES1BSG0	13.8336	0) (13.8336	180	
	20 B-022 21 B-023	RES1 RES1		122009.72 128956.1	2	4	2.661951566 2.363482631				3.852046 483.74 4.086535 483.79			3 1.214046 5 1.743903		R12B R12B	108 108	24.71952	26927.67			23.20732	11894.85	0	0	. 0		ES1BSG0 ES1BSG0	14.4672 13.8336	0) (14.4672 13.8336	180 180	
	22 B-024	RES1		117236.35	2	4	0.994				2.833157 483.8			3 1.838928		R12B	108		29537.19				13993.58	0	0	. 0		ES1BSG0		0) 0		180	
	23 B-025	RES1	64210	166303.9	2	3	-0.100611052				2.860723 483.8			7 2.957868		R12N	107		29654.27		23	22.83147	18984.71	0	0	0		ES1NBFT1		O) (9.471	180	
	24 B-027	RES1		84990.85	2	5	5.492057531				3.439799 483.8			7 -2.03629		R12N	107	0	0			0	0	0	0	0	0						0	0 Depti
	25 B-028	RES3A		113159.69	2	7	10				2.766985 483.7			-7.11888		R3A1N	204	0	0			0	0	0	0	0	0	ECADOS.	40.000	_		40.57-	0	0 Depti
	26 B-029 27 B-030	RES1		91639.38	2	4	1.686626891				3.541205 483.8			7 1.82612		R12B R12B	108 108		23029.43			23.78284	10897.18 12742.44	0	0	0		ES1BSG0 ES1BSG0	12.672 14.96	0) (180 180	
	27 B-030 28 B-031	RES1 COM1	40131 : 38340	103939.29 99300.6	1	3	1.576400004 0.360120002				3.510613 483.9 3.872121 483.8		3.507697	7 1.931297 1 3.51669		C1LN	217	25.65649 17.03338	26667.1 16914.15				61764.88	13208.13	1	70.68358817				n) (14.96 3.4506	360	
	29 B-032	RES1		64933.89	3	4	0.658302925				3.241465 483.9			2 2.570219		R13B	110	22.85109	14837.9			27.57022		0	0	0		ES1BSG0		d) 0	11.3344	180	
	30 B-033	RES1	32726	84760.34	3	4	0.871680952	1982	40.99988	-76.4635	3.00812 483.9	579	3.010552	2 2.13887	1 1	R13B	110	20.69436	17540.54	42380	26	27.13887	11501.45	0	0	0	0 F	ES1BSG0	17.4416	0) 0	17.4416	180	360 Depth
	31 B-034	RES1		402281.39	2	4	2.265110808				2.999981 483.9			0.739539		R12B	108			201140.5		17.47908		0	0	0		ES1BSG0	17.952	0) (17.952	180	
	32 B-035	COM1		245708.12	2	4	2.176889023				3.034444 484.0			0.85517		C1LB	217	7.841363					55343.49	28441.92	1	27.08960102				0) (360	
	33 B-036 34 B-037	RES1 RES1		199857.35 72007.18	2	4	1.701810545 1.887018036				3.077094 484.09 3.97605 483.9			9 1.374308 2 2.092174		R13B R12B	110 108		32468.46 18920.93			23.87154 25.36869		0	0	0		ES1BSG0		0) (24.4728 16.2624	180 180	
	35 B-038	RES1		200025.7	2	4	1.92834956				4.567879 483.6			2 2.638172		R12B	108			100012.5		27.55269		0	0	0		ES1BSG0	19.9584	0		19.9584	180	
	36 B-039	RES1		114503.9	2	4	2.200661742				4.628679 483.			5 2.426398		R12B	108	27.27919		57251.5		26.70559		0	0	0		ES1BSG0		O) 0		180	
	37 B-040	RES1	29319	75936.21	3	4	2.271366659	1248	40.9988	-76.4637	4.607155 483.6	056	4.610056	5 2.338689	9 1	R13B	110	21.69345	16473.14	37968	26	27.33869	10379.95	0	0	0	0 F	ES1BSG0	10.9824	Ö) (10.9824	180	360 Depth
	38 B-041	RES1		90704.39	3	4	2.075613985				4.577939 483.5			2.502235		R13B	110		20418.54			27.50223		0	0	0		ES1BSG0		0		11.5632	180	
	39 B-042 40 B-043	RES1 RES1		120015.42 98430.36	3	4	2.699737508 1.778650142				5.350337 483.54 4.713005 483.54			4 2.630706 5 2.966736		R13B R12B	110 108		27787.71 28446.47			27.63071 28.86694	16580.5	0	0	0		ES1BSG0	15.6288 9.7592	0) (15.6288 9.7592	180 180	
	40 B-043 41 B-044	RES1		145366.34	2	4	1.778030142				4.615868 483.6			5 2.676476		R12B	108		40745.26				20137.48	0	0	. 0		ES1BSG0		0		25.3792	180	
	42 B-045	RES1		200442.69	2	4	0.988162238		40.99886		4.691152 483.6			7 3.703884		R12B	108		65182.58			31.81554		0	0	0		ES1BSG0		O) 0	30.8176	180	
	43 B-046	RES1	75203	194775.77	1	4	2.165534777	1330	40.99905	-76.4629	4.753698 483.7	317	4.758309	2.59277	5 1	R11B	704	43.14942	84044.29	97387.5	535	23.77832	23157.12	0	0	0	0 F	ES1BSG0	11.704	0) (11.704	180	360 Depth
	44 B-048	RES1		140675.85	1	4	3.015499198				5.746198 483.			7 2.622788		R11B	704	43.35952				23.86836		0	0	0		ES1BSG0		0	,		180	
	45 B-050	RES1		175534.66	1	4	2.443423119 1.264012376		40.99932		3.903815 483.9 2.815883 483.9			7 1.459294		R11B R12B	704 108	35.21505 24.70589	61814.39		535 24	20.37788 23.18824		0	0	0		ES1BSG0	11.3168 9.504	0) (11.3168	180 180	
	46 B-051 47 B-052	RES1 RES1		76428.31 123053.49	3	4	1.34379804				0.65663 484.0		0.506498	9 1.74117 3 -0.837		R13B	110		12705.71			9.138896		0	0	. 0	0	ESIBSGU	9.504	U	, ,	9.504	180	0 360 Depti 0 Depti
	48 B-053	RES1		144117.96	3	4	3.657283242				0.448244 483.9		0.329001			R13B	110	3	4323.51			3.358588		0	0	0	0						0	0 Depti
	49 B-054	RES1	40820	105723.8	3	4	2.690217263	1440	40.99912	-76.4617	2.429659 483.8	882	2.393045	-0.2971	7 1	R13B	110	11.40565	12058.4	52861.5	26	12.91979	6829.595	0	0	0	0						0	0 Depti
	50 B-055	RES1		118163.57	2	4	2.970999456				4.695395 483.8			1 1.570212		R12B	108		28183.13			21.99148		0	0	0		ES1BSG0	15.0304	0) (15.0304	180	
	51 B-056	COM1		143952.2	1	7	-0.268228033				5.679567 483.6			5 5.953864		C1LN	217	22.86159			90		119148.1	18520.32	1	89.769318		OM1NBS(0			450	
	52 B-057 53 B-058	RES1 RES1		120383.2 127505.7	3	4	3.469259284 2.261153878				5.757796 483.7 5.746178 483.7			2 2.280622 5 3.487842		R12B R13B	108 110	26.84187 27.92705				26.12249	18161.71	0	0	. 0		ES1BSG0 ES1BSG0		0) (180 180	
	54 B-059	RES1		131489.12	3	4	3.106615397				5.669703 483.6			7 2.567355		R13B	110	22.83677	30027.85		26	27.56735		0	0	. 0		ES1BSG0	16.6496	0) (16.6496	180	360 Depti
	55 B-060	RES1		160396.11	2	4	1.602809001				5.535691 483.6			3.9210		R12B	108	33.60535			24		26212.14	0	0	0		ES1BSG0	17.3536	d) 0	17.3536	180	
	56 B-061	RES1		124004.02		4	3.288226328				5.573701 483.5			2.28349		R13B		21.41745				27.28349		0	0	0		ES1BSG0		0		14.6432		
	57 B-062	RES1		68818.89	2	4	2.352586198				5.558649 483.5			3.207373		R12B	108	30.03687					10264.03	0				ES1BSG0		0			180	
	58 B-063 59 B-064	RES1 RES1		50295.21 158518.36	2	4	2.265002558 2.596399441				5.550318 483.5 5.520655 483.5			7 3.286635 5 2.925776		R12B R12B	108 108	30.43317 28.77733				30.14654 28 7031	7581.101 22749.79	0		0		ES1BSG0 ES1BSG0		0) (180 180	
	60 B-065	RES1		95322.36	2	4	-0.641757616				5.338833 483.4			6.00745		R12B	108		41984.31				20031.83	0		0		ES1BSG6		34.912		73.3152	270	
	61 B-066	RES1		120626.66	3	4	1.664803843				4.640378 483.4			2 2.92681		R13B	110	24.63408					16843.5	0		0		ES1BSG0		0			180	
	62 B-067	RES1		102582.13	3	4	1.644263799				5.841966 483.3			2 4.213849		R13B	110	32.06924					14984.08	0	0	0		ES1BSG4	12.4432	0) 0		270	
	63 B-068	COM1		197668.8	1	7	0.491274513				5.607913 483.6			5.11694		C1LN	217	20.35082					155336.8	27560		85.58470648				0		10		
	64 B-069	COM1		377181.7	2	7	0.21985076				5.522305 483.5			5.298962		C1LN P12P	217		78819.09				299839.3	39335.01		86.49481187				0		14.2725		
	65 B-071 66 B-072	RES1 RES1		174193.04 105151.41	2	4 1	1.917433968 1.335404575				3.196913 484.1 4.124041 484.			4 1.25362 7 2.784622		R12B R13B	108 110			87096.5 52575.5			17223.63 14607.9	0	0	0		ES1BSG0 ES1BSG0		0		24.2	180 180	
	67 B-073	COM1		209686.4	3	4	1.682328041				3.242588 484.2			3 1.559245		C1LB	217			209686			73280.9	28841.54	1	41.06641098				0				
	68 B-074	RES3A		123154.5	2	4	2.326288011				3.246903 484.2			5 0.92232		R3A1B	205	14.76698					11508.31	0				ES3ANBS(d		11.1397	180	
	69 B-075	RES1		182105.49	3	4	3.306986815				2.310155 484.3			1 -1.0808		R13B	110			91052.5		7.919204		0	0	0	0						0	о вери
	70 B-076	RES1		201973.38	2	4	2.960234323				3.595434 483.7			0.623555		R12B	108			100986.5			17417.25	0		0		ES1BSG0		0		18.0576	180	
	71 B-077	RES1		93807.21	2	4	1.184				2.771984 483.7			5 1.581715		R12B	108			46903.5			10352.54	0				ES1BSG0		0			180	
	72 B-078 73 B-080	RES1 RES1		142683.1 132988.73	3	4 1	2.958400832 1.697607187				4.227438 483.5 4.625683 483.6			1 1.2192: 9 2.92898:		R13B R13B	110 110	15.31526 24.64492		71341.5 66494		23.09605 27.92898		0				ES1BSG0 ES1BSG0		0		21.4632	180 180	
	74 B-081	RES1		170111.2	3	4	2.247				5.561846 483.5			1 3.315331		R13B	110			85055.5			24083.75	0		-		ES1BSG0		0				
	75 B-082	RES1		108168.76	3	4	1.733335544				4.756678 483.6			7 3.004613		R13B		25.02767				28.00461		0				ES1BSG0		d				
	76 B-083 gara	RES1		18119.64	2	7	2.055742347				6.714155 483.6			4 4.645382		R12N	107	21.29076				31.22691		0	0	0	0 F	ES1NBSG	0	0) 0	-	270	
	77 B-084	COM1		385935.9	1	3	1.551941824				3.563546 483.6			7 1.995055		C1LN	217	13.97528					161787.4	13111.67		48.91099873				0) 0			
	78 B-085	RES1		119782.32	1	4	2.76246094				4.715561 483.6			9 1.957718		R11B	704	38.70403				21.87315		0		-		ES1BSG0		0			180	
	79 B-086 80 B-087	RES1 RES1		79134.86 87301.13	3	4 4	2.493467744 2.203				4.656311 483.6 4.630522 483.			2 2.159594 3 2.428763		R13B R13B	110 110	20.79797 22.14381				27.15959 27.42876		0		0		ES1BSG0 ES1BSG0		0		12.3376 11.8624	180 180	
	81 B-088	RES1		114364.04	3	4	3.047				4.60163 483.6			5 1.554576		R13B	110	17.32746					14165.63	0		0		ES1BSG0		n) (180	
	82 B-089	RES1		130352.11	3	4	2.748068846				4.586106 483.5			7 1.839229		R13B	110		24812.99				17073.6	0	0	0		ES1BSG0		d) 0		180	
	83 B-090	RES1		152496.61	3	4	2.651888757				4.562739 483.5			3 1.912342		R13B	110		29697.15			26.56171		0	0	0		ES1BSG0	27.544	0) 0	27.544	180	
	84 B-091.1	RES1		143944.43	3	4	2.761171672				4.548648 483.5			9 1.776168		R13B	110		26855.64				18626.96	0		0		ES1BSG0		0		25.9864	180	
	85 B-092	RES1	57880	149909.2	3	4	3.06460731	. 2228	40.99841	-76.4639	5.572471 483.4	752	5.705569	2.640962	2 1	R13B	110	23.20481	34786.1	74954.5	26	27.64096	20718.14	0	0	0	0 F	ES1BSG0	19.6064	0) (19.6064	180	360 Depth

State Stat	INPUT FIELD ID STRUCTURE	Occupancy/	Market		undation 1st Floor Height above	Total SF Latit	ude Longitude '	oth of Lee Flood od Lee Elev	OUPUT	Depth of Flood from	Depth of Flood in Floo Structure Expec		Bldg Depth	-	Bldg Loss Conter		1 Content	Content	ommercial nventory	Comm Inventory Depth	% Comm Inventory	Comm Inventory Debris ID	Debris_Fin	Debris from	Debris from Foundation	Debris	in Days Ma to estore R	lax Days to GridName Restore
1	TILLOS	Lonning	Value x CLR	Stories	Grade (Ft)		1100	ou lee Liev	TILLES	Ground	•	ica. Occupio	•	Dumage	yy vuide	ID	Damage	2 2033 44	Cost (\$)	-	Damage	Loss \$\$		Struc	Toundation			
1				3						5.451352									0	(0			0	0			360 Depth.tif
1				3																(0			360 Depth.tif
1				3																(,				0			360 Depth.tif
1		RES1	43790 113416.1	3		1792 40.9	99813 -76.4646	4.837 483.3667				. R13B	110	24.73991	28059.02 56				0	() 0	0 RES1BSG0		0	0	15.7696	180	360 Depth.tif
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No				2																() 0			0	-			360 Depth.tif
**************************************				1															9404.85	-	92.07899575			0	0			630 Depth.tif
The column				2																(0			0				450 Depth.tif
1				3																() 0			0				360 Depth.tif
Second S				3																() 0			0				360 Depth.tif
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C. Self C. Self C. Self Self C. Self Self C. Self Self C. Self				1						5.248427	6.049339 1		217						22847.24	:	90.09867726			0	0			630 Depth.tif
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Mary Wilson Wil			58342 151105.78	2	4 1.38601569					5.577049	4.191034 1	. R12B	108			2.5 24	33.7641	13 25509.65	0	(0	0 RES1BSG4	17.1864	0	0	17.1864		450 Depth.tif
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14 15 15 15 15 15 15 15				2	4 3.124448818															(0 RES1BSG0	17.952	0	0	17.952		360 Depth.tif
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1	120 B-129		37861 98059.99	2	4 3.114822716	1133 41.0	00146 -76.4631 2.4	03604 485.0872		2.408684	-0.70614 1	. R12B	108	15.46931	15169.05 4902	9.5 24	10.3508	39 5074.989	0	(0	0					-	0 Depth.tif
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17 5-15 18 18 18 18 18 18 18				3															0	(0			0	0			450 Depth.tif
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10 5-90 105				2															0	() 0	0	10.250	Ü	Ü	10.250		0 Depth.tif
11 1-4 12 12 13 14 13 13 13 13 13 14 14				2															0	(0			0	0			360 Depth.tif
12 12 12 12 12 13 13 13				2															0	() 0			0	0			360 Depth.tif
148 144 861 569 14000 1400				3															0	() 0			0	0			360 Depth.tif
15				3																(0			0	0	0		360 Depth.tif
10 9-46 951 957 9766.00 2 4 1389909 74.00 38991 4866.00 1867.00 1869.0				2															-	() 0			0	0			360 Depth.tif
13 14-147 14-148 15-14				2															0	() 0			0	0			360 Depth.tif
29 5-9-9-2 65.1 10.0955 20.9968 2 4 1.09600358 31.08 40.9902 76.698 1.7962 2.68841 1 1.818 10 2.50500 2.68841 1 1.818 10 2.50500 1.98841 1 1.818 1.09 2.50500 1.98841 1.09 1.		RES3A		3															0	(0			0	0			360 Depth.tif
40 \$1-502 \$853.6 \$7.906 \$16236.5 \$3 \$4 \$1,959031.5 \$2.906 \$0.99962. \$7.6666. \$4,9220.5 \$4,9220.5 \$4,9220.5 \$2.906.5				2															0	(0			0	0			360 Depth.tif
141 B-151-2 R51				3															0	() 0			0	0			360 Depth.tif
148 81-512 81-51 24223 6277757 3 4 1.7400104 1476 40.99989 7.64644 44.940074 48.14881 4.45366 27.73549 1 81.38 10 22.54781 1.7400154				3															0	(0			0	0			360 Depth.tif
144 8154 8151 7222 6273757 3 4 1954213452 1218 4909987 74-664 4-838184 483-4273 441688 248-5477 1 8138 10 2.46978 300846 63 247-6478 63 248-6478 63 248-6478 63 248-6478 63 248-6478 63 248-6478 63 248-6478 63 248-6488				2															0	() 0			0				360 Depth.tif
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147 B-157 R53A 388800 106992 3 3 184859171 1492 409889 -76.6690 4.50948 483.9312 4.5593 83.93 5.0017 1193 1.75096 483.9312 4.5593 83.93 5.0017 1193 1.75096 4.5593 83.93 1.75096 4.7593 83.93 1.75096 1.7593 83.93 1.75096 4.7593 83.93 1.75096 1.7593 83.93 1.75096				3		2872 40.9	99891 -76.4666 5.3	76001 483.3916												(0				360 Depth.tif
148 B-1542 R51				3															0	(0			0	0			360 Depth.tif
149 B-159 RESI 3968 B-102786.74 2 3 0.096164168 954 40.09996 -76.4675 5.006499 483.1289 5.0614 40.01967 150 B-160.2 COM1 12.0327 32778.383 3 4 3.611318418 31.05 40.99844 -76.4678 4.07896 483.159 3.23992 3.09295 3.0				3 3																(0				360 Depth.tif
150 B-1602 COM1 12657 327730.83 3 4 3.61314851 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 43159 372 409849 .76.4676 417586 .76.4676 417586 .76.4676 417586 .76.4676 .76.4766 .76.476 .				2																(0				450 Depth.tif
152 B-163 RESIA 5374 13914.516 3 4 2.61059422 2200 40.99843 -76.4681 50.3541 483.0356	150 B-160.2	COM1	126537 327730.83	3	4 3.611314851	3572 40.9				3.923992	0.312677 1	. C1LB	217	3.501418	11475.2 327	730 90	9.50425	55 31148.3				3062.18127 COM1NBS(6.4296	0		6.4296		540 Depth.tif
153 8-164-1 RE51 4264 14643-76 8 5 4 2.61059427 2240 40,9982 5-76.481 493849 483.0195 42915 2318556 1 R138 110 21.597.8 075920.5 2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				2																(0	0			360 Depth.tif
154 B-165 2nd R51 Se626 151841.34 2 3 8 .75 1120 40.9982 -76.4682 4.966386 483 4.966389 -3.7835 1 R12M 107 0 0 75920.5 23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				3																(0			360 Depth.tif
156 B-170 RES1 89064 230675.76 2 4 4.328300142 1991 40.9967 .76.4704 4.807072 482.5 4.770894 0.442684 1 18.28 108 19.88537 4870.75 115337.5 24 16.88537 19475.16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	154 B-165 2nd	RES1	58626 151841.34	2	3 8.75	1120 40.	.9982 -76.4682 4.9	66336 483		4.966499	-3.7835 1	R12N	107	0	0 7592	20.5 23		0 0		() 0	0						0 Depth.tif
157 B-172 COM1 95.62 246728.58 1 3 -0.447332097 30082 40.9974 -76.4681 4.637308 483 483 4.624875 507207 1 C1N 21 20.21662 4988.0.07 246728 90 78.36104 19333.6 207264.98 1 85.36103583 176923.54 COM1NBF 75.205 0 0 75.205 450 630 Depth 159 B-174 RES1 50623 131113.57 2 4 2.981 1628 40.99833 -76.4669 4.215473 483.216 4.215484 1.234487 1 R12 108 22.17424 29073.1 65555.5 24 19.6493 12877.87 0 0 0 0 0 0 RESIBSGO 14.3264 0 0 14.3264 180 360 Depth 160 B-175 RES1 50958 131981.22 2 4 3.5547136003 1528 40.99841 -76.4666 5.277303 483.2756 5.27741 1.52883 1 R12 10.000 1 RESIBSGO 13.464 180 360 Depth 161 B-176 RES1 50958 131981.22 2 4 3.5547136003 1528 40.99841 -76.4666 5.277303 483.2756 5.2741 1.52883 1 R12 10.000 1 RESIBSGO 13.464 180 360 Depth 162 B-177 RES1 3040 78759.31 2 4 3.708246256 1446 40.99842 -76.4665 5.305421 483.3047 5.30598 1.59712 1 R12 108 23.98856 18893.15 39379.5 24 22.18398 8735.942 0 0 0 0 0 0 RESIBSGO 12.7248 0 0 12.7248 180 360 Depth 164 B-179 RES1 3385 876.66 2 4 2.54545776 1104 40.9983 -76.4662 2.888048 1 R12 10 R				3															-	(17 5300	_	•	17 5200	0	0 Depth.tif
158 B-173 RE51 8802 22997.18 2 2 8 1728 40.99753 -76.4667 5.167792 483 5.165399 -2.8346 1 R.12N 107 0 0 14.998.5 23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				2 1																(360 Depth.tif 630 Depth.tif
160 B-175 RE51 50958 131981.22 2 4 3.547136003 1528 40.99841 -76.4666 8.744438 483.2439 4 3.560775186 1560 40.99847 -76.4666 5.277303 483.2756 5.277303 483.				2	2 8	1728 40.9												0 0		(0		3	· ·		0	0 Depth.tif
161 B-176 RES1 45732 118445.88 2 4 3.650775186 150 40.99847 -76.4666 5.277303 483.2756 146 40.99852 -76.4665 5.277303 483.2756 146 40.99852 -76.4665 5.30541 483.047 1528 1.99712 1 R128 108 24.13419 2858.74 59222.5 24 22.38787 13258.66 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				2																(0				360 Depth.tif
162 B-177 RES1 30409 78759.31 2 4 3.708246256 144 40.99852 76.4665 5.305421 483.3047 5.99859 15.99712 1 R12B 108 23.98856 18893.15 39379.5 24 22.18398 8735.942 0 0 0 0 RES1BSGO 12.7248 0 0 0 12.7248 180 360 Depth 163 B-178.1 ga AGR1 2160 5594.4 1 3 1.134974951 0 40.99812 76.4662 5.98099 483.2426 5.98099 483.2426 5.98099 483.2426 5.98099 483.2426 5.98099 483.2426 5.98099 5.99845 4.84346 1 ALIN 616 24.06076 1345.959 5.994 460 65.84346 3683.283 0 116 10 0 AGRISIBSGO 12.7248 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				2																								360 Depth.tif 360 Depth.tif
163 B-178.1 ga AGR1 2160 5594.4 1 3 1.134974951 0 40.99812 -76.4662 5.98093 483.2426 5.978435 4.84346 1 A1LN 616 24.06076 1345.959 5594 460 65.84346 3683.283 0 116 100 0 AGR1NBFT 0 0 0 0 0 0 30 210 Depth 164 B-179 RE51 33852 87676.68 2 4 2.45945776 1104 40.9983 -76.4662 4.88518 483.293 4 2.948986597 180 40.99887 -76.4664 4.76322 483.347 4.75838 1.809394 1 R138 110 18.85636 2196.19 5807 160 B-181.2 RE51 7877 204032.43 3 4 2.956919712 2912 40.99867 -76.4662 4.34028 483.347 4.259681 1.574179 1 R138 110 17.44567 1.574179 1 R138 110 1.57				2																								360 Depth.tif
165 B-180 RES1 44855 116174.45 3 4 2.948986597 1820 40.99857 -76.4664 4.763232 483.347 4.75838 1.809394 1 R13B 110 18.85636 21906.19 58087 26 26.04697 15129.9 0 0 0 0 0 RES1BSG0 16.016 0 0 16.016 180 360 Depth 160 B-181.2 RES1 40638 105522.42 3 4 2.685465474 1352 40.9987 -76.4661 4.28137 483.48 1.00 18.95648 1.574179 1 R13B 110 17.4507 18.85636 21906.19 58087 26 26.04697 15129.9 0 0 0 0 0 RES1BSG0 25.6256 0 0 25.6256 180 360 Depth 160 B-182 RES1 40638 1.05522.42 3 4 2.685465474 1352 40.9987 -76.4661 4.28137 483.48 1.00 17.4507 18.9568 1.809394 1 R13B 110 17.4507 18.9568 1.2913 1.00 1.00 0 0 0 RES1BSG0 25.6256 0 0 25.6256 180 360 Depth 160 B-184 gara RES1 9208 23848.72 1 7 0.048333937 0 40.9984 -76.4656 5.439146 483.3829 5.440469 5.392135 1 R11N 129 55.35281 13200.54 11924 45 60.35281 7196.469 0 0 0 0 RES1BSG0 9.2928 0 0 9.2928 180 360 Depth 160 B-184 gara RES1 9208 23848.72 1 7 0.048333937 0 40.9984 -76.4656 5.439146 483.3829 5.440469 5.392135 1 R11N 129 55.35281 13200.54 11924 45 60.35281 7196.469 0 0 0 0 0 RES1BSG0 9.2928 0 0 0 270 450 Depth 160 B-184 gara RES1 9208 23848.72 1 7 0.048333937 0 40.9984 -76.4656 5.439146 483.3829	163 B-178.1 ga	AGR1	2160 5594.4	1	3 1.134974951	0 40.9	99812 -76.4662 5.9	80993 483.2426		5.978435	4.84346 1	A1LN	616	24.06076	1345.959 5	594 460	65.8434	16 3683.283				0 AGR1NBFT	0			0	30	210 Depth.tif
166 B-181.2 RES1 7877 204032.43 3 4 2.956919712 2912 40.99867 -76.4662 4.340228 483.3722 4.29593 1.322613 1 R13B 110 15.93568 32513.88 102016 26 23.61307 24089.11 0 0 0 0 RES1BSG0 25.6256 0 0 25.6256 180 360 Depth 169 B-184 gara RES1 9208 23848.72 1 7 0.048333937 0 40.9984 -76.4656 5.439146 483.3829 5.440469 5.392135 1 R1N 129 55.35281 1320.54 11924 45 60.35281 7196.469 0 0 0 0 RES1BSG0 9.2928 0 0 0 270 450 Depth				2																(0				360 Depth.tif
167 B-182 RES1 40638 105252.42 3 4 2.685465474 1352 40.99871 -76.4661 4.281375 483.403 4.259645 1.574179 1 R13B 110 17.44507 18361.29 52626 26 24.8709 13088.56 0 0 0 0 RES1BSG0 11.8976 0 0 11.8976 180 360 Depth 1				3																(0				360 Depth.tif
169 B-184 gara RES1 9208 23848.72 1 7 0.048333937 0 40.9984 -76.4656 5.439146 483.3829 5.440469 5.392135 1 R11N 129 55.35281 13200.54 11924 45 60.35281 7196.469 0 0 0 0 RESINBSG 0 0 0 0 270 450 Depth	167 B-182	RES1	40638 105252.42	3	4 2.685465474	1352 40.9	99871 -76.4661 4.2	81375 483.403		4.259645	1.574179 1	. R13B	110	17.44507	18361.29 52	626 26	24.870	9 13088.56	0			0 RES1BSG0	11.8976		0	11.8976	180	360 Depth.tif
a <mark>n en la companya de la companya de</mark>				1																(0	0	9.2928		360 Depth.tif
1/0 07-10 1 1/14/2/ UBICATICAL USECULA TO 1/14/2/ UBICATICAL USECULA TO 1/14/2/ USECULA T	169 B-184 gara 170 B-185.1	RES1 RES1	9208 23848.72 60405 156448.95	3	7 0.048333937 4 1.704831867								129 110						0	(0	0	0 25.9776	270 180	360 Depth.tif

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INPL	FIFID ID STRUCTURE	Occupancy/	Total Coun / County Fair Assess		# of Fou	ındation	1st Floor Height above	Total SF Lati	tude Lon	Depth Depth	of Lee Flood	OUPUT Flo	ood [']		odng St			% Bldg Bl	dg Loss Cont		epth	% Contents	ontent Com	nercial	omm entory	% Comm Inventory	Comm Inventory Debris ID	Dehris Fin	Debris from	Debris from		lin Days M to	ax Days to GridName
FIELI	os Piero io Sikocioke	Zoning	Market Value x	St	tories 1	Туре	Grade (Ft)	TOTAL ST LATE	tuue Lon	Flood I	Lee Elev	FIFI DS	ound	Structure Expe (Ft)	cted? Occi		image ID	Damage	\$\$ Valu	e \$\$ Da	mage	Damage L	nss SS	(\$) D	onth	Damage	Loss \$\$	Deblis_riii	Struc	Foundation	Total I		lestore Gridinalile Struc
	171 B-186	RES1	46182 11961	1 20	2	1	2.569962627	2022 40	00000 7	C 1650 1 167	731 483.468		F t) 56331	1.896368	1 D1			25.48184 3	0470 09 E0	805.5	24 :	24.27458 14	1517 52	0	age ID	0	0 RES1BSG0	24.9216	0	0	24.9216	180	360 Depth.tif
	171 B-180 172 B-187.2	RES1	76558 19828		2	4	3.783947409				217 483.5054			0.290507				19.58101 3				16.58101 16		0	0	0	0 RES1BSG0			0	27.7376	180	360 Depth.tif
	173 B-188	RES1	57211 14817		2	4	2.312567093				582 483.5369			1.863409	1 R1			25.31705 3				24.04386 17		0	0	0	0 RES1BSG0			0		180	360 Depth.tif
	174 B-189 175 B-190	RES1 RES1	36923 9563 48493 12559		2	4	2.789650096 2.962222389				921 483.2703		25905 51717	4.4694 4.189494	1 R1		108 110	36.347 3 31.94747 4			24 26 :	34.8776 16 29.18949 18		0	0	0	0 RES1BSG4 0 RES1BSG4	10.7008 22.528		0	10.7008 22.528	270 270	450 Depth.tif 450 Depth.tif
	176 B-191	COM1	4224 1094		1	7	0.45				206 483.3025			4.853998			217	19.708 2				76.53998 83		0	1 8	3.68598623	0 COM1NBS			0	0	450	630 Depth.tif
	177 B-192	COM1	47868 12397		2	7	8.67				724 483.2567			-3.07064			217	0			90	0		528.16	1	0	0		_			0	0 Depth.tif
	178 B-193 179 B-194	RES1 RES1	45483 11780 41423 10728		3	4	1.468338844 1.560748295			6.4657 6.250 6.4658 6.160				4.791552 4.60089	1 R1			34.95776 4 34.00445 3				29.79155 17 29.60089 15		0	0	0	0 RES1BSG4 0 RES1BSG4	15.2064 13.0592		0	15.2064 13.0592	270 270	450 Depth.tif 450 Depth.tif
	180 B-195	RES1	65177 16880		3	4	3.092921348				694 483.1442			3.045978	1 R1			25.27587 4				28.04598 23		0	0	0	0 RES1BSG0	11.264		0	11.264	180	360 Depth.tif
	181 B-196	RES1	40446 10475		3	4	3.412781968				471 483.1152			2.700919	1 R1			23.50459 2				27.70092 14		0	0	0	0 RES1BSG0	12.32		0		180	360 Depth.tif
	182 B-197 183 B-198	RES1 RES1	37619 9743 42538 11017		3	4	2.494278057 1.475444638				924 483.1502 869 483.0853			2.668321 4.679705	1 R1		110 108	23.3416 2 37.39852 4				27.66832 13 35.71882 19		0	0	0	0 RES1BSG0 0 RES1BSG4	12.9976 15.1008		0	12.9976 15.1008	180 270	360 Depth.tif 450 Depth.tif
	184 B-199	RES1	38498 9970		3	4	3.244619221				881 483.0173			3.119522				25.71713 2				28.11952 14		0	0	0	0 RES1BSG0	14.3616		0	14.3616	180	360 Depth.tif
	185 B-200	RES1	38498 9970		3	4	3.776608371				067 483.0125			2.858534	1 R1			24.29267 2				27.85853 13		0	0	0	0 RES1BSG0			0	14.3616	180	360 Depth.tif
	186 B-201 187 B-202	RES1 RES1	47787 12376 69988 18126		2	4	2.892061103 2.703			6.4665 6.0320 6.4669 5.055	725 483.0563			3.140384 2.354368	1 R1		110 108	25.8423 27.0631 4				28.14038 2 26.41747 2	17414.4 3943.21	0	0	0	0 RES1BSG0 0 RES1BSG0			0	16.0688 22.3168	180 180	360 Depth.tif 360 Depth.tif
	188 B-204	RES1	15525 4020		1	3	1.204193518			6.4674 6.0010				4.797085	1 R1			51.78251 2				56.78251 1:		0	0	0	0 RES1NBFT4		0	0	0	270	450 Depth.tif
	189 B-205	RES1	46078 11934		2	4	3.120311108			6.4667 7.018				3.901448	1 R1			33.50724 3				32.60579		0	0	0	0 RES1BSG0			0	13.7984	180	360 Depth.tif
	190 B-206 191 B-207	RES1 RES1	28726 7440 89494 23178		2	4	2.512892985 2.472820359	680 40 1966 40		6.4664 7.272 6.4661 6.2420				4.861436 3.869513	1 R1			38.30718 2 33.34757 7	3500.54 7295.99 115			36.44574 13 32.47805 37		0	0	0	0 RES1BSG4 0 RES1BSG0	5.984 17.3008		0	5.984 17.3008	270 180	450 Depth.tif 360 Depth.tif
	192 B-208	RES1	30518 7904		2	4	2.492533512			6.4664 7.000				4.509984	1 R1			36.54992 2				35.03993 13		0	0	0	0 RES1BSG4	9.3016		0		270	450 Depth.tif
	193 B-209	RES1	43520 1127		3	4	4.193232571			6.4663 6.9010				2.730517	1 R1			23.65258 2				27.73052 15		0	0	0	0 RES1BSG0	13.112		0	13.112	180	360 Depth.tif
	194 B-210 195 B-211	RES1 RES1	48092 12455 37000 9	8.28 5830	2	4	1.529095588 1.403707817			76.466 6.203 6.4658 7.468	743 483.0367 663 483			4.697233 6.021129	1 R1			37.48616 4 38.06339 3				35.78893 22 32.06339 15		0	0	0	0 RES1BSG4 0 RES1BSG6	13.9832 12.6072		0 30.9		270 270	450 Depth.tif 450 Depth.tif
	196 B-212	RES1	52573 13616		1	4	2.472205325				518 483.0307			3.569233			704	49.4154 6				26.13847 17		0	0	0	0 RES1BSG0			0		180	360 Depth.tif
	197 B-213.2	RES1	58040 1503		3	4	2.414269905			6.4658 6.491				3.719925				29.31955 4				28.71993 2:		0	0	0	0 RES1BSG0	25.6344		0	25.6344	180	360 Depth.tif
	198 B-214 199 B-215	RES1 RES1	40614 10519 54524 14121		2	4	1.975373701 2.591666563				774 483.1029			4.986385 4.194172	1 R1			38.93192 4 34.97086				36.94554 19 33.77669 23		0	0	0	0 RES1BSG4 0 RES1BSG4	12.7072 20.9088		0	12.7072 20.9088	270 270	450 Depth.tif 450 Depth.tif
	200 B-216	COM1	91573 23717		1	0	0.746		.99461 -7		4.5 482.5	0.76	4.5	3.754			217	17.508 4			90	65.048 15		376.58	1	73.294	12735.9905 COM1NBF			0	4.5396	360	540 Depth.tif
	201 B-217	RES1	47835 12389		2	7	0.076575045	896 40	.99525 -70	6.4725 6.443		6.43	34193	6.357618	1 R1			24.71524	30620.2			40.78809 25	5266.59	0	0	0	0 RES1NBSG	6.0928	0	0	6.0928	270	450 Depth.tif
	202 B-219	COM1	42240 1094		2	7	8.125			6.4728 6.477			80997	-1.644			217	0			90	0	0	6063.2	1	0	0	0.00			0.00	0	0 Depth.tif
	203 B-220.1 f- 204 B-220.10 f	COM1 COM1		84.2 54.4	1	7	1.046628784 0.579	4488 40	.99588 -7(.99568 -7(266 482.5 7.5 482.5	8.83	7.5	7.845365 6.921	1 C1		217 217	29.38146 2 25.763 1			90 : 90	86.69073 85 84.842 35		645.76 922.32	1 9		2456.46552 COM1NBS(28399.6771 COM1NBS(0	0.96 11.22	450 450	630 Depth.tif 630 Depth.tif
	205 B-220.11 f	COM1	74880 1939		2	7	0.435900251			6.4676 7.998	811 483		00573	7.564673	1 C1			28.25869 5			90	86.12935 16		43312	1 9		132656.284 COM1NBS			0	52	450	630 Depth.tif
	206 B-220.12 f	COM1		90.9	1	7	0.765958168			6.4664 9.5110				8.67506	1 C1			32.70024 2				87.67506 79		13780			12908.4233 COM1NBS			0	8.6	540	720 Depth.tif
	207 B-220.13 f 208 B-220.14 f	COM1 COM1	45360 1174 0	82.4	2	7	0.879166505 0.060227223			6.4673 7.9933 76.467 7.0394				7.110562 6.963357	1 C1			26.44225 3 25.89007	1064.88 1. O			85.22112 10 84.92671	0 0119.5	86814 0		1.92671429	79964.8632 COM1NBS 0 COM1NBS			0	31.5 0	450 450	630 Depth.tif 630 Depth.tif
	209 B-220.15 f	COM1	15840 410	25.6	2	7	3.060526308			6.4665 7.004				3.944591	1 C1			17.88918 7	339.037	11025		67.33509 2	7624.22	15158			11427.6923 COM1NBS		0	0	3.96	360	540 Depth.tif
	210 B-220.16 f	COM1		09.5	1	7	-0.333753762				212 483.2594			6.600332	1 C1		217	24.801 1				84.20066 44		3927.3			3581.72367 COM1NBS		0	0	1.425	450	630 Depth.tif
	211 B-220.17 f 212 B-220.18 f	COM1 COM1		.88.8 18.4	1	7	0.391595992 -0.012273915			6.4629 6.4379 6.4631 6.1683	976 483.2974			6.018339 6.18015	1 C1			23.05502 2 23.54045 3			90 : 90	83.03668 92 83.3603 12		8268 11024			7444.23254 COM1NBS 9961.31951 COM1NBS		0	0	3 4	450 450	630 Depth.tif 630 Depth.tif
	213 B-220.19 f	COM1		16.1	1	7	0.511223586	12035 40		76.466 9.698				9.190856				34.76342 3				88.19086 7		921.15			78104.1411 COM1NBS		0	0	51.7505	540	720 Depth.tif
	214 B-220.2 f-	COM1	0	0	1	7	0.779757065			6.4695 7.1334				6.385937	1 C1			24.15781	0			83.77187	0	0	1 9	0.77187339	0 COM1NBS		-	0	•	450	630 Depth.tif
	215 B-220.20 f 216 B-220.21 f	COM1 COM1		48.9 81.5	1	7	-0.083859572 1.709097138			6.4658 10.460 6.4652 11.65				10.54805 9.968805	1 C1		217 217	40.1922 2 37.87522	0517.31 2795.57			89.54805 45 88.96881 65		4490.4 9686.4	1 1 9		61265.88 COM1NBS 37689.6999 COM1NBS			0		540 540	720 Depth.tif 720 Depth.tif
	217 B-220.22 f	COM1		57.4	1	7	0.204266374			6.4657 11.29				11.1559				42.77952 8				90.1559 18		19292			18357.4772 COM1NBS			0	12.04	540	720 Depth.tif
	218 B-220.23 f	COM1		62.8	1	7	0.651392072			6.4666 12.46				11.80629	1 C1			46.03147 1						0710.4			48583.7546 COM1NBS			0	31.648	540	720 Depth.tif
	219 B-220.24 f 220 B-220.25 f	COM1 COM1		.61.6	2	7	0.555361974 4.384206576			6.4673 10.503 6.4675 11.49				9.946991 7.112628	1 C1			37.78796 2 26.45051 4				88.94699 47 85.22526 13		3927.3 852.47			3728.85317 COM1NBS(29340.1473 COM1NBS(0	2.451 11.5575	540 450	720 Depth.tif 630 Depth.tif
	221 B-220.26 f	COM1	0	0	1	7	1.002981384			6.4679 10.48				9.484301				35.93721	0		90	88.4843	0	0		4.48430137	0 COM1NBS			0	0	540	720 Depth.tif
	222 B-220.27 f	COM1	0	0	1	7	-0.537200791			6.4683 9.625				10.18384				38.73537	0	-		89.18384	0	0	1	95	0 COM1NBS		·	0	0	540	720 Depth.tif
	223 B-220.28 f 224 B-220.29 f	COM1 COM1	0	0	1	7	0.520750741			6.4671 11.50 6.4669 11.50				10.98001 11.45599	1 C1		217 217	41.92005 44.27993	0	0	90 i	89.98001 90.45599	0	0	1 1 9	95 95.45598569	0 COM1NBS	. 0	0	0	0	540 540	720 Depth.tif 720 Depth.tif
	224 B-220.291 225 B-220.3 f-	COM1	15840 410	25.6	2	4	2.946694702			6.4696 4.239					1 C1			10.66861 4	376.798	11025	90	31.33956 12	2857.05	15158			5609.52117 COM1NBS	3.96	0	0	3.96	360	540 Depth.tif
	226 B-220.30 f	COM1	12920 334	62.8	1	7	0.275426119	7360 40	.99303 -7	6.4666 11.82	457 482.5		93845	11.66303	1 C1	LN 2	217	45.31513 1	5163.35	3462	90	90.66303 30		0710.4		95.6630266	48511.1034 COM1NBS	31.648	0	0	31.648	540	720 Depth.tif
	227 B-220.31 f 228 B-220.32 f	COM1 COM1	0 14130 365	0 96.7	1	7	0.289 1.146363289		.99296 -71	6.4668 1 6.4666 11.68	11.5 482.5 783 482.5	11 '		11.211 10.62826	1 C1		217 217	43.055 40.51306 1	0 1826 16		90 90 :	90.211 89.62826 32	0 2800.36 2	0 043.25	1	95.211	0 COM1NBS0 25691.0875 COM1NBS0			0	0 16.8775	540 540	720 Depth.tif 720 Depth.tif
	228 B-220.321 229 B-220.33 f	COM1		96.7	1	7	0.355330734		.99346 -71 .99327 -71						1 C1			41.04241 1				89.7606 32		043.25 043.25	1		25691.0875 COM1NBS			0		540	720 Depth.tif
	230 B-220.34 f	COM1	12920 334	62.8	_	7	-0.149997614	7360 40	.99332 -70	6.4662 10.970	037 482.5	10.9	96638	11.11638	1 C1	LN 2	217	42.58188 1	1248.75		90	90.11638 30	0154.74	0710.4	1 9	5.11637678	48233.8951 COM1NBS	31.648		0	31.648	540	720 Depth.tif
	231 B-220.35 f 232 B-220.36 f	COM1 COM1	12920 334 0	62.8 0	1	7 7	0.172889674 -0.198528649		.99339 - .99352 -7	76.466 10.8 6.4657 10.523				10.66464 10.72142	1 C1			40.65854 1 40.88569	3605.16 :			89.66464 30 89.72142	0003.58 n	0710.4 0	1	95 95	48174.88 COM1NBS 0 COM1NBS			0	31.648 0	540 540	720 Depth.tif 720 Depth.tif
	232 B-220.361 233 B-220.37 f	COM1	0	0	1	7	-0.198328649			6.4657 10.52. 6.4653 10.50!					1 C1			40.88569	0			89.59771	0	0	1	95 95	0 COMINBS			0	0	540	720 Depth.tif
	234 B-220.38 f	COM1		3310	1	7	0.683377758	4000 4	0.9935 -70	6.4648 11.48	435 482.5	11.4	48428	10.8009	1 C1	LN 2	217	41.20361 9			90	89.8009 20		27560	1	95	26182 COM1NBS	17.2		0		540	720 Depth.tif
	235 B-220.39 f 236 B-220.4 f-	COM1 COM1		3310	1	7	0.491658276 0.483842602			6.4645 11.13				10.65238	1 C1		217	40.6095 9				89.65238 20		27560 776.44	1	95	26182 COM1NBS			0		540 450	720 Depth.tif
	236 B-220.4 f- 237 B-220.40 f	COM1 COM1		61.5 0360	_	7	0.483842602			6.4693 5.5013 6.4643 10.948					1 C1			20.05441 2 39.86131 4				78.09068 98 89.46533 92		62010	1 8		21082.4422 COM1NBS 58909.5 COM1NBS			0	8.99 38.7	450 540	630 Depth.tif 720 Depth.tif
	238 B-220.41 f	COM1	16200 4	1958	1	7	0.399099376	7200 40	.99403 -	76.464 11.53	354 482.5	11.5	52897	11.12987	1 C1	LN 2	217	42.64934 1	7894.81	1958	90	90.12987 37	7816.69	49608		5.12986753	47192.0247 COM1NBS	30.96	0	0	30.96	540	720 Depth.tif
	239 B-220.42 f	COM1		65.5	1	7	0.326451261			6.4643 11.69				11.41536	1 C1			44.07681 2				90.41536		895.01			63828.1156 COM1NBS			0	41.7487	540	720 Depth.tif
	240 B-220.43 f 241 B-220.44 f	COM1 COM1		0360 64.9	1	7 7	1.000935475 0.785331856			6.4641 12.47! 6.4642 13.48				11.47612 12.69042	1 C1			44.38061 4 49.76167 2				90.47612 93 91.69042 50		62010 8268			59204.7432 COM1NBS 7994.36377 COM1NBS			30	38.7 92.52	540 720	720 Depth.tif 900 Depth.tif
	242 B-220.45 f	COM1		0360	1	7	1.101		.99465 -7		12.5 482.5				1 C1		217	43.995 4			90	90.399 93		62010	1		59156.9199 COM1NBS			0		540	720 Depth.tif
	243 B-220.46 f	COM1		1282	1	7	1.046		0.9946 -7		12.5 482.5			11.454	1 C1		217	44.27 2			90	90.454 46		60632	1		57875.6693 COM1NBS			0		540	720 Depth.tif
	244 B-220.47 f 245 B-220.48 f	COM1 COM1		57.4 .96.3	1	/ 7	0.136426806 0.371994799			6.4642 12.494 6.4637 11.43				12.40044 11.07317	1 C1			48.60177 9 42.36583				91.40044 18 90.07317 19		19292 6398.2			18597.5733 COM1NBS 15590.2879 COM1NBS			70 0		720 540	900 Depth.tif 720 Depth.tif
	246 B-220.49 f	COM1	79920 2069		1	7	0.190965117			6.4635 12.49				12.69124	1 C1			49.76498 1				91.69124 18		152958			147896.994 COM1NBS			-		720	900 Depth.tif
	247 B-220.5 f-	COM1	4720 122	24.8	1	4	2.305400264	1312 40	.99546 -7	6.4689 6.385	321 482.5	6.3	74236	4.068835	1 C1	LB 2	217	18.13767 2	217.149	12224	90	68.68835 83		039.68		6.61951829	6926.15927 COM1NBS	3.28	0	0	3.28	450	630 Depth.tif
	248 B-220.50 f 249 B-220.51 f	COM1 COM1	0	-	1	7	1.079871265 -3.710734786			76.463 11.53 6.4625 7.404				10.30608 11.29661	1 C1		217 217	39.2243 43.48303	0			89.30608 90.29661	0	0	1	95 95.29660696	0 COM1NBS			0	0	540 540	720 Depth.tif 720 Depth.tif
	250 B-220.52 f	COM1	0		_	7	1.340414172			6.4624 9.694					1 C1			30.82724	0			87.20681	0	0		3.20680892	0 COMINBS			0	-	540	720 Depth.tif
	251 B-220.53 f	COM1		.21.2	1	7	0.688963401	1300 40	.99601 -7	6.4621 7.515	618 482.5	7.5:	18397	6.829433	1 C1	LN 2	217	25.4883 3			90	84.65887	10261.5	8957	1 9	1.65886691	8209.88471 COM1NBS	3.25		0	3.25	450	630 Depth.tif
	252 B-220.54 f	COM1		21.8	-	7 7	0.855841804			6.4619 7.6414				6.811586	1 C1			25.43476 1				84.62317 66		5787.6 13780			5302.78273 COM1NBS			0	2.1 5	450 450	630 Depth.tif
	253 B-220.6 f- 254 B-220.7 f-	COM1 COM1	3510 90 0	90.9	-	7	-0.000465869 2.707847961			6.4691 6.1169 6.4677 11.483				6.132284 8.776078	1 C1			23.39685 2 33.10431	0			83.26457 75 87.77608	0	0		3.77607786	12438.4575 COM1NBS(0 COM1NBS(0	0	540	630 Depth.tif 720 Depth.tif
	255 B-220.8 f-	COM1	74880 1939	39.2	1	7	-0.044	20800 40			6.5 482.5			6.544	1 C1		217		7771.05 19		90	84.088 16	53079.4	43312	1		130540.035 COM1NBS		0	0	52	450	630 Depth.tif

			Total	otal									Depth of	Depth of			Bldg				Content	s .			Comm							N	1in Days N	lax Davs
INPUT FIELDS	FIELD ID STRUCTURE	ID Occupancy/	County Fair Asse	unty essed		Foundation	1st Floor n Height above	Total SF	Latitude	Longitude	epth of Lee F		from	Flood in	Flooding	Struc	Depth	-	Bldg Loss		Depth	Content	Content	Commercial Inventory	Inventory	% Comm Inventory	Comm Inventory	y Debris ID	Debris_Fin	from	Debris from	Debris	to	to GridNam
FIELDS		Zoning	Market Value	e x CLR	Stories	Туре	Grade (Ft)			'	lood Lee Ele	lev FIELDS	Ground	(Ft)	Expected?	Occup ID	Damage ID	Damage	\$\$	Value \$\$	Damage ID	Damage	Loss \$\$	Cost (\$)	Depth Damage ID	Damage	Loss \$\$			Struc	Foundation	Total I	Restore I Struc	Restore Struc
	256 B-220.9 f-	COM1		(\$) 93939.2	1	7	-0.273070724	20800	40.99596	-76.4681	6.761898 4	482.5	(Ft) 6.805468	3 7.078538	1	C1LN	217	26.31415	51033.41	193939	90	85.1570	8 165152.8	143312		92.07853833	3 131959.59	95 COM1NBS(52	0	0	52	450	630 Depth.tif
	257 B-221	RES1	259279 671		2	3	-4.135752118			-76.4737		482.5		10.88183	1	R12N	107		261103.9			59.7636		0) 0		0 RES1NBFT8		20.332	37.536		360	720 Depth.tif
	258 B-226	RES1		3447.06	2	4	2.222849221				-13.4344 488.		-13.4466		0	R12B	0	0		116723.5			0 0	0		0		0					0	0 Depth.tif
	259 B-227.1 260 B-228	RES1 RES1		3246.31	3	4	3.510460719 2.399823175				0.604887 484.		0.613711		1	R13B R13B	110 110	3.309752	8547.301 10497.67				1 6722.79 4 5044.797	0) 0	•	0					0	0 Depth.tif
	260 B-228 261 B-229	RES1	38113 98 51093 132	3712.67 2330.87	3	4	3.222861823				1.721863 484 2.400492 484.			-0.68268 -0.83579	1	R13B	110		13667.61				5 6053.767	0) 0		0					0	0 Depth.tif 0 Depth.tif
	262 B-230	RES1		2128.89	3	4	2.714607571				2.817971 484.			0.102373	1	R13B	110		11243.99			15.7166		0) () 0)	0 RES1BSG0	18.7704	0	0	18.7704	180	360 Depth.tif
	263 B-231	RES1	45226 117	7135.34	3	4	2.479113127	1920	41.00117	-76.4632	2.840127 484.	1.8251	2.840323	0.361209	1	R13B	110	12.72242	14902.41	58567.5	26	17.5284	7 10265.98	0) () 0)	0 RES1BSG0	16.896	0	0	16.896	180	360 Depth.tif
	264 B-232	RES1		9917.02	3	4	2.445362348				1.179568 484.			-1.38434	1	R13B	110	8.462647				7.61566		0) () 0		0					0	0 Depth.tif
	265 B-233	RES1		5604.67	2	4	-0.405576106				1.413624 484. 2.041874 484		1.393914		1	R12B	108		23898.56				3 11279.56	0) () 0		0 RES1BSG0	17.8464	0	0	17.8464	180	360 Depth.tif
	266 B-234 267 B-235	RES1 RES1		5322.35 55345.7	3	4	2.529137255 2.353497069				2.041874 484. 2.405813 484		2.051697	7 -0.47744 9 0.021192	1	R13B R13B	110 110		11632.94 7869.096				1 6139.175 4 4949.342	0) () 0		0 RES1BSG0	9.3632	0	0	9.3632	180	0 Depth.tif 360 Depth.tif
	268 B-236	RES1		5296.49	3	4	-0.102048234				2.227778 484.			2.343841	1	R13B	110		14181.77				4 8927.217	0) () 0)	0 RES1BSG0	9.3632	0	0	9.3632	180	360 Depth.tif
	269 B-237	RES1		402.49	2	4	0.4584605	1767			2.530892 483.			2.071251	1	R12B	108		66950.45		24	25.28	5 32289.2	0) (0)	0 RES1BSG0	15.5496	0	0	15.5496	180	360 Depth.tif
	270 B-238	RES1		3065.16	3	4	2.525013673				2.973303 483.			0.44882	1	R13B	110		13937.84				4 9802.437	0) () 0)	0 RES1BSG0		0	0	14.6696	180	360 Depth.tif
	271 B-239	RES1		0476.46	2	4	2.169556754				2.992277 483.			0.816872	1	R12B	108		20731.96				4 8858.84	0) (0)	0 RES1BSG0	12.9184	0	0	12.9184	180	360 Depth.tif
	272 B-240 273 B-241	RES1 RES1		2058.96 L512.37	2	4	4.65 1.786196956				2.152221 484. 3.023516 484.			2.45285 1.239594	1	R12B R13B	108 110		5697.088 29564.79				3 2805.142 7 22213.45	0) () 0		0 RES1BSG0	18.1368	0	0	18.1368	180	0 Depth.tif 360 Depth.tif
	274 B-242	RES1		9041.56	3	4	2.19386437				3.122255 484.			0.930836	1	R13B	110		19273.41				5 14957.93	0) () 0		0 RES1BSG0	18.4976	0	0	18.4976	180	360 Depth.tif
	275 B-243	RES1		1397.74	2	4	1.468167108				3.125233 484.			1.672452	1	R12B	108		20561.02				6 9582.082	0) () 0		0 RES1BSG0		0	0	10.2432	180	360 Depth.tif
	276 B-244	RES1	35164 91	L074.76	3	4	3.07864005	2792	41.00056	-76.4637	2.342564 484.	1.3424	2.339351	-0.73929	1	R13B	110	10.52142	9582.279	45537	26	9.82497	3 4473.998	0) () 0)	0					0	0 Depth.tif
	277 B-245	RES1		7282.97	2	4	1.641391222				2.291692 484.			0.688095	1	R12B	108	20.37619					9 10189.57	0) () 0		0 RES1BSG0		0	0	16.5792	180	360 Depth.tif
	278 B-246	RES1		1079.12	2	4	1.65843755				2.347307 484. 2.422709 494			0.611373	1	R12B	108	20.22275 17.59078					5 11546.04 5 5845.373	0) () 0	•	0 RES1BSG0	15.5408	0	0	15.5408	180	360 Depth.tif
	279 B-247 280 B-248	RES1 RES1	32839 85 55508 143	5053.01 8765.72	1	4	2.708016919 4.202604424				2.422798 484. 0.97608 484.			3 -0.28184 -3.76046		R12B R11B	108 704	17.59078		71882.5			0 0	0) () 0)	0					0	0 Depth.tif 0 Depth.tif
	281 B-249	RES1		3945.73	2	4	2.181714474				1.552042 484.		1.553687		1	R12B	108	-	22036.49				8 7625.15	0) () 0	,)	0					0	0 Depth.tif
	282 B-250	RES1		5941.07	3	4	2.643789217				2.008879 484.		2.036922		1	R13B	110		14770.82				3 7361.901	0) () 0)	0					0	0 Depth.tif
	283 B-251	RES1		753.62	2	3	1.480765473				1.656456 484.		1.656617		1	R12N	107	11.17585					4 3016.75	0	-) 0		O RES1NBFT(0	0	9.84	180	360 Depth.tif
	284 B-252	COM1		74825.1	1	7	1.284288009				1.450435 484.		1.455698		1	C1LN	217	2.371281					3 4574.683	7516.99		8.628073335		41 COM1NBS(1.9638	0	0	1.9638	360	540 Depth.tif
	285 B-253	RES1		0147.55	3	4	2.236057201				2.162766 484.	34.515	2.18029	-0.05577 -0.21582	1	R13B	110		9528.248 9271.698			14.6096	3 5854.59 8 5405.626	0) 0)	0					0	0 Depth.tif
	286 B-254 287 B-255	RES1 RES1		0147.55 7645.58	2	4	1.841862726 2.500409618			-76.4633 -76.4673		33.211	4.195379		1	R13B R12B	110 108	24.47485					9 12306.4	0) 0)	0 RES1BSG0	14.2032	0	0	14.2032	180	0 Depth.tif 360 Depth.tif
	288 B-256	RES3A		161616	3	4	2.877892959				4.04278	483		1.183705	1	R3A3B	205		25726.89				2 15798.87	0) () 0		O RESIDIO		0		13.2348	180	360 Depth.tif
	289 B-257.3	RES1		57497.9	3	4	3.279334384			-76.4679		483		0.720666	1	R13B	110		21169.69				6 15784.87	0) () 0		0 RES1BSG0		0	0		180	360 Depth.tif
	290 B-258	RES1		1053.25	3	4	3.047542869	1443	40.99788	-76.468	4.001942	483		0.956811	1	R13B	110		14477.54				8 11288.54	0) () 0		0 RES1BSG0	12.6984	0	0	12.6984	180	360 Depth.tif
	291 B-259	RES1		L509.84	3	4	2.299531023			-76.4678		483		1.735401	1	R13B	110		24213.97				7 16883.79	0) (0)	0 RES1BSG0	15.18	0	0	15.18	180	360 Depth.tif
	292 B-260	RES1		7197.46	3	4	3.057168666				4.031916 483.			0.979346	1	R13B	110		21942.65				2 17178.03	0) (0)	0 RES1BSG0	26.8928	0	0	26.8928	180	360 Depth.tif
	293 B-260.1 294 B-262	RES1 RES1		7068.01 96658.8	3	4	2.695801041 2.629263679			-76.4677 -76.4676	3.041378 4.062726 483.	483		1.348223 1.435225		R13B R13B	110 110	16.61135	17226.53 16056.2		26 26		1 12709.57 3 11684.08	0) () 0)	0 RES1BSG0 0 RES1BSG0	14.6432 12.32	0	0	14.6432 12.32	180 180	360 Depth.tif 360 Depth.tif
	295 B-263	RES1		11162.8	2	4	3.063828177			-76.4674		33.088		1.268902	1	R12B	108	22.34451					1 11050.79	0) () 0)	0 RES1BSG0		0	0	13.5168	180	360 Depth.tif
	296 B-264	RES1	61418 159	9072.62	3	4	2.831573696	2882	40.99823	-76.4672	4.167974 483.	3.1442	4.176419	1.344846	1	R13B	110	16.06907	25561.4	79536	26	23.7242	3 18869.3	0) () 0)	0 RES1BSG0	25.3616	0	0	25.3616	180	360 Depth.tif
	297 B-270	AGR1		5050.5	1	3	3.347517541			-76.4647		33.516		2.098751	1	A1LN	616		575.4478				7 2246.304	0	116	52.46878736	5	0 AGR1NBFT	0	0	0	0	30	210 Depth.tif
	298 h-001 buil	RES1	144712 374		1	4	-0.853782812		40.99564			482.5		11.62667	1	R11B	704		303591.2				9 73086.78	0) (0)	0 RES1BSG8	25.5102	80.032	62.525	168.0672	360	720 Depth.tif
	299 h-002 buil 300 h-003 shed	RES1 AGR1	47011 121 3650	9453.5	0	0	-12.98790097 0.862733919			-76.477 -76.4627	-8.11361 4 5.873619 487.	482.5		5.216225 5.005382	0	R12B A1LN	0 616	0 25.02691	2265 704		0 460		0 0 6 6238.98	0		,		0 0 AGR1NBFT	0	0	0	0	30	0 Depth.tif 210 Depth.tif
	301 h-004	RES3A		19261.8	1	7	1.764422455				3.881852 486.			1.954448	1	R3A1N	204	24.59003					3 8027.087	0) 100		0 RES3ANBS		0	0	0	180	360 Depth.tif
	302 h-005	RES1		5845.53	3	3	7.244547816				-5.85283 483.			-13.2136		R13N	0	0		52922.5			0 0	0) (0		0					0	0 Depth.tif
	303 h-006	RES1	79470 20	5827.3	2	4	1.67338565	1604	41.00114	-76.4671	1.941953 483.	3.4849	1.956982	0.283597	1	R12B	108	19.56719	40274.57	102913.5	24	16.5671	9 17049.88	0) () 0)	0 RES1BSG0	14.1152	0	0	14.1152	180	360 Depth.tif
	304 h-007	RES1		2134.08	2	4	1.399141502				1.102888 483.			-0.55981	1	R12B	108		13306.51		24		6 4731.559	0) (0		0		_	_		0	0 Depth.tif
	305 h-009	RES1		33967.8	2	3	2.077167295				2.715341 484.			0.566424	1	R12N	107		9711.979				2 4072.094	0) (0		O RESINBETO		0	0	4.592	180	360 Depth.tif
	306 h-010 307 h-011 2nd	RES1 RES1		9629.56 5415.27	3	3	0.577821185 7.11				2.905187 485. 3.913006 485.		3.930389	2.41695 -3.17961	1	R11B R13N	704 109	41.91865	29187.54 0				5 8094.667 0 0	0) 0		0 RES1BSG0	6.2304	0	0	6.2304	180	360 Depth.tif 0 Depth.tif
	308 h-012	RES1		0678.49	1	4	2.91370146				0.23016 486.		0.226869		1	R11B	704	4.384345					3 1561.857	0) () 0	•	0					0	0 Depth.tif
	309 h-013.1	RES1		3227.07	2	4	2.552919448	1072			4.352333 486.			1.800763	1	R12B	108	25.00382	18309.54		24	23.6053		0) () 0)	0 RES1BSG0	9.4336	0	0	9.4336	180	360 Depth.tif
	310 h-014.1	RES1		334.54	2	4	2.598521548				4.461299 486.			1.86017		R12B	108	25.30085					9 10609.44	0) (0		0 RES1BSG0		0		12.1792	180	360 Depth.tif
	311 h-016.1	RES1	39333 101		3	4	3.548573168				5.546585 488.			1.998533	1	R13B	110		20365.43				7 13748.98	0		0		0 RES1BSG0		0		18.1632	180	360 Depth.tif
	312 h-017	RES1		819.63	3	4	2.605442156				5.078743 488. 5.225078 488			2.596607 -0.58145	1	R13B P13N	110	22.98304					1 14601.23	0) 0		0 RES1BSG0	15.6288	0	0	15.6288	180	360 Depth.tif
	313 h-018 2nd 314 h-019	RES1 RES1		7624.86 91116.2	3 2	4	2.583018333				5.325978 488. 3.665962 487.			1.07604		R13N R12B	109 108	2.092733 21.3802	19480.78				7 1576.598 8 8442.935	0) 0		0 RES1BSG0	12.7072	0	0	12.7072	180	0 Depth.tif 360 Depth.tif
	315 h-020	RES1		59570	2	4	1.016604549				2.732155 487.			1.67158		R12B	108	24.3579					6 6761.511	0) 0		0 RES1BSG0	10.56	0	0	10.56	180	360 Depth.tif
	316 h-021	RES1		59570	2	4	1.34021794				2.850475 487.			1.559398		R12B	108	23.79699					8 6527.616	0) (0		0 RES1BSG0		0	0	10.56	180	360 Depth.tif
	317 h-022.1	COM1		79901.5	1	4	3.325253554				4.377637 488.			1.095872		C1LB	217	9.479359					5 21999.9	7992.4		32.72569344		32 COM1NBS(2.088	0	0	2.088	360	540 Depth.tif
	318 h-023	RES1		L5488.1	3	4	2.854			-76.4641		489.1		-3.754		R13B	0	0	0				0 0	0		0		0					0	0 Depth.tif
	319 h-024	RES1	90854 235		2	4	-2.882416912				-1.57547 483.			1.331303		R12B	0	0		117655.5			0 0	0) 0		0					0	0 Depth.tif
	320 h-025 321 h-026	RES1 RES1	57873 149 58596 151		2	4	-0.294588543			-76.4679 -76.4746	-1.51054 483. 4.870486	482.5		9.66185 5.07518		R11B R12B	0 108	0 39 3759		74945.5 75881.5			0 0 9 28361.39	0) 0		0 0 RES1BSG4	21.296	0	0	21.296	0 270	0 Depth.tif 450 Depth.tif
	322 h-028	RES1	57055 147		3	3	503.718		40.99755			. 32.3		5.07518		R13N	0	0	0				0 0	0) 0		0	21.230	J	Ü	21.230	0	0 Depth.tif
	323 h-029	RES1		635.77	2	4	2.69168189				6.49645 484.	1.8368		3.808969		R12B	108		24993.47			32.2358	8 12190.8	0) () 0		0 RES1BSG0	6.8904	0	0	6.8904	180	360 Depth.tif
	324 h-031	RES1		04791.4	3	3	8.75				6.305531 484.			-2.43874		R13N	109	0					0 0	0) (0		0					0	0 Depth.tif
	325 h-032	RES1	71326 184		2	3	10.625				6.11294 483.			-4.59013		R12N	107	0					0 0	0		0		0					0	0 Depth.tif
	326 h-033	RES1	31642 81 62551 162		2	3	10.625 10				5.363318 483. 6.2362 483.			-5.25702		R12N P12N	107	0					0 0	0		0		0					0	0 Depth.tif
	327 h-035 gara 328 h-037	RES1 RES1	62551 162 115554 299		1	4	5.24		40.99907		U.23U2 483.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		-3.68703 -3.1711		R12N R11B	107 704	0	0	81003.5 149642			0 0	0) 0		0					0	0 Depth.tif 0 Depth.tif
	329 h-038	RES1	51383 133		2	4	2.1		41.00395					2.42483		R12B	108			66540.5			2 17765.86	0) 0		0 RES1BSG0	16.0864	0	0	16.0864	180	360 Depth.tif
	330 h-039	RES1	41036 106		3	4	1.57		41.00441					2.699363		R13B	110			53141.5			6 14719.86	0) (0		0 RES1BSG0		0		12.3904	180	360 Depth.tif
	331 h-040	RES1	47531 123		2	4	2.96		41.00495					1.734326		R12B	108	24.67163					8 14243.42	0		0		0 RES1BSG0	11.6512	0	0	11.6512	180	360 Depth.tif
	332 h-050 tel	RES1		3405.84	3	7	9.33		41.00387			400.5		-5.18849		R13N	109	0	0				0 0	0		0	•	0					0	0 Depth.tif
	333 m-003	COM1		55526.7	1	7	0.579977306					482.5		-0.96753		C1LN P12B	108	19 52975	20511.00				0 0	68073.2) 0		0					0	0 Depth.tif
	334 m-004 335 m-005	RES1 RES1	42718 110 49610 12)639.62 28489.9	2	4	0.17452147 1.887618055			-76.4774 -76.4767		482.5 482.5		-0.09225 -10.4055		R12B R12B	108 0	18.53875		55319.5 64244.5			2 8442.861 0 0	0) 0		0					U n	0 Depth.tif 0 Depth.tif
	336 m-006	RES1		91064.3	1	4	3.00000763			-76.4781		482.5		-10.4033		R11B	0	0	0				0 0	0) 0		0					0	0 Depth.tif
	337 m-007	COM1	455232 1179		2	4	2.024306367			-76.4774		482.5		0.429554		C1LB	217			1179050			1 145132.9	126583.08		15.5979686	5 19744.389	91 COM1NBS(33.0696	0	0	33.0696	360	540 Depth.tif
	338 m-008	RES1	29347 76		2	4	-1.202432437			-76.4768		482.5		2.61276		R12B	108	27.83828					4 10432.49	0		0		0 RES1BSG0	9.8736	0	0	9.8736	180	360 Depth.tif
	339 m-009	AGR1		L745.64	0	0	3.19137609			-76.4763		482.5		4.484703		A1LN	616	21.90822					7 14239.65	0				0 AGR1NBFT	0	0	0	0	30	210 Depth.tif
	340 m-010 belo	RES1	43463 112	2569.17	2	4	1.671121526	1794	40.98032	-76.4719	7.300672	482.5	7.383752	5.71263	1	R12B	108	42.56315	47912.91	56284.5	24	40.5631	5 22830.77	0) () 0)	0 RES1BSG4	15.7872	0	0	15.7872	270	450 Depth.tif

INPUT FIELDS	FIELD ID STRUCTURE	Occupancy Zoning	Market A	Total County ssessed lue x CLR (\$)	# of Stories	Foundation Type	1st Floor Height above Grade (Ft)	Total SF Latitude	Longitude	Depth of Flood Lee		Depth of Flood from Ground (Ft)	Depth of Flood in Structure E: (Ft)	Floodng xpected?	Struc Occup ID	Bldg Depth Damage ID	% Bldg Damage	Bldg Loss \$\$	Contents	Contents Depth Damage ID	% Contents Damage Content Loss \$\$	Commercia Inventory Cost (\$)	Comm Inventory Depth Damage ID	% Comm Inventory Damage	Comm Invento Loss \$\$	y Debris ID D	ebris_Fin	Debris from Struc	Debris from Foundation	Debris Total F		to GridName estore Struc
	341 m-011	RES1	43036 1	11463.24	1	0	5.7	1428 40.97705	-76.472	1.914062	481.5	1.84899	-3.85101	1	R11N	129	0	(55731.5	45	0	0	0 0		0	0					0	0 Depth.tif
	342 m-014	RES1	22096	57228.64	2	4	0.741101932	1008 40.97697	-76.4722	-0.67943	481.5	-0.65658	-1.39768	0	R12B	0	0	(28614	0	0	0	0 0		0	0					0	0 Depth.tif
	343 m-015.1	RES1	36737	95148.83	2	4	1.741521616	1868 40.97709	-76.4722	-0.07269	481.5	-0.11604	-1.85756	0	R12B	0	0		47574	0	0	0	0 0		0	0					0	0 Depth.tif
	344 m-016	RES1	27292	70686.28	2	4	1.673955672	1353 40.97726	-76.4721	-1.71217	481.5	-1.687	-3.36095	0	R12B	0	0		35343	0	0	0	0 0		0	0					0	0 Depth.tif
	345 m-018.2 ga	RES1	82050	212509.5	2	4	0.289580253	2811 40.98022	-76.4726	0.468148	482.5	0.46277	0.173189	1	R12B	108	19.34638	41112.	3 106254.5	24	16.34638 17368.7	6	0 0		0	0 RES1BSG0	24.7368	0	0	24.7368	180	360 Depth.tif
	346 m-019.1	RES1	42812 1	.10883.08	2	4	-1.868504285	1800 40.97858	-76.4719	-3.43511	482	-3.38707	-1.51857	0	R12B	0	0		55441.5	0	0	0	0 0		0	0					0	0 Depth.tif
	347 m-020	RES1		12517.17	2	4	-1.283515186	3288 40.97984	-76.4723	-1.504	482.5	-1.50315	-0.21963	0	R12B	0	0		156258.5	0	0	0	0 0		0	0					0	0 Depth.tif
	348 m-021 fenc	COM1	40658 1	.05304.22	0	0	0.6507704	0 40.97832	-76.4733	-9.86465	482.2225	-9.51347	-10.1642	0	C1LN	0	0		105304	0	0	0	0 0		0	0					0	0 Depth.tif
	349 m-022	RES1	47702 1	.23548.18	1	4	-0.22855277	1232 40.98134	-76.4742	-1.91911	482.5	-1.74327	-1.51472	0	R11B	0	0		61774	0	0	0	0 0		0	0					0	0 Depth.tif
	350 m-024	COM1	139032 3	60092.88	1	7	-0.795891249	9688 40.98663		2.43425	482.5			1	C1LN	217	16.45413	59249.9	360092	90	58.72475 211463.	1 66750.3	2 1	67.4976919	95 45054.92	54 COM1NBS(17.4384	0	0	17.4384	360	540 Depth.tif
	351 m-025.1 bu		461130 1	.194326.7	2	7	-0.618989087	4038 40.97824			482	6.529396		1	R3A1N	204	43	513560.	2 597163	81	50.74192 30301	2	0 0		0	O RES3ANBS(27.4584	0	0	27.4584	270	450 Depth.tif
	352 m-026	RES1	67188 1	74016.92	1	4	5.170381556	1620 40.99064	-76.478	-19.1739	482.5	-18.1476	-23.318	0	R11B	0	0	(87008	0	0	0	0 0		0	0					0	0 Depth.tif
	353 m-027	RES1	88060	228075.4	1	4	5.252830233	1830 40.99096	-76.4781	-24.6621	482.5	-24.1074	-29.3603	0	R11B	0	0		114037.5	0	0	0	0 0		0	0					0	0 Depth.tif
	354 m-028	RES1	131594 3	40828.46	1	4	1.028815775	2160 40.9919	-76.4783	-31.1997	482.5	-31.1038	-32.1326	0	R11B	0	0		170414	0	0	0	0 0		0	0					0	0 Depth.tif
	355 m-031	RES1		89971.42	2	4	-1.176534261	1503 40.98104	-76.4737	-2.67668	482.5	-2.74534		0	R12B	0	0		44985.5	0	0	0	0 0		0	0					0	0 Depth.tif
	356 m-032	RES1	24170	62600.3	2	4	2.204876165	2952 40.99536	-76.4766	6.435298	482.5	6.436244	4.231368	1	R12B	108	35.15684	22008.1	31300	24	33.92547 10618.6	7	0 0		0	0 RES1BSG4	25.9776	0	0	25.9776	270	450 Depth.tif

WEST END FLOOD MITIGATION STUDY

COLUMBIA COUNTY, PENNSYLVANIA

Appendix H

Opinion of Probable Costs

WEST END FLOOD MITIGATION STUDY COLUMBIA COUNTY, PENNSYLVANIA

Appendix H – Opinion of Probable Costs

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Alternate 1 System Floodwall Around Fairgrounds Summary of Opinion of Total Project Cost

Columbia County - We	st Stu	dy Levee Costs
Alternate AlignmentSheet Pile Fairgrou		Around Perimeter of
Summary of Project C	osts	(2022 Costs)
Item Description		Cost
SubTotal Construction Cost with 25% Contingency	\$	25,133,842.85
Stream Channelization		\$3,000,000.00
Total Construction Cost with 25% Contingency	\$	28,133,842.85
Environmental/Cultural resources	\$	500,000.00
Legal, Administration of Grant	\$	275,000.00
Engineering/Geotechnical	\$	2,450,000.00
Permitting	\$	300,000.00
Construction Inspection	\$	675,000.00
Total Project Cost	\$	32,333,842.85

Alternate 2 System (Preferred System) Itemized Opinion of Probable Construction Cost

Date Rev: 3.31.2022					
Line Item	Item Description		Cost		
1	Project Maintenance and Protection of Traffic (Entire Project)	s	125,000		
2	Project Sign	s	5,000		
3	Section A - W. First Street Levee- Station 0+35 to Sta.11+50 = 1115 LF	\$ 1,540,850			
4	R/W Takes	s	600,000		
5	MSE Levee (Single Sided) Sta 11+50 to 17+60 = 610 LF	s	1,126,000		
6	R/W Takes	S	350,000		
8	Sheetpile Floodwall Sta 16+50 to 22+25 = 575 LF		1,719,72		
9	R/W Takes		375,000		
10	Earth Levee Sta 22+25 To 25+55(Rt. 11 Closure) = 330 LF		426,00		
11	Route 11 Closure Structure	S	488,92		
12	Earth Levee Station 26+20 to Station 30+41 = 421 LF (Bloom University Property)		423,350		
13	Closure Structure 2A Floodbreak 24 Foot Width - 7 Feet High		455,30		
14	Closure Structure 2B		358,47		
15	MSE Levee - Sta 31+60 to Sta. 40+45 - Ave. 11' Height 885' Length		1,299,160		
16	Closure 3 - Stoplogs- Sta 40+45 to 40+75 8' Ht. X 30' Wide		409,70		
17	MSE Levee- 40+75 to Sta. 46+00 - Ave. 11' Height 525' Length	\$ 769,623			
18	Closure 4 - Sta 46+00 to Sta 46+30 - 10' Ht. X 30' Width	h \$ 409,425			
19	MSE Levee - Station 46+30 to 46+90 = 60 LF	\$ 93,800			
21	Closure 5 - Sta 46+90 to Sta 47+30 - 10' Ht. X 40' Width	\$ 463,775			
22	MSE Levee (Single Sided) Sta 47+30 to 60+00 - Length = 1270' Ave 12' High	s	1,952,00		

23	Concrete retaining Wall Tie-out to existing system at 6th Street		175,000
24	PUMPING STATION 1 (Fairgrounds)20,000 GPM	s	1,200,100
25	Drainage Items	\$	363,350
26	Roadway / Paving Items	s	328,325
27	Miscellaneous Items	\$	319,050
28	Electrical Utility Trench w/conduits for Primary Feed		90,000
29	Utilities		63,000
30	Erosion and Sedimentation Control	s	220,200
31	Fairgrounds	s	130,000
33	SubTotal Opinion of Construction Cost for Schematic Level Design		16,280,145
34	Project Mobilization and Demobilization 8% of Subtotal	\$	1,302,412
36	Opinion of Probable Construction Cost	S	17,582,556
37	Contingencies - 25%	\$	4,395,639
38	Total	\$	21,978,195
39	Induced Flooding Mitigation		
40	Stream Channelization	s	3,000,000
41	Total Project Construction Cost	\$	24,978,195

Alternate 2 System Summary of Opinion of Total Project Cost

Columbia County - West Study Levee Costs					
Summary of Project Costs (2022 Costs with 25% Contingency)					
Item Description		Cost			
Maintenance of Traffic	\$	156,250.00			
New Levees	\$	16,801,399.69			
Stormwater Pumping Station	\$	1,500,000.00			
Drainage Items	\$	454,187.50			
Roadway Items / Miscellaneous Work	\$	1,438,343.75			
Mobilization	\$	1,628,014.48			
Subtotal	\$	21,978,195.41			
TOTAL Construction	\$	21,978,195			
Flood Mitigation - Stream Channelization/ Property Elevations	\$	3,000,000.00			
Environmental/Cultural resources	\$	500,000.00			
Legal, Administration of Grant	\$	275,000.00			
Engineering/Geotechnical	\$	2,300,000.00			
Permitting	\$	300,000.00			
Construction Inspection	\$	675,000.00			
Total Project Cost with 25% Contingency	\$	29,028,195			